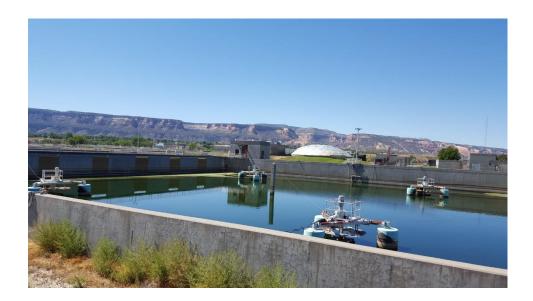


PERSIGO WASTEWATER TREATMENT PLANT Geotechnical Investigation

2145 River Road Grand Junction, Colorado 81505



October 22, 2019 WJE No. 2019.3776



Prepared for: **Ms. Kirsten Armbruster** Project Engineer City of Grand Junction, Public Works 333 West Avenue, Bldg C Grand Junction, Colorado 81501

Prepared by: Wiss, Janney, Elstner Associates, Inc. 3609 South Wadsworth Boulevard, Suite 400 Lakewood, Colorado 80235 303.914.4300 tel | 303.914.3000 fax



PERSIGO WASTEWATER TREATMENT PLANT Geotechnical Investigation

2145 River Road Grand Junction, Colorado 81505

ami from

Daniel Franco, PE

Peter A. Stauffer, PE

October 22, 2019 WJE No. 2019.3776

Grand Junction

Prepared for: **Ms. Kirsten Armbruster** Project Engineer City of Grand Junction, Public Works 333 West Avenue, Bldg C Grand Junction, Colorado 81501

Prepared by: Wiss, Janney, Elstner Associates, Inc. 3609 South Wadsworth Boulevard, Suite 400 Lakewood, Colorado 80235 303.914.4300 tel | 303.914.3000 fax



TABLE OF CONTENTS

| Purpose and Scope | 1 |
|---|----|
| Site Conditions and Background | 1 |
| Site Geology | 2 |
| Site Investigation | 3 |
| Drilling Program | 3 |
| Laboratory Testing | 4 |
| Subsurface Conditions | 6 |
| Topsoil | 6 |
| Lean Clay | 6 |
| Poorly Graded Sand | 6 |
| Clayey Sand | 6 |
| Gravel and Cobble | |
| Well Graded Sand with Clay and Gravel | 7 |
| Mancos Shale | 7 |
| Groundwater | |
| Geotechnical Engineering Discussion and Recommendations | 7 |
| Lateral Earth Pressures | |
| Groundwater Conditions | 8 |
| Subgrade Foundation Performance | 8 |
| Preliminary Recommendations for Additional Facilities | 8 |
| Primary Clarifiers | 9 |
| Anaerobic Digesters | 9 |
| Aeration Basins | 10 |
| Final Clarifiers | 11 |
| Additional Recommendations for Final Geotechnical Investigation | 11 |
| General Information | 12 |
| Figures | |
| Appendix I - Detailed Borehole Logs and Piezometer As-Builts | |
| A second in H. L. I. T. et D. evelte | |

Appendix II - Lab Test Results



PERSIGO WASTEWATER TREATMENT PLANT Geotechnical Investigation

2145 River Road Grand Junction, Colorado 81505

PURPOSE AND SCOPE

At the request of the City of Grand Junction (CGJ), Wiss, Janney, Elstner Associates, Inc. (WJE) has completed a geotechnical investigation at the Persigo Wastewater Treatment Plant (herein referred to as PWWTP) located at 2145 River Road in Grand Junction, Colorado. The geotechnical investigation is part of the full scope of work for the PWWTP Structural Assessment as outlined in RFP-4653-19-DH, dated June 21, 2019. WJE has not been provided results of prior geotechnical investigations at the site, as it is our understanding that none exist. The objectives of our work are: characterize the subsurface conditions; including soils, bedrock, and groundwater levels for use in the engineering evaluation of the existing facilities; provide preliminary geotechnical recommendations for use in rehabilitation, modification, or improvement of existing facilities as needed; and provide preliminary recommendations for potential new construction at the PWWTP. The specific structures/facilities at the PWWTP to be assessed and evaluated by WJE for this current study include the Raw Sewage Pump Station, Primary Clarifiers, Aeration Basin, Aerobic Digesters, Sludge Processing Unit, and the Anaerobic Digesters.

The scope of work for the geotechnical investigation included:

- Review of available geologic and background information at the PWWTP
- Drilling and sampling 7 boreholes at the PWWTP, near the existing structures that are being assessed and evaluated by WJE
- Installation of 2 piezometers for future monitoring of groundwater levels
- Laboratory testing of selected soil samples
- Engineering evaluation of the results of the field investigation and laboratory testing programs
- Preparation of this report, summarizing our findings and providing preliminary geotechnical recommendations

Included with this report are Table 1: Summary of Laboratory Test Results; Table 2: Equivalent Fluid Unit Weights for "Active" and "At Rest" Conditions; Figure 1: Geologic Map; Figure 2: Borehole Location Map; Figure 3: Summarized Borehole Logs; and Figure 4: Borehole Log Legend. Detailed borehole and piezometer construction diagrams are provided in Appendix I; and laboratory test result sheets are included in Appendix II.

SITE CONDITIONS AND BACKGROUND

The PWWTP site encompasses approximately 50 acres and is located roughly 1.5 miles west of the intersection of U.S Route 6 and Interstate I-70, and 0.8 miles north of the Colorado River. The site gently slopes down to the southwest toward the Colorado River. The preconstruction topographic relief at PWWTP was approximately 12 feet. The post construction topographic relief, including the built-up areas, is approximately 20 feet. Groundwater conditions are expected to be relatively shallow due to the proximity of the site to the Colorado River and nearby gravel pits, where standing water is observed in the pits.

Construction of the PWWTP was completed in 1984, after which the plant has been in service for 35 years. The design capacity of the plant is 25 million gallons per day. Construction drawings indicate that the



PWWTP was designed to allow for future expansion of selected plant facilities. The main facilities that comprise the existing PWWTP include:

- Operation Building
- Headworks
- Grit Removal Units
- Raw Sewage Pump Station
- Primary Clarifier 1 and 2
- Primary Sludge Pump Station
- Aeration Basin
- Aeration Basin Control Unit
- Final Clarifier 1, 2, and 3
- Chlorine Unit
- Chlorine Contact Basins
- Plant Water Pump Station
- Anaerobic Digester 1 and 2
- Sludge Processing Unit
- Aerobic Digester
- Sludge Drying Beds
- Flow Equalization Basins

There are two existing piezometers that we understand have been used to monitor groundwater levels, one of which is located approximately 15 feet west of the Operations Building, and the other is located approximately 50 feet east of the Final Clarifiers. There are two additional piezometers located on the east side of the Flow Equalization Basin that could provide groundwater information; however, PWWTP site personnel were uncertain about the details regarding construction of these piezometers.

The foundation for the Raw Sewage Pump Station is located approximately 20 feet below the ground surface. This foundation is the deepest of any of the structures at the site. The Primary Clarifiers, Aeration Basin, and sections of the Anaerobic Digesters are built on pads. Grade around these facilities was built up with fill.

The foundation types for the structures included in our structural assessment are mat foundations and spread footings, according to "as-built" drawings. During the course of the field work completed for this study, WJE personnel observed the structural foundation at only two core holes located within the Raw Sewage Pump Station, in which no cracking was observed. According to the "as-built" drawings, the mat foundations for the structures are up to 2 feet thick and typically have a 3 to 4 inch sub-slab with a waterproofing membrane, and/or a 3 inch topping slab. The dimensions of the spread footing foundations vary. Of the structures WJE evaluated for this study, the Sludge Processing Unit and the Aerobic Digester have spread footing foundations, while the Raw Sewage Pump Station, Primary Clarifiers, Aeration Basins, and the Anaerobic Digesters have mat foundations.

SITE GEOLOGY

The project site is located in the Colorado Grand Valley near the Colorado River, and is situated between The Colorado National Monument approximately 2.5 miles to the south, and the Book Cliffs approximately 10 miles to the northeast (Figure 1A). A series of regional faults, including the Redlands Fault, are located 2.4 miles southwest of the PWWTP. Bedrock gently dips at approximately 3 to 11 degrees to the northeast at the project site. The site is underlain by the Mancos Shale, which is covered by contemporary overburden



soils containing gravels, sands, silts, and clays. Geological units that underlie the site range from Holocene to Upper Cretaceous in age.

Geologic mapping by Scott and Harding (2001) indicates the southern portion of the site, nearest to the Colorado River, consists of "chiefly gravel in a sand matrix (Qfp)" that is part of the Colorado River floodplain and stream channels. The northern portion of the site consists of a "light-gray sandy clay and silty clay (Qsw) deposited on very gentle slopes north of the Colorado River, derived from the Mancos Shale," (Scott and Harding, 2001). The Mancos Shale outcrops approximately 5 miles northeast of the PWWTP site. Bedrock underlying overburden soils is the Mancos Shale, which is described as "chiefly mediumdark-gray, dark-gray, brownish-gray, and brownish-black fissile shale that weathers to light gray". Based on subsurface profiles provided with the geological mapping (Figure 1B), the Mancos Shale is expected to be 15 to 30 feet below the ground surface at the project site. The Mancos Shale was encountered at approximately 20 feet below the ground surface at one of the boreholes completed for the subsurface investigation. In general, descriptions provided with the geological mapping (Scott and Harding, 2001) are consistent with the materials encountered during the subsurface investigation.

SITE INVESTIGATION

Drilling Program

The 2019 drilling program at the PWWTP was designed to generally define soil, bedrock, and groundwater conditions at and around the existing PWWTP structures. A total of 7 boreholes were drilled for the investigation at locations shown on Figure 2. Boreholes B-2 and B-5 were completed as piezometers, while the remaining boreholes were backfilled with soil cuttings. The summary borehole logs are provided in Figure 3, with the legend and notes provided on Figure 4. Detailed borehole logs and piezometer construction diagrams are provided in Appendix I.

The boreholes were drilled by HRL Compliance Solutions between September 11 and 13, 2019, using a track mounted Diedrich D90 drill rig. The boreholes were advanced using two methods: 4-inch diameter solid stem auger, and 6-inch diameter ODEX casing. Borehole depths ranged from 14-1/2 to 27 feet below the existing ground surface. Each borehole was logged by a WJE geotechnical engineer.

Subsurface materials were typically sampled at 5 foot intervals using a 2-inch inner diameter California split-barrel sampler. The sampler was driven with a 140-pound hammer falling a vertical distance of 30 inches. The hammer blows were provided by an automatic hammer. The number of blows required to advance the sampler 12 inches was recorded as the penetration resistance or N value. The N values provided in this report were not corrected to account for the diameter of the California sampler. Penetration resistance values provide an indication of the consistency or relative density of the subsurface materials encountered. Sampling was done in general accordance with the Standard Penetration Test (SPT) as described in ASTM D1586, *Standard Test Method for Standard Penetration Test (SPT) and Split-Barrel Sampling of Soils*. When using the ODEX drilling method, grab samples were collected at selected depths. The groundwater levels were recorded during drilling for all boreholes, and Borehole B-1 was checked 24 hours after drilling before the hole was backfilled. Water level in Borehole B-2 was measured again approximately 24 hours after the piezometer was installed.

Piezometers were installed in Boreholes B-2 and B-5 to permit monitoring of groundwater levels. The bottoms of Piezometers B-2 and B-5 are 17 and 20 feet 7 inches below the ground surface, respectively. The piezometers were constructed with 2-inch inner diameter schedule 40 PVC pipe. The lower 10 feet of



the piezometer pipe is machine slotted (10 slot), which is connected to the solid PVC pipe which extends 3 feet above ground surface. A clean 10-20 silica sand was placed in the annulus around the entire slotted PVC pipe section and extending approximately 2 feet above the slotted section. Bentonite chips were placed above the 10-20 silica sand to seal off the screened interval, and were placed up to about 2 feet below the ground surface. Concrete was placed from the top of the bentonite seal to the ground surface, and a circular lockable steel protective cover which extends approximately 3 feet above ground surface was placed in the concrete. As-built construction diagrams of Piezometers B-2 and B-5 are included in Appendix I with the detailed borehole logs.

Laboratory Testing

Laboratory testing was performed on selected samples obtained from the boreholes to characterize the physical and engineering properties of soil and bedrock materials at the PWWTP. Laboratory tests were conducted by Advanced Terra Testing, Inc. (ATT), of Lakewood, Colorado, in general accordance with ASTM procedures. Laboratory testing included:

- Water Content (ASTM D2216)
- Density (ASTM D7263)
- Atterberg Limits (ASTM D4318)
- Grain Size Distribution (ASTM D6913)
- Swell/Consolidation (Denver Swell)
- Unconfined Compressive Strength (ASTM D2166)

Laboratory test results are summarized on Table 1 on the following page, and are shown on the summary logs on Figure 3 and the detailed logs in Appendix I. Test result sheets are provided in Appendix II.



Table 1 - Summary of Laboratory Test Results

| | Sample | | | (| Gradation | | Atterb | erg Limits | S | well/Consolidation | | Unconfined Compression | on Strength Test | | |
|----------|-------------------------|------------------------------------|---------------------------------|---------------|-------------|--------------|---------------------|----------------------------|---------------------------------|--------------------|----------------------------|--------------------------------|-------------------|---|--|
| Borehole | Sample Depth (ft) | In situ Moisture Content (%) | In situ Dry Density (pcf) | Gravel (%) | Sand (%) | Fines (%) | Liquid Limit (%) | Plasticity Index (%) | Inundation Pressure (psf) | Swell/Cons. (%) | Swell Pressure (psf) | Axial Strain at Peak Stress(%) | Peak Stress (psf) | Material Type | |
| | 0 | 14.2 | - | | | | | | | | | | | | |
| | 4 | 14.5 | 113 | 4 | 41 | 55 | 28 | 14 | | | | | | CL - Sandy lean CLAY, trace gravel | |
| B-1 | 7 | 12.8 | 121 | | | | | | | | | | | | |
| D-1 | 15.5 | 9.4 | 116 | | | | | | | | | | | | |
| | 20 | | | 7 | 89 | 4 | | | | | | | | SP - poorly graded SAND, trace gravel | |
| | 26 | | | 20 | 76 | 4 | | | | | | | | SP - poorly graded SAND with gravel | |
| | 0 | 7.1 | 105 | | | | | | | | | | | | |
| B-2 | 3 | 11.5 | 113 | 0 | 1 | 99 | 41 | 23 | | | | | | CL - Lean CLAY, trace sand | |
| B-2 | 7 | 29.6 | 92 | 0 | 17 | 83 | | | | | | | | *CL - Lean CLAY with sand | |
| | 12 | 8.1 | 121 | | | | | | | | | | | | |
| | 0 | 9.9 | 126 | | | | | | | | | | | | |
| B-3 | 4 | 19.8 | 108 | 0 | 1 | 99 | 38 | 20 | | | | | | CL - Lean CLAY, trace sand | |
| | 9 | 28.7 | 94 | 0 | 2 | 98 | 34 | 17 | 1080 | -1.5 | N/A | 13 | 410 | CL - Lean CLAY, trace sand | |
| | 0 | 6.8 | 117 | | | | | | | | | | | | |
| B-4 | 4 | 20.5 | 102 | 0 | 1 | 99 | 45 | 27 | | | | | | CL - Lean CLAY, trace sand | |
| | 9 | 21.8 | 103 | 0 | 51 | 49 | | | | | | | | *SC - Clayey SAND | |
| | 0 | 14.8 | 112 | 0 | 9 | 91 | 38 | 21 | | | | | | CL - Lean CLAY, trace sand | |
| B-5 | 6 | 18.4 | 92 | 0 | 82 | 18 | | | | | | | | *SC - Clayey SAND | |
| | 20 | 9.2 | 122 | | | | | | 2400 | 0.4 | 4680 | | | | |
| | 0 | 11.7 | 100 | | | | | | | | | | | | |
| | 4 | 16.1 | 112 | 2 | 18 | 80 | 36 | 20 | | | | | | CL - Lean CLAY with sand | |
| B-6 | 9 | 16.6 | 115 | 0 | 1 | 99 | 36 | 19 | 1080 | 0.1 | 1830 | 12 | 4350 | CL- Lean CLAY, trace sand | |
| | 14 | 28.3 | 95 | 0 | 0 | 100 | 34 | 18 | | | | | | CL- Lean CLAY | |
| | 19 | 8.2 | 125 | 37 | 52 | 11 | | | | | | | | SW-SC - Well graded SAND with clay and gravel | |
| | 0 | 6.5 | 115 | | | | | | | | | | | | |
| B-7 | 4 | 15.3 | 113 | 0 | 22 | 78 | 30 | 14 | | | | | | CL - Lean CLAY with sand | |
| | 9 | 28.3 | 92 | | | | | | | | | | | | |

Notes:

(1) Laboratory testing completed by Advanced Terra Testing, Inc. Lakewood, Colorado.

(2) (*) denotes estimated soil classification.



Persigo Waste Water Treatment Plant Geotechnical Investigation October 22, 2019 Page 6

SUBSURFACE CONDITIONS

Following are descriptions of the different materials encountered during the September 2019 geotechnical investigation as presented in this report. The borehole logs (Figures 3 and 4 and Appendix I) and laboratory test result sheets (Appendix II) should be referred to for detailed information.

Topsoil

Topsoil material was encountered in all boreholes ranging from the ground surface to about 1-1/2 feet below the ground surface. The topsoil was a clay soil with trace amounts of sand and gravel, with organic material including grass roots. The moisture of the topsoil ranged from dry to moist, and the color was dark brown.

Lean Clay

The predominant near-surface material encountered at the site is a lean clay with varying amounts of sand and gravel. Lean clay was encountered in all of the boreholes extending from just below the topsoil to depths ranging from 0.5 to 20 feet. Dry unit weights (dry densities) ranged from 92 to 126 pounds per cubic foot (pcf). Moisture contents ranged from 6.5 to 29.6 percent (%). N values ranged from 2 to 44, indicating the material consistency ranges from soft to hard. The lower blow counts were typically obtained in the lean clays below the groundwater level. Plasticity index values range from 14 to 27. Unconfined compressive strength tests on two samples provided strengths of 410 and 4,350 pounds per square foot (psf), respectively. Volumetric changes measured when test specimens were wetted at an applied stress corresponding to overburden stress ranged from 1.5% compression to 0.1% swell. The material color ranged from tan to light and dark brown.

Poorly Graded Sand

Sand with varying amounts of gravel underlies the lean clay, extending to the bottom of the boreholes at depths 27 and 17 feet in Boreholes B-1 and B-2, respectively. Due to difficulties drilling and sampling this material, just one drive sample was obtained using the California split-sampler, and several grab samples were obtained. The drive sample was found to have a moisture content of 8.1 %, and a dry unit weight of 121 pcf. The N value recorded for the one drive sample was 48, indicating the material relative density is dense. The material color was gray to brown.

Clayey Sand

Clayey sand underlies the lean clay in Boreholes B-4, B-5, and B-7, extending to depths of 14, 8-1/2, and 15-1/2 feet, respectively. Dry unit weights ranged from 92 to 103 pcf, and moisture contents ranged from 18.4 to 21.8 %. N values ranged from 15 to 24, indicating the material consistency is medium dense. The material color was light to dark brown.

Gravel and Cobble

Gravel and cobble materials were encountered in Boreholes B-4 and B-5 beneath lean clay and clayey sand, extending to depths of 17-1/2 and 20 feet, respectively. Gravel and cobble sizes and percentages by weight could not be determined accurately due to difficulty drilling and sampling these materials. Nearby fill materials containing native gravel and cobbles indicate that the maximum cobble size is likely approximately 3 to 4 inches. Gravel and cobble cuttings were collected during drilling, but no laboratory testing was performed on these samples due to crushing of the material that resulted from drilling with the ODEX system.



Well Graded Sand with Clay and Gravel

Well graded sand with clay and gravel underlies the lean clay in Borehole B-6, and extends to the bottom of the borehole at 23 feet depth. One sample of this material was obtained using the California split-sampler. The moisture content was determined to be 8.2 %, and the dry unit weight 125 pcf. The N value recorded for the one sample is 45, indicating the material relative density is medium dense. The material color was gray and brown.

Mancos Shale

A dark olive gray shale bedrock was encountered during drilling in Borehole B-5 at an approximate depth of 20 feet bgs. The N value was 50 blows to achieve 1 inch of sampler penetration, indicating the material consistency is very hard. Laboratory test results for dry unit weight and moisture content were 122 pcf and 9.2 %, respectively. The volumetric change measured when the test specimen was wetted at an applied stress corresponding to overburden was 0.4% swell.

Groundwater

Groundwater was encountered in Boreholes B-1, B-2, B-3, B-4, and B-5 at 5-1/2 to 8 feet depth below ground surface (bgs). At Boreholes B-6 and B-7, which were drilled in areas that had been built up by placement of fill, groundwater was encountered at 15 and 9 feet bgs, respectively. These groundwater levels were measured during drilling and shortly after drilling was completed. Groundwater levels may fluctuate significantly in response to numerous factors such as seasonal irrigation and climatic variations.

Groundwater readings were measured on September 13, 2019, at the four existing piezometers and the two new piezometers installed at Boreholes B-2 and B-5. Groundwater levels measured at existing and new piezometers on September 13, 2019 are consistent with one another and ranged from 7 to 9 feet bgs. The groundwater level measured at the existing piezometer west of the operations building was 7-1/2 feet bgs. The groundwater level for the existing piezometer east of the final clarifier was measured at 7 feet bgs. Groundwater levels measured at the existing piezometers east of the flow equalization basin were 7-1/2 and 9 feet bgs. Groundwater levels measured at the new piezometers, Piezometer B-2 (Borehole B-2) and Piezometer B-5 (Borehole B-5), were 8 and 7 feet bgs, respectively.

GEOTECHNICAL ENGINEERING DISCUSSION AND RECOMMENDATIONS

Lateral Earth Pressures

The majority of the facilities at the PWWTP extend below the ground surface and thereby have lateral earth pressures acting against them. The lateral earth pressures will depend on the type of subsurface material present, as well as drainage and groundwater conditions. Where foundations extend below the groundwater level, the lateral pressures acting on the wall increase as a result of the water pressure. In addition, the lateral earth pressure acting on a foundation wall will vary depending on whether or not the wall is restrained from moving. Where a foundation or retaining wall deflects in response to lateral earth pressures, this is referred to as active conditions. Where a foundation wall is restrained and does not deflect due to the lateral earth pressures, this is referred to as the at-rest conditions. At rest earth pressures will be greater than active earth pressures.

Lateral earth pressures are typically estimated using an "equivalent fluid pressure." The lateral earth pressure acting on a wall at a particular depth is calculated as the depth below the ground surface times the



equivalent fluid unit weight. Where the wall extends below the groundwater level, the lateral earth pressure is calculated as the lateral pressure at the groundwater level, calculated as described above, plus the depth below the groundwater level times the equivalent fluid unit weight corresponding to conditions below the groundwater level.

Table 2, below, provides equivalent unit weights for active and at rest conditions and for conditions above and below the groundwater level. These values apply to the case where lean clay soils as described in this report bear against the foundation walls. For the existing PWWTP facilities, the boreholes completed for this study indicate that lean clay materials extend to depths below the bottom or to very near the bottom of all of the foundation walls.

| Condition | Equivalent Fluid Unit Weight, pcf |
|-----------------------------------|-----------------------------------|
| Active - Above Groundwater Level | 37 |
| Active - Below Groundwater Level | 80 |
| At Rest - Above Groundwater Level | 57 |
| At Rest - Below Groundwater Level | 91 |

Table 2 - Equivalent Fluid Unit Weights for "Active" and "At Rest" Conditions

Groundwater Conditions

The depth to groundwater ranged from 7 to 9 feet below the ground surface, except in areas that have been built up with fill. This groundwater range is based on depths measured during drilling, and readings obtained in the existing and new piezometers measured on September 11 to 13, 2019. Groundwater levels measured in the existing four piezometers agree with groundwater levels measured during the drilling program and with measurements in Piezometers B-2 and B-5. It is likely that groundwater levels have varied due to seasonal irrigation and changes in climatic conditions. In order to develop an understanding of how the groundwater level varies, WJE recommends that PWWTP site personnel obtain and record readings at the existing and new piezometers on a monthly basis for a period of 1 to 2 years.

Subgrade Foundation Performance

Considering that it has been approximately 35 years since construction of the PWWTP, and given the subsurface conditions as described in this report, we expect there will be minimal new distress due to foundation or slab-on-ground movement at the facility. Minor structure movement may have occurred during initial loading and soon thereafter. It is also possible that very minor structure movement has occurred due to changing loading conditions and large fluctuations in the groundwater level. Swell/consolidation testing indicates that subsurface materials at the site exhibit minimal volume change when wetted.

Details regarding the performance of the structures WJE evaluated for this study are provided in the WJE Structural Assessment Report.

Preliminary Recommendations for Additional Facilities

We understand that enlargement of the PWWTP could be undertaken in the future and could involve construction of new facilities including Anaerobic Digesters, Primary Clarifiers, Aeration Basins, and Final Clarifiers. Locations for the new facilities are shown on the "Overall Site Plan" drawing. Subsurface investigations completed for this study included boreholes located in the vicinity of these proposed



facilities. In the following sections we provide preliminary recommendations for foundation design and construction of these facilities based the findings of the geotechnical investigation as described in this report. Final geotechnical investigations should be completed for these facilities once the new facility locations have been selected and details of the proposed structures are known. We also provide preliminary geotechnical recommendations for these facilities based on where the future structures are shown on the drawings, and the results of this study.

Primary Clarifiers

The existing Primary Clarifiers are located in the central portion of the plant site. The existing structures measure approximately 118 feet at their outer diameter. The structures consist of a conventionally reinforced 8-inch thick concrete mat foundation, with a 2-inch thick grout layer, both of which have a 1:12 slope downwards towards the center of the clarifier. The perimeter walls consist of conventionally reinforced 10-inch thick concrete with two mats of reinforcing. The concrete structure extends approximately 2 feet above grade, and approximately 9 feet below grade. Borehole B-3 was drilled near where it appears that the additional Primary Clarifiers may be constructed. Based on the condition encountered in Borehole B-3, we offer the following preliminary comments and recommendations:

- Foundations similar to those constructed for the existing Primary Clarifiers appear to be a reasonable alternative for new Primary Clarifiers should they be constructed in this area. Design criteria for the foundation should be developed as part of the final geotechnical investigation work. Lateral earth pressures for preliminary design can be estimated using the equivalent fluid unit weights provided in this report. A relatively low N value (2/12) was obtained at 9 feet depth in Borehole B-3. Final geotechnical investigations should further investigate this depth interval to evaluate the potential affect soft lean clays could have on foundation design and construction. It may be prudent to "over-excavate" and replace soft clay if present at or near the mat bearing elevation.
- Excavations for the foundations may extend below the groundwater table. This should be confirmed based on monitoring of piezometer water levels as recommended in this report. Should it be determined that construction dewatering will be required, final geotechnical investigations should include slug testing to evaluate permeability characteristics of the lean clay soils for estimation of dewatering quantities, and for evaluation and design of dewatering alternatives if needed. In addition, final geotechnical investigation work should include development of design and construction recommendations for excavation support alternatives.
- If settlement of these structures is critical, final geotechnical investigations should include Shelby-tube sampling of the lean clay materials and consolidation testing, including time rate measurements for each load increment. However, it is possible, depending on the geometry and other details of the new clarifiers, that these structures *could* be considered to have what is sometimes called a "compensated foundation." This means that the Clarifier, even when full of effluent, weighs the same or less than any soil excavated to allow its construction. If so, settlement concerns may be less crucial. Nevertheless, soft conditions at bearing elevations may introduce constructability issues, which must be considered in design and construction.

Anaerobic Digesters

The existing Anaerobic Digesters are located on the west side of the plant, west of the Primary Clarifiers. The existing circular structures measure approximately 70 feet at their outer diameter. The structures extend approximately 20 feet above grade, and approximately 10 feet below grade. The structures consist of a



conventionally reinforced 12-inch thick concrete mat foundation within the digesters, with a conventionally reinforced 14-inch thick concrete slab and 3-inch thick topping within the pump room located between the two tanks. Borehole B-4 was drilled near where it appears that additional Anaerobic Digesters may be constructed. Based on the condition encountered in Borehole B-4, we offer the following preliminary comments and recommendations:

- Mat foundations, similar to the foundations constructed for the existing facilities are a reasonable alternative for new Anaerobic Digesters should they be constructed in this area. Design criteria for the new mat foundation should be developed as part of the final geotechnical investigation work. Lateral earth pressures for preliminary design can be estimated using the equivalent fluid unit weights provided in this report.
- Excavations for the foundations for new Anaerobic Digesters are expected to extend slightly below the groundwater table. This should be confirmed based on monitoring of piezometer water levels as recommended in this report. Should it be determined that construction dewatering will be required, final geotechnical investigations should include slug testing to evaluate permeability characteristics of the lean clay soils for estimation of dewatering quantities, and for evaluation and design of dewatering alternatives if appropriate. In addition, final geotechnical investigation work should include development of design and construction recommendations for excavation support alternatives.
- If total or differential settlement of these structures is critical, final geotechnical investigations should include Shelby-tube sampling of the lean clay materials and consolidation testing including time rate measurements for each load increment. Since the Anaerobic Digesters extend significantly above grade, it is unlikely that these foundations can be considered to be "compensated."

Aeration Basins

The existing Aeration Basins are located in the south central portion of the plant site. The existing aeration basins measure approximately 123 feet in the north-south direction, and 275 feet in the east-west direction. The aeration basin blower room is situated at the center of the structure (oriented in the north-south direction), and is approximately 30 feet in width. The basin walls extend approximately 2 feet above grade, and approximately 19 feet below grade. To the east and west of the basin blower room, the structure is split equally in the east-west direction by interior basin baffle walls, such that four individual open-air basins are present. The structure of the aeration basin consists of a conventionally reinforced 16-inch thick concrete slab foundation, with a 3-inch thick topping slab. The slab is thickened to 24-inches over an area that is six feet square below the 12-inch square interior columns. The exterior face of the foundation slab is waterproofed with continuous waterproofing that extends up the full height of the perimeter walls. The perimeter walls primarily consist of conventionally reinforced 12-inch thick concrete. Borehole B-6 was drilled near where it appears that the additional Aeration Basins may be constructed. Based on the condition encountered in Borehole B-6, we offer the following preliminary comments and recommendations:

 Mat foundations, similar to the foundations constructed for the existing basins, are likely a reasonable alternative for new Aeration Basins should they be constructed in this area to a similar bearing elevation. Allowable bearing pressures should be developed as part of the final geotechnical investigation work. Lateral earth pressures for preliminary design can be estimated using the equivalent fluid unit weights provided in this report.



- Excavations for foundations for new Aeration Basins, if similar to the existing basins, will extend below
 the groundwater table, and will likely bottom in lean clay. Final geotechnical investigations should
 include slug testing in this area to evaluate permeability characteristics of the lean clay soils for
 estimation of dewatering quantities that will be required, and for evaluation and design of dewatering
 alternatives. In addition, final geotechnical investigations should include development of design and
 construction recommendations for excavation support alternatives.
- If settlement of these structures is critical, final geotechnical investigations should include assessment of the compressibility of the deep clayey sand materials including time rate measurements for each load increment. As with the Clarifiers, it is possible that the Aeration Basins may be considered to have "compensated foundations." This should be evaluated when final layout and details are determined.

Final Clarifiers

The existing Final Clarifiers are located at the south end of the plant site. The existing structures are approximately 118 feet at their outer diameter. The structures consist of a conventionally reinforced 12-inch thick concrete mat foundation, which has a 1:12 slope downwards towards the center of the clarifier. The concrete structure extends approximately 2 feet above grade, and approximately 15 feet below grade. Borehole B-7 was drilled near where it appears that the additional Final Clarifiers may be constructed. Based on the condition encountered in Borehole B-7, we offer the following preliminary comments and recommendations:

- Foundations similar to the foundations constructed for the existing clarifiers are likely a reasonable alternative for new Final Clarifiers should they be constructed in this area. Design criteria for the foundation should be developed as part of the final geotechnical investigation work. Lateral earth pressures for preliminary design can be estimated using the equivalent fluid unit weights provided in this report.
- Excavations for new Final Clarifiers, if similar to the existing clarifiers, will extend well below the groundwater table, and will extend into clayey sand that underlies the lean clay encountered at Borehole B-7. Furthermore, it appears that Borehole B-7 did not extend to the bottom of the existing Final Clarifiers. Final geotechnical investigations should extend below the bottom of the new clarifiers and should include slug testing to evaluate permeability characteristics for estimation of dewatering quantities that will be required, and for evaluation and design of dewatering alternatives. In addition, final geotechnical investigations should include development of design and construction recommendations for excavation support alternatives.
- If settlement of these structures is critical, final geotechnical investigations should include assessment of the compressibility of the lean clay and deep clayey sand materials including time rate measurements for each load increment. As with the Clarifiers and Aeration Basins, it is possible that the Final Clarifiers may be considered to have "compensated foundations." This should be evaluated when final layout and details are determined.

Additional Recommendations for Final Geotechnical Investigation

Final geotechnical investigations for new facilities at the PWWTP should be planned when the layout and details of the proposed new facilities have been reasonably defined. As noted above, some of the existing, as well as some of the new facilities, may be considered to have "compensated foundations." However, facilities that cannot be considered to have compensated foundations should be investigated and designed



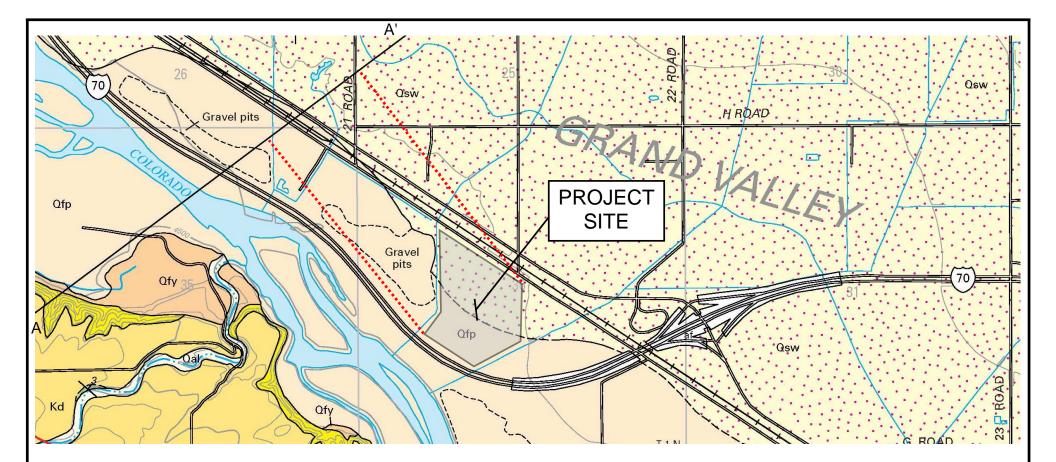
to address potential deep seated settlement. The fact that the existing facilities have generally performed adequately suggests that settlement has not been a significant problem. Nevertheless, we recommend that final investigations for new facilities that cannot reasonably be considered to have a "compensated foundation" include at least one boring to Mancos Shale bedrock for each structure.

GENERAL INFORMATION

Information in this report is intended to provide a geotechnical assessment of the site subsurface conditions, and to provide preliminary recommendations for geotechnical design and construction criteria based on these conditions; no other use is intended or authorized. Additional final geotechnical investigations will be required to support the design and construction of additions to existing facilities or for construction of new structures at the site. The report is based on the subsurface investigation, laboratory test results, site observations, analyses as described herein, and past experience with similar conditions. Variations can and do occur in geological materials, and departures from conditions portrayed in this report are possible. The conclusions and recommendations presented in this report are subject to the limitations and explanations contained herein.



FIGURES



DESCRIPTION OF MAP UNITS

| Qfp |
|-----|
|-----|

Qsw

Km

Flood-plain and stream-channel deposits (Holocene and late Pleistocene) —Chiefly gravel in a sand matrix

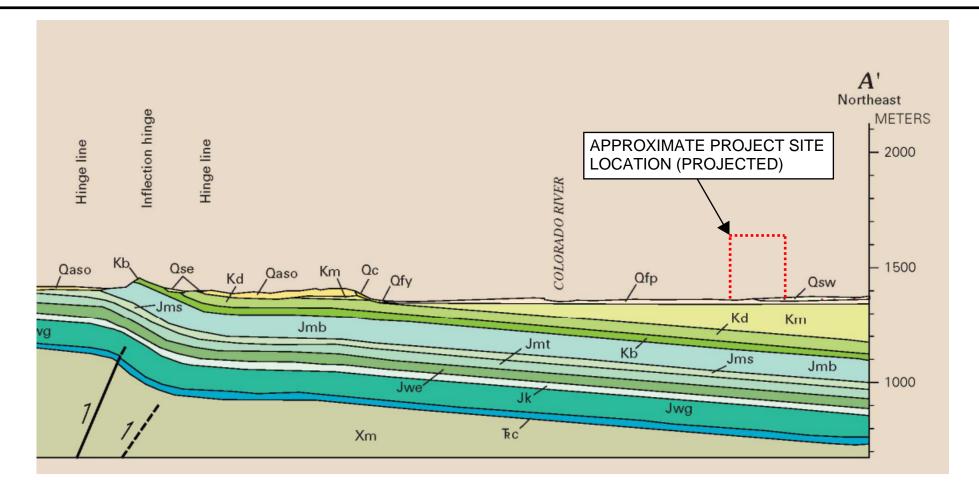
- Sheetwash deposits (Holocene and late Pleistocene)—Light-gray sandy clay and silty clay deposited on very gentle slope north of the Colorado River, derived from the Mancos Shale
- Mancos Shale (Upper Cretaceous)—Chiefly medium-dark-gray, dark-gray, brownish-gray, and brownish-black fissile shale that weathers light gray

NOTES:

- 1. THE GEOLOGIC MAP SHOWN IS TAKEN FROM GEOLOGIC MAPPING BY SCOTT AND HARDING, 2001.
- 2. SEE FIGURE 1B FOR SUBSURFACE PROFILE ALONG A-A' .

| WIF Engineers Architects | Project | PERSIGO WASTE WATER TREATMENT PLANT | Proj. No. | |
|---|-------------|--|-----------|-----------|
| MATERIALS SCIENTISTS | | 2145 RIVER ROAD, GRAND JUNCTION, CO | Date | |
| Wiss, Janney, Elstner Associates, Inc. 3609 South Wadsworth Boulevard, Suite 400 | Sheet Title | | Drawn | FIGURE 1A |
| Lakewood, Colorado 80235 | | GEOLOGIC MAP OF COLORADO NATIONAL MONUMENT AND | Checked | |
| 303.914.4300 tel 303.914.3000 fax www.wje.com | | ADJACENT AREAS, MESA COUNTY, COLORADO | Scale | |

© copyright Wiss, Janney, Elstner Associates, Inc.



DESCRIPTION OF MAP UNITS



Qsw

Km

Flood-plain and stream-channel deposits (Holocene and late Pleistocene) —Chiefly gravel in a sand matrix

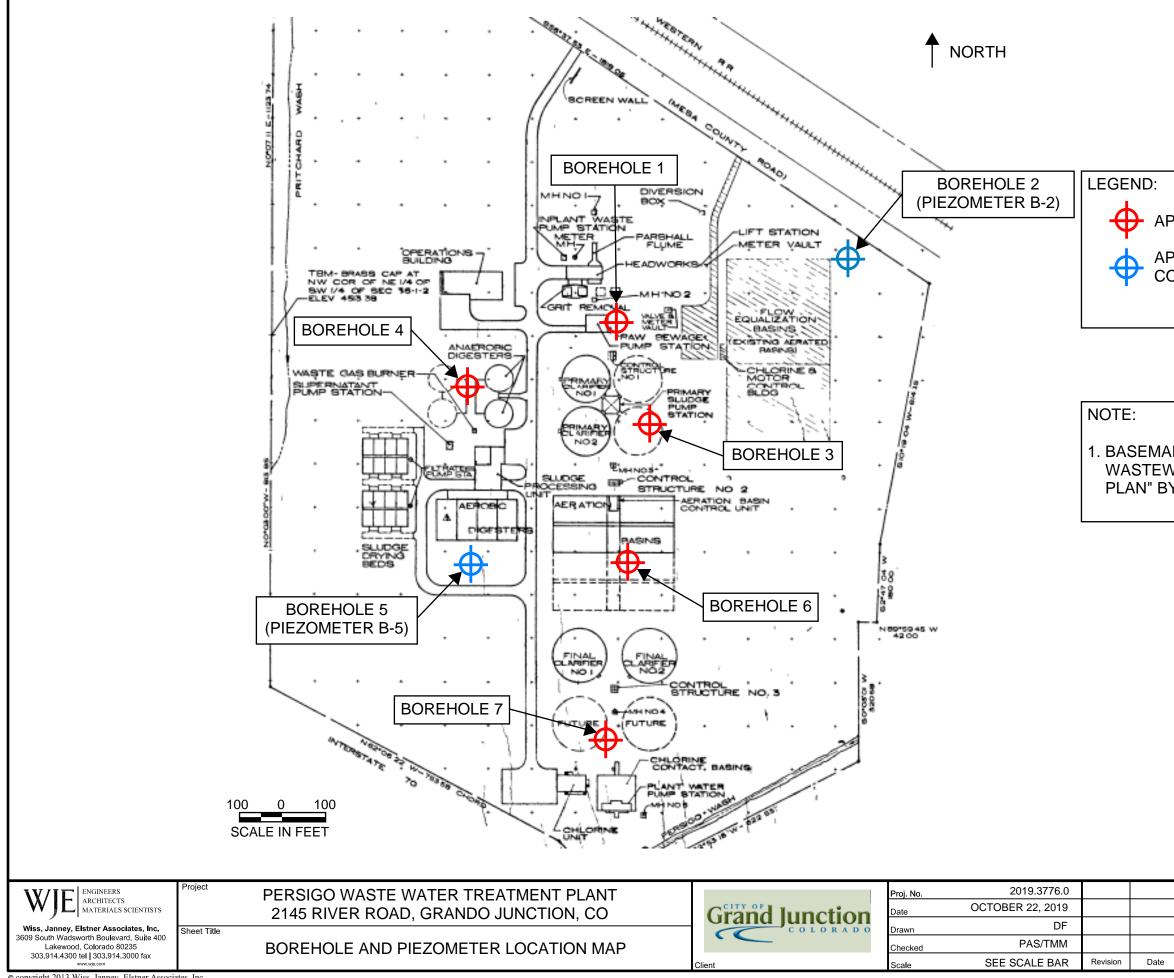
- Sheetwash deposits (Holocene and late Pleistocene)—Light-gray sandy clay and silty clay deposited on very gentle slope north of the Colorado River, derived from the Mancos Shale
- Mancos Shale (Upper Cretaceous)—Chiefly medium-dark-gray, dark-gray, brownish-gray, and brownish-black fissile shale that weathers light gray

NOTES:

- 1. THE GEOLOGIC SUBSURFACE PROFILE SHOWN IS TAKEN FROM GEOLOGIC MAPPING BY SCOTT AND HARDING, 2001.
- 2. SEE FIGURE 1A FOR GEOLOGIC MAP.

| W/I ENGINEERS | Project | PERSIGO WASTE WATER TREATMENT PLANT | Proj. No. | |
|---|-------------|--|-----------|-----------|
| ARCHITECTS | | FERSIGO WASTE WATER TREATMENT FLANT | | |
| MATERIALS SCIENTISTS | | 2145 RIVER ROAD, GRAND JUNCTION, CO | Date | |
| | | | | |
| Wiss, Janney, Elstner Associates, Inc. | Sheet Title | | Drawn | FIGURE 1B |
| 3609 South Wadsworth Boulevard, Suite 400 | | | | |
| Lakewood, Colorado 80235 | | GEOLOGIC MAP OF COLORADO NATIONAL MONUMENT AND | Checked | |
| 303.914.4300 tel 303.914.3000 fax | | ADJACENT AREAS, MESA COUNTY, COLORADO | | 1 |
| www.wje.com | | | Scale | |

© copyright Wiss, Janney, Elstner Associates, Inc.



© copyright 2013 Wiss, Janney, Elstner Associates, Inc.

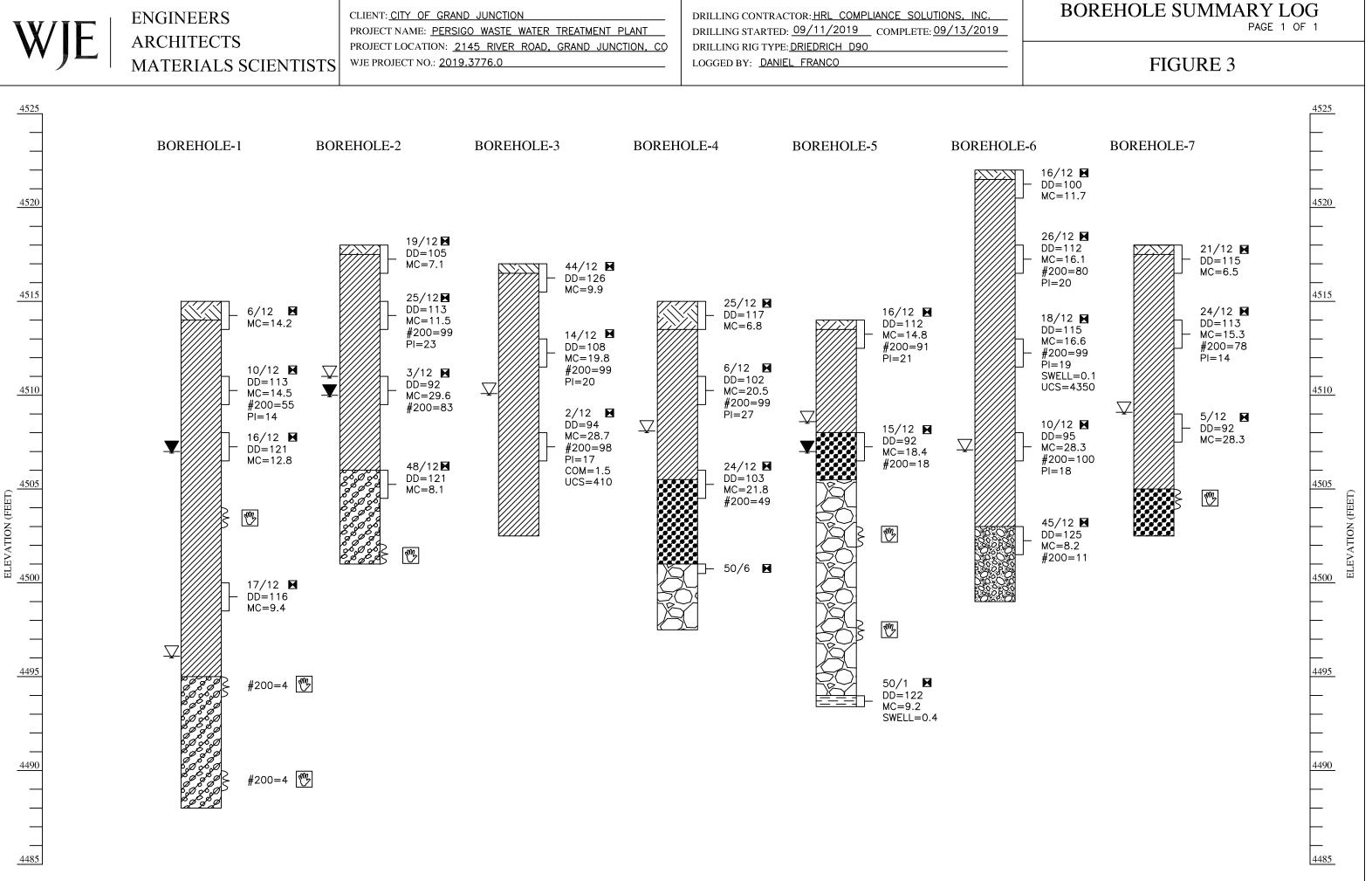
APPROXIMATE BOREHOLE LOCATION.

APPROXIMATE BOREHOLE LOCATION COMPLETED AS A PIEZOMETER.

1. BASEMAP TAKEN FROM PLAN SHEET "PERSIGO WASH WASTEWATER TREATMENT PLANT - OVERALL SITE PLAN" BY HDR DATED MARCH 18, 1981.

| FI | G | UF | R | Е | 2 |
|----|----------------------------------|----------|---|---|---|
| • | $\mathbf{\overline{\mathbf{v}}}$ | <u> </u> | | | _ |

Description



Diag ë ucted Constri Borir (CAD)\Detailed Boreholes Geotech\Soil 1 TREATMENT PLANT (TMM)\2B WASTEWATER PERSIGO 1 P:\2019\2019.3xxx\2019.3776.0

Lege

| | ENGINEERS | PROJE |
|-------|----------------------|--------|
| | ARCHITECTS | PROJE |
| VV JL | MATERIALS SCIENTISTS | CLIEN |
| | | WIE DE |

Т

PROJECT NAME: PERSIGO WASTE WATER TREATMENT PLANT

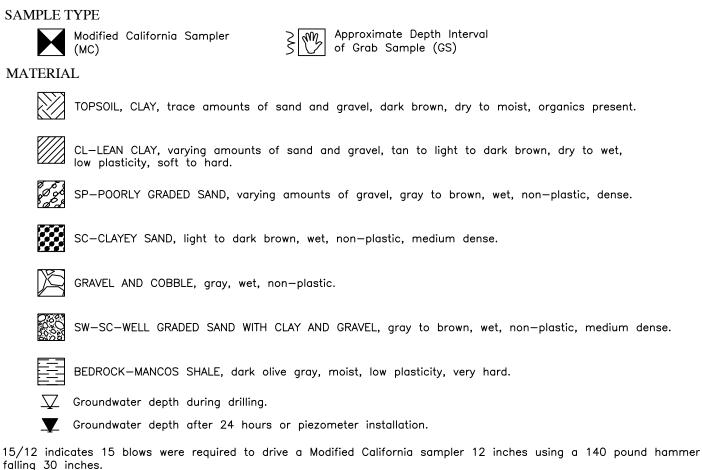
PROJECT LOCATION: 2145 RIVER ROAD, GRAND JUNCTION, CO

FIGURE 4

CLIENT: CITY OF GRAND JUNCTION

WJE PROJECT NO.: 2019.3776.0

BOREHOLE SUMMARY LOG LEGEND



LABORATORY TEST

DD= Dry Density (Ibs/ft³) MC= Moisture Content (%) #200= Fines Passing No. 200 sieve (%) PI= Plasticity Index SWELL= Swell upon wetting (%) COM= Compression upon wetting (%) UCS= Unconfined Compressive Strength (Ibs/ft²)

NOTES

- 1. The boreholes were drilled from September 11 to 13, 2019. A 4-inch diameter solid stem auger and a 6-inch diameter ODEX drill stem powered by a Diedrich D90 were used to advance the boreholes.
- The lines between materials represent the approximate contact between materials and transitions may be gradual.
 Groundwater was encountered during drilling. Refer to borehole logs for groundwater information.
- 4. Borehole locations are approximate as shown on Figure 2. Borehole locations are based on measurements from existing structures. The latitude and longitude coordinates listed in the detailed borehole logs were obtained from Google Earth.
- 5. Borehole elevations are based on "as recorded" drawings titled "Site Layout & Grading Plan South Half" and "Site Layout & Grading Plan North Half," dated on May 1985, by Henningson, Durham, & Richardson (HDR).



APPENDIX I - DETAILED BOREHOLE LOGS AND PIEZOMETER AS-BUILTS

| W | /]] | ARCHITECTS MATERIALS SCIENTISTS | | BOREHOLE: B-1 PAGE 1 OF 1 | | | | | | | | | | |
|---|--|--|-------------|---|---|-------------------------------------|-------------------------|--------------------------------|----------------|-------|---------------|-------|-----------|-------------------------|
| CLIEN | NT: <u>CI</u> | TY OF GRAND JUNCTION | | | PROJECT NAME: PERSIGO WASTE WATER TREATMENT PLANT | | | | | | | | | |
| WJE F | PROJE | CT NO.: <u>2019.3776.0</u> | | PROJECT LOCATION: 2145 RIVER ROAD, GRAND JUNCTION, CO | | | | | | | | | | |
| DRILLING STARTED: <u>09/12/2019</u> COMPLETE: <u>09/12/2019</u> DRILLING CONTRACTOR: <u>HRL COMPLIANCE SOLUTIONS, INC.</u> DRILLING RIG TYPE: <u>DIEDRICH D90</u> HOLE DIAMETER(IN.): <u>6</u> LOGGED BY: <u>DANIEL FRANCO</u> | | | | | | DELEVA NATES: OBEDR H TO G | <u>39.11</u> ROCK (I | <u>3650</u> • T): <u>NO</u> | N 108 T ENC | DUNTE | RED | DRILL | ING | |
| H | LOG | | TYPE | UE | JRE T (%) | VSITY (F | | AIN S RIBU (%) | IZE TION | | TERB LIMIT | | TT (%) | 3AK (PSF) |
| o DEPTH (FT) | GRAPHIC LOG | MATERIAL DESCRIPTION | SAMPLE TYPE | N VALUE | MOISTURE CONTENT (%) | DRY DENSITY (PCF) | GRAVEL | SAND | FINES | ΡL | LL | Id | COM/SWELL | UCS PEAK STRESS, (PS |
| | | TOPSOIL CL — sandy lean CLAY, trace gravel, brown, moist, low plasticity, medium stiff | | <u>6</u> 12 | 14.2 | _ | | | | | | | | |
| | | stiff | | <u>10</u> 12 | 14.5 | 113 | 4 | 41 | 55 | 14 | 28 | 14 | | |
| 10 | | Ţstiff | X | <u>16</u> 12 | 12.8 | 121 | | | | | | | | |
| | | increasing gravel content in cuttings | 8 22 | | | | | | | | | | | |
| | | stiff | | <u>17</u> 12 | 9.4 | 116 | | | | | | | | |
| | 000000 | SP — poorly graded SAND, trace gravel, brown, wet, non-plastic | ₩2 | | | | 7 | 89 | 4 | | | | | |
| 25 | 00000000000000000000000000000000000000 | with gravel | 1 | | | | 20 | 76 | 4 | | | | | |
| | - - | Bottom of borehole at 27.0 feet. | | | | | | | | | | | | |
| <u>30</u> COM | MENT | S: 24 hours after drilling, depth to groundwa | ter v | was 8 | B feet. | I | 1 | | I | | 1 | 1 | I | L |

| WJ | E ENGINEERS ARCHITECTS MATERIALS SCIENTISTS | | | | | | | BC | | HOL Ge 1 (| | 3-2 | |
|--|--|---------------------------------------|---|---|------------------------|-----------------|----------------------|-------|--------|---------------|------|-----------|-------------------------|
| CLIENT: C | ITY OF GRAND JUNCTION | | | PROJECT NAME: PERSIGO WASTE WATER TREATMENT PLANT | | | | | | | | | |
| WJE PROJE | BCT NO.: 2019.3776.0 | | PROJECT LOCATION: 2145 RIVER ROAD, GRAND JUNCTION, CO | | | | | | | | | | |
| DRILLING DRILLING DRILLING LOGGED B | | GROUNE COORDE DEPTH T _DEPT | NATES: O BEDR | <u>39.11</u> ROCK (I | 4518* T): <u>NO</u> | N 108 T ENCO | DUNTE | RED | DRILLI | NG | | | |
| H | | TYPE | UE | JRE T (%) | SITY (| | AIN S RIBU (%) | | | TERB LIMIT | | TT (%) | EAK (PSF) |
| DEPTH (FT) GRAPHIC LOG | MATERIAL DESCRIPTION | SAMPLE TYPE | N VALUE | MOISTURE CONTENT (%) | DRY DENSITY (PCF) | GRAVEL | SAND | FINES | ΡL | TT | Id | COM/SWELL | UCS PEAK STRESS, (PS |
| | TOPSOIL CL — lean CLAY, trace sand, tan to light brown, dry, low plasticity, stiff | | <u>19</u> 12 | 7.1 | 105 | | | | | | | | |
| | very stiff | X | <u>25</u> 12 | 11.5 | 113 | 0 | 1 | 99 | 18 | 41 | 23 | | |
| | \bigvee with sand, wet, soft | H | <u>3</u> 12 | 29.6 | 92 | 0 | 17 | 83 | | | | | |
| | increasing gravel content in cuttings | | 12 | 2010 | 02 | Ū | | | | | | | |
| | SP — poorly graded SAND with gravel, brown, wet, non—plastic, dense | | <u>48</u> 12 | 8.1 | 121 | | | | | | | | |
| | | E. | | | | | | | | | | | |
| | Bottom of borehole at 17.0 feet. | | | | | | | | | | | | |
| | | | | | | | | | | | | | |
| _ 25 | | | | | | | | | | | | | |
| COMMEN | S: After piezometer installation, depth to grou | undw | ater | was 8 1 | feet. | | | | | | | | |

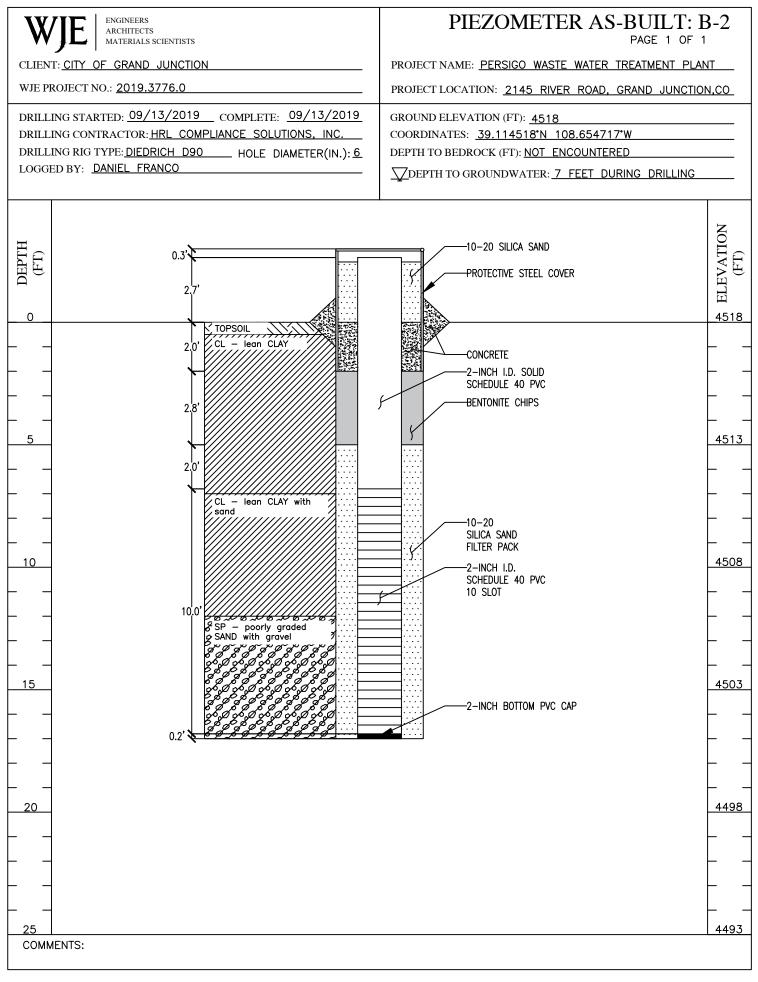
| W | /JI | ENGINEERS ARCHITECTS MATERIALS SCIENTISTS | | BOREHOLE: B-3 PAGE 1 OF 1 | | | | | | | | | | | |
|---------------------|---|---|-------------|------------------------------|---|---------------------------|---------------------------------|-----------------------------------|---|-------|---------------|-------|-----------|---------------------------|--|
| CLIEN | T: <u>CI</u> | TY OF GRAND JUNCTION | | | PROJECT NAME: PERSIGO WASTE WATER TREATMENT PLANT | | | | | | | | | | |
| | | CT NO.: <u>2019.3776.0</u> | | | PROJECT LOCATION: 2145 RIVER ROAD, GRAND JUNCTION, CO | | | | | | | | | | |
| DRILL DRILL | DRILLING STARTED: <u>09/13/2019</u> COMPLETE: <u>09/13/2019</u> DRILLING CONTRACTOR: <u>HRL COMPLIANCE SOLUTIONS, INC.</u> DRILLING RIG TYPE: <u>DIEDRICH D90</u> HOLE DIAMETER(IN.): <u>4</u> LOGGED BY: <u>DANIEL FRANCO</u> | | | | | DELEVA NATES: OBEDR | <u>39.1</u> ROCK (I ROUNI | 12971* FT): <u>NO</u> DWATE | <u>N 108</u> T ENCO R: <u>7</u> F | DUNTE | RED | DRILL | NG | | |
| H | LOG | | TYPE | UE | JRE T (%) | VSITY () | | AIN S RIBU (%) | | | TERB LIMIT | | LL (%) | îAK (PSF) | |
| o DEPTH (FT) | GRAPHIC | MATERIAL DESCRIPTION | SAMPLE TYPE | N VALUE | MOISTURE CONTENT (%) | DRY DENSITY (PCF) | GRAVEL | SAND | FINES | ΡL | TT | Id | COM/SWELL | UCS PEAK STRESS, (PSF) | |
| | | TOPSOIL CL — lean CLAY, tan to light brown, dry, low plasticity, hard | | <u>44</u> 12 | 9.9 | 126 | | | | | | | | | |
| | | trace sand, stiff | | <u>14</u> 12 | 19.8 | 108 | 0 | 1 | 99 | 18 | 38 | 20 | | | |
| _ <u>10</u> | | moist, soft | | <u>2</u> 12 | 28.7 | 94 | 0 | 2 | 98 | 17 | 34 | 17 | -1.5 | 410 | |
| | | | | | | | | | | | | | | | |
| | | Bottom of borehole at 14.5 feet. | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | |
| 25 | | | | | | | | | | | | | | | |
| COMN | IENT: | S: | | | | | | | | | | | | | |

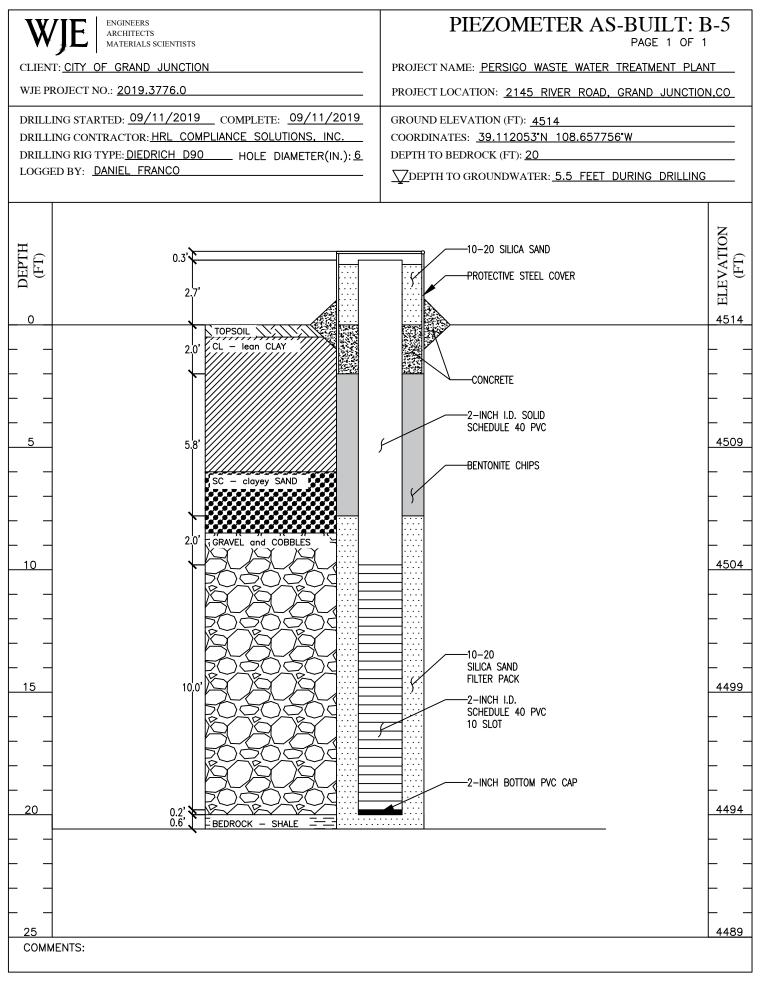
| W | /] F | ENGINEERS ARCHITECTS MATERIALS SCIENTISTS | | | | | | BC | | HOL GE 1 | | B-4 | | | |
|--------------------|---|--|-------------|---|---|--|--------------------------|-------------------------|----------------|-------------|---------------|--------|-----------|-------------------------|--|
| CLIEN | T: <u>CI</u> | Y OF GRAND JUNCTION | | | PROJECT NAME: PERSIGO WASTE WATER TREATMENT PLANT | | | | | | | | | | |
| WJE PI | ROJE | CT NO.: <u>2019.3776.0</u> | | PROJECT LOCATION: 2145 RIVER ROAD, GRAND JUNCTION, CO | | | | | | | | | | | |
| DRILL DRILL | DRILLING STARTED: <u>09/11/2019</u> COMPLETE: <u>09/11/2019</u> DRILLING CONTRACTOR: <u>HRL_COMPLIANCE_SOLUTIONS, INC.</u> DRILLING RIG TYPE: <u>DIEDRICH_D90</u> HOLE_DIAMETER(IN.): <u>6</u> LOGGED BY: <u>DANIEL_FRANCO</u> | | | | | D ELEVA NATES: O BEDF TH TO G | <u>39.1 ′</u> ROCK (I | 3219* FT): <u>NO</u> | N 108 T ENC | OUNTE | RED | DRILLI | NG | | |
| н | FOG | | TYPE | UE | JRE T (%) | YTI2 | | AIN S RIBU' (%) | | | TERB LIMIT | | TT (%) | EAK (PSF) | |
| o DEPTH (FT) | GRAPHIC | MATERIAL DESCRIPTION | SAMPLE TYPE | N VALUE | MOISTURE CONTENT (%) | DRY DENSITY (PCF) | GRAVEL | SAND | FINES | ΡL | LL | Id | COM/SWELL | UCS PEAK STRESS, (PS | |
| | | TOPSOIL very stiff CL — lean CLAY, trace sand, light brown, dry, low plasticity | | <u>25</u> 12 | 6.8 | 117 | | | | | | | | | |
| _ 5 | | medium stiff | | <u>6</u> 12 | 20.5 | 102 | 0 | 1 | 99 | 18 | 45 | 27 | | | |
| | | ∇ | | | | | | | | | | | | | |
| _ 10 | | SC — clayey SAND, light brown, wet, non-plastic, medium dense | X | <u>24</u> 12 | 21.8 | 103 | 0 | 51 | 49 | | | | | | |
| | | GRAVEL and COBBLE, gray, wet, non-plastic, dense | | <u>50</u> 6 | | | | | | | | | | | |
| <u> 15</u> _ | | GRAVEL and COBBLE, gray, wet, non-plasac, dense | | | | | | | | | | | | | |
| | | Bottom of borehole at 17.5 feet. | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | |
| COMM | IENT: | 5: | | | | | | | | | | | | | |

| WJE ENGINEERS ARCHITECTS MATERIALS SCIENTISTS | | | | BOREHOLE: B-5 PAGE 1 OF 1 | | | | | | | | | |
|---|---|---------------|------------------|---|---|-------------|-----------------------|-------|--------|---------------------|--------|-----------|--------------------------|
| CLIENT: CI | TY OF GRAND JUNCTION | | | PROJECT NAME: PERSIGO WASTE WATER TREATMENT PLANT | | | | | | | | | |
| WJE PROJE | WJE PROJECT NO.: 2019.3776.0 | | | | PROJECT LOCATION: 2145 RIVER ROAD, GRAND JUNCTION, CO | | | | | | | | |
| DRILLING | STARTED: <u>09/11/2019</u> COMPLETE: <u>09/11/2</u> CONTRACTOR: <u>HRL COMPLIANCE SOLUTIONS, INC</u> | C. | - | GROUNI COORDI | NATES: | <u>39.1</u> | 2053 | N 108 | .65775 | 56 ° W | | | |
| | RIG TYPE: <u>DIEDRICH D90</u> HOLE DIAMETER(IN Y: <u>DANIEL FRANCO</u> | l.): <u>6</u> | | DЕРТН Т ∑DЕРТ | | | | | FEET | DURIN | g dril | LING | |
| HOG I | OOG | | | EE (%) ITY | SITY | | AIN S RIBU' (%) | | | ATTERBERG LIMITS | | | 3AK (PSF) |
| O DEPTH (FT) GRAPHIC LOG | MATERIAL DESCRIPTION | SAMPLE TYPE | N VALUE | MOISTURE CONTENT (%) | DRY DENSITY (PCF) | GRAVEL | SAND | FINES | ΡL | LL | Id | COM/SWELL | UCS PEAK STRESS, (PSI |
| | TOPSOIL CL — lean CLAY, trace sand, light brown, dry, low plasticity, stiff | | <u>16</u> 12 | 14.8 | 112 | 0 | 9 | 91 | 17 | 38 | 21 | | |
| | SC - clayey SAND, light brown, wet, non-plastic, medium dense GRAVEL and COBBLE, gray, wet, non-plastic | | 1 <u>5</u> 12 | 18.4 | 92 | 0 | 82 | 18 | | | | | |
| | BEDROCK — SHALE, dark olive gray, moist, low plasticity, very hard | <u>***</u> | <u>50</u> | 9.2 | 122 | | | | | | | 0.4 | |
| 25 COMMENT | Bottom of borehole at 20.6 feet. S: After piezometer installation, depth to grou | Jindw | ater | was 7 · | feet. | | | | | | | | |

| WJE ENGINEERS ARCHITECTS MATERIALS SCIENTISTS | | | | | BOREHOLE: B-6 PAGE 1 OF 1 | | | | | | | | | |
|---|---|---|-------------|-----------------|---|----------------------|-----------------------------------|------|--------------|---------------|--------|--------------|--------------|-------------------------|
| CLIEN | CLIENT: CITY OF GRAND JUNCTION | | | | PROJECT NAME: PERSIGO WASTE WATER TREATMENT PLANT | | | | | | | | | |
| WJE F | WJE PROJECT NO.: 2019.3776.0 | | | | PROJEC | Γ LOCA | TION: | 2145 | RIVER | ROAD, | GRAN | <u>D JUN</u> | CTION. | <u>_CO_</u> |
| DRILI DRILI | LING (LING I | STARTED: <u>09/12/2019</u> COMPLETE: <u>09/12/2</u> CONTRACTOR: <u>HRL COMPLIANCE SOLUTIONS, INC</u> RIG TYPE: <u>DIEDRICH D90</u> HOLE DIAMETER(IN |). | . | GROUND ELEVATION (FT): <u>4522</u> COORDINATES: <u>39.112133'N 108.656501'W</u> DEPTH TO BEDROCK (FT): <u>NOT_ENCOUNTERED</u> | | | | | | | | | |
| LOGG | ED B | Y: DANIEL FRANCO | | • | <u>∑</u> DEP1 | TH TO G | ROUNI | WATE | R: <u>15</u> | FEET [| DURING | DRILL | ING | |
| H | LOG | | rype | Ε | JRE T (%) | () | GRAIN SIZE DISTRIBUTION (%) | | | TERB LIMIT | | LL (%) | EAK (PSF) | |
| o DEPTH (FT) | GRAPHIC LOG | MATERIAL DESCRIPTION | SAMPLE TYPE | N VALUE | N VALUE MOISTURE CONTENT (%) | DRY DENSITY (PCF) | GRAVEL | SAND | FINES | ΡL | LL | Id | COM/SWELL | UCS PEAK STRESS, (PS |
| | | TOPSOIL CL — lean CLAY, light brown, dry, low plasticity, stiff | X | <u>16</u> 12 | 11.7 | 100 | | | | | | | | |
| | | with sand, brown, dry to slightly moist, very stiff | | <u>26</u> 12 | 16.1 | 112 | 2 | 18 | 80 | 16 | 36 | 20 | | |
| | | trace sand, moist, stiff | | <u>18</u> 12 | 16.6 | 115 | 0 | 1 | 99 | 17 | 36 | 19 | 0.1 | 4350 |
| _ <u>15</u> | | ∑ brown and gray, wet, stiff | | 10 12 | 28.3 | 95 | 0 | 0 | 100 | 16 | 34 | 18 | | |
| 20 | 000000000000000000000000000000000000000 | SW—SC — well graded SAND with clay and gravel, gray and brown, wet, non—plastic, medium dense | | <u>45</u> 12 | 8.2 | 125 | 37 | 52 | 11 | | | | | |
| | | Bottom of borehole at 23.0 feet. | | | | | | | | | | | | |
| 25 COM | | S: | | | | | | | | | | | | |
| | | | | | | | | | | | | | | |

| WJEE ENGINEERS ARCHITECTS MATERIALS SCIENTISTS | | | | BOREHOLE: B-7 PAGE 1 OF 1 | | | | | | | | | |
|--|---|-------------|---------------------|---|---|--------|----------------------|-------|----|---------------------|----|-----------------------|-------------------|
| CLIENT: C | CLIENT: CITY OF GRAND JUNCTION | | | | PROJECT NAME: PERSIGO WASTE WATER TREATMENT PLANT | | | | | | | | |
| WJE PROJI | WJE PROJECT NO.: 2019.3776.0 | | | | PROJECT LOCATION: 2145 RIVER ROAD, GRAND JUNCTION, CO | | | | | | | | |
| DRILLING DRILLING | STARTED: <u>09/13/2019</u> COMPLETE: <u>09/13/2</u> CONTRACTOR: <u>HRL_COMPLIANCE_SOLUTIONS, INC</u> RIG TYPE: <u>DIEDRICH_D90</u> HOLE_DIAMETER(IN |). | - | GROUND ELEVATION (FT): <u>4518</u> COORDINATES: <u>39.110957'N 108.656657'W</u> DEPTH TO BEDROCK (FT): <u>NOT_ENCOUNTERED</u> | | | | | | | | | |
| LOGGED E | Y: <u>DANIEL FRANCO</u> | | - | $\sum DEPTH TO GROUNDWATER: 9 FEET DURING DRILLING$ | | | | | | | | | |
| H 100 | LOG H TYPE | | 0E | JRE T (%) | VITY () | | AIN S RIBU (%) | | | ATTERBERG LIMITS | | LL (%) | EAK (PSF) |
| o DEPTH (FT) GRAPHIC L | MATERIAL DESCRIPTION | SAMPLE TYPE | N VALUE MOISTURI | MOISTURE CONTENT (%) | DRY DENSITY (PCF) | GRAVEL | SAND | FINES | ΡL | LL | Id | COM/SWELL UCS PEAK | UCS PE STRESS, |
| | TOPSOIL CL — lean CLAY with sand, brown, dry, low plasticity, very stiff | | <u>21</u> 12 | 6.5 | 115 | | | | | | | | |
| | moist, very stiff | | 24 12 | 15.3 | 113 | 0 | 22 | 78 | 16 | 30 | 14 | | |
| - 10 | ↓ wet, soft | | <u>5</u> 12 | 28.3 | 92 | | | | | | | | |
| | SC — clayey SAND, dark brown, wet, non-plastic | ₩3 | | | | | | | | | | | |
| | Bottom of borehole at 15.5 feet. | | | | | | | | | | | | |
| | | | | | | | | | | | | | |
| 25 COMMEN | rs: | | | | | | | | | | | | |





Legend.dwg



APPENDIX II - LAB TEST RESULTS



| CLIENT Wiss Janney Elstner | | | JOB NO. | 3020-012 |
|---|---|--|--|---|
| PROJECT Persigo WWTP PROJECT NO | | | LOCATION | Grand Junction CO |
| BORING NO. DEPTH SAMPLE NO. | B-1 4' | B-2 3' | B-2 7' | B-3 4' |
| DATE SAMPLED DATE TESTED TECHNICIAN DESCRIPTION | 09/30/19 CT | 09/30/19 ALH | 09/30/19 TAF | 09/30/19 CT |
| Mass of Wet Soil and Pan (g): Mass of Dry Soil and Pan (g): Mass of Pan (g): Moisture (%): | 273.19 260.48 172.73 14.5 | 546.03 506.58 163.99 11.5 | 95.52 74.41 3.12 29.6 | 365.24 348.60 264.74 19.8 |
| Diameter (in): Height (in): Mass of Wet Soil and Ring (g): Mass of Ring (g): Wet Density (lbs/ft ³): Dry Density (lbs/ft ³): Wet Density (kg/m ³): Dry Density (kg/m ³): | 1.94 1.00 128.54 27.99 129.9 113.4 2080 1817 | 1.94 3.92 490.77 108.37 126.1 113.1 2020 1811 | 1.94 1.00 120.52 27.99 119.5 92.2 1914 1477 | 1.94 1.00 128.53 27.99 129.9 108.4 2080 1736 |
| BORING NO. DEPTH SAMPLE NO. | B-4 4' | B-4 9' | B-6 19' | B-7 4' |
| DATE SAMPLED DATE TESTED TECHNICIAN DESCRIPTION | 09/30/19 TAF | 09/30/19 TAF | 09/30/19 TAF | 09/30/19 ALH |
| Mass of Wet Soil and Pan (g): Mass of Dry Soil and Pan (g): Mass of Pan (g): Moisture (%): | 97.69 81.60 3.09 20.5 | 100.02 82.65 3.10 21.8 | 107.32 99.41 3.09 8.2 | 272.67 259.27 171.78 15.3 |
| Diameter (in): Height (in): Mass of Wet Soil and Ring (g): Mass of Ring (g): | 1.94 1.00 122.59 27.49 122.8 | 1.94 1.00 125.00 27.99 125.3 | 1.94 1.00 132.36 27.99 134.8 | 1.94 1.00 128.93 27.99 130.4 |
| Wet Density (Ibs/ft³): Dry Density (Ibs/ft³): Wet Density (kg/m³): Dry Density (kg/m³): NOTES | 122.8 101.9 1967 1633 | 125.3 102.8 2007 1647 | 134.8 124.6 2159 1995 | 130.4 113.0 2088 1811 |
| Data entry by: SPH Checked by: KMS File name: 3020012_Moisture | Date: Date: and Density AS ⁻ | 10 219 | _ | |



| CLIENT Wiss Janney Elstner | | | JOB NO. | 3020-012 | | | |
|---|--|--|--|--|--|--|--|
| PROJECT Persigo WWTP PROJECT NO | | | LOCATION | Grand Junction CO | | | |
| BORING NO. DEPTH SAMPLE NO. | B-1 0' | B-1 7' | B-1 15.5' | B-2 0' | | | |
| DATE SAMPLED DATE TESTED TECHNICIAN DESCRIPTION | 10/01/19 CAL | 10/01/19 CAL | 10/01/19 CAL | 10/01/19 CAL | | | |
| Mass of Wet Soil and Pan (g): Mass of Dry Soil and Pan (g): Mass of Pan (g): Moisture (%): | 345.19 303.17 6.66 14.2 | 427.22 379.47 6.54 12.8 | 309.00 283.02 6.73 9.4 | 351.20 328.49 6.67 7.1 | | | |
| Diameter (in): Height (in): Mass of Wet Soil and Ring (g): Mass of Ring (g): Wet Density (lbs/ft³): Dry Density (lbs/ft³): Wet Density (kg/m³): Dry Density (kg/m³): | Density Not Possible | 1.93 3.99 420.64 0.00 137.0 121.4 2194 1945 | 1.93 3.12 302.44 0.00 126.9 116.0 2033 1858 | 1.94 3.98 344.67 0.00 112.1 104.7 1796 1678 | | | |
| BORING NO. DEPTH SAMPLE NO. DATE SAMPLED DATE TESTED TECHNICIAN | B-2 12' 10/01/19 CAL | B-3 0' 10/01/19 CAL | B-4 0' 10/01/19 CAL | B-6 0' 10/01/19 CAL | | | |
| DESCRIPTION Mass of Wet Soil and Pan (g): Mass of Dry Soil and Pan (g): Mass of Pan (g): Moisture (%): | 288.62 267.38 6.68 8.1 | 435.67 397.17 6.72 9.9 | 353.73 331.71 6.50 6.8 | 249.74 224.22 6.41 11.7 | | | |
| Diameter (in): Height (in): Mass of Wet Soil and Ring (g): Mass of Ring (g): Wet Density (lbs/ft³): Dry Density (lbs/ft³): Wet Density (kg/m³): Dry Density (kg/m³): | 1.93 2.80 386.36 104.00 131.1 121.2 2100 1942 | 1.93 4.04 429.14 0.00 138.1 125.7 2212 2014 | 1.93 3.61 347.37 0.13 124.8 116.9 1999 1872 | 1.93 2.85 243.38 0.00 111.7 100.0 1790 1602 | | | |
| NOTES * filing required due to gravel, side wall voids due to gravel Data entry by: KMS Date: 10/2/2019 Checked by: Cmc Date: 10/2/2019 File name: 3020012Moisture and Density ASTM D7236_1.xls | | | | | | | |



| CLIENT Wiss Janney Elstner | | | JOB NO. | 3020-012 |
|--|--|--|---|--|
| PROJECT Persigo WWTP PROJECT NO | | | LOCATION | Grand Junction CO |
| BORING NO. DEPTH SAMPLE NO. DATE SAMPLED | B-5 0' | B-5 6' | B-6 4' | B-6 14' |
| DATE SAMPLED DATE TESTED TECHNICIAN DESCRIPTION | 10/01/19 TAF | 10/01/19 TAF | 10/01/19 TAF | 10/01/19 TAF |
| Mass of Wet Soil and Pan (g): Mass of Dry Soil and Pan (g): Mass of Pan (g): Moisture (%): | 516.09 465.41 123.24 14.8 | 223.75 210.64 139.49 18.4 | 273.34 259.36 172.36 16.1 | 267.45 246.55 172.73 28.3 |
| Diameter (in): Height (in): Mass of Wet Soil and Ring (g): Mass of Ring (g): Wet Density (lbs/ft³): Dry Density (lbs/ft³): Wet Density (kg/m³): Dry Density (kg/m³): | 1.94 3.96 502.47 109.33 128.0 111.5 2051 1786 | 1.94 1.00 112.38 27.98 108.3 91.5 1735 1465 | 1.94 1.00 129.18 27.98 129.9 111.9 2081 1793 | 1.94 1.00 123.29 27.98 122.3 95.4 1960 1527 |
| BORING NO. DEPTH SAMPLE NO. DATE SAMPLED DATE TESTED TECHNICIAN DESCRIPTION | | | | |
| Mass of Wet Soil and Pan (g): Mass of Dry Soil and Pan (g): Mass of Pan (g): Moisture (%): | | | | |
| Diameter (in): Height (in): Mass of Wet Soil and Ring (g): Mass of Ring (g): Wet Density (lbs/ft ³): Dry Density (lbs/ft ³): Wet Density (kg/m ³): Dry Density (kg/m ³): NOTES | | | | |
| Data entry by: CAL | Data | 10/2/2010 | | |
| Checked by: KM6 | Date: Date: and Density AST | 10/4/19 | | |



| CLIENT Wiss Janney Elstner | | | JOB NO. | 3020-012 | | | | |
|---|---|--|-----------|-------------------|--|--|--|--|
| PROJECT Persigo WWTP PROJECT NO | | | LOCATION | Grand Junction CO | | | | |
| BORING NO. DEPTH SAMPLE NO. DATE SAMPLED | B-7 0' | B-7 9' | | | | | | |
| DATE TESTED TECHNICIAN DESCRIPTION | 10/01/19 CAL * | 10/01/19 CAL | | | | | | |
| Mass of Wet Soil and Pan (g): Mass of Dry Soil and Pan (g): Mass of Pan (g): Moisture (%): | 365.04 343.20 6.68 6.5 | 351.51 275.52 6.73 28.3 | | | | | | |
| Diameter (in): Height (in): Mass of Wet Soil and Ring (g): Mass of Ring (g): Wet Density (lbs/ft ³): Dry Density (lbs/ft ³): Wet Density (kg/m ³): | 1.93 3.81 358.50 0.00 122.4 114.9 1961 | 1.92 3.84 345.08 0.00 117.8 91.8 1887 | , | | | | | |
| Dry Density (kg/m ³): | 1841 | 1471 | | | | | | |
| BORING NO. DEPTH SAMPLE NO. DATE SAMPLED DATE TESTED TECHNICIAN DESCRIPTION | | | 5 | | | | | |
| Mass of Wet Soil and Pan (g): Mass of Dry Soil and Pan (g): Mass of Pan (g): Moisture (%): | | | | | | | | |
| Diameter (in): Height (in): Mass of Wet Soil and Ring (g): Mass of Ring (g): Wet Density (lbs/ft ³): Dry Density (lbs/ft ³): Wet Density (kg/m ³): Dry Density (kg/m ³): | | | | | | | | |
| NOTES | *B-7 @ 0' Filling | required due to | o gravel. | | | | | |
| Data entry by: KMS Date: 10/2/2019 Checked by: | | | | | | | | |



| CLIENT JOB NO. PROJECT PROJECT NO. LOCATION | Wiss Janney Elstner 3020-012 Persigo WWTP Grand Junction CO | | BORING NO. DEPTH SAMPLE NO. DATE SAMPLED DESCRIPTION | B-1 0' liner |
|---|--|-------------|---|--------------------|
| | | Antip De | er 3020-012 Wiss Janney Estas Persigo WWTP n Grand Junction CT | |
| NOTES | Density No | nt Possible | | |
| | | | | 2 |
| | | | | |
| File name: | 3020012lmage_19_10_02 | 2_06_35_04 | | |



ADVANCED TERRA TESTING

| CLIENT JOB NO. PROJECT PROJECT NO. LOCATION DATE TESTED TECHNICIAN | Wiss Janney Elstne 3020-012 Persigo WWTP Grand Junction CO 10/08/19 TAF | r | - | DEPTH SAMPLE NO. DATE SAMPLED | | |
|---|--|---|---|---|---|---|
| | 1 | | Plastic Limits | 5 | | |
| Mass of Wet Pan Mass of Dry Pan Mass of Pan (g): Moisture (%) | | 7.79 6.97 1.07 13.9 | 6.86 6.17 1.17 13.8 | | | |
| | | | Liquid Limits | | | |
| Number of Blows Mass of Wet Pan Mass of Dry Pan Mass of Pan (g): Moisture (%) | | 15 7.92 6.34 1.13 30.3 | 17 8.03 6.46 1.16 29.7 | 21 8.05 6.49 1.10 28.9 | 23 8.27 6.70 1.14 28.1 | 32 7.58 6.19 1.11 27.4 |
| | | | Plastic Index | | | |
| | Plastic Limit: Liquid Limit: Plastic Index: | 14 28 14 | Atter | berg Classification: Method: | CL A | |
| 40 | Flow Curve | | | | ticity Chart | |
| 35 (%) 30 25 20 10 | 15 20 Number of Blov | 25 30 | 50 40 30 31 30 35 0 | | | CH MH 60 70 80 |
| NOTES | | | | | Liquid Limit | |
| 4 | CAL KMS 3020012 Atterberg | ASTM D431 | Date Date | e: 10/9/2019 e: 10/9/2019 | | |



| ADVANCED TERRA TESTING | | | | | |
|---|--|---|--|---|----------------------|
| CLIENTWiss Janney ElsJOB NO.3020-012PROJECTPersigo WWTPPROJECT NOLOCATIONGrand JunctionDATE TESTED10/04/19TECHNICIANCAL | | - | BORING NO. DEPTH SAMPLE NO. DATE SAMPLED SAMPLED BY DESCRIPTION | B-2 3' | |
| | 1 | Plastic Limit | S | | |
| Mass of Wet Pan and Soil (g): Mass of Dry Pan and Soil (g): Mass of Pan (g): Moisture (%) | 6.64 5.81 1.14 17.8 | 7.43 6.50 1.14 17.3 | | | |
| | 0 | Liquid Limit | S | | |
| Number of Blows Mass of Wet Pan and Soil (g): Mass of Dry Pan and Soil (g): Mass of Pan (g): Moisture (%) | 15 10.40 7.58 1.15 43.9 | 17 9.77 7.15 1.09 43.2 | 23 10.05 7.44 1.17 41.7 | 29 9.21 6.87 1.07 40.4 | |
| | | Plastic Inde | | | |
| Plastic Limit Liquid Limit Plastic Index | : 41 | | erberg Classification: Method: | CL A | |
| Flow Cu | | | Pla | sticity Chart | |
| 50 48 46 44 42 40 10 15 Number of | 20 25 30 Blows | - 4 Sastic Index 1 | | CL ML 30 40 50 Liquid Limit | CH MH 60 70 80 |
| NOTES | Δ | | | | |
| Data entry by: CAL Checked by: <u>5PH</u> File name: 3020012_Atter | Derg ASTM D431 | | te: 10/7/2019 te: 10-7-19 | | |



-1

| JOB PRC PRC LOC DAT | ENT 3 NO. DJECT DJECT NO. CATION TE TESTED CHNICIAN | Wiss Janney Elstner 3020-012 Persigo WWTP Grand Junction CO 10/08/19 ALH | | • | BORING NO. DEPTH SAMPLE NO. DATE SAMPLED SAMPLED BY DESCRIPTION | | |
|---|---|---|-------------------------------------|--|--|----------------------|----------------------|
| | | | | Plastic Limit | \$ | | |
| Mas Mas | | n and Soil (g): and Soil (g): | 8.36 7.25 1.17 18.3 | 8.32 7.21 1.15 18.2 | | | |
| | | | | | | | |
| _ | | | | Liquid Limits | | | |
| Number of Blows Mass of Wet Pan and Soil (g): Mass of Dry Pan and Soil (g): Mass of Pan (g): | | and Soil (g): and Soil (g): | 16 7.63 5.79 1.04 | 25 9.36 7.10 1.14 | 28 11.01 8.32 1.13 | | |
| Mois | sture (%) | | 38.7 | 37.9 | 37.4 | | |
| - | | | | Plastic Index | [| | |
| | | Plastic Limit: Liquid Limit: Plastic Index: | 18 38 20 | - Atte | rberg Classification: Method: | | |
| | 40 | Flow Curve | | | | sticity Chart | |
| Moisture (%) | 40 38 36 34 32 30 10 | 15 20 Number of Blow | 25 30 s | 50 44 50 31 31 32 35 | | CL ML 30 40 50 | CH MH 60 70 80 |
| NOT | TES | | | | | Liquid Limit | |
| | | | | | | | |
| Che | a entry by: cked by: name: | CAL KMS 3020012_Atterberg | ASTM D4318 | | e: 10 9 9/2019 e: 10 9 9 | | |



-1

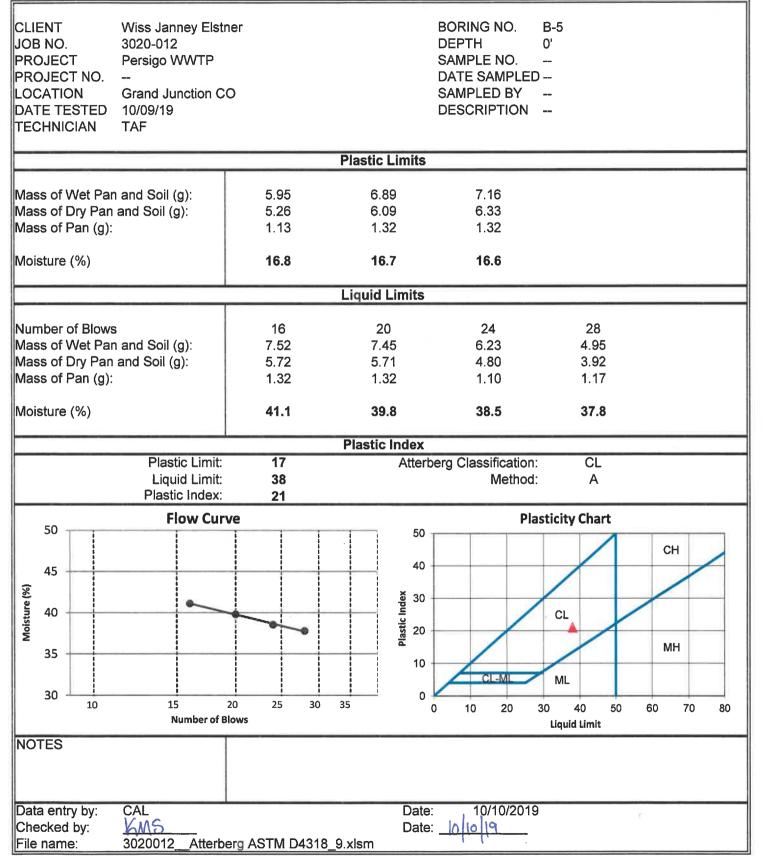
ADVANCED TERRA TESTING

| CLIENT JOB NO. PROJECT PROJECT N LOCATION DATE TEST TECHNICIAI | Grand Junction CO ED 10/04/19 | | - | DEPTH SAMPLE NO. DATE SAMPLED | |
|--|--|---|--|---|--|
| | | | Plastic Limits | ; | |
| Mass of Dry Mass of Pan | | 7.94 6.95 1.09 | 7.89 6.92 1.13 | | |
| Moisture (%) | | 16.9 | 16.8 | | |
| | | | Liquid Limits | | |
| | Pan and Soil (g): Pan and Soil (g): (g): | 15 8.96 6.94 1.15 34.8 | 23 9.38 7.30 1.14 33.8 | 28 8.71 6.82 1.13 33.2 | |
| | | | | | |
| | Plastic Limit: | 17 | Plastic Index | berg Classification: | CL |
| | Liquid Limit: Plastic Index: | 34 17 | , | Method: | A |
| 40 | Flow Curve | 2 | | | ticity Chart |
| 38 38 36 34 32 30 1 | 0 15 20 Number of Blox | | - 40 40 <u>a a a 30</u> <u>b a a 30</u> <u>c a a a a a a a a a a a a a a a a a a a</u> | | CL CL MH ML 0 40 50 60 70 80 Liquid Limit |
| NOTES | | | - | | |
| Data entry by Checked by: File name: | SPH | g ASTM D4318 | Date Date 3_2.xlsm | | |



| y Elstner VTP tion CO | | SAMPLED BY | | |
|---|--|---|--|---|
| | Plastic Limits | | | |
| 8.20 7.14 1.15 17.7 | 8.22 7.17 1.15 17.4 | | | |
| | Liquid Limits | | | |
| 17 11.27 8.03 1.09 46.8 | 21 10.55 7.59 1.09 | 28 8.80 6.44 1.11 44.1 | 31 9.94 7.26 1.10 43.6 | |
| | Plastic Index | | | |
| Limit: 18 Limit: 45 ndex: 27 | | | | |
| v Curve | • | Pla | sticity Chart | |
| 20 25 30 ber of Blows | 40 - | CL-ML 0 10 20 | | CH MH 60 70 80 |
| | | | | |
| | Date: Date: | | | |
| | VTP tion CO 8.20 7.14 1.15 17.7 11.27 8.03 1.09 46.8 Limit: 18 Limit: 45 ndex: 27 v Curve | VTP tion CO Plastic Limits 8.20 7.14 7.14 1.15 1.77 1.15 1.77 1.15 1.77 1.15 1.77 1.15 1.77 1.15 1.09 1.09 1.09 46.8 45.5 Plastic Index Limit: 18 Atterb Limit: 45 ndex: 27 v Curve \int_{20}^{20} 25 30 35 ber of Blows | VTP tion CO Plastic Limits 8.20 8.20 7.14 7.17 1.15 17.7 1.15 17.7 1.15 17.7 1.15 17.7 1.15 17.7 1.15 | $\begin{array}{c} \text{DEPTH} & 4'\\ \text{SAMPLE NOD}\\ \text{DATE SAMPLED DYDESCRIPTION}\\ \hline \\ \hline$ |

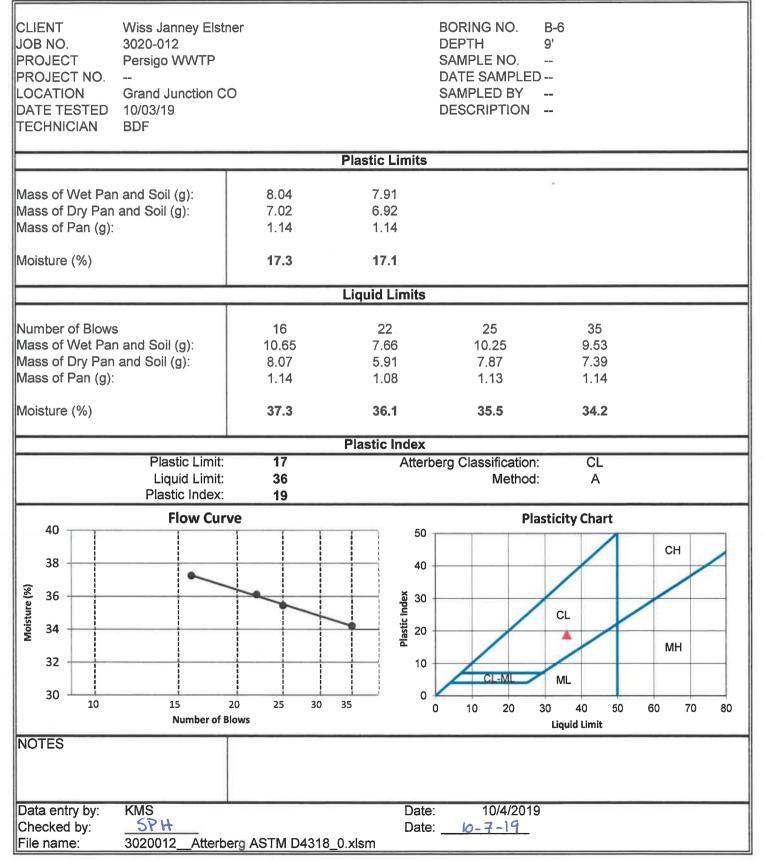






| ADVANCED | RRA TESTING | | | | | |
|---|---|--|--|--|-------------------------|------------|
| CLIENT JOB NO. PROJECT PROJECT NO. LOCATION DATE TESTED TECHNICIAN | Wiss Janney Elstr 3020-012 Persigo WWTP Grand Junction Co 10/09/19 ALH | | | BORING NO. DEPTH SAMPLE NO. DATE SAMPLED SAMPLED BY DESCRIPTION | | |
| | | | Plastic Limits | | | |
| Mass of Wet Par Mass of Dry Pan Mass of Pan (g): Moisture (%) | and Soil (g): | 8.44 7.42 1.16 16.3 | 8.44 7.42 1.09 16.1 | | | |
| | | | Liquid Limits | | | |
| Number of Blows Mass of Wet Par Mass of Dry Pan Mass of Pan (g): Moisture (%) | n and Soil (g): and Soil (g): | 19 11.71 8.83 1.12 37.4 | 28 12.64 9.62 1.17 35.7 | 33 11.43 8.79 1.10 34.3 | | |
| | | | Plastic Index | | | |
| | Plastic Limit: Liquid Limit: Plastic Index: | 16 36 20 | | berg Classification: Method: | | |
| 40 | Flow Curv | /e | | | asticity Chart | |
| 40 38 36 36 34 32 | | ~ | 50 40 30 10 10 | CL-ML | CL ML | CH MH |
| 30 <u>10</u> | 15 Number of B | 20 25 30 Iows | 35 0 | | 30 40 5 Liquid Limit | 0 60 70 80 |
| NOTES Data entry by: Checked by: File name: | CAL <u>KMS</u> 3020012Atterbe | erg ASTM D431 | Date Date 8_8.xlsm | |) | |







| TESTING | | | | | |
|--|--|---|--|--|---|
| liss Janney Elstner 020-012 ersigo WWTP rand Junction CO 0/08/19 AF | | • | DEPTH SAMPLE NO. DATE SAMPLED SAMPLED BY | 14' | |
| | | Plastic Limits | | | |
| id Soil (g): d Soil (g): | 8.77 7.73 1.13 15.9 | 8.63 7.66 1.33 15.4 | | | |
| | | Liquid Limits | | | |
| d Soil (g): d Soil (g): | 17 7.72 5.97 1.15 | 19 7.29 5.70 1.15 | 23 7.86 6.12 1.12 | 25 7.86 6.13 1.08 | 28 7.86 6.19 1.15 |
| | 36.1 | 35.2 | 34.7 | 34.1 | 33.2 |
| | | Plastic Index | | | |
| Plastic Limit: Liquid Limit: Plastic Index: | 16 34 18 | Atter | berg Classification: Method: | CL A | |
| Flow Curve | | | Plast | ticity Chart | |
| 15 20 Number of Blows | 25 30 | 50 40 <u>30</u> <u>10</u> 35 0 | | | CH MH 60 70 80 |
| | | | | Liquia Limit | |
| AL <u>MS</u> 20012_Atterberg | ASTM D4318 | Date | | | |
| | riss Janney Elstner 120-012 ersigo WWTP rand Junction CO 10/08/19 AF d Soil (g): d Soil (g): d Soil (g): flow Curve Flow Curve Flow Curve 15 20 Number of Blows | riss Janney Elstner 120-012 ersigo WWTP rand Junction CO 108/19 AF d Soil (g): 8.77 d Soil (g): 7.73 1.13 15.9 d Soil (g): 7.72 5.97 1.15 36.1 Plastic Limit: 16 Liquid Limit: 34 Plastic Index: 18 Flow Curve 15 20 25 30 Number of Blows | iss Janney Elstner 120-012 ersigo WWTP rand Junction CO 1/08/19 AF Plastic Limits d Soil (g): 1.773 7.66 1.13 15.9 15.9 15.4 Cliquid Limits 17 19 7.72 7.29 5.97 5.70 1.15 1.15 36.1 35.2 Plastic Index: Plastic Index: 18 Flow Curve 15 10 15 10 15 10 15 10 15 10 15 10 15 10 15 10 15 10 15 10 15 10 10 10 10 10 10 10 10 10 15 20 25 30 35 20 10 10 10 15 20 10 15 20 10 15 20 10 15 20 10 15 20 15 20 10 10 15 20 10 10 15 20 10 10 15 20 10 10 15 20 10 10 15 20 10 10 15 20 10 15 20 10 15 20 10 15 20 10 15 20 10 15 20 10 15 20 25 30 35 10 1 | iss Janney Elstner 220-012 prsigo WWTP rand Junction CO 708/19 NF $Plastic Limits$ $Plastic Limits$ $\frac{Plastic Limits}{15.9}$ $\frac{Plastic Limits}{15.9}$ $\frac{17}{1.13}$ $\frac{19}{1.13}$ $\frac{23}{1.15}$ $\frac{17}{1.15}$ $\frac{19}{1.15}$ $\frac{23}{1.15}$ $\frac{17}{1.15}$ $\frac{19}{1.15}$ $\frac{23}{1.15}$ $\frac{17}{1.15}$ $\frac{19}{1.15}$ $\frac{23}{1.15}$ $\frac{112}{1.15}$ $\frac{115}{1.15}$ $\frac{112}{1.15}$ 11 | iss Janney Elstner BORING NO. B-6 prisgo WWTP DEPTH 14' and Junction CO SAMPLED 0. V08/19 DATE SAMPLED V V8 DESCRIPTION DATE SAMPLED DY DATE SAMPLED V V08/19 SAMPLED DY V7 DESCRIPTION V8 Liquid Limits U 17 19 23 25 15.9 15.4 U 17 19 23 25 15.9 15.4 U 17 19 23 25 15 oil (g): 7.72 7.29 7.86 7.86 15 oil (g): 1.15 1.15 1.12 1.08 36.1 35.2 34.7 34.1 Plastic Limit: 16 Method: A Liquid Limit: 34 15 20 25 30 35 <td< td=""></td<> |



| ADVANCED TER | RATESTING | | | | | | | |
|---|---|-------------------------------------|----------|--|--|----------------------------|-----------------------------|----------------------|
| JOB NO. PROJECT PROJECT NO. LOCATION DATE TESTED | Wiss Janney Elstner 3020-012 Persigo WWTP Grand Junction CO 10/08/19 ALH | | i. | | BORING NO. DEPTH SAMPLE NO DATE SAMP SAMPLED B DESCRIPTIC | 4' LED Y | | |
| | 1 | | Pla | stic Limits | ; | | | |
| Mass of Wet Pan Mass of Dry Pan a Mass of Pan (g): Moisture (%) | | 8.52 7.50 0.97 15.7 | | 8.72 7.70 1.15 15.5 | | | | |
| | | | | | | | | |
| | 1 | | Liq | uid Limits | | | | |
| Number of Blows Vass of Wet Pan Vass of Dry Pan a Vass of Pan (g): | | 18 11.75 9.20 1.11 | - | 20 11.98 9.40 1.08 | 27 11.38 9.02 1.14 | | 31 11.36 9.03 1.13 | |
| Moisture (%) | | 31.5 | | 31.0 | 30.0 | | 29.5 | |
| | | | Pla | stic Index | | | | |
| | Plastic Limit: Liquid Limit: Plastic Index: | 16 30 14 | • | Atter | berg Classificat Meth | | CL A | |
| 40 | Flow Curve | | | | | Plasticity | Chart | |
| 35 Woisting 30 25 20 10 | 15 20 Number of Blows | | | 50 40 30 20 <u>Jastic</u> 10 0 | CL-ML | CL ML 30 4 Liquid | 0 50 Limit | CH MH 60 70 80 |
| NOTES | < | | | | | | | |
| Checked by: | CAL CAL CAS 3020012Atterberg | ASTM D43 | 18 4.xls | | e: 10/9/20 e: 10/9/19 |)19 | 5 | |



ADVANCED TERRA TESTING

| CLIENT JOB NO. PROJECT PROJECT N LOCATION DATE TEST TECHNICIAI | Grand Junction (ED 10/01/19 | | - | BORING NO. DEPTH SAMPLE NO. DATE SAMPLED DESCRIPTION | | |
|--|--|-----------------------------|------------------------------|--|-----------------------------|----------------------------------|
| | c Moisture Wet Pan and Soil (g) s Dry Pan and Soil (g) Mass of Pan (g) Moisture (%) | : 260.48 : 172.73 | | Sample Data ass of Sample (g): ass of Sample (g): | | |
| Sieve Num | ber Sieve Size (mm) | Mass of Pan and Soil (g) | Mass of Pan (g) | Mass of Individual Retained Soil (g) | Correction Factor | Percent Passing by Weight (%) |
| 3" | 76.2 | | | | let er | |
| 1.5" | 38.1 | | | | | |
| 3/4" | 19.05 | | | | | 100.0 |
| 3/8" | 9.53 | 2.5 | | 2.5 0.51 | 1.00 <u>1.00</u> 1.00 | 97.2 96.6 96.0 95.5 |
| #4 | 4.75 | 0.51 | | | | |
| #10 | 2.00 | 0.49 | | 0.49 | | |
| #20 | 0.850 | 0.50 | | 0.50 | 1.00 | |
| #40 | 0.425 | 2.0 | | 2.0 | 1.00 | 93.2 |
| #60 | 0.250 | 12.5 | | 12.5 | 1.00 | 78.9 |
| #100 | 0.150 | 12.5 | | 12.5 | 1.00 | 64.7 |
| #140 | 0.106 | 4.4 | | 4.4 | 1.00 | 59.7 |
| #200 | 0.075 | 3.8 | | 3.8 | 1.00 | 55.3 |
| | 1.5" 3/4" | | sing vs Log of Pa #10 #20 | #40 #60 #100 # | #140 #200 | |
| 00 Meiðht | | | | | | |
| 80 × 80 | | | - | X | | |
| L / V | | | | | | |
| b 60 | | | | ~ | | |
| f 60 50 40 | | | | | 1 | |
| 8 40 | Gravel (+#4) | | Sands (+#200) | | Silts & Clays (-# | 200) |
| | | 6 | (î | â | | |
| ent | | #+) p | - + br | (+#20 | | |
| 20 10 | | Course Sand (*** 0) | v Weijirm Sind (+#40) | Samé (+#200) | | |
| e 10 | | 2 C | de diur | | | |
| 0 | | | | | | |
| 100 | | 10 | 1 Particle Size (mm |) | 0.1 | 0.01 |
| | | USCS CI | assification AST | M D 2487 | | |
| | tterberg Classification | | | of Curvature - C _c : | | |
| A | | | | of Uniformity - C _u : | | |
| A | Group Symbol | | | | | |
| A | Group Symbol: USCS Classification: | | Coemolent | | | |
| | USCS Classification | | | | | |
| A Data entry by Checked by: | USCS Classification | | Date: | 10/9/2019 | | |



ADVANCED TERRA TESTING

| CLIENT JOB NO. PROJECT PROJECT NO. LOCATION DATE TESTED TECHNICIAN | Wiss Janney Elst 3020-012 Persigo WWTP Grand Junction C 10/01/19 BNF | | | BORING NO. DEPTH SAMPLE NO. DATE SAMPLED DESCRIPTION | | |
|--|---|-----------------------------|--|--|----------------------|----------------------------------|
| Mass W | loisture of Fines (et Pan and Soil (g): (g): Mass of Pan (g): Moisture (%): | 302.45 124.06 | Total Dry Ma | Sample Data ass of Sample (g): ass of Sample (g): Split Fraction: mple Fraction (g): | 1433.1 #4 | 13 |
| Sieve Number | Sieve Size (mm) | Mass of Pan and Soil (g) | Mass of Pan (g) | Mass of Individual Retained Soil (g) | Correction Factor | Percent Passing by Weight (%) |
| 3" 1.5" 3/4" | 76.2 38.1 19.05 | 0.0 0.0 0.0 | | | | |
| 3/8" #4 #10 | 9.53 4.75 2.00 | 33.7 61.2 8.66 | - | 33.7 61.2 8.66 | 1.00 1.00 0.93 | 97.6 93.4 88.8 |
| #20 #40 #60 | 0.850 0.425 0.250 | 0.87 11.9 70.8 | | 0.87 11.9 70.8 | 0.93 0.93 0.93 | 88.4 82.2 45.1 |
| #100 #140 #200 | 0.150 0.106 0.075 | 61.9 10.7 6.15 | - | 61.9 10.7 6.15 | 0.93 0.93 0.93 | 12.7 7.2 3.9 |
| 100 3" | 1.5" 3/4" 3 | | sing vs Log of Pa #10 #20 | | #140 #200 | |
| 00 pt 60 minutes for the second secon | | | | | | |
| 50 50 40 30 20 20 10 | Gravel (+#4) | (0) send (+#10) | Sands (+#200) | Sand (+#2(0) | Siits & Clays (-# | 200) |
| ີສີ 10 0 100 | | 10 | المعلم المعلم Particle Size (mm | e e | 0.1 | 0.01 |
| | berg Classification: Group Symbol: SCS Classification: | | | M D 2487 of Curvature - C _c : of Uniformity - C _u : | | |
| Data entry by: Checked by: File name: | KMS | Size Analysis AST | Date: Date: M D6913_4.xlsm | 10/2/2019 <i>10/3/2019</i> | | |



ADVANCED TERRA TESTING

| CLIENT JOB NO. PROJECT PROJECT NO. OCATION DATE TESTED FECHNICIAN | Wiss Janney Elst 3020-012 Persigo WWTP Grand Junction C 10/01/19 BNF | | | BORING NO. DEPTH SAMPLE NO. DATE SAMPLED DESCRIPTION | | |
|---|--|--|--------------------------------|--|----------------------|----------------------------------|
| | t Pan and Soil (g): Pan and Soil (g): Pan and Soil (g): Mass of Pan (g): Moisture (%): | 332.90 123.12 | Total Dry Ma | Sample Data ass of Sample (g): ass of Sample (g): Split Fraction: mple Fraction (g): | 1083.9 #4 | |
| Sieve Number | Sieve Size (mm) | Mass of Pan and Soil (g) | Mass of Pan (g) | Mass of Individual Retained Soil (g) | Correction Factor | Percent Passing by Weight (%) |
| 3" | 76.2 | 0.0 | | | | |
| 1.5" | 38.1 | 0.0 | | | | |
| 3/4" | 19.05 | 0.0 | | | | 100.0 |
| 3/8" | 9.53 | 116.1 | | 116.1 | 1.00 | 89.3 |
| #4 | 4.75 | 104.4 | | 104.4 | 1.00 | 79.7 |
| #10 | 2.00 | 8.40 | | 8.40 | 0.80 | 76.5 75.7 |
| #20 | 0.850 | 2.03 | - | 2.03 | 0.80 | |
| #40 | 0.425 | 12.1 | | 12.1 | 0.80 | 71.1 |
| #60 | 0.250 | 86.1 | 1 | 86.1 | 0.80 | 38.4 |
| #100 | 0.150 | 72.6 | | 72.6 | 0.80 | 10.8 6.3 4.0 |
| #140 | 0.106 | 11.9 | | 11.9 | 0.80 0.80 | |
| #200 | 0.075 | 6.10 | | 6.10 | 0.80 | 4.0 |
| | 1.5" 3/4" 3 | | sing vs Log of Pa #10 #20 | | #140 #200 | |
| 100 | 1.5 5/4 5 | /8 #4 1 | #10 #20 | #40 #00 #100 | 140 #200 | |
| 00 60 10 10 10 10 10 10 10 1 | | | | | | |
| 80 | | | | | | |
| ≥ ₇₀ | | | * | | | |
| | | | | \backslash | | |
| 5 50 | | | | | | |
| u 50 | Gravel (+#4) | | Sands (+#200) | | Silts & Clays (-# | 200) |
| Aq 60 50 40 | | - | 6 | × × | | |
| t ³⁰ | | 0 | (0+++) pur s | (0)22#+) | | |
| ម៉ូ 20 | | and the second s | S and | Sand (+ | | |
| 30 20 20 10 10 10 10 10 10 10 10 10 10 10 10 10 | | Course Sand (**10) | We | | | |
| - ₀ | | | 2 | | | |
| 100 | | 10 | 1 Particle Size (mm |) | 0.1 | 0.01 |
| | | USCS CI | assification AST | M D 2487 | | |
| Atterb | erg Classification: | | Coefficient | of Curvature - C _c : | 0.93 | |
| | Group Symbol: | | | of Uniformity - C _u : | | |
| US | CS Classification: | | | - , - u. | | |
| Data entry by: | KMS | | Date: | 10/2/2019 | | |
| Checked by: | CAL | | Date: | | | |
| File name: | | Size Analysis AST | | | | |



ADVANCED TERRA TESTING

IF.

| CLIENT JOB NO. PROJECT PROJECT LOCATION DATE TES TECHNICI, | NO. N STED | Wiss Janney Els 3020-012 Persigo WWTP Grand Junction (10/01/19 ALH | | | | BORING NO. DEPTH SAMPLE NO. DATE SAMPLED DESCRIPTION | B-2 3' | |
|--|--|--|-----------------------|--------------|-----------------------------|--|----------------------|----------------------------------|
| | ss We | isture t Pan and Soil (g) y Pan and Soil (g) Mass of Pan (g) Moisture (%) | 506.58 163.99 | | | Sample Data ass of Sample (g): ass of Sample (g): | | |
| Sieve Nur | mber | Sieve Size (mm) | Mass of Pa Soil (g | | Mass of Pan (g) | Mass of Individual Retained Soil (g) | Correction Factor | Percent Passing by Weight (%) |
| 3" | | 76.2 | | | | | | |
| 1.5" | | 38.1 | | | | | | |
| 3/4" | | 19.05 | | | | | | |
| 3/8" | | | | | | | | |
| #4 | | 4.75 | | | No 110 | | | 41 - 2 |
| #10 | | 2.00 | 0.0 | | 0.0 | | | 100.0 |
| #20 | #20 0.850 #40 0.425 #60 0.250 #100 0.150 | | 0.17 | | 0.0 | 0.17 | 1.00 | 100.0 |
| #40 | | | 0.26 | | 0.0 | 0.26 | 1.00 | 99.9 |
| #60 | | | 0.19 | | 0.0 | 0.19 | 1.00 | 99.8 |
| #100 | | | 0.45 | | 0.0 | 0.45 | 1.00 | 99.7 |
| #140 |) | 0.106 | 0.87 | | 0.0 | 0.87 | 1.00 | 99.4 |
| #200 |) | 0.075 | 2.54 | | 0.0 | 2.54 | 1.00 | 98.7 |
| 100 | 3" | 1.5" 3/4" | Percer 3/8" #4 | | sing vs Log of P #10 #20 | | #140 #200 | |
| 보 90 — | | | | | | | | |
| 00 N Neight | | | | | | | | |
| × 70 | | | | | • | | | |
| 2 | | | | | | | | |
| | | | | | | | | |
| busse 40 | | Gravel (+#4) | | | Sands (+#200) | | Silts & Clays (+ | \$200) |
| | | | | (0) | 40) | (0 | | |
| <u> </u> | | | | Sand (+#) 0) | Me fitum S and (+ a a d) | (0)7#+)) | | |
| 9 20 | | | | e Sar | S E | Sand | | |
| ല് 10 | - | | | Colifse | Mediu | ů Ľ | | |
| 0 | 1 | | | | | | | |
| 100 | | | 10 | | 1 Particle Size (mm |) | 0.1 | 0.01 |
| | _ | | US | CS CI | assification AST | M D 2487 | | |
| | Atterb | erg Classification | CL | | Coefficient | of Curvature - C _c : | | |
| | | Group Symbol | | | | of Uniformity - Cu: | | |
| | US | CS Classification | | | cocincient | $\mathbf{O}_{\mathbf{U}}$ | | |
| Data entry I | | CAL | Louin Olay | | Date: | 10/7/2019 | | |
| Checked by | | SPH | | | Date: | 10-7-19 | | |
| File name: | y. | | Size Analys | ie AQT | M D6913_6.xlsm | | | |
| ne name. | | | Size Analys | 10 70 1 | IVI DUB I 3_0.XISIII | | | |



ADVANCED TERRA TESTING

ſř

| CLIENT JOB NO. PROJECT PROJECT N LOCATION DATE TEST TECHNICIA | Grand Junction C ED 10/01/19 | | | BORING NO. DEPTH SAMPLE NO. DATE SAMPLED DESCRIPTION | | |
|---|--|-----------------------------|------------------------------|--|----------------------|----------------------------------|
| | ic Moisture s Wet Pan and Soil (g): ss Dry Pan and Soil (g): Mass of Pan (g): Moisture (%): | 74.41 3.12 | | Sample Data ass of Sample (g): ass of Sample (g): | | |
| Sieve Num | nber Sieve Size (mm) | Mass of Pan and Soil (g) | Mass of Pan (g) | Mass of Individual Retained Soil (g) | Correction Factor | Percent Passing by Weight (%) |
| 3" | 76.2 | 0.0 | | | | |
| 1.5" | 38.1 | 0.0 | | | | |
| 3/4" | 19.05 | 0.0 | | | | |
| 3/8" | 9.53 | 0.0 | | | | |
| #4 | 4.75 | 0.0 | | | | |
| #10 | 2.00 | 0.0 | | | | 100.0 |
| #20 | 0.850 | . 0.54 | | 0.54 | 1.00 | 99.2 |
| #40 | 0.425 | 0.39 | | 0.39 | 1.00 | 98.7 |
| #60 | 0.250 | 0.50 | | 0.50 | 1.00 | 98.0 |
| #100 | 0.150 | 1.29 | | 1.29 | 1.00 | 96.2 |
| #140 | 0.106 | 2.76 | | 2.76 | 1.00 | 92.3 |
| #200 | 0.075 | 6.67 | | 6.67 | 1.00 | 83.0 |
| | " 1.5" 3/4" 3 | | sing vs Log of Pa #10 #20 | | #140 #200 | |
| 00 08 00 00 00 00 00 00 00 00 00 00 00 0 | | | | | | |
| 08 e | | | | | | |
| 1 : 10 + 1 | | | | | | |
| | | | | | | |
| bassing 40 | | | | | | |
| <i>S</i> 40 | Gravel (+#4) | | Sands (+#200) | | Silts & Clays (-# | 200) |
| e 40 | | 6 | 6 | | | |
| t ³⁰ | | Contrae Setup | Sand (+#4.0) | Sand (+#200) | | |
| ³⁰ 20 10 | | 2 S | 8 | +) pure | | |
| a 10 | | 8 | Medium | හි ම E | | |
| | | Ŭ | ž | L. | | |
| 100 | | 10 | 1 Particle Size (mm |) | 0.1 | 0.01 |
| | | USCS CI | assification AST | M D 2487 | | |
| | Atterberg Classification: | | | of Curvature - C _c : | | |
| (| Group Symbol: | | , | of Uniformity - C_u : | | |
| | USCS Classification: | | Coenicient | $O_{\rm u}$ | | |
| Data ontar h | | | Deter | 40/0/0040 | _ | |
| Data entry b | | | Date: | 10/2/2019 | | |
| Checked by File name: | | Cine Anellicie ACT | Date: | 10/3/2019 | | |
| rile name: | 3020012Grain | Size Analysis AST | IVI DO913_2.XISM | | | |



| ADVANCED | ERRA TESTING | | | | | | | |
|--|---|-----------------------------|--|---|----------------------|----------------------------------|--|--|
| CLIENT JOB NO. PROJECT PROJECT NO. LOCATION DATE TESTED TECHNICIAN | Wiss Janney Elst 3020-012 Persigo WWTP Grand Junction C 10/01/19 ALH | | - | | | | | |
| | oisture et Pan and Soil (g): y Pan and Soil (g): Mass of Pan (g): Moisture (%): | 348.60 264.74 | | Sample Data ass of Sample (g): ass of Sample (g): | | | | |
| Sieve Number | Sieve Size (mm) | Mass of Pan and Soil (g) | Mass of Pan (g) | Mass of Individual Retained Soil (g) | Correction Factor | Percent Passing by Weight (%) | | |
| 3" 1.5" 3/4" | 76.2 38.1 19.05 | | | | | | | |
| 3/8" #4 #10 | 9.53 4.75 2.00 | 0.00 | | 100.0 | | | | |
| #20 #40 #60 | 0.850 0.425 0.250 | 0.13 0.05 0.03 | | 0.13 0.05 0.03 | 1.00 1.00 1.00 | 99.8 99.8 99.7 | | |
| #100 #140 #200 | 0.150 0.106 0.075 | 0.06 0.05 0.22 | 0.06 1.00 99. 0.05 1.00 99. 0.22 1.00 99. | | | | | |
| 3"· | 1.5" 3/4" 3 | | sing vs Log of P #10 #20 | article Size #40 #60 #100# | 41.40.#200 | | | |
| 100 90 80 70 60 50 50 40 | Gravel (+#4) | | - Sands (+#200) | | | | | |
| H 30 | Giava (* ** 4) | Course Sand (+#10) | | Flive Sank (+#2:0) | Silts & Clays (# | | | |
| 0 1 00 | | 10 | 1 Particle Size (mm |) | 0.1 | 0.01 | | |
| US | berg Classification: Group Symbol: SCS Classification: | CL CL | Coefficient | of Curvature - C _c : of Uniformity - C _u : | | | | |
| Data entry by: Checked by: File name: | CAL KMS 3020012_Grain | Size Analysis AST | Date: Date: M D6913_13.xlsr | 10/9/2019 10/9/2019 | | | | |



ADVANCED TERRA TESTING

5

| CLIENT JOB NO. PROJECT PROJECT NO LOCATION DATE TESTE TECHNICIAN | Grand Junct D 10/01/19 | TP | | | | | BORING NO. DEPTH SAMPLE NO. DATE SAMPLEI DESCRIPTION | B-3 9') | | |
|--|--|----------------------|-----------------------|-------------|-------------|------------------------|--|------------------------|-------------------|----------------------------------|
| | Moisture Wet Pan and Soi Dry Pan and Soi Mass of Par Moisture | l (g): 2 n (g): 1 | 243.43 139.91 | | | | Sample Data ass of Sample (g): ass of Sample (g): | | | |
| Sieve Numb | , | mm) | Mass of Pa Soil (g | | Mass of | Pan (g) | Mass of Individual Retained Soil (g) | F | rection actor | Percent Passing by Weight (%) |
| 3" | 76.2 | | | | | | | | | |
| 1.5" | | | | | | | | | | |
| 3/4" | | | | | | | | | | - |
| 3/8" | 3/8" 9.53 #4 4.75 #10 2.00 #20 0.850 | | | | | | | | | |
| #4 | | | | | | | | | | |
| #10 | | | 0.0 | | 0.0 | 0 | | | | |
| #20 | | | 0.04 | ŀ | 0.0 | D | 0.04 | | 1.00 | 100.0 |
| #40 | 0.425 | | 0.04 | Ļ – | 0.0 | D | 0.04 | | 1.00 | 99.9 |
| #60 | #60 0.250 #100 0.150 | | 0.09 |) | 0.0 | C | 0.09 | | 1.00 | 99.8 |
| #100 | | | 0.18 | 3 | 0.0 | | 0.18 | | 1.00 | 99.7 |
| #140 | 0.106 | | 0.43 | | 0.0 | | 0.43 | | 1.00 | 99.2 |
| #200 | 0.075 | | 1.21 | | 0.0 | | 1.21 | | 1.00 | 98.1 |
| | | | | | | | article Size | | | |
| 3" | 1.5" 3/4" | 3/8 | | | #10 | #20 | #40 #60 #100 | #140 #20 | 0 | |
| 100 | * * | | • | | 1 | * | * * * | | _ | |
| 00 Meight | | | | | | | | | | |
| 1 80 | | | | | | | | | | |
| 70 | | | | | | | | | | |
| <u>م</u> م | | | | | | | | | | |
| D 00 | | | | | | | | | | |
| b 50 b | Gravel (+#4) | | | | Sands (+ | (200) | | | Silts & Clays (-# | (200) |
| 6 40 | | | | | | | | - | | |
| 00 | | _ | | (0 # | | +840) | 6 | | | |
| 20 20 10 | | | | Sand (+# 0) | _ | Sand (+#40) | Fine Sama (+#200) | | | |
| u 10 | | | | Course S | | Medlum S | e Sa | | | |
| _ | | | | បី | | Me | ιĔ | | | |
| 0 + 100 | | 10 |) | | Particle S | 1 i ze (mm) |) | 0.1 | | 0.01 |
| | · · · · · · · · · · · · · · · · · · · | | 21 | SCS CH | assificatio | | M D 2487 | | | |
| ΔΗ | erberg Classifica | tion: C | | | | | of Curvature - C _c : | | _ | |
| Au | Group Sym | | | | | | | | | |
| | | | | | COE | | of Uniformity - C _u : | | | |
| Data ant | USCS Classifica | uon: L | ean clay | | | D : | 10,000 | | | |
| Data entry by: | | | | | | Date: | 10/7/2019 | | | |
| Checked by: | KMS | nain O | | | M Doodo | Date: | 10/7/19 | | | |
| File name: | 3020012G | rain S | ize Analys | SIS AS I | W D6913 | _r.xism | 1.1 | | | |



ADVANCED TERRA TESTING

[F

| Sieve Number Sieve Size (mm) Soil (g) Mass of Pan (g) Individual Retained Soil (g) Factor by W 3" 76.2 | nt Passing /eight (%) |
|--|------------------------------|
| Sieve Number Sieve Size (mm) Mass of Pan and Soil (g) Mass of Pan (g) Individual Retained Soil (g) Correction Factor Perce by W 3" 76.2 | eight (%) |
| 1.5" 38.1 3/4" 19.05 3/8" 9.53 #4 4.75 #10 2.00 0.0 0.0 0.0 1.00 #20 0.850 0.04 0.0 0.0 1.00 #40 0.425 0.06 0.0 0.06 1.00 #40 0.425 0.06 0.0 0.06 1.00 #40 0.425 0.06 0.0 0.10 1.00 #100 0.150 0.08 0.0 0.08 1.00 #140 0.106 0.05 0.0 0.05 1.00 #200 0.075 0.10 0.0 0.10 1.00 Percent Passing vs Log of Particle Size 100 3" 1.5" 3/4" 3/8" #4 #10 #20 #40 #60 #100 #140 #200 10 | |
| 3/4" 19.05 | |
| 3/8" 9.53 #4 4.75 #10 2.00 0.0 0.0 0.0 1.00 #20 0.850 0.04 0.0 0.0 1.00 #40 0.425 0.06 0.0 0.06 1.00 #40 0.425 0.06 0.0 0.06 1.00 #40 0.425 0.06 0.0 0.06 1.00 #40 0.150 0.08 0.0 0.10 1.00 #100 0.150 0.08 0.0 0.05 1.00 #140 0.106 0.05 0.0 0.10 1.00 #200 0.075 0.10 0.0 0.10 1.00 100 3''' 1.5''' 3/4''' 3/8''' #4 #10 #20 #40 #60 #100 #140 #200 | |
| #4 4.75 #10 2.00 0.0 0.0 0.0 1.00 1.00 1.00 #20 0.850 0.04 0.0 0.0 1.00 1.00 #40 0.425 0.06 0.0 0.06 1.00 1.00 #60 0.250 0.10 0.0 0.10 1.00 #100 0.150 0.08 0.0 0.08 1.00 #140 0.106 0.05 0.0 0.05 1.00 #200 0.075 0.10 0.0 0.10 1.00 #200 3" 1.5" 3/4" 3/8" #4 #10 #20 #40 #60 #100 #140 #200 | |
| #10 2.00 0.0 0.0 0.0 1.00 #20 0.850 0.04 0.0 0.0 1.00 #40 0.425 0.06 0.0 0.06 1.00 #60 0.250 0.10 0.0 0.10 1.00 #100 0.150 0.08 0.0 0.08 1.00 #140 0.106 0.05 0.0 0.05 1.00 #200 0.075 0.10 0.0 0.10 1.00 #200 0.375 0.10 0.0 0.10 1.00 #200 0.375 0.10 0.0 0.10 1.00 #200 3/4" 3/8" #4 #10 #20 #40 #60 #100 #140 #200 | |
| #20 0.850 0.04 0.0 0.0 1.00 #40 0.425 0.06 0.0 0.06 1.00 #60 0.250 0.10 0.0 0.10 1.00 #100 0.150 0.08 0.0 0.08 1.00 #140 0.106 0.05 0.0 0.105 1.00 #200 0.075 0.10 0.0 0.10 1.00 #200 3" 1.5" 3/4" 3/8" #4 #10 #20 #40 #60 #100 #140 #200 | |
| #40 0.425 0.06 0.0 0.06 1.00 #60 0.250 0.10 0.0 0.10 1.00 #100 0.150 0.08 0.0 0.08 1.00 #140 0.106 0.05 0.0 0.05 1.00 #200 0.075 0.10 0.0 0.10 1.00 #200 0.075 0.10 0.0 0.10 1.00 #200 0.075 0.10 0.0 0.10 1.00 #200 0.075 0.10 0.0 0.10 1.00 #4 #10 #20 #40 #60 #100 #140 #200 | 00.0 |
| #60 0.250 0.10 0.0 0.10 1.00 #100 0.150 0.08 0.0 0.08 1.00 #140 0.106 0.05 0.0 0.05 1.00 #200 0.075 0.10 0.00 0.10 1.00 #200 0.075 0.10 0.0 0.10 1.00 #200 0.375 0.10 0.0 0.10 1.00 #200 0.375 0.10 0.0 0.10 1.00 #200 3" 1.5" 3/4" 3/8" #4 #10 #20 #40 #60 #100 #140 #20 | 99.9 |
| #100 0.150 0.08 0.0 0.08 1.00 #140 0.106 0.05 0.0 0.05 1.00 #200 0.075 0.10 0.0 0.10 1.00 #200 0.075 0.10 0.0 0.10 1.00 #200 0.075 0.10 0.0 0.10 1.00 #200 0.075 0.10 0.0 0.10 1.00 #200 0.075 0.10 0.0 0.10 1.00 #200 3" 1.5" 3/4" 3/8" #4 #10 #20 #40 #60 #100 #140 #200 | 99.9 |
| #140 0.106 0.05 0.0 0.05 1.00 #200 0.075 0.10 0.0 0.10 1.00 #200 0.075 0.10 0.0 0.10 1.00 0.0 0.10 0.10 0.10 1.00 #200 0.75 0.10 0.0 0.10 1.00 0.0 0.10 0.10 0.10 1.00 1.00 100 3" 1.5" 3/4" 3/8" #4 #10 #20 #40 #60 #100 #140 #200 | 99.7 |
| #200 0.075 0.10 0.0 0.10 1.00 Percent Passing vs Log of Particle Size 100 3" 1.5" 3/4" 3/8" #4 #10 #20 #40 #60 #100 #140 #200 | 99.6 |
| Percent Passing vs Log of Particle Size 3" 1.5" 3/4" 3/8" #4 #10 #20 #40 #60 #100 #140 #200 | 99.6 |
| 100 ^{3"} 1.5" 3/4" 3/8" #4 #10 #20 #40 #60 #100 #140 #200 | 99.5 |
| 90 | |
| 5 8 0 | |
| | |
| ₹ ₇₀ | |
| | |
| | |
| Gravel (+#4) Sands (+#200) Silts & Clays (-#200) | |
| | |
| | |
| 20 20 20 20 20 20 20 20 20 20 20 20 20 2 | |
| And Control Control Control 30 30 30 30 20 30 30 30 30 30 30 < | |
| | |
| 100 10 1 0.1 Particle Size (mm) | 0.01 |
| USCS Classification ASTM D 2487 | |
| Atterberg Classification: CL Coefficient of Curvature - C _c : | |
| Group Symbol: CL Coefficient of Uniformity - C _u : | |
| USCS Classification: Lean Clay | |
| Data entry by: CAL Date: 10/7/2019 | |
| Checked by: $5PH$ Date: $10-7-19$ | |
| File name: 3020012_Grain Size Analysis ASTM D6913_8.xlsm | |



ADVANCED TERRA TESTING

| CLIENT JOB NO. PROJECT PROJECT LOCATIO DATE TE TECHNIC | t no. N Sted | Wiss Janney Elst 3020-012 Persigo WWTP Grand Junction C 10/01/19 BNF | | | BORING NO. DEPTH SAMPLE NO. DATE SAMPLED DESCRIPTION | | |
|--|--------------------|---|-----------------------------|-------------------|--|----------------------|----------------------------------|
| | ass We | isture Pan and Soil (g): Pan and Soil (g): Mass of Pan (g): Moisture (%): | 82.65 3.10 | | Sample Data ass of Sample (g): ass of Sample (g): | | |
| Sieve N | | Sieve Size (mm) | Mass of Pan and Soil (g) | Mass of Pan (g) | Mass of Individual Retained Soil (g) | Correction Factor | Percent Passing by Weight (%) |
| 3" | | 76.2 | 0.0 | | | | |
| 1.5 | | 38.1 | 0.0 | | | | |
| 3/4 | | 19.05 | 0.0 | | | | |
| 3/8 | | 9.53 | 0.0 | | | | |
| #4 | | 4.75 | 0.0 | | | | |
| #10 | | 2.00 | 0.0 | | 0.0 | 1.00 1.00 | 100.0 99.9 |
| #20 | | 0.850 | 0.0 | | 0.0 | | |
| #40 | | 0.425 | 1.6 | | 1.6 | 1.00 | 97.9 |
| #6 | | 0.250 | 3.9 | | 3.9 | 1.00 | 93.0 |
| #10 | | 0.150 | 8.1 | | 8.1 | 1.00 | 82.8 |
| #14 | | 0.106 | 12.3 | <u> </u> | 12.3 | 1.00 | 67.3 |
| #20 | 0 | 0.075 | 14.1 | | 14.1 | 1.00 | 49.6 |
| | | | | sing vs Log of Pa | | | |
| 100 უ | 3" | 1.5" 3/4" 3 | /8" #4 | #10 #20 | #40 #60 #100 | #140 #200 | |
| ± 90 - | | | | | ~ | | |
| 08 Neight | | | | | | | |
| | | | | | | | |
| | | | | | | X | |
| 5 60 + | + | | | | | | |
| Bassing - 05 90 - 05 90 - 05 | - | 01/1//// | | | | | (2020) |
| 8 40 + | - | Gravel (+#4) | | Sands (+#200) | | Silts & Clays (4 | (200) |
| | | | 6 | 40) | <u>(</u> | | |
| 5 20 - | | | (+) pu | (++ | (+#200) | | |
| | | | Course Sand (+#10) | s mil | L R S S S | | |
| | | | ů | Medi | i. | | |
| | | | 10 | 4 | | | |
| 100 | 0 | | 10 | Particle Size (mm |) | 0.1 | 0.01 |
| | | | 11000.01 | · | | | |
| | ا ما م | ora Clossification | | assification AST | | | |
| | Atterb | erg Classification: | | | of Curvature - C _c : | | |
| | | Group Symbol: | | Coefficient | of Uniformity - C _u : | | |
| Detr | | CS Classification: | | | | | |
| Data entr | | KMS | | Date: | 10/2/2019 | | |
| | - | 2020012 Croin | Qian Analusia A07 | Date: | 10/3/2019 | | |
| File name | ð. | 3020012Grain | Size Analysis AST | 1.xism | | | |



| ADVANCED | ERRA TESTIN | G | | | | | | | | |
|--|--------------------------------------|------------|-------------------------|--------------------|-------------------------|---------------------------------------|---|----------|---------------------|--------------------------------|
| CLIENT JOB NO. PROJECT PROJECT NO. LOCATION DATE TESTED TECHNICIAN | Grand Junction CO ED 10/03/19 | | | | - | | BORING NO. DEPTH SAMPLE NO. DATE SAMPLE DESCRIPTION | | | |
| | et Pan and bry Pan and Mass of | ·••• | 465.41 123.24 | | | | Sample Data ass of Sample (g ass of Sample (g | | | |
| Sieve Numbe | Sieve S | ize (mm) | Mass of P Soil (| | Mass of | f Pan (g) | Mass of Individual Retained Soil (| | orrection Factor | Percent Passir by Weight (% |
| 3" | | 6.2 | | | | - | | | | - |
| 1.5" | | 8.1 | | | | | | | | |
| 3/4" | 19 | 0.05 | | | - · | | | | | |
| 3/8" | | .53 | | | | | | | | |
| #4 | | .75 | 0.0 | | | | | | | 100.0 |
| #10 | 2. | .00 | 1.4 | ŀ | | - | 1.4 | | 1.00 | 99.6 |
| #20 | 0.8 | 850 | 1.1 | | | | 1.1 | | 1.00 | 99.3 |
| #40 | 0.4 | 425 | 2.1 | | | | 2.1 | | 1.00 | 98.7 |
| #60 | 0.3 | 250 | 6.2 | 2 | | | 6.2 | | 1.00 | 96.9 |
| #100 | 0.1 | 150 | 7.7 | , | | | 7.7 | | 1.00 | 94.6 |
| #140 | 0.1 | 106 | 4.3 | 3 | | | 4.3 | | 1.00 | 93.4 |
| #200 | 0. | 075 | 7.1 | | | | 7.1 | | 1.00 | 91.3 |
| 100 - 3" | 1.5" | 3/4" 3 | Perce 3/8" #4 | | sing vs #10 | Log of Pa #20 | #40 #60 #10 | 0 #140 # | 200 | |
| | | | | | - | | | | 1 | |
| 00 Veight | | | | | | | | | | |
| ⁰⁸ e | | | | | 1 | | | | | |
| 70 | | | | | - | | | | | |
| a 60 | | | | | | | | | | |
| | | | | | | | | | | |
| SS 40 | Gravei (+# | (4) | | | Sands | (+#200) | | | Silts & Clays (| -#200) |
| Sec 40 | | | | 6 | | ô | 6 | | | |
| t ³⁰ | | | | (#+) F | | +) p | (+#200 | | | |
| ຍິ 20 | | | | s and | | S S S S S S S S S S S S S S S S S S S | Sand | | | |
| Bercent Passing by 00 b 00 c 00 c | | | | Co.rse S.nd (+# 0) | _ | Medium Sand (++4 0) | | | | |
| | | | | | | - | | | | |
| 100 | | | 10 | | Particle | 1 Size (mm |) | 0.1 | | 0.01 |
| | | | | SCS CI | assificat | tion AST | M D 2487 | | | |
| Atte | rberg Clas | sification | | 0000 | | | of Curvature - C | · | | 31 |
| Alle | - | | | | | | of Uniformity - C | - | | |
| | | Symbol: | | , | | Jenicient | or ofmorthity - C | 'u | | |
| | JSCS Class | sincation: | Lean Ciay | / | - | Deter | 10/10/00/ | 10 | | |
| Data entry by: | CAL | | | | | Date: | 10/10/201 | 19 | | |
| Checked by: | <u>KM5</u> 302001: | | Size Analy | | | Date: | | | | |
| File name: | | | | | | | | | | |



| ADVANCED II: | RRA TESTING | | | | | |
|--|---|-----------------------------|----------------------------------|---|----------------------|----------------------------------|
| CLIENT JOB NO. PROJECT PROJECT NO. LOCATION DATE TESTED TECHNICIAN | Wiss Janney Elst 3020-012 Persigo WWTP Grand Junction C 10/03/19 ASE | | - | DEPTH SAMPLE NO. DATE SAMPLED DESCRIPTION | | |
| | bisture It Pan and Soil (g): y Pan and Soil (g): Mass of Pan (g): Moisture (%): | 210.64 139.49 | | Sample Data ass of Sample (g): ass of Sample (g): | | |
| Sieve Number | Sieve Size (mm) | Mass of Pan and Soil (g) | Mass of Pan (g) | Mass of Individual Retained Soil (g) | Correction Factor | Percent Passing by Weight (%) |
| 3" 1.5" 3/4" | 76.2 38.1 19.05 | 0.0 0.0 0.0 | | | | |
| 3/8" #4 #10 | 9.53 4.75 2.00 | 0.0 0.0 0.0 | | | | 100.0 |
| #20 #40 #60 | 0.850 0.425 0.250 | 0.0 1.9 12.9 | | 0.0 1.9 12.9 | 1.00 1.00 1.00 | 99.9 97.3 79.2 |
| #100 #140 #200 | 0.150 0.106 0.075 | 26.2 9.9 7.2 | | 26.2 9.9 7.2 | 1.00 1.00 1.00 | 42.4 28.4 18.4 |
| | 1.5" 3/4" 3 | | sing vs Log of Pa #10 #20 | | <i>‡</i> 140 #200 | |
| 00 90 80 70 60 90 70 70 60 | | | | | | |
| 20 C C C C C C C C C C C C C C C C C C C | Gravel (+#4) | Course Sand (+#) 0) | Sands (+#200) | a (+#230) | Silts & Clays (# | 200) |
| 1 0 1 0 1 00 | | 10 | 1 | Hite Constant | 0.1 | 0.01 |
| | | | Particle Size (mm | | | |
| US | erg Classification: Group Symbol: CS Classification: | | Coefficient | of Curvature - C _c : of Uniformity - C _u : | | |
| Data entry by: Checked by: File name: | KMS | Size Analysis AST | Date: Date: M D6913_9.xlsm | 10/7/2019 / <i>\${\\$\$\\$\$</i> | | |



ส

| CLIENT | | | | | | | | | | |
|--|------------------|---|-------------------------|--|--|---|-------------------|-------------------|--|--|
| | | Wiss Janney Els | tner | | | | B-6 | | | |
| JOB NO. | | 3020-012 | | | | | 4' | | | |
| PROJECT | | Persigo WWTP | | | | SAMPLE NO. | | | | |
| PROJECT | NO. | | | | | DATE SAMPLED | 6. m | | | |
| | 1 | Grand Junction (| 0 | | | DESCRIPTION | | | | |
| DATE TES | | 10/03/19 | | | | | | | | |
| TECHNICIA | | ASE | | | | | | | | |
| | 11.4 | AGE . | | | | | | | | |
| Hygroscop | | | 070.05 | | T (1) () () | Sample Data | 101.0 | | | |
| | | Pan and Soil (g): | | | | ass of Sample (g): | | | | |
| IVIa | iss Dry | Pan and Soil (g): | | | Total Dry Ivia | ass of Sample (g): | 07.0 | | | |
| | | Mass of Pan (g): | | | | | | | | |
| | | Moisture (%): | 16.1 | | | 1 | | 1 | | |
| | | | Maga of D | | | Mass of | Correction | Percent Passin | | |
| Sieve Nun | mber | Sieve Size (mm) | Mass of Pa | | Mass of Pan (g) | Individual | | | | |
| | | | Soil (| g) | • | Retained Soil (g) | Factor | by Weight (%) | | |
| 3" | | 76.2 | | _ | | | | | | |
| - | | | | | | | | | | |
| 1.5" | | 38.1 | | | | 2 | | | | |
| 3/4" | 3/8" 9.53 | | | | | | | | | |
| | | | 0.0 | | | | | 100.0 98.1 | | |
| #4 | | 4.75 | 1.7 | | | 1.7 | 1.00 | 98.1 | | |
| #10 | | 2.00 | 0.38 | | | 0.4 | 1.00 | 97.6 | | |
| #20 | | | 0.31 | | | 0.3 | 1.00 | 97.3 | | |
| #40 | | 0.425 | 1.3 | | | 1.3 | 1.00 | 95.8 | | |
| #60 | | 0.250 | 3.2 | | | 3.2 | 1.00 | 92.1 | | |
| #100 |) | 0.150 | 4.7 | | | 4.7 | 1.00 | 86.7 | | |
| #140 | | 0.106 | 2.5 | | | 2.5 | 1.00 | 83.9 | | |
| #200 | | 0.075 | 3.1 | | - | 3.1 | 1.00 | 80.3 | | |
| | | 0.010 | 0.1 | | | | | | | |
| | | | Perce | nt Pas | sina vs Loa of P | article Size | | | | |
| 100 | 3" | 1.5" 3/4" | Perce 3/8" #4 | | sing vs Log of P #10 #20 | | #140 #200 | | | |
| 100 | 3" | 1.5" 3/4" | | | | | #140 #200 | | | |
| 100 | 3" | 1.5" 3/4" | | | | | #140 #200 | | | |
| 001 90 | 3" | 1.5" 3/4" | | | | | #140 #200 | | | |
| 100 90 80 70 | 3" | 1.5" 3/4" | | | | | #140 #200 | | | |
| 100 90 80 70 | 3" | 1.5" 3/4" | | | | | #140 #200 | | | |
| 100 90 80 70 | 3" | 1.5" 3/4" | | | | | #140 #200 | | | |
| 100 90 80 70 | 3" | 1.5" 3/4" Gravel (+#4) | | | | | #140 #200 | ¥200) | | |
| 100 90 80 70 | 3" | | | | #10 #20 | #40 #60 #100 | | #200) | | |
| 100 90 80 70 | 3" | | | | #10 #20 | #40 #60 #100 | | #200) | | |
| 100 90 80 70 | 3" | | | S nd (+** 0) | #10 #20 | #40 #60 #100 | | #200) | | |
| 100 90 80 70 | 3" | | | S nd (+** 0) | #10 #20 | #40 #60 #100 | | #200) | | |
| Dercent Lassing by Meight 00 0 | 3" | | | | #10 #20 | #40 #60 #100 | | #200) | | |
| 00 0 00 0 0 00 0 0 00 0 0 00 0 0 00 0 0 | 3" | | 3/8" #4 | S nd (+** 0) | #10 #20 | #40 #60 #100 | Silts & Clays (-1 | | | |
| Decent Lassing by Meight 00 0 00 0 00 0 00 0 00 0 00 0 00 0 00 0 00 0 00 0 00 0 00 0 00 0 00 0 00 0 00 0 00 0 00 0 00 0 | 3" | | | S nd (+** 0) | #10 #20 | #40 #60 #100; | | #200) | | |
| 00 0 90 90 90 90 0 0 0 00 0 0 0 0 0 0 0 | 3" | | 3/8" #4 | Course Sind (++ 0) | #10 #20 Sands (+#200) | #40 #60 #100; | Silts & Clays (-1 | | | |
| Bercent Passing by Weight 00 00 00 00 00 00 00 00 00 0 | | | 3/8" #4 10 | Course Sind (++ 0) | #10 #20 Sands (+#200) Sands (+#200) (0) Pure Second Second Second S | #40 #60 #100; | Silts & Clays (-1 | | | |
| Bercent Passing by Weight 00 Bercent Passing by Weight 00 Context Passing by Meight 00 Context Passing by Meight 0 | | Gravel (+#4) | 3/8" #4 | Course Sind (++ 0) | #10 #20 Sands (+#200) Sands (+#200) Sands (+#200) Particle Size (mm assification AST Coefficient | #40 #60 #100 | Silts & Clays (-1 | | | |
| Bercent Passing by Weight 00 00 00 00 00 00 00 00 00 00 00 00 00 | Atterbo | Gravel (+#4) erg Classification Group Symbol | 3/8" #4 | 00 use (144 (144 0) 00 see (144 (144 0) 00 see (144 0) | #10 #20 Sands (+#20) Sands (+#200) Sands (+#200) Particle Size (mm assification AST Coefficient Coefficient | #40 #60 #100; () () () () () () () () () () | Silts & Clays (-1 | | | |
| 100 00 90 00 00 00 00 00 100 0 100 100 100 100 | Atterba | Gravel (+#4) erg Classification Group Symbol CS Classification | 3/8" #4 | 00 use (144 (144 0) 00 see (144 (144 0) 00 see (144 0) | #10 #20 Sands (+#200) Sands (+#200) Sands (+#200) Particle Size (mm assification AST Coefficient Coefficient coefficient | #40 #60 #100 | Silts & Clays (-1 | | | |
| Bercent Passing by Weight 00 Bercent Passing by Meight 00 Cont Pass | Atterbe US | Gravel (+#4) erg Classification Group Symbol | 3/8" #4 | 00 use (144 (144 0) 00 see (144 (144 0) 00 see (144 0) | #10 #20 Sands (+#20) Sands (+#200) Sands (+#200) Particle Size (mm assification AST Coefficient Coefficient | #40 #60 #100 | Silts & Clays (-1 | | | |



ADVANCED TERRA TESTING

12

| | | _ | | | | | | | | | | | | |
|--|---------------------|--------------------------|--|------------------|--------------------|-------------|-------------------------------|--------------------|---------------------------------|---|-------------------|---------------------|--------|---------------------------|
| CLIENT JOB NO. PROJEC ⁻ PROJEC ⁻ LOCATIO DATE TE TECHNIC | T NO. DN STED | 3020-0 Persig | o WWTP | | | | | | DEP [.] SAM DATI | ING NO. TH PLE NO. E SAMPLE CRIPTION | | | | |
| Hygrosco | opic Mo | isture | of Fines | _ | _ | _ | | | Sam | ple Data | | | _ | |
| M | ass Wet | Pan ar Pan ar Mass | nd Soil (g) nd Soil (g) of Pan (g) isture (%) | : 246. : 123. | 66 | | Tota | al Dry N | lass of lass of S | Sample (g) Sample (g) plit Fraction Fraction (g) |): 255.(n: #4 |) | | ŕ |
| Sieve N | | | Size (mm | 11 | s of Pa Soil (g | | Mass of | Pan (g) |) 👘 Ir | Mass of ndividual ined Soil (g | | orrection Factor | | ent Passing Neight (%) |
| 3" | | | 76.2 | | 0.0 | | - | _ | | | | | | |
| 1.5 | | | 38.1 | | 0.0 | | - | - | | | | | | |
| 3/4 | | | 9.05 | | 0.0 | | - | - | | | | | | |
| 3/8 | | | 9.53 | | 0.0 | | - | - | | | | | | |
| #4 | | | 4.75 2.00 | | 0.0 | | | - | | | | | | |
| #1 | | | 2.00).850 | | 0.0 | | - | - | | | | | | |
| #4 | | |).425 | | 0.0 | | - | - | | | | | | |
| #6 | | |).250 | | 0.0 | | _ | _ | | 0.0 | | 1.00 | | 100.0 |
| #10 | | |).150 | | 0.0 | | | _ | | 0.0 | | 1.00 | | 99.9 |
| #14 | | |).106 | | 0.1 | | - | - | | 0.1 | | 1.00 | | 99.9 99.7 |
| #19 | | |).075 | | 0.2 | | | _ | | 0.2 | | 1.00 | | 99.1 99.1 |
| 17410 | | | | - | | at Boo | aina ya I | on of F | Portiola | | | 1.00 | | |
| | 3" | 1.5" | 3/4" | 3/8" | #4 | | <mark>sing vs L</mark> #10 | .0g 01 F #20 | #40 | | 0 #140 # | 200 | | |
| 100 | 1 | • | • | | 1 | | • | - | | | - | 1 | | |
| g by Weight 90 – 08 00 – 08 | | | | | | | | | · · | | | | | |
| bussed 40 – | - | Gravel (| '+#A\ | - | - | | Sonda (| #100) | | | | Silta & Claus (| #200) | |
| Se 40 - | - | Glaver | .+#4) | _ | | | Sands (| +#200) | - | | | Silts & Clays (| -#200) | |
| | | | | | _ | () # | | (0) | | (0) | | ļ | | |
| 8 20 - | | | | _ | _ | Sand (+# 0) | | -) pung | | ** | | | | |
| - 00 Gent - 10 - | | | | | | Course S | | Medium Sand (+#40) | | e Sar | | | | |
| 0 - | | | | | | ദ | | Me | | Ē | | | | |
| 100 | D | | | 10 | | | Particle | 1 Size (mr | n) | | 0.1 | | | 0.01 |
| | | | | | US | SCS CI | assificat | ion AS | FM D 2 | 487 | | | | |
| | Atterb | erg Cla | ssification | : CL | | | Co | oefficien | t of Cu | rvature - C | .; | | | |
| | | | up Symbol | | Oleve | | Co | efficien | t of Un | iformity - C | .: | | | |
| Dete anto | | | ssification | . Lear | Clay | | | D -4 | | 4014/004 | 0 | | | |
| Data entry Checked | | KMS SPI | aio - | | | | | Date | | 10/4/201 | a | | | |
| File name | | 30200 | | Qizo | Analys | | | Date 5 vien | | 0-7-19 | | | | |
| n ne name | | 30200 | | i Size | Analys | NS AO I | M D6913 | _o.xisn | | | | | | |



| ADVA | NCED TEF | IRA TEST | 1130 | | | | | | | | | | | |
|---|-----------------|---------------------------------|------------------------|-----------------|---------------------|--|---------------------------|--|--------------------------|-----------------------------------|--------------------------------------|---------|------------------|-----------------------------|
| CLIENT JOB NO. | | Wiss Janney Elstner 3020-012 | | | | | • | | BOR DEP | ING NO. | B- 14 | - | | |
| | - | | | -D | | | | | | | | 4 | | |
| PROJECT PROJECT | | Persig | go WWT | Р | | | | | | PLE NO. | | | | |
| | | O | 1 1 | - 00 | | | | | | E SAMPI | | | | |
| | | | Junctio | n CO | | | | | DES | CRIPTIO | - N | | | |
| DATE TES | | 10/04/ | 19 | | | | - | | | | | | | |
| TECHNICI | IAN | TAF | | | | | | | | | | | | |
| Hygrosco | - | | | | | | | | Sam | ple Data | | | | |
| | | | nd Soil (| | | | | | | | | | | |
| Ma | ass Dry | | nd Soil (| | | | Total | Dry M | ass of | Sample | (g): 73 | 3.9 | | |
| | | | of Pan (| | | | - | | | | | | | |
| | | Mc | oisture (| %): 2 8 | 8.9 | | | | | | | | | |
| Sieve Nu | Imber | Sieve | Size (m | m) | lass of P Soil (| | Mass of F | Pan (g) | li | ndividual | (a) | | | Percent Pass by Weight (|
| 3" | 3'' 76.2 | | | | | Sample Data Total Wet Mass of Sample (g): 95.2 Total Dry Mass of Sample (g): 73.9 Mass of Pan (g) Mass of Individual Retained Soil (g) Correction Factor 0.0 1.00 0.2 1.00 sing vs Log of Particle Size #40 #60 #100 #140 #200 | | | | | | | | |
| 1.5" | | | 38.1 | | | | | | | | | | | |
| 3/4" | | | 19.05 | | | | | | | | | | | |
| 3/8" | | | 9.53 | | | | | | | | | | | |
| #4 | | | 4.75 | | | | | | | | | | | |
| #10 | | | 2.00 | | | | | | | | | | | |
| #20 | | | 0.850 | | | | | | | | | | | |
| #40 | | | 0.425 | | 0.0 | | - | | | | | | | |
| #60 | | | 0.250 | | 0.0 | | | | | 0.0 | | 1.00 | | 100.0 |
| #100 | | | 0.150 | | 0.01 | | | | | | | | | 100.0 |
| #14(| | | 0.106 | | 0.01 | | | | | | | | | 100.0 |
| #200 | | | 0.075 | | 0.2 | | | | | | | | | 99.7 |
| | | | | | | | sina vs La | a of P | article | | | | | 00.1 |
| 100 | 3" | 1.5" | 3/4" | 3/8 | | | - | - | | | 100 #14 | 10 #200 |) | |
| | | 3 | 0.4% | | | | | | | | | | | |
| 6 ight | | | | | | | | | 1 | | | | | |
| | 1 | | | | | | | | | | | | | |
| A 70 60 | 1 | | | | - | | | | | | _ | | | |
| | | | | | | _ | - | | - | | | | | |
| bassing 40 – | - | 0 | /- # 0 | | | | | | | | | | | |
| isi 40 — | - | Gravel | (+#4) | _ | | _ | Sands (+# | 200) | | | | S | ilts & Clays (-# | \$200) |
| 4 30 | | | | | | (0) | | (0 * | _ | 6 | | | | |
| in so | | | | | | Co irse Sind (+#10) | | S nd (***0) | | (+#200) | | | | |
| | | | | - | | e e | | n Sar | | Sand | | | | |
| 2 20 | | | | | | SI O | | Medium | | E | | | | |
| 20 Letterner 20 Letterner 10 Letterner | - | | | | | 0 | | | - i - | | | | | |
| 0 | | | | | | 0 | | | | | | | | |
| _ | | | | 10 | | | Particle Si | 1 ze (mm | | | 0 | .1 | | 0.0 |
| 0 | | | | 10 | | | | | - | 487 | 0 | .1 | | 0.0 |
| 0 | Atterbe | erg Cla | ssificatio | | U | | assificatio | n AST | MD2 | | | .1 | | 0.0 |
| 0 | Atterbe | - | ssificatio | on: C | U: | | issificatio Coe | n AST fficient | MD2 of Cu | rvature - | C _c : | .1 | | 0.0 |
| 0 | | Grou | up Symb | on: C ool: C | Us L L | | issificatio Coe | n AST fficient | MD2 of Cu | | C _c : | .1 | | 0.0 |
| 0 100 | USC | Grou CS Cla | up Symb | on: C ool: C | U: | | issificatio Coe | n AST fficient fficient | M D 2 of Cu of Uni | rvature - formity - | C _c : C _u : | .1 | | 0.0 |
| 0 | US(| Grou | up Symb Issificatio | on: C ool: C | Us L L | | issificatio Coe | n AST fficient fficient Date: | M D 2 of Cu of Uni | rvature - formity - 10/9/20 | C _c : C _u : | .1 | | 0.0 |



ADVANCED TERRA TESTING

| | Control Controls | | | | | | | | | |
|--|---|-----------------------------|------------------------|--|----------------------|---------------------------------|--|--|--|--|
| CLIENT JOB NO. PROJECT PROJECT NO. LOCATION DATE TESTED TECHNICIAN | Grand Junction C | | | BORING NO. DEPTH SAMPLE NO. DATE SAMPLED DESCRIPTION | B-6 19' | | | | | |
| Hygroscopic N | | | | Sample Data | | | | | | |
| | Vet Pan and Soil (g): Dry Pan and Soil (g): Mass of Pan (g): Moisture (%): | 99.41 3.09 | | ass of Sample (g): ass of Sample (g): | | | | | | |
| Sieve Number | , , | Mass of Pan and Soil (g) | Mass of Pan (g) | Mass of Individual Retained Soil (g) | Correction Factor | Percent Passin by Weight (%) | | | | |
| 3" | 76.2 | 0.0 | _ | | | | | | | |
| 1.5" | 38.1 | 0.0 | | | | | | | | |
| 3/4" | 19.05 | 0.0 | | 0.0 | | 100.0 | | | | |
| 3/8" | 9.53 | 19.0 | | 19.0 | 1.00 | 80.3 | | | | |
| #4 | 4.75 | 16.2 | 44.44 | 16.2 | 1.00 | 63.5 | | | | |
| #10 | 2.00 | 13.6 | | 13.6 | 1.00 | 49.4 | | | | |
| #20 | 0.850 | 6.5 | | 6.5 | 1.00 | 42.6 | | | | |
| #40 | 0.425 | 12.6 | | 12.6 | 1.00 | 29.5 | | | | |
| #60 | 0.250 | 10.8 4.4 | | 10.8 | 1.00 | | | | | |
| #100 | | | | 4.4 | 1.00 | 18.3 13.7 12.2 11.2 | | | | |
| #140 | 0.106 | 1.5 | | 1.5 | 1.00 | | | | | |
| #200 | 0.075 | 0.9 | | 0.9 | 1.00 | 11.2 | | | | |
| | | | sing vs Log of Pa | | | | | | | |
| 100 🕂 🛉 | 1.5" 3/4" 3 | /8" #4 : | #10 #20 | #40 #60 #100 | #140 #200 | | | | | |
| 90 Meight | | | | | | | | | | |
| . B 80 | | | | | | | | | | |
| Š 70 | | | | | | | | | | |
| | | | | | | | | | | |
| 5 60 | | | | | | | | | | |
| October October <t< td=""><td>Gravel (+#4)</td><td></td><td>Sands (+#200)</td><td></td><td>Citta & Ciava / #</td><td>10001</td></t<> | Gravel (+#4) | | Sands (+#200) | | Citta & Ciava / # | 10001 | | | | |
| ଝ 40 | Graver (+#4) | | Salids (Thinking) | | Silts & Clays (-# | (200) | | | | |
| ± 30 | | 6 | (0) | ę. | | | | | | |
| b 20 | | Course Sand (+#10) | () () (+++ () | (0) () () | | | | | | |
| <u>0</u> 20 | | ග මූ | S E | o a | | | | | | |
| | | ů | Me | Ê | | | | | | |
| 0 | | 10 | - i | 1 | | | | | | |
| 100 | | 10 | 1 Particle Size (mm |) | 0.1 | 0.01 | | | | |
| | | | assification AST | | | | | | | |
| Atte | rberg Classification: | | | of Curvature - C _c : | 1 30 | | | | | |
| | Group Symbol: | | | of Uniformity - C_u : | | | | | | |
| 1 | ISCS Classification: | | Coencient | or officiently - G_{u} : | 110.74 | | | | | |
| | | | D-1 | 40/0/0040 | | | | | | |
| Data entry by: | KMS | | Date: | 10/2/2019 | | | | | | |
| Checked by: File name: | 3020012 Grain | Size Analysis AST | | 10/8/19 | | | | | | |
| | | Size Analysis AST | INI DOB 13_0.XISM | | | | | | | |



ADVANCED TERRA TESTING

| CLIENT JOB NO. PROJECT PROJECT NO. LOCATION DATE TESTED TECHNICIAN | Wiss Janney Elst 3020-012 Persigo WWTP Grand Junction C 10/01/19 ALH | | - | BORING NO. DEPTH SAMPLE NO. DATE SAMPLED DESCRIPTION | | |
|--|---|-----------------------------|------------------------------|--|----------------------|----------------------------------|
| | loisture et Pan and Soil (g): ry Pan and Soil (g): Mass of Pan (g): Moisture (%): | 259.27 171.78 | | Sample Data ass of Sample (g): ass of Sample (g): | | - |
| Sieve Number Sieve Size (mm) | | Mass of Pan and Soil (g) | Mass of Pan (g) | Mass of Individual Retained Soil (g) | Correction Factor | Percent Passing by Weight (%) |
| 3" | 76.2 | | | | | |
| 1.5" | 38.1 | | | | | |
| 3/4" | 19.05 | | | | | |
| 3/8" | 9.53 | | | | | |
| #4 | 4.75 | | | | | |
| #10 | 2.00 | 0.0 | | | | 100.0 |
| #20 | 0.850 | 0.13 | | 0.13 | 1.00 | 99.9 |
| #40 | 0.425 | 0.23 | | 0.23 | 1.00 | 99.6 |
| #60 | 0.250 | 0.66 | | 0.66 | 1.00 | 98.8 |
| #100 | 0.150 | 4.5 | | 4.5 | 1.00 | 93.7 |
| #140 | 0.106 | 0.106 6.6 | | 6.6 | 1.00 | 86.2 |
| #200 | 0.075 | 7.2 | 4 , - | 7.2 | 1.00 | 78.0 |
| 100 3" | 1.5" 3/4" 3 | | sing vs Log of Pa #10 #20 | #40 #60 #100 | #140 #200 | |
| 90 60 60 60 60 60 60 60 60 | | | ~ | ~ | | |
| 6 80 | | | | | ~ | |
| ₹ 70 | | | | | | |
| | | | | | | |
| ອີ ⁶⁰ | | | | | | |
| | Gravel (+#4) | | Sands (+#200) | | Silts & Clays (-# | 1200) |
| b ussed 40 d | | | | | | 200, |
| | | 6 # | (0 +#+) Pu | (0 + | | |
| 3 20 | | ++) pu s |) pu | | | |
| | | Ise S | in mil | e Sa | | |
| _ | | CO | We | Ê | | |
| 0 + - 100 | | 10 | 1 Particle Size (mm |) . | 0.1 | 0.01 |
| | | USCS CI | assification AST | M D 2487 | | |
| Δttor | berg Classification: | | | of Curvature - C _c : | | |
| Aller | - | | | | | |
| | Group Symbol: SCS Classification: | | | of Uniformity - C _u : | | |
| Data entry by: | CAL | | Date: | ,10/9/2019 | | |
| Checked by: | KMB | | Date: | 10/9/19 | | |
| File name: | 3020012Grain | Size Analysis AST | M D6913_10.xlsn | | | |

One Dimensional Swell / Collapse



[F

Denver Swell

| CLIENT Wiss Janney Elstner JOB NO. 3020-012 PROJECT Persigo WWTP PROJECT NO LOCATION Grand Junction CO DATE TESTED 09/20/19 TECHNICIAN ALH | Sample C | | B-3 9' |
|--|-------------------------------------|--|---------------------------------------|
| Before Test Mass of Wet Soil and F After Test Mass of Wet Soil and F | | Initial Wet Density (p Initial Dry Density (p | |
| Mass of Dry Soil, Ring, and I | | Initial Wet Density (kg/r | |
| Diame | eter (in): 1.94 | Initial Dry Density (kg/r | m³): 1503 |
| | ght (in): 0.90 | Initial Moisture (| |
| | Ring (g): 241.69 Pan (g): 159.32 | Final Wet Density (p Final Dry Density (p | |
| Inundation Loa | | Final Wet Density (kg/r | |
| Inundation Loa | | Final Dry Density (kg/r | |
| | eter ID: ATT-15 | Final Moisture (| |
| | Swell / Col | apse Data | |
| Collap | ose (%): -1.53 | Swell Pressure (p | • |
| | (0/) | Swell Pressure (kF | Pa): |
| Load (psf) Deformation (in) Strain 112 0.0000 0.0 | | Strain Versus Vert | ical Stress |
| 1079 -0.0227 -2. | | Q | |
| Inudated -0.0365 -4. | 06 | | |
| 1488 -0.0412 -4. | 58 -0.5 | | |
| | -1 | | |
| | | | |
| | -1.5 | | |
| | 8 -2 | | |
| | i. | | |
| | -2.5 | | · · · · · · · · · · · · · · · · · · · |
| | -3 | | |
| | | | |
| | -3.5 | | |
| | -4 | | |
| | | | ×. |
| | -4.5 | | 0 |
| | -5 | | |
| | 10 | 100 Stress (p | 1000 10000 |
| | Initi | | |
| | | _ | |
| Data entry by: SPH | Date: | 9/24/2019 | |
| Checked by: <u>CAC</u> File name: 3020012_Swell Colapse | e ASTM D4546_2.xls | 9/25/19 | |
| | | | |

÷

One Dimensional Swell / Collapse



Denver Swell

| CLIENT JOB NO. PROJECT PROJECT NO LOCATION DATE TESTEI TECHNICIAN | Grand Junction C | | | BORING NO. DEPTH SAMPLE NO. DATE SAMPLED SAMPLED BY DESCRIPTION | B-5 20' |
|---|--|--|---|--|--|
| | | | | Conditions | |
| After Te | Ma Ma Inundat Inundatio | il and Ring (g) | : 343.53 : 346.92 : 491.57 : 1.94 : 0.90 : 251.12 : 155.81 : 2404 : 115 | Initial Wet Density (Initial Dry Density (Initial Wet Density (kg Initial Dry Density (kg Initial Moisture Final Wet Density (Final Wet Density (kg Final Dry Density (kg Final Dry Density (kg | (pcf): 121.5 /m ³): 2124 /m ³): 1945 (%): 9.2 (pcf): 139.6 (pcf): 123.3 /m ³): 2236 /m ³): 1975 |
| | | | Swell / C | ollapse Data | |
| | | Swell (%) | | Swell Pressure (| psf): 4682 |
| | | | | Swell Pressure (k | |
| Load (psf) 112 2404 Inudated 2953 6513 | Deformation (in) 0.0000 -0.0068 -0.0028 -0.0034 -0.0104 | Strain (%) 0.00 -0.76 -0.31 -0.38 -1.16 | 0 -0.2 -0.4 (%) -0.6 -0.8 -1 -1.2 -1.4 -1.2 | Strain Versus Ver | tical Stress |
| Data entry by: | SPH | | @ Date | Stress (nitial Loading Inundation e: 9/24/2019 | psf) |
| Checked by: File name: | CAL | Colapse ASTN | Date | e: <u>9/25/2019</u> | |

One Dimensional Swell / Collapse



IF.

Denver Swell

| CLIENT OB NO. | Wiss Janney Elst 3020-012 | ner | | BORING NO. DEPTH | B-6 9' | |
|--|--------------------------------|----------------------------------|------------------|---|-----------------------|------------|
| PROJECT PROJECT NO OCATION DATE TESTEI ECHNICIAN | Grand Junction C D 09/20/19 | 0 | | SAMPLE NO. DATE SAMPLED SAMPLED BY DESCRIPTION | | |
| | | | Sample (| Conditions | | |
| Before Te | est Mass of Wet So | il and Ring (g) | | Initial Wet Dens | tv (pcf): 134.3 | |
| | est Mass of Wet So | | | Initial Dry Dens | | |
| M | ass of Dry Soil, Ring | | | Initial Wet Density | | |
| | | Diameter (in) | | Initial Dry Density | | |
| | | tial Height (in) | | | ure (%): 16.6 | |
| | | ass of Ring (g) | | Final Wet Dens | | |
| | | ass of Pan (g) ion Load (psf) | | Final Dry Dens Final Wot Density | | |
| | | on Load (psi) | | Final Wet Density Final Dry Density | | |
| | | Oedometer ID | | | ure (%): 17.4 | |
| | | | | llapse Data | | |
| | | Swell (%) | : 0.11 | | re (psf): 1833 | |
| | D (P () | 01 1 10/2 | | Swell Pressur | e (kPa): 88 | |
| Load (psf) 113 | Deformation (in) 0.0000 | Strain (%) | - | Strain Versus V | ertical Stress | |
| 1079 | -0.0048 | 0.00 -0.53 | 0 | 0 | | |
| Inudated | -0.0038 | -0.33 | Ű | | | |
| 1488 | -0.0040 | -0.44 | -0.1 | | | |
| 2954 | -0.0074 | -0.82 | | | | |
| | | | -0.2 | | | |
| | | | | | | |
| | | | -0.3 | | | |
| | | | 8 | | | |
| | | | %) -0.4 | | 0. | |
| | | | et s -0.5 | | 0 | |
| | | | -0.5 | | | |
| | | | -0.6 | | | |
| | | | -0.7 | | | |
| | | | -0.8 | | | |
| | | | | | | 0 |
| | | | -0.9 | 100 | 1000 | 1000 |
| | | | | | ss (psf) | 1000 |
| | | | @ Ini | tial Loading ——— Inunda | tion Load ···· • Fina | al Loading |
| ata entry by: | SPH | | Date: | 9/24/2019 | | |
| hecked by: | CAL | | Date: | | | |
| ile name: | | Colapse ASTN | 1 D4546_0.xls | | | |



ASTM D 2166

CLIENT Wiss Janney Elstner BORING NO. B-3 JOB NO. 3020-012 DEPTH 9' PROJECT Persigo WWTP SAMPLE NO. -PROJECT NO. DATE SAMPLED LOCATION Grand Junction CO DESCRIPTION liner DATE TESTED 09/23/19 TECHNICIAN CAL **Test Parameters** 0.039167455 Strain Rate (in/min): Strain Rate (cm/min): 0.099485336 Raw Data Files: WJE_UCS_B-3_9_.txt Moisture & Density Data Mass of Wet Soil and Pan (g): 377.34 Initial Wet Density (pcf): 122.8 Mass of Dry Soil and Pan (g): 294.36 Initial Dry Density (pcf): 95.3 Mass of Pan (g): 6.94 Initial Wet Density (kg/m³): 1967 Mass of Wet Soil (g): 370.4 Initial Dry Density (kg/m³); 1526 Initial Diameter (in): 1.93 Initial Moisture (%): 28.9 Initial Height (in): 3.95 **Test Results** Peak Stress (psf): 410 Axial Strain at Peak Stress(%): 13.0 Peak Stress (kPa): 20 Height to Diameter Ratio: 2.0:1 **Displacement vs. Stress** 450 400 350 300 Stress (psf) 250 200 150 100 50 0 0.0000 0.1000 0.2000 0.3000 0.4000 0.5000 0.6000 **Displacement (in)** NOTES: Data entry by: CAL Date: 9/24/2019 SPH Checked by: 9-24-19 Date: File name: 3020012__UCS ASTM D2166_0.xlsm



Image Attachment

ADVANCED TERRA TESTING

15

| CLIENT JOB NO. PROJECT PROJECT NO. LOCATION | Wiss Janney Elstner 3020-012 Persigo WWTP Grand Junction CO |
|---|---|
| | CLIENT WJE ATT JOB NO. 3020-012 BORING B-3 DEPTH 9' SAMPLE NO. TEST TYPE CONFINING STRESS |
| NOTES | |
| File name: | 3020012lmage_19_09_24_06_45_04 |

CLIENT JOB NO. PROJECT PROJECT NO. LOCATION DATE TESTED TECHNICIAN Wiss Janney Elstner 3020-012 Persigo WWTP --Grand Junction CO 09/23/19 CAL

| BORING NO. | B-3 |
|--------------|-------|
| DEPTH | 9' |
| SAMPLE NO. | |
| DATE SAMPLED | |
| DESCRIPTION | liner |

| Displacement (in) | Displacement (cm) | Strain (%) | Average Cross Sectional Area (in ²) | Load (lbs) | Load (N) | Stress (psf) | Stress (kPa) |
|-------------------|-------------------|------------|--|------------|----------|--------------|--------------|
| 0.0000 | 0.000 | 0.00 | 2.91 | 0.0 | 0 | 0 | 0 |
| 0.0041 | 0.010 | 0.10 | 2.92 | 0.1 | 0.4 | 4.0 | 0.2 |
| 0.0085 | 0.022 | 0.22 | 2.92 | 0.1 | 0.4 | 3.9 | 0.2 |
| 0.0125 | 0.032 | 0.32 | 2.92 | 0.1 | 0.5 | 5.4 | 0.3 |
| 0.0166 | 0.042 | 0.42 | 2.93 | 0.3 | 1.4 | 16 | 0.8 |
| 0.0207 | 0.053 | 0.52 | 2.93 | 0.4 | 1.7 | 19 | 0.9 |
| 0.0248 | 0.063 | 0.63 | 2.93 | 0.6 | 2.6 | 29 | 1.4 |
| 0.0292 | 0.074 | 0.74 | 2.94 | 0.6 | 2.8 | 31 | 1.5 |
| 0.0335 | 0.085 | 0.85 | 2.94 | 0.6 | 2.5 | 28 | 1.3 |
| 0.0376 | 0.096 | 0.95 | 2.94 | 0.9 | 3.8 | 42 | 2.0 |
| 0.0418 | 0.106 | 1.06 | 2.94 | 0.9 | 3.8 | 42 | 2.0 |
| 0.0458 | 0.116 | 1.16 | 2.95 | 0.9 | 4.0 | 44 | 2.1 |
| 0.0498 | 0.126 | 1.26 | 2.95 | 1.2 | 5.2 | 57 | 2.7 |
| 0.0538 | 0.137 | 1.36 | 2.95 | 1.2 | 5.2 | 57 | 2.7 |
| 0.0579 | 0.147 | 1.47 | 2.96 | 1.2 | 5.2 | 57 | 2.8 |
| 0.0623 | 0.158 | 1.58 | 2.96 | 1.4 | 6.1 | 67 | 3.2 |
| 0.0663 | 0.168 | 1.68 | 2.96 | 1.3 | 5.8 | 63 | 3.0 |
| 0.0703 | 0.179 | 1.78 | 2.97 | 1.5 | 6.8 | 74 | 3.6 |
| 0.0744 | 0.189 | 1.89 | 2.97 | 1.5 | 6.8 | 74 | 3.5 |
| 0.0786 | 0.200 | 1.99 | 2.97 | 1.5 | 6.9 | 75 | 3.6 |
| 0.0829 | 0.211 | 2.10 | 2.98 | 1.8 | 7.8 | 85 | 4.1 |
| 0.0870 | 0.221 | 2.21 | 2.98 | 1.8 | 7.8 | 85 | 4.1 |
| 0.0910 | 0.231 | 2.31 | 2.98 | 1.8 | 7.8 | 85 | 4.0 |
| 0.0950 | 0.241 | 2.41 | 2.99 | 2.1 | 9.3 | 101 | 4.8 |
| 0.0991 | 0.252 | 2.51 | 2.99 | 2.1 | 9.1 | 99 | 4.7 |
| 0.1031 | 0.262 | 2.61 | 2.99 | 2.1 | 9.5 | 103 | 4.9 |
| 0.1073 | 0.273 | 2.72 | 2.99 | 2.4 | 11 | 117 | 5.6 |
| 0.1113 | 0.283 | 2.82 | 3.00 | 2.4 | 11 | 114 | 5.5 |
| 0.1155 | 0.293 | 2.93 | 3.00 | 2.6 | 11 | 123 | 5.9 |
| 0.1197 | 0.304 | 3.03 | 3.00 | 2.6 | 11 | 123 | 5.9 |
| 0.1238 | 0.314 | 3.14 | 3.01 | 2.7 | 12 | 129 | 6.2 |
| 0.1279 | 0.325 | 3.24 | 3.01 | 2.9 | 13 | 136 | 6.5 |
| 0.1319 | 0.335 | 3.34 | 3.01 | 2.8 | 13 | 135 | 6.5 |
| 0.1360 | 0.345 | 3.45 | 3.02 | 2.9 | 13 | 136 | 6.5 |
| 0.1402 | 0.356 | 3.55 | 3.02 | 3.1 | 14 | 147 | 7.0 |
| 0.1443 | 0.367 | 3.66 | 3.02 | 3.1 | 14 | 145 | 7.0 |
| 0.1484 | 0.377 | 3.76 | 3.03 | 3.1 | 14 | 146 | 7.0 |
| 0.1525 | 0.387 | 3.87 | 3.03 | 3.3 | 15 | 156 | 7.5 |
| 0.1568 | 0.398 | 3.97 | 3.03 | 3.2 | 13 | 154 | 7.4 |
| 0.1615 | 0.410 | 4.09 | 3.04 | 3.3 | 15 | 155 | 7.4 |
| 0.1655 | 0.420 | 4.20 | 3.04 | 3.3 | 15 | 155 | 7.4 |
| 0.1697 | 0.431 | 4.30 | 3.04 | 3.5 | 16 | 166 | 7.9 |
| 0.1742 | 0.442 | 4.42 | 3.05 | 3.7 | 17 | 176 | 8.4 |

CLIENT JOB NO. PROJECT PROJECT NO. LOCATION DATE TESTED TECHNICIAN Wiss Janney Elstner 3020-012 Persigo WWTP --Grand Junction CO 09/23/19 CAL

| BORING NO. | B-3 |
|--------------|-------|
| DEPTH | 9' |
| SAMPLE NO. | |
| DATE SAMPLED | |
| DESCRIPTION | liner |

| Displacement (in) | Displacement (cm) | Strain (%) | Average Cross Sectional Area (in ²) | Load (lbs) | Load (N) | Stress (psf) | Stress (kPa) |
|-------------------|-------------------|------------|--|------------|----------|--------------|--------------|
| 0.1782 | 0.453 | 4.52 | 3.05 | 3.7 | 16 | 174 | 8.3 |
| 0.1822 | 0.463 | 4.62 | 3.05 | 3.7 | 17 | 175 | 8.4 |
| 0.1866 | 0.474 | 4.73 | 3.06 | 3.7 | 17 | 175 | 8.4 |
| 0.1906 | 0.484 | 4.83 | 3.06 | 4.0 | 18 | 190 | 9.1 |
| 0.1947 | 0.495 | 4.94 | 3.06 | 4.0 | 18 | 188 | 9.0 |
| 0.1989 | 0.505 | 5.04 | 3.07 | 4.0 | 18 | 185 | 8.9 |
| 0.2030 | 0.516 | 5.15 | 3.07 | 4.3 | 19 | 200 | 10 |
| 0.2072 | 0.526 | 5.25 | 3.07 | 4.2 | 19 | 196 | 9 |
| 0.2112 | 0.536 | 5.35 | 3.08 | 4.2 | 19 | 196 | 9 |
| 0.2156 | 0.548 | 5.47 | 3.08 | 4.4 | 20 | 206 | 10 |
| 0.2200 | 0.559 | 5.58 | 3.09 | 4.6 | 20 | 213 | 10 |
| 0.2245 | 0.570 | 5.69 | 3.09 | 4.8 | 21 | 224 | 11 |
| 0.2287 | 0.581 | 5.80 | 3.09 | 4.8 | 21 | 225 | 11 |
| 0.2328 | 0.591 | 5.90 | 3.10 | 4.8 | 21 | 225 | 11 |
| 0.2368 | 0.601 | 6.00 | 3.10 | 5.1 | 23 | 235 | 11 |
| 0.2412 | 0.613 | 6.11 | 3.10 | 5.1 | 23 | 239 | 11 |
| 0.2452 | 0.623 | 6.22 | 3.11 | 5.0 | 22 | 234 | 11 |
| 0.2494 | 0.633 | 6.32 | 3.11 | 5.4 | 24 | 249 | 12 |
| 0.2535 | 0.644 | 6.43 | 3.11 | 5.3 | 24 | 246 | 12 |
| 0.2576 | 0.654 | 6.53 | 3.12 | 5.3 | 24 | 245 | 12 |
| 0.2618 | 0.665 | 6.64 | 3.12 | 5.4 | 24 | 247 | 12 |
| 0.2661 | 0.676 | 6.75 | 3.12 | 5.5 | 24 | 253 | 12 |
| 0.2701 | 0.686 | 6.85 | 3.13 | 5.4 | 24 | 250 | 12 |
| 0.2744 | 0.697 | 6.96 | 3.13 | 5.5 | 25 | 253 | 12 |
| 0.2788 | 0.708 | 7.07 | 3.13 | 5.7 | 25 | 262 | 13 |
| 0.2828 | 0.718 | 7.17 | 3.14 | 5.7 | 25 | 261 | 13 |
| 0.2877 | 0.731 | 7.29 | 3.14 | 6.0 | 26 | 273 | 13 |
| 0.2919 | 0.741 | 7.40 | 3.15 | 5.8 | 26 | 267 | 13 |
| 0.2960 | 0.752 | 7.50 | 3.15 | 6.0 | 27 | 272 | 13 |
| 0.3002 | 0.763 | 7.61 | 3.15 | 6.3 | 28 | 285 | 14 |
| 0.3043 | 0.773 | 7.71 | 3.16 | 6.2 | 28 | 282 | 14 |
| 0.3084 | 0.783 | 7.82 | 3.16 | 6.3 | 28 | 288 | 14 |
| 0.3125 | 0.794 | 7.92 | 3.16 | 6.5 | 29 | 295 | 14 |
| 0.3165 | 0.804 | 8.02 | 3.17 | 6.6 | 29 | 300 | 14 |
| 0.3206 | 0.814 | 8.13 | 3.17 | 6.6 | 29 | 299 | 14 |
| 0.3246 | 0.824 | 8.23 | 3.17 | 6.5 | 29 | 294 | 14 |
| 0.3289 | 0.835 | 8.34 | 3.18 | 6.5 | 29 | 294 | 14 |
| 0.3331 | 0.846 | 8.44 | 3.18 | 6.8 | 30 | 308 | 15 |
| 0.3371 | 0.856 | 8.54 | 3.19 | 6.8 | 30 | 306 | 15 |
| 0.3413 | 0.867 | 8.65 | 3.19 | 6.8 | 30 | 305 | 15 |
| 0.3454 | 0.877 | 8.76 | 3.19 | 6.9 | 31 | 312 | 15 |
| 0.3494 | 0.887 | 8.86 | 3.20 | 7.0 | 31 | 314 | 15 |
| 0.3535 | 0.898 | 8.96 | 3.20 | 7.0 | 31 | 313 | 15 |

| CLIENT | Wiss Janney Elstner | BORING NO. | B-3 |
|-------------|---------------------|--------------|-------|
| JOB NO. | 3020-012 | DEPTH | 9' |
| PROJECT | Persigo WWTP | SAMPLE NO. | |
| PROJECT NO. | | DATE SAMPLED | |
| LOCATION | Grand Junction CO | DESCRIPTION | liner |
| DATE TESTED | 09/23/19 | | |
| TECHNICIAN | CAL | | |

| Displacement (in) | Displacement (cm) | Strain (%) | Average Cross Sectional Area (in ²) | Load (Ibs) | Load (N) | Stress (psf) | Stress (kPa) |
|-------------------|-------------------|------------|--|------------|----------|--------------|--------------|
| 0.3578 | 0.909 | 9.07 | 3.20 | 7.0 | 31 | 313 | 15 |
| 0.3620 | 0.919 | 9.18 | 3.21 | 7.1 | 32 | 320 | 15 |
| 0.3672 | 0.933 | 9.31 | 3.21 | 7.2 | 32 | 322 | 15 |
| 0.3713 | 0.943 | 9.41 | 3.22 | 7.2 | 32 | 321 | 15 |
| 0.3758 | 0.955 | 9.53 | 3.22 | 7.4 | 33 | 329 | 16 |
| 0.3802 | 0.966 | 9.64 | 3.22 | 7.4 | 33 | 330 | 16 |
| 0.3842 | 0.976 | 9.74 | 3.23 | 7.4 | 33 | 332 | 16 |
| 0.3883 | 0.986 | 9.84 | 3.23 | 7.4 | 33 | 328 | 16 |
| 0.3925 | 0.997 | 9.95 | 3.24 | 7.7 | 34 | 340 | 16 |
| 0.3966 | 1.007 | 10.05 | 3.24 | 7.7 | 34 | 342 | 16 |
| 0.4006 | 1.018 | 10.15 | 3.24 | 7.6 | 34 | 338 | 16 |
| 0.4050 | 1.029 | 10.27 | 3.25 | 7.9 | 35 | 349 | 17 |
| 0.4091 | 1.039 | 10.37 | 3.25 | 7.9 | 35 | 350 | 17 |
| 0.4133 | 1.050 | 10.48 | 3.25 | 7.9 | 35 | 348 | 17 |
| 0.4175 | 1.060 | 10.58 | 3.26 | 7.9 | 35 | 349 | 17 |
| 0.4216 | 1.071 | 10.69 | 3.26 | 8.1 | 36 | 357 | 17 |
| 0.4256 | 1.081 | 10.79 | 3.27 | 8.2 | 36 | 360 | 17 |
| 0.4298 | 1.092 | 10.89 | 3.27 | 8.1 | 36 | 355 | 17 |
| 0.4339 | 1.102 | 11.00 | 3.27 | 8.4 | 37 | 369 | 18 |
| 0.4381 | 1.113 | 11.11 | 3.28 | 8.4 | 37 | 368 | 18 |
| 0.4422 | 1.123 | 11.21 | 3.28 | 8.4 | 37 | 370 | 18 |
| 0.4464 | 1.134 | 11.32 | 3.29 | 8.5 | 38 | 371 | 18 |
| 0.4504 | 1.144 | 11.42 | 3.29 | 8.7 | 39 | 380 | 18 |
| 0.4546 | 1.155 | 11.52 | 3.29 | 8.7 | 39 | 380 | 18 |
| 0.4588 | 1.165 | 11.63 | 3.30 | 8.7 | 38 | 378 | 18 |
| 0.4630 | 1.176 | 11.74 | 3.30 | 8.6 | 38 | 376 | 18 |
| 0.4670 | 1.186 | 11.84 | 3.30 | 8.9 | 40 | 387 | 19 |
| 0.4712 | 1.197 | 11.94 | 3.31 | 9.0 | 40 | 390 | 19 |
| 0.4756 | 1.208 | 12.06 | 3.31 | 9.0 | 40 | 390 | 19 |
| 0.4797 | 1.218 | 12.16 | 3.32 | 8.9 | 40 | 388 | 19 |
| 0.4840 | 1.229 | 12.27 | 3.32 | 9.1 | 41 | 396 | 19 |
| 0.4888 | 1.242 | 12.39 | 3.33 | 9.1 | 40 | 394 | 19 |
| 0.4933 | 1.253 | 12.50 | 3.33 | 9.2 | 41 | 396 | 19 |
| 0.4973 | 1.263 | 12.61 | 3.33 | 9.4 | 42 | 406 | 19 |
| 0.5015 | 1.274 | 12.71 | 3.34 | 9.4 | 42 | 406 | 19 |
| 0.5057 | 1.284 | 12.82 | 3.34 | 9.4 | 42 | 404 | 19 |
| 0.5099 | 1.295 | 12.93 | 3.35 | 9.4 | 42 | 402 | 19 |
| 0.5140 | 1.306 | 13.03 | 3.35 | 9.5 | 42 | 410 | 20 |



ASTM D 2166

| | | TERRA TESTING | 2 | | | | | | | | | | |
|--------------------------|--|-----------------------------|--|-------------------|-----------|----------------------|---|--------------|-------------------------------------|----------------------------|--|--------|--|
| PRC PRC LOC DAT | ENT NO. DJECT DJECT NO. CATION TE TESTED CHNICIAN | | Wiss Janr 3020-012 Persigo W Grand Jur 09/24/19 CAL train Rate (in ain Rate (cm | /WTP nction CC |) | t Parame 8 | BORING DEPTH SAMPLE DATE SA DESCRIF | NO. MPLED | | B-6 9' liner | | | |
| | | | Raw Data | Files: WJ | E UCS B | -69.txt | | | | | | | |
| - | | | | | | e & Dens | ity Nata | | | _ | | | |
| | Mass c Initial | | g): 335.6 g): 6.74 g): 397.6 n): 1.92 | 6 6 | | | Initial V Initial I Initial Wet Initial Dry Initial Dry | | sity (pcf): (kg/m³): (kg/m³): | | 130.0 107.5 2082 1722 20.9 | | |
| | | | | | Te | est Resul | ts | | | | | | |
| | | k Stress (ps Stress (kPa | | | | Axi | al Strain at Height to | | | | 12.0 2.1:1 | | |
| Stress (psf) | 5000 4500 4000 3500 3000 2500 2000 1500 1000 500 0 0.0000 | 0.1000 | 0.2 | | 0.3000 | | vs. Stress | 0.50 | 200 | 0.6 | | 0.7000 | |
| | | | | I | Displacen | nent (in) | | | | | | | |
| Che | ES: a entry by: cked by: name: | | CAL SPH 3020012 | UCS AS | STM D21 | 66_1.xlsn | Date: Date: | | 25/2019 25-19 | | | | |



Image Attachment

| CLIENT JOB NO. PROJECT PROJECT NO. LOCATION | Wiss Janney Elstner 3020-012 Persigo WWTP Grand Junction CO | |
|---|---|-------------------------------------|
| | CLIENT ATT JOB NO. BORING DEPTH SAMPLE NO. TEST TYPE CONFINING STRESS | WJE 3020-012 B-C 9' UCS |
| NOTES | | 2 |
| File name: | 3020012lmage_19_09_2 | 25_06_54_26 |

CLIENT JOB NO. PROJECT PROJECT NO. LOCATION DATE TESTED TECHNICIAN Wiss Janney Elstner 3020-012 Persigo WWTP --Grand Junction CO 09/24/19 CAL

| BORING NO. | B-6 |
|--------------|-------|
| DEPTH | 9' |
| SAMPLE NO. | |
| DATE SAMPLED | |
| DESCRIPTION | liner |

| Displacement (in) | Displacement (cm) | Strain (%) | Average Cross Sectional Area (in ²) | Load (lbs) | Load (N) | Stress (psf) | Stress (kPa |
|-------------------|-------------------|------------|--|------------|----------|--------------|-------------|
| 0.0000 | 0.000 | 0.00 | 2.90 | 0 | 0 | 0 | 0 |
| 0.0021 | 0.005 | 0.05 | 2.90 | 0.6 | 3 | 28 | 1 |
| 0.0042 | 0.011 | 0.10 | 2.90 | 2.1 | 9 | 103 | 5 |
| 0.0066 | 0.017 | 0.16 | 2.90 | 3.8 | 17 | 188 | 9 |
| 0.0087 | 0.022 | 0.22 | 2.90 | 4.5 | 20 | 221 | 11 |
| 0.0107 | 0.027 | 0.27 | 2.91 | 5.4 | 24 | 265 | 13 |
| 0.0130 | 0.033 | 0.32 | 2.91 | 5.9 | 26 | 290 | 14 |
| 0.0150 | 0.038 | 0.37 | 2.91 | 6.3 | 28 | 311 | 15 |
| 0.0173 | 0.044 | 0.43 | 2.91 | 7.1 | 31 | 350 | 17 |
| 0.0194 | 0.049 | 0.48 | 2.91 | 8.0 | 35 | 393 | 19 |
| 0.0215 | 0.055 | 0.53 | 2.91 | 8.1 | 36 | 399 | 19 |
| 0.0237 | 0.060 | 0.59 | 2.92 | 8.6 | 38 | 423 | 20 |
| 0.0257 | 0.065 | 0.64 | 2.92 | 9.5 | 42 | 468 | 22 |
| 0.0281 | 0.071 | 0.70 | 2.92 | 10 | 45 | 499 | 24 |
| 0.0304 | 0.077 | 0.76 | 2.92 | 11 | 47 | 525 | 25 |
| 0.0324 | 0.082 | 0.81 | 2.92 | 11 | 50 | 550 | 26 |
| 0.0344 | 0.087 | 0.86 | 2.92 | 12 | 53 | 582 | 28 |
| 0.0365 | 0.093 | 0.91 | 2.92 | 12 | 54 | 599 | 29 |
| 0.0389 | 0.099 | 0.97 | 2.93 | 13 | 57 | 632 | 30 |
| 0.0410 | 0.104 | 1.02 | 2.93 | 14 | 61 | 670 | 32 |
| 0.0430 | 0.109 | 1.07 | 2.93 | 14 | 63 | 695 | 33 |
| 0.0452 | 0.115 | 1.12 | 2.93 | 15 | 66 | 728 | 35 |
| 0.0473 | 0.120 | 1.18 | 2.93 | 15 | 67 | 742 | 36 |
| 0.0494 | 0.125 | 1.23 | 2.93 | 16 | 71 | 786 | 38 |
| 0.0514 | 0.131 | 1.28 | 2.94 | 17 | 75 | 827 | 40 |
| 0.0535 | 0.136 | 1.33 | 2.94 | 18 | 78 | 858 | 41 |
| 0.0556 | 0.141 | 1.38 | 2.94 | 18 | 80 | 881 | 42 |
| 0.0576 | 0.146 | 1.43 | 2.94 | 19 | 83 | 912 | 44 |
| 0.0597 | 0.152 | 1.48 | 2.94 | 19 | 86 | 942 | 45 |
| 0.0619 | 0.157 | 1.54 | 2.94 | 20 | 88 | 973 | 47 |
| 0.0639 | 0.162 | 1.59 | 2.95 | 20 | 91 | 995 | 48 |
| 0.0659 | 0.167 | 1.64 | 2.95 | 21 | 93 | 1018 | 49 |
| 0.0680 | 0.173 | 1.69 | 2.95 | 22 | 96 | 1059 | 51 |
| 0.0701 | 0.178 | 1.74 | 2.95 | 22 | 99 | 1085 | 52 |
| 0.0722 | 0.183 | 1.80 | 2.95 | 23 | 103 | 1127 | 54 |
| 0.0743 | 0.189 | 1.85 | 2.95 | 24 | 105 | 1155 | 55 |
| 0.0764 | 0.194 | 1.90 | 2.95 | 24 | 108 | 1180 | 56 |
| 0.0788 | 0.200 | 1.96 | 2.96 | 25 | 110 | 1201 | 58 |
| 0.0810 | 0.206 | 2.01 | 2.96 | 25 | 113 | 1234 | 59 |
| 0.0830 | 0.211 | 2.06 | 2.96 | 26 | 117 | 1278 | 61 |
| 0.0851 | 0.216 | 2.12 | 2.96 | 26 | 118 | 1286 | 62 |
| 0.0872 | 0.221 | 2.17 | 2.96 | 27 | 120 | 1315 | 63 |
| 0.0894 | 0.227 | 2.22 | 2.96 | 28 | 123 | 1349 | 65 |

CLIENT Wiss Janney Elstner BORING NO. B-6 JOB NO. 3020-012 DEPTH 9' PROJECT Persigo WWTP SAMPLE NO. ----PROJECT NO. DATE SAMPLED ------LOCATION Grand Junction CO DESCRIPTION liner DATE TESTED 09/24/19 **TECHNICIAN** CAL

| Displacement (in) | Displacement (cm) | Strain (%) | Average Cross Sectional Area (in ²) | Load (Ibs) | Load (N) | Stress (psf) | Stress (kPa) |
|-------------------|-------------------|------------|--|------------|----------|--------------|--------------|
| 0.0914 | 0.232 | 2.27 | 2.97 | 28 | 127 | 1381 | 66 |
| 0.0937 | 0.238 | 2.33 | 2.97 | 29 | 128 | 1400 | 67 |
| 0.0959 | 0.244 | 2.38 | 2.97 | 29 | 131 | 1430 | 68 |
| 0.0982 | 0.249 | 2.44 | 2.97 | 30 | 135 | 1469 | 70 |
| 0.1003 | 0.255 | 2.49 | 2.97 | 31 | 136 | 1482 | 71 |
| 0.1024 | 0.260 | 2.55 | 2.97 | 31 | 140 | 1522 | 73 |
| 0.1044 | 0.265 | 2.60 | 2.98 | 32 | 141 | 1536 | 74 |
| 0.1064 | 0.270 | 2.65 | 2.98 | 33 | 145 | 1573 | 75 |
| 0.1085 | 0.276 | 2.70 | 2.98 | 33 | 146 | 1586 | 76 |
| 0.1107 | 0.281 | 2.75 | 2.98 | 33 | 148 | 1610 | 77 |
| 0.1129 | 0.287 | 2.81 | 2.98 | 34 | 152 | 1647 | 79 |
| 0.1150 | 0.292 | 2.86 | 2.98 | 35 | 155 | 1677 | 80 |
| 0.1178 | 0.299 | 2.93 | 2.99 | 35 | 156 | 1688 | 81 |
| 0.1198 | 0.304 | 2.98 | 2.99 | 36 | 159 | 1726 | 83 |
| 0.1219 | 0.310 | 3.03 | 2.99 | 36 | 161 | 1746 | 84 |
| 0.1239 | 0.315 | 3.08 | 2.99 | 36 | 162 | 1754 | 84 |
| 0.1261 | 0.320 | 3.14 | 2.99 | 37 | 166 | 1792 | 86 |
| 0.1285 | 0.326 | 3.20 | 2.99 | 38 | 168 | 1813 | 87 |
| 0.1311 | 0.333 | 3.26 | 3.00 | 39 | 171 | 1851 | 89 |
| 0.1333 | 0.339 | 3.32 | 3.00 | 39 | 175 | 1886 | 90 |
| 0.1355 | 0.344 | 3.37 | 3.00 | 40 | 177 | 1908 | 91 |
| 0.1378 | 0.350 | 3.43 | 3.00 | 40 | 178 | 1918 | 92 |
| 0.1400 | 0.356 | 3.48 | 3.00 | 41 | 183 | 1969 | 94 |
| 0.1422 | 0.361 | 3.54 | 3.00 | 41 | 184 | 1986 | 95 |
| 0.1442 | 0.366 | 3.59 | 3.01 | 42 | 187 | 2019 | 97 |
| 0.1464 | 0.372 | 3.64 | 3.01 | 43 | 189 | 2037 | 98 |
| 0.1484 | 0.377 | 3.69 | 3.01 | 43 | 192 | 2060 | 99 |
| 0.1504 | 0.382 | 3.74 | 3.01 | 44 | 194 | 2089 | 100 |
| 0.1525 | 0.387 | 3.79 | 3.01 | 44 | 197 | 2119 | 101 |
| 0.1547 | 0.393 | 3.85 | 3.01 | 45 | 200 | 2152 | 103 |
| 0.1567 | 0.398 | 3.90 | 3.02 | 46 | 202 | 2173 | 104 |
| 0.1589 | 0.404 | 3.95 | 3.02 | 46 | 205 | 2199 | 105 |
| 0.1611 | 0.409 | 4.01 | 3.02 | 47 | 207 | 2223 | 106 |
| 0.1631 | 0.414 | 4.06 | 3.02 | 48 | 212 | 2268 | 109 |
| 0.1652 | 0.420 | 4.11 | 3.02 | 48 | 212 | 2272 | 109 |
| 0.1672 | 0.425 | 4.16 | 3.02 | 48 | 215 | 2302 | 110 |
| 0.1693 | 0.430 | 4.21 | 3.03 | 49 | 217 | 2324 | 111 |
| 0.1713 | 0.435 | 4.26 | 3.03 | 49 | 219 | 2338 | 112 |
| 0.1734 | 0.440 | 4.31 | 3.03 | 50 | 221 | 2360 | 113 |
| 0.1755 | 0.446 | 4.36 | 3.03 | 50 | 223 | 2386 | 114 |
| 0.1776 | 0.451 | 4.42 | 3.03 | 51 | 226 | 2418 | 116 |
| 0.1798 | 0.457 | 4.47 | 3.03 | 52 | 230 | 2454 | 118 |
| 0.1824 | 0.463 | 4.54 | 3.04 | 52 | 231 | 2465 | 118 |

CLIENT JOB NO. PROJECT PROJECT NO. LOCATION DATE TESTED TECHNICIAN Wiss Janney Elstner 3020-012 Persigo WWTP --Grand Junction CO 09/24/19 CAL

| BORING NO. | B-6 |
|--------------|-------|
| DEPTH | 9' |
| SAMPLE NO. | |
| DATE SAMPLED | _ |
| DESCRIPTION | liner |

| Displacement (in) | Displacement (cm) | Strain (%) | Average Cross Sectional Area (in²) | Load (lbs) | Load (N) | Stress (psf) | Stress (kPa) |
|-------------------|-------------------|------------|---------------------------------------|------------|----------|--------------|--------------|
| 0.1844 | 0.468 | 4.59 | 3.04 | 53 | 234 | 2496 | 120 |
| 0.1865 | 0.474 | 4.64 | 3.04 | 53 | 238 | 2531 | 121 |
| 0.1886 | 0.479 | 4.69 | 3.04 | 54 | 239 | 2548 | 122 |
| 0.1907 | 0.484 | 4.74 | 3.04 | 54 | 242 | 2571 | 123 |
| 0.1927 | 0.489 | 4.79 | 3.04 | 55 | 245 | 2605 | 125 |
| 0.1947 | 0.495 | 4.84 | 3.05 | 56 | 248 | 2633 | 126 |
| 0.1968 | 0.500 | 4.89 | 3.05 | 56 | 250 | 2653 | 127 |
| 0.1988 | 0.505 | 4.94 | 3.05 | 57 | 252 | 2674 | 128 |
| 0.2009 | 0.510 | 5.00 | 3.05 | 57 | 254 | 2694 | 129 |
| 0.2032 | 0.516 | 5.05 | 3.05 | 57 | 256 | 2712 | 130 |
| 0.2053 | 0.521 | 5.11 | 3.05 | 58 | 258 | 2733 | 131 |
| 0.2074 | 0.527 | 5.16 | 3.06 | 59 | 262 | 2778 | 133 |
| 0.2094 | 0.532 | 5.21 | 3.06 | 59 | 264 | 2790 | 134 |
| 0.2116 | 0.537 | 5.26 | 3.06 | 59 | 264 | 2797 | 134 |
| 0.2137 | 0.543 | 5.31 | 3.06 | 60 | 268 | 2836 | 136 |
| 0.2157 | 0.548 | 5.36 | 3.06 | 61 | 269 | 2845 | 136 |
| 0.2177 | 0.553 | 5.41 | 3.06 | 61 | 272 | 2876 | 138 |
| 0.2199 | 0.559 | 5.47 | 3.07 | 62 | 274 | 2896 | 139 |
| 0.2225 | 0.565 | 5.53 | 3.07 | 62 | 276 | 2916 | 140 |
| 0.2245 | 0.570 | 5.58 | 3.07 | 63 | 279 | 2945 | 141 |
| 0.2266 | 0.576 | 5.64 | 3.07 | 63 | 280 | 2954 | 141 |
| 0.2291 | 0.582 | 5.70 | 3.07 | 64 | 283 | 2982 | 143 |
| 0.2312 | 0.587 | 5.75 | 3.08 | 64 | 287 | 3016 | 144 |
| 0.2334 | 0.593 | 5.80 | 3.08 | 65 | 288 | 3031 | 145 |
| 0.2356 | 0.598 | 5.86 | 3.08 | 65 | 290 | 3045 | 146 |
| 0.2377 | 0.604 | 5.91 | 3.08 | 65 | 291 | 3059 | 146 |
| 0.2398 | 0.609 | 5.96 | 3.08 | 66 | 293 | 3078 | 147 |
| 0.2418 | 0.614 | 6.01 | 3.08 | 67 | 296 | 3110 | 149 |
| 0.2439 | 0.620 | 6.07 | 3.09 | 67 | 298 | 3125 | 150 |
| 0.2462 | 0.625 | 6.12 | 3.09 | 67 | 300 | 3146 | 151 |
| 0.2487 | 0.632 | 6.19 | 3.09 | 68 | 301 | 3154 | 151 |
| 0.2510 | 0.638 | 6.24 | 3.09 | 68 | 305 | 3190 | 153 |
| 0.2530 | 0.643 | 6.29 | 3.09 | 69 | 308 | 3219 | 154 |
| 0.2553 | 0.648 | 6.35 | 3.09 | 69 | 307 | 3216 | 154 |
| 0.2575 | 0.654 | 6.40 | 3.10 | 70 | 309 | 3233 | 155 |
| 0.2595 | 0.659 | 6.45 | 3.10 | 70 | 312 | 3257 | 156 |
| 0.2616 | 0.664 | 6.51 | 3.10 | 71 | 314 | 3283 | 157 |
| 0.2637 | 0.670 | 6.56 | 3.10 | 71 | 317 | 3312 | 159 |
| 0.2658 | 0.675 | 6.61 | 3.10 | 72 | 318 | 3318 | 159 |
| 0.2679 | 0.680 | 6.66 | 3.11 | 72 | 320 | 3341 | 160 |
| 0.2700 | 0.686 | 6.71 | 3.11 | 73 | 323 | 3367 | 161 |
| 0.2723 | 0.692 | 6.77 | 3.11 | 73 | 324 | 3372 | 161 |
| 0.2747 | 0.698 | 6.83 | 3.11 | 73 | 325 | 3381 | 162 |

CLIENT JOB NO. PROJECT PROJECT NO. LOCATION DATE TESTED TECHNICIAN Wiss Janney Elstner 3020-012 Persigo WWTP --Grand Junction CO 09/24/19 CAL BORING NO.B-6DEPTH9'SAMPLE NO.--DATE SAMPLED--DESCRIPTIONliner

| Displacement (in) | Displacement (cm) | Strain (%) | Average Cross Sectional Area (in ²) | Load (lbs) | Load (N) | Stress (psf) | Stress (kPa) |
|-------------------|-------------------|------------|--|------------|----------|--------------|--------------|
| 0.2769 | 0.703 | 6.89 | 3.11 | 74 | 328 | 3408 | 163 |
| 0.2789 | 0.708 | 6.94 | 3.11 | 74 | 329 | 3422 | 164 |
| 0.2810 | 0.714 | 6.99 | 3.12 | 74 | 331 | 3440 | 165 |
| 0.2832 | 0.719 | 7.04 | 3.12 | 75 | 333 | 3460 | 166 |
| 0.2854 | 0.725 | 7.10 | 3.12 | 75 | 336 | 3484 | 167 |
| 0.2875 | 0.730 | 7.15 | 3.12 | 76 | 337 | 3494 | 167 |
| 0.2899 | 0.736 | 7.21 | 3.12 | 76 | 338 | 3506 | 168 |
| 0.2919 | 0.741 | 7.26 | 3.13 | 77 | 341 | 3528 | 169 |
| 0.2941 | 0.747 | 7.31 | 3.13 | 77 | 342 | 3545 | 170 |
| 0.2964 | 0.753 | 7.37 | 3.13 | 77 | 344 | 3558 | 170 |
| 0.2985 | 0.758 | 7.42 | 3.13 | 78 | 345 | 3570 | 171 |
| 0.3005 | 0.763 | 7.47 | 3.13 | 78 | 347 | 3581 | 171 |
| 0.3028 | 0.769 | 7.53 | 3.13 | 78 | 348 | 3592 | 172 |
| 0.3048 | 0.774 | 7.58 | 3.14 | 79 | 350 | 3616 | 173 |
| 0.3068 | 0.779 | 7.63 | 3.14 | 79 | 352 | 3627 | 174 |
| 0.3089 | 0.785 | 7.68 | 3.14 | 79 | 353 | 3635 | 174 |
| 0.3110 | 0.790 | 7.73 | 3.14 | 80 | 354 | 3649 | 175 |
| 0.3132 | 0.796 | 7.79 | 3.14 | 80 | 357 | 3678 | 176 |
| 0.3162 | 0.803 | 7.86 | 3.15 | 81 | 359 | 3693 | 177 |
| 0.3184 | 0.809 | 7.92 | 3.15 | 81 | 360 | 3698 | 177 |
| 0.3205 | 0.814 | 7.97 | 3.15 | 81 | 362 | 3719 | 178 |
| 0.3226 | 0.819 | 8.02 | 3.15 | 82 | 363 | 3724 | 178 |
| 0.3247 | 0.825 | 8.08 | 3.15 | 82 | 365 | 3746 | 179 |
| 0.3268 | 0.830 | 8.13 | 3.15 | 82 | 366 | 3757 | 180 |
| 0.3288 | 0.835 | 8.18 | 3.16 | 83 | 368 | 3778 | 181 |
| 0.3308 | 0.840 | 8.23 | 3.16 | 83 | 370 | 3788 | 181 |
| 0.3331 | 0.846 | 8.28 | 3.16 | 83 | 370 | 3795 | 182 |
| 0.3353 | 0.852 | 8.34 | 3.16 | 83 | 371 | 3802 | 182 |
| 0.3374 | 0.857 | 8.39 | 3.16 | 84 | 373 | 3821 | 183 |
| 0.3395 | 0.862 | 8.44 | 3.17 | 84 | 375 | 3837 | 184 |
| 0.3416 | 0.868 | 8.50 | 3.17 | 85 | 376 | 3844 | 184 |
| 0.3438 | 0.873 | 8.55 | 3.17 | 85 | 378 | 3862 | 185 |
| 0.3458 | 0.878 | 8.60 | 3.17 | 85 | 379 | 3870 | 185 |
| 0.3479 | 0.884 | 8.65 | 3.17 | 85 | 380 | 3875 | 186 |
| 0.3499 | 0.889 | 8.70 | 3.17 | 86 | 381 | 3888 | 186 |
| 0.3521 | 0.894 | 8.76 | 3.18 | 86 | 384 | 3911 | 187 |
| 0.3541 | 0.899 | 8.81 | 3.18 | 87 | 386 | 3933 | 188 |
| 0.3562 | 0.905 | 8.86 | 3.18 | 87 | 387 | 3939 | 189 |
| 0.3582 | 0.910 | 8.91 | 3.18 | 87 | 389 | 3954 | 189 |
| 0.3604 | 0.915 | 8.96 | 3.18 | 88 | 390 | 3969 | 190 |
| 0.3625 | 0.921 | 9.02 | 3.19 | 88 | 391 | 3973 | 190 |
| 0.3647 | 0.926 | 9.07 | 3.19 | 88 | 393 | 3996 | 191 |
| 0.3668 | 0.932 | 9.12 | 3.19 | 89 | 394 | 3997 | 191 |

CLIENT JOB NO. PROJECT PROJECT NO. LOCATION DATE TESTED TECHNICIAN Wiss Janney Elstner 3020-012 Persigo WWTP --Grand Junction CO 09/24/19 CAL

| | BORING NO. | B-6 |
|---|--------------|-------|
| * | DEPTH | 9' |
| | SAMPLE NO. | |
| | DATE SAMPLED | |
| | DESCRIPTION | liner |
| | | |

| Displacement (in) | Displacement (cm) | Strain (%) | Average Cross Sectional Area (in²) | Load (lbs) | Load (N) | Stress (psf) | Stress (kPa) |
|-------------------|-------------------|---------------|---------------------------------------|------------|----------|--------------|--------------|
| 0.3689 | 0.937 | 9.17 | 3.19 | 89 | 395 | 4003 | 192 |
| 0.3710 | 0.942 | 9.23 | 3.19 | 89 | 397 | 4026 | 193 |
| 0.3730 | 0.947 | 9.28 | 3.19 | 89 | 397 | 4022 | 193 |
| 0.3753 | 0.953 | 9.33 | 3.20 | 90 | 399 | 4040 | 193 |
| 0.3774 | 0.959 | 9.39 | 3.20 | 90 | 401 | 4056 | 194 |
| 0.3794 | 0.964 | 9.44 | 3.20 | 90 | 401 | 4053 | 194 |
| 0.3816 | 0.969 | 9.49 | 3.20 | 91 | 403 | 4078 | 195 |
| 0.3837 | 0.975 | 9.54 | 3.20 | 91 | 404 | 4086 | 196 |
| 0.3858 | 0.980 | 9.59 | 3.21 | 91 | 405 | 4092 | 196 |
| 0.3879 | 0.985 | 9.65 | 3.21 | 91 | 407 | 4103 | 196 |
| 0.3900 | 0.991 | 9.70 | 3.21 | 92 | 407 | 4110 | 197 |
| 0.3921 | 0.996 | 9.75 | 3.21 | 92 | 407 | 4105 | 197 |
| 0.3943 | 1.002 | 9.81 | 3.21 | 92 | 410 | 4133 | 198 |
| 0.3966 | 1.007 | 9.86 | 3.22 | 92 | 411 | 4137 | 198 |
| 0.3987 | 1.013 | 9.92 | 3.22 | 93 | 412 | 4148 | 199 |
| 0.4013 | 1.019 | 9.98 | 3.22 | 93 | 413 | 4156 | 199 |
| 0.4035 | 1.025 | 10.03 | 3.22 | 93 | 414 | 4163 | 199 |
| 0.4059 | 1.031 | 10.09 | 3.22 | 93 | 416 | 4173 | 200 |
| 0.4080 | 1.036 | 10.15 | 3.23 | 94 | 416 | 4178 | 200 |
| 0.4102 | 1.042 | 10.20 | 3.23 | 94 | 417 | 4185 | 200 |
| 0.4124 | 1.047 | 10.26 | 3.23 | 94 | 418 | 4191 | 201 |
| 0.4144 | 1.053 | 10.31 | 3.23 | 94 | 420 | 4204 | 201 |
| 0.4166 | 1.058 | 10.36 | 3.23 | 94 | 420 | 4208 | 201 |
| 0.4191 | 1.065 | 10.42 | 3.24 | 95 | 422 | 4220 | 202 |
| 0.4211 | 1.070 | 10.47 | 3.24 | 95 | 423 | 4229 | 202 |
| 0.4233 | 1.075 | 10.53 | 3.24 | 95 | 423 | 4226 | 202 |
| 0.4260 | 1.082 | 10.59 | 3.24 | 95 | 424 | 4235 | 203 |
| 0.4281 | 1.087 | 10.65 | 3.24 | 96 | 426 | 4253 | 204 |
| 0.4305 | 1.093 | 10.71 | 3.25 | 96 | 426 | 4251 | 204 |
| 0.4326 | 1.099 | 10.76 | 3.25 | 96 | 427 | 4255 | 204 |
| 0.4347 | 1.104 | 10.81 | 3.25 | 96 | 429 | 4270 | 204 |
| 0.4368 | 1.109 | 10.86 | 3.25 | 96 | 428 | 4264 | 204 |
| 0.4389 | 1.115 | 10.92 | 3.25 | 97 | 429 | 4272 | 205 |
| 0.4414 | 1.121 | 10.98 | 3.26 | 97 | 430 | 4281 | 205 |
| 0.4440 | 1.128 | 11.04 | 3.26 | 97 | 432 | 4291 | 205 |
| 0.4468 | 1.135 | 11.11 | 3.26 | 97 | 433 | 4296 | 206 |
| 0.4488 | 1.140 | 11.16 | 3.26 | 97 | 433 | 4294 | 206 |
| 0.4509 | 1.145 | 11.21 | 3.26 | 98 | 434 | 4305 | 206 |
| 0.4529 | 1.150 | 11.26 | 3.27 | 98 | 434 | 4301 | 206 |
| 0.4550 | 1.156 | 11.32 | 3.27 | 98 | 435 | 4308 | 206 |
| 0.4571 | 1.161 | 11.37 | 3.27 | 98 | 435 | 4311 | 206 |
| 0.4592 | 1.166 | 11. 42 | 3.27 | 98 | 436 | 4309 | 206 |
| 0.4616 | 1.172 | 11.48 | 3.27 | 98 | 437 | 4316 | 207 |

CLIENT JOB NO. PROJECT PROJECT NO. LOCATION DATE TESTED TECHNICIAN Wiss Janney Elstner 3020-012 Persigo WWTP --Grand Junction CO 09/24/19 CAL

| BORING NO. | B-6 |
|--------------|-------|
| DEPTH | 9' |
| SAMPLE NO. | |
| DATE SAMPLED | |
| DESCRIPTION | liner |
| | |

| $\begin{array}{ c c c c c c c c c c c c c c c c c c c$ | Displacement (in) | Displacement (cm) | Strain (%) | Average Cross Sectional Area (in²) | Load (ibs) | Load (N) | Stress (psf) | Stress (kPa) |
|--|-------------------|-------------------|------------|---------------------------------------|------------|----------|--------------|--------------|
| $\begin{array}{c c c c c c c c c c c c c c c c c c c $ | 0.4637 | 1.178 | 11.53 | 3.28 | 98 | 438 | 4326 | 207 |
| $\begin{array}{c c c c c c c c c c c c c c c c c c c $ | 0.4661 | 1.184 | 11.59 | 3.28 | 98 | 437 | 4320 | 207 |
| $\begin{array}{c c c c c c c c c c c c c c c c c c c $ | 0.4681 | 1.189 | 11.64 | 3.28 | 99 | 439 | 4333 | 207 |
| $\begin{array}{c c c c c c c c c c c c c c c c c c c $ | 0.4702 | 1.194 | 11.69 | 3.28 | 99 | 439 | 4329 | 207 |
| 0.47691.21111.863.29994414343208 0.4791 1.21711.913.29994414341208 0.4811 1.22211.963.29994424346208 0.4833 1.22812.023.29994424346208 0.4854 1.23312.173.30994424346208 0.4874 1.24312.173.30994424347208 0.4874 1.24312.173.30994424337208 0.4874 1.24812.223.301004434343208 0.4957 1.25912.333.311004434338208 0.4967 1.25912.333.311004434343208 0.4967 1.26412.443.311004444336208 0.5023 1.27612.493.311004444331208 0.5044 1.29112.643.321004444332207 0.5166 1.2971.3763.321004444323207 0.5160 1.30812.813.321004444324207 0.5171 1.31312.863.331004444324207 0.5161 1.30812.813.321004444324207 0.5161 1.39513.073.33100 <td>0.4725</td> <td>1.200</td> <td>11.75</td> <td>3.28</td> <td>99</td> <td>438</td> <td>4321</td> <td>207</td> | 0.4725 | 1.200 | 11.75 | 3.28 | 99 | 438 | 4321 | 207 |
| 0.4791 1.217 11.91 3.29 99 441 4341 208 0.4811 1.222 11.96 3.29 99 441 4340 208 0.4854 1.233 12.07 3.30 99 442 4345 208 0.4874 1.238 12.07 3.30 99 442 4340 208 0.4874 1.238 12.17 3.30 99 442 4340 208 0.4894 1.248 12.22 3.30 100 443 4344 208 0.4935 1.253 12.27 3.30 100 443 4343 208 0.4937 1.264 12.38 3.31 100 443 4335 208 0.4977 1.264 12.38 3.31 100 444 4345 208 0.5002 1.271 12.44 3.31 100 444 4345 208 0.5033 1.286 12.59 3.32 100 444 4337 208 0.5043 1.281 12.64 3.32 100 444 4332 207 0.5150 1.303 12.76 3.32 100 444 4332 207 0.5160 1.297 12.70 3.33 100 444 4322 207 0.5150 1.308 12.81 3.32 100 444 4322 207 0.514 1.324 12.97 3.33 100 444 </td <td>0.4747</td> <td>1.206</td> <td>11.81</td> <td>3.29</td> <td>99</td> <td>441</td> <td>4341</td> <td>208</td> | 0.4747 | 1.206 | 11.81 | 3.29 | 99 | 441 | 4341 | 208 |
| 0.4811 1.222 11.96 3.29 99 441 4340 208 0.4833 1.228 12.02 3.29 99 442 4346 208 0.4874 1.233 12.07 3.30 99 442 4346 208 0.4874 1.233 12.12 3.30 99 442 4340 208 0.4944 1.243 12.12 3.30 99 442 4337 208 0.4914 1.243 12.27 3.30 100 443 4344 208 0.4957 1.259 12.33 3.31 100 443 4338 208 0.4977 1.264 12.38 3.31 100 444 4345 208 0.5023 1.276 12.49 3.31 100 444 4337 208 0.5043 1.281 12.64 3.32 100 444 4337 208 0.5084 1.297 12.76 3.32 100 444 4332 207 0.5130 1.303 12.76 3.32 100 444 4328 207 0.5130 1.303 12.261 3.33 100 444 4322 207 0.5133 13.91 12.97 3.33 100 444 4322 207 0.5133 13.92 13.02 3.33 100 444 4322 207 0.5133 13.91 13.28 3.34 100 443 | 0.4769 | 1.211 | 11.86 | 3.29 | 99 | 441 | 4343 | 208 |
| 0.4833 1.228 12.02 3.29 99 442 4346 208 0.4854 1.233 12.07 3.30 99 442 4346 208 0.4854 1.243 12.12 3.30 99 442 4337 208 0.4894 1.243 12.17 3.30 100 443 4344 208 0.4935 1.263 12.27 3.30 100 443 4338 208 0.4935 1.259 12.33 3.31 100 443 4335 208 0.4977 1.264 12.38 3.31 100 444 4341 208 0.5002 1.276 12.49 3.31 100 444 4341 208 0.5023 1.276 12.49 3.31 100 444 4331 207 0.5043 1.281 12.64 3.32 100 444 4331 207 0.5106 1.308 12.81 3.32 100 444 4322 207 0.5130 1.333 | 0.4791 | 1.217 | 11.91 | 3.29 | 99 | 441 | 4341 | 208 |
| 0.4854 1.233 12.07 3.30 99 442 4345 208 0.4874 1.238 12.12 3.30 99 442 4340 208 0.4894 1.243 12.17 3.30 99 442 4344 208 0.4894 1.248 12.22 3.30 100 443 4343 208 0.4957 1.259 12.33 3.31 100 443 4335 208 0.4957 1.254 12.38 3.31 100 443 4335 208 0.5002 1.271 12.44 3.31 100 444 4341 208 0.5023 1.276 12.49 3.31 100 444 4337 208 0.5043 1.281 12.54 3.32 100 444 4332 207 0.5106 1.297 12.70 3.32 100 444 4328 207 0.5130 1.308 12.81 3.32 100 444 4328 207 0.5130 1.308 | 0.4811 | 1.222 | 11.96 | 3.29 | 99 | 441 | 4340 | 208 |
| 0.4874 1.238 12.12 3.30 99 442 4307 208 0.4894 1.243 12.17 3.30 99 442 4337 208 0.4914 1.248 12.22 3.30 100 443 4344 208 0.4957 1.259 12.33 3.31 100 443 4335 208 0.4977 1.264 12.38 3.31 100 443 4335 208 0.5002 1.276 12.49 3.31 100 444 4341 208 0.5003 1.281 12.54 3.31 100 444 4331 208 0.5043 1.281 12.64 3.32 100 444 4331 207 0.5064 1.291 12.64 3.32 100 444 4332 207 0.5160 1.297 12.70 3.32 100 444 4322 207 0.5150 1.308 12.81 | 0.4833 | 1.228 | 12.02 | 3.29 | 99 | 442 | 4346 | 208 |
| 0.4894 1.243 12.17 3.30 99 442 4337 208 0.4914 1.248 12.22 3.30 100 443 4344 208 0.4935 1.253 12.27 3.30 100 443 4343 208 0.4957 1.264 12.38 3.31 100 443 4335 208 0.5002 1.271 12.44 3.31 100 444 4341 208 0.5023 1.276 12.49 3.31 100 444 4331 208 0.5063 1.281 12.64 3.32 100 444 4331 207 0.5106 1.297 12.76 3.32 100 444 4332 207 0.5130 1.303 12.76 3.32 100 444 4321 207 0.5150 1.308 12.81 3.32 100 444 4323 207 0.5171 1.313 12.86 | 0.4854 | 1.233 | 12.07 | 3.30 | 99 | 442 | 4345 | 208 |
| 0.4914 1.248 12.22 3.30 100 443 4344 208 0.4935 1.253 12.27 3.30 100 443 4343 208 0.4957 1.259 12.33 3.31 100 443 4338 208 0.4957 1.264 12.38 3.31 100 443 4335 208 0.5002 1.271 12.44 3.31 100 444 4345 208 0.5023 1.276 12.49 3.31 100 444 4331 208 0.5043 1.286 12.59 3.32 100 444 4332 207 0.5106 1.297 12.70 3.32 100 444 4326 207 0.5130 1.303 12.76 3.32 100 444 4326 207 0.5165 1.308 12.81 3.33 100 444 4321 207 0.5171 1.313 12.86 | 0.4874 | 1.238 | 12.12 | 3.30 | 99 | 442 | 4340 | 208 |
| 0.4935 1.253 12.27 3.30 100 443 4343 208 0.4957 1.259 12.33 3.31 100 443 4335 208 0.4977 1.264 12.38 3.31 100 443 4335 208 0.5002 1.271 12.44 3.31 100 444 4345 208 0.5003 1.276 12.49 3.31 100 444 4337 208 0.5043 1.281 12.54 3.31 100 444 4337 208 0.5063 1.286 12.59 3.32 100 444 4331 207 0.5106 1.297 12.70 3.32 100 444 4325 207 0.5130 1.303 12.76 3.32 100 444 4321 207 0.5150 1.308 12.81 3.32 100 444 4321 207 0.514 1.324 12.97 3.33 100 444 4314 207 0.5246 1.335 | 0.4894 | 1.243 | 12.17 | 3.30 | 99 | 442 | 4337 | 208 |
| 0.4957 1.259 12.33 3.31 100 443 4338 208 0.4977 1.264 12.38 3.31 100 443 4335 208 0.5002 1.271 12.44 3.31 100 444 4345 208 0.5023 1.276 12.49 3.31 100 444 4337 208 0.5043 1.281 12.54 3.31 100 444 4332 207 0.5106 1.297 12.70 3.32 100 444 4331 207 0.5130 1.303 12.76 3.32 100 444 4325 207 0.5130 1.303 12.76 3.32 100 444 4325 207 0.5150 1.308 12.81 3.32 100 444 4321 207 0.5171 1.319 12.91 3.33 100 444 4314 207 0.5234 1.329 13.02 | 0.4914 | 1.248 | 12.22 | 3.30 | 100 | 443 | 4344 | 208 |
| 0.4977 1.264 12.38 3.31 100 443 4335 208 0.5002 1.271 12.44 3.31 100 444 4345 208 0.5023 1.276 12.49 3.31 100 444 4337 208 0.5043 1.281 12.54 3.31 100 444 4337 208 0.5063 1.286 12.59 3.32 100 444 4332 207 0.5106 1.297 12.64 3.32 100 444 4328 207 0.5130 1.303 12.76 3.32 100 444 4325 207 0.5150 1.308 12.81 3.32 100 444 4325 207 0.5151 1.313 12.86 3.33 100 444 4321 207 0.5153 1.319 12.91 3.33 100 444 4314 207 0.5256 1.335 13.07 | 0.4935 | 1.253 | 12.27 | 3.30 | 100 | 443 | 4343 | 208 |
| $\begin{array}{c ccccccccccccccccccccccccccccccccccc$ | 0.4957 | 1.259 | 12.33 | 3.31 | 100 | 443 | 4338 | 208 |
| 0.5023 1.276 12.49 3.31 100 444 4341 208 0.5043 1.281 12.54 3.31 100 444 4339 208 0.5063 1.286 12.59 3.32 100 444 4337 208 0.5084 1.297 12.64 3.32 100 444 4332 207 0.5106 1.297 12.70 3.32 100 444 4328 207 0.5130 1.303 12.76 3.32 100 444 4323 207 0.5150 1.308 12.81 3.32 100 444 4323 207 0.5171 1.313 12.86 3.33 100 444 4321 207 0.5214 1.329 13.02 3.33 100 444 4314 207 0.5234 1.329 13.02 3.33 100 444 4314 207 0.5266 1.335 13.07 3.33 100 443 4299 206 0.5376 1.340 | 0.4977 | 1.264 | 12.38 | 3.31 | 100 | 443 | 4335 | 208 |
| 0.5043 1.281 12.54 3.31 100 444 4339 208 0.5063 1.286 12.59 3.32 100 444 4337 208 0.5084 1.291 12.64 3.32 100 444 4332 207 0.5106 1.297 12.70 3.32 100 444 4328 207 0.5130 1.303 12.76 3.32 100 444 4325 207 0.5150 1.308 12.81 3.32 100 444 4323 207 0.5171 1.313 12.86 3.33 100 444 4321 207 0.5171 1.313 12.86 3.33 100 444 4318 207 0.5141 1.324 12.97 3.33 100 444 4314 207 0.5266 1.335 13.07 3.33 100 444 4312 206 0.5276 1.340 13.12 3.34 100 443 4299 206 0.5318 1.351 | 0.5002 | 1.271 | 12.44 | 3.31 | 100 | 444 | 4345 | 208 |
| 0.50631.28612.593.3210044443372080.50841.29112.643.3210044443322070.51061.29712.703.3210044443312070.51301.30312.763.3210044443282070.51501.30812.813.3210044443252070.51711.31312.863.3310044443212070.51931.31912.913.3310044443182070.52141.32412.973.3310044443142070.52561.33513.073.3310044443122060.52761.34013.123.3410044342992060.52761.34013.123.3410044342952060.53181.35113.233.3410044342952060.53391.36613.283.349944342872050.53601.36113.333.349944142692040.54011.37213.483.359944142642040.54211.37713.483.359944042522040.54631.38813.593.359944042522040.54631.38813.643.36984384218202 </td <td>0.5023</td> <td>1.276</td> <td>12.49</td> <td>3.31</td> <td>100</td> <td>444</td> <td>4341</td> <td>208</td> | 0.5023 | 1.276 | 12.49 | 3.31 | 100 | 444 | 4341 | 208 |
| 0.50841.29112.643.3210044443322070.51061.29712.703.3210044443312070.51301.30312.763.3210044443282070.51501.30812.813.3210044443252070.51711.31312.863.3310044443212070.51931.31912.913.3310044443182070.52141.32913.023.3310044443142070.52561.33513.073.3310044443122060.52761.34013.123.3410044342992060.52761.34013.123.3410044342992060.52761.34013.123.3410044342992060.52761.34013.123.3410044342992060.52761.34113.233.349944342672050.53801.36113.333.359944142642040.54211.37713.483.359944142642040.54211.37713.483.359944042522040.54421.38813.593.359944042522040.54631.38813.593.35994404252204 </td <td>0.5043</td> <td>1.281</td> <td>12.54</td> <td>3.31</td> <td>100</td> <td>444</td> <td>4339</td> <td>208</td> | 0.5043 | 1.281 | 12.54 | 3.31 | 100 | 444 | 4339 | 208 |
| 0.51061.29712.703.3210044443312070.51301.30312.763.3210044443282070.51501.30812.813.3210044443252070.51711.31312.863.3310044443232070.51931.31912.913.3310044443212070.52141.32412.973.3310044443182070.52341.32913.023.3310044443122060.52761.34013.123.3410044342992060.52761.34513.173.3410044342992060.53181.35113.233.349944342872050.53001.36113.333.349944242792050.53001.36113.383.359944142642040.54011.37713.483.359944042522060.54631.38813.593.359944042502030.54631.38813.593.359944042502030.54631.38813.643.369843742192020.55041.39813.693.36984384218202 | 0.5063 | 1.286 | 12.59 | 3.32 | 100 | 444 | 4337 | 208 |
| 0.51301.30312.763.3210044443282070.51501.30812.813.3210044443252070.51711.31312.863.3310044443232070.51931.31912.913.3310044443212070.52141.32412.973.3310044443182070.52341.32913.023.3310044443142070.52561.33513.073.3310044443122060.52761.34013.123.3410044342992060.52971.34513.173.3410044342952060.53181.35113.233.349944342872050.53601.36113.333.349944142692040.54011.37213.433.359944142692040.54011.37713.483.359944042522040.54111.37713.483.359944042522040.54421.38813.593.359944042502030.54631.38813.593.359943942342030.54631.38813.643.369843742192020.55041.39813.693.36984384218202 | 0.5084 | 1.291 | 12.64 | 3.32 | 100 | 444 | 4332 | 207 |
| 0.51501.30812.813.3210044443252070.51711.31312.863.3310044443232070.51931.31912.913.3310044443212070.52141.32412.973.3310044443182070.52341.32913.023.3310044443142070.52561.33513.073.3310044443122060.52761.34013.123.3410044342992060.52971.34513.173.3410044342952060.53181.35113.233.349944342672050.53601.36113.333.349944142692040.54011.37213.483.359944142642040.54211.37713.483.359944042522040.54421.38213.533.359944042502030.54631.38813.593.359944042502030.54631.38813.593.369843742192020.55041.39813.693.36984384218202 | 0.5106 | 1.297 | 12.70 | 3.32 | 100 | 444 | 4331 | 207 |
| 0.51711.31312.863.3310044443232070.51931.31912.913.3310044443212070.52141.32412.973.3310044443182070.52341.32913.023.3310044443142070.52561.33513.073.3310044443122060.52761.34013.123.3410044342992060.52971.34513.173.3410044342952060.53181.35113.233.349944342872050.53601.36113.333.349944242792050.53801.36713.383.359944142642040.54011.37713.483.359944042522040.54421.38213.533.359944042502030.54631.38813.593.359944042502030.54631.38813.593.359943942342030.54631.39313.643.369843742192020.55041.39813.693.36984384218202 | 0.5130 | 1.303 | 12.76 | 3.32 | 100 | 444 | 4328 | 207 |
| 0.51931.31912.913.3310044443212070.52141.32412.973.3310044443182070.52341.32913.023.3310044443142070.52561.33513.073.3310044443122060.52761.34013.123.3410044342992060.52971.34513.173.3410044342992060.53181.35113.233.3410044342952060.53391.35613.283.349944342872050.53601.36113.333.349944142692040.54011.37213.433.359944142642040.54211.37713.483.359944042522040.54421.38213.533.359944042502030.54631.38813.593.359944042502030.54631.38813.593.359943942342030.54631.39313.643.369843742192020.55041.39813.693.36984384218202 | 0.5150 | 1.308 | 12.81 | 3.32 | 100 | 444 | 4325 | 207 |
| 0.52141.32412.973.3310044443182070.52341.32913.023.3310044443142070.52561.33513.073.3310044443122060.52761.34013.123.3410044342992060.52971.34513.173.3410044342992060.53181.35113.233.3410044342952060.53391.35613.283.349944342872050.53601.36113.333.349944142692040.53801.36713.483.359944142642040.54211.37713.483.359944042502030.54631.38813.593.359944042502030.54631.38813.593.369843742192020.55041.39813.693.36984384218202 | 0.5171 | 1.313 | 12.86 | 3.33 | 100 | 444 | 4323 | 207 |
| 0.52341.32913.023.3310044443142070.52561.33513.073.3310044443122060.52761.34013.123.3410044342992060.52971.34513.173.3410044342992060.53181.35113.233.3410044342952060.53391.35613.283.349944342872050.53601.36113.333.349944242792050.53801.36713.383.359944142692040.54011.37213.433.359944042522040.54211.37713.483.359944042502030.54631.38813.593.359944042502030.54631.38813.593.369843742192020.55041.39813.693.36984384218202 | 0.5193 | 1.319 | 12.91 | 3.33 | 100 | 444 | 4321 | 207 |
| 0.52561.33513.073.3310044443122060.52761.34013.123.3410044342992060.52971.34513.173.3410044342992060.53181.35113.233.3410044342952060.53391.35613.283.349944342872050.53601.36113.333.349944242792050.53801.36713.383.359944142692040.54011.37213.433.359944042522040.54211.37713.483.359944042502030.54631.38813.593.359944042502030.54631.38813.693.369843742192020.55041.39813.693.36984384218202 | 0.5214 | 1.324 | 12.97 | 3.33 | 100 | 444 | 4318 | 207 |
| 0.52761.34013.123.3410044342992060.52971.34513.173.3410044342992060.53181.35113.233.3410044342952060.53391.35613.283.349944342872050.53601.36113.333.349944242792050.53801.36713.383.359944142692040.54011.37213.433.359944042522040.54211.38213.533.359944042502030.54631.38813.593.359944042342030.54631.39313.643.369843742192020.55041.39813.693.36984384218202 | 0.5234 | 1.329 | 13.02 | 3.33 | 100 | 444 | 4314 | 207 |
| 0.52971.34513.173.3410044342992060.53181.35113.233.3410044342952060.53391.35613.283.349944342872050.53601.36113.333.349944242792050.53801.36713.383.359944142692040.54011.37213.433.359944142642040.54211.37713.483.359944042522040.54631.38813.593.359944042502030.54631.39313.643.369843742192020.55041.39813.693.36984384218202 | 0.5256 | 1.335 | 13.07 | 3.33 | 100 | 444 | 4312 | 206 |
| 0.53181.35113.233.3410044342952060.53391.35613.283.349944342872050.53601.36113.333.349944242792050.53801.36713.383.359944142692040.54011.37213.433.359944142642040.54211.37713.483.359944042522040.54421.38213.533.359944042502030.54631.38813.593.359943942342030.54831.39313.643.369843742192020.55041.39813.693.36984384218202 | 0.5276 | 1.340 | 13.12 | 3.34 | 100 | 443 | 4299 | 206 |
| 0.53391.35613.283.349944342872050.53601.36113.333.349944242792050.53801.36713.383.359944142692040.54011.37213.433.359944142642040.54211.37713.483.359944042522040.54421.38213.533.359944042502030.54631.38813.593.359943942342030.54831.39313.643.369843742192020.55041.39813.693.36984384218202 | 0.5297 | 1.345 | 13.17 | 3.34 | 100 | 443 | 4299 | 206 |
| 0.53601.36113.333.349944242792050.53801.36713.383.359944142692040.54011.37213.433.359944142642040.54211.37713.483.359944042522040.54421.38213.533.359944042502030.54631.38813.593.359943942342030.54831.39313.643.369843742192020.55041.39813.693.36984384218202 | 0.5318 | 1.351 | 13.23 | 3.34 | 100 | 443 | 4295 | 206 |
| 0.53801.36713.383.359944142692040.54011.37213.433.359944142642040.54211.37713.483.359944042522040.54421.38213.533.359944042502030.54631.38813.593.359943942342030.54831.39313.643.369843742192020.55041.39813.693.36984384218202 | 0.5339 | 1.356 | 13.28 | 3.34 | 99 | 443 | 4287 | 205 |
| 0.54011.37213.433.359944142642040.54211.37713.483.359944042522040.54421.38213.533.359944042502030.54631.38813.593.359943942342030.54831.39313.643.369843742192020.55041.39813.693.36984384218202 | 0.5360 | 1.361 | 13.33 | 3.34 | 99 | 442 | 4279 | 205 |
| 0.54211.37713.483.359944042522040.54421.38213.533.359944042502030.54631.38813.593.359943942342030.54831.39313.643.369843742192020.55041.39813.693.36984384218202 | 0.5380 | 1.367 | 13.38 | 3.35 | 99 | 441 | 4269 | 204 |
| 0.54421.38213.533.359944042502030.54631.38813.593.359943942342030.54831.39313.643.369843742192020.55041.39813.693.36984384218202 | 0.5401 | 1.372 | 13.43 | 3.35 | 99 | 441 | 4264 | 204 |
| 0.54631.38813.593.359943942342030.54831.39313.643.369843742192020.55041.39813.693.36984384218202 | 0.5421 | 1.377 | 13.48 | 3.35 | 99 | 440 | 4252 | 204 |
| 0.54831.39313.643.369843742192020.55041.39813.693.36984384218202 | 0.5442 | 1.382 | 13.53 | 3.35 | 99 | 440 | 4250 | 203 |
| 0.5504 1.398 13.69 3.36 98 438 4218 202 | 0.5463 | 1.388 | 13.59 | 3.35 | 99 | 439 | 4234 | 203 |
| | 0.5483 | 1.393 | 13.64 | 3.36 | 98 | 437 | 4219 | 202 |
| | 0.5504 | 1.398 | 13.69 | 3.36 | 98 | 438 | 4218 | 202 |
| 0.5526 1.404 13.74 3.36 98 436 4204 201 | 0.5526 | 1.404 | 13.74 | 3.36 | 98 | 436 | 4204 | 201 |

CLIENT JOB NO. PROJECT PROJECT NO. LOCATION DATE TESTED TECHNICIAN Wiss Janney Elstner 3020-012 Persigo WWTP --Grand Junction CO 09/24/19 CAL

| 6 |
|----|
| |
| |
| |
| ər |
| |

| Displacement (in) | Displacement (cm) | Strain (%) | Average Cross Sectional Area (in ²) | Load (lbs) | Load (N) | Stress (psf) | Stress (kPa) |
|-------------------|-------------------|------------|--|------------|----------|--------------|--------------|
| 0.5549 | 1.409 | 13.80 | 3.36 | 98 | 435 | 4191 | 201 |
| 0.5570 | 1.415 | 13.85 | 3.36 | 98 | 434 | 4176 | 200 |
| 0.5591 | 1.420 | 13.90 | 3.37 | 97 | 433 | 4161 | 199 |
| 0.5611 | 1.425 | 13.95 | 3.37 | 97 | 431 | 4146 | 199 |
| 0.5632 | 1.431 | 14.01 | 3.37 | 97 | 430 | 4126 | 198 |
| 0.5652 | 1.436 | 14.06 | 3.37 | 96 | 429 | 4116 | 197 |
| 0.5672 | 1.441 | 14.11 | 3.37 | 96 | 427 | 4096 | 196 |
| 0.5693 | 1.446 | 14.16 | 3.38 | 96 | 426 | 4086 | 196 |
| 0.5713 | 1.451 | 14.21 | 3.38 | 96 | 425 | 4072 | 195 |
| 0.5738 | 1.457 | 14.27 | 3.38 | 95 | 422 | 4039 | 193 |
| 0.5759 | 1.463 | 14.32 | 3.38 | 95 | 421 | 4024 | 193 |
| 0.5780 | 1.468 | 14.37 | 3.38 | 94 | 418 | 3999 | 191 |
| 0.5802 | 1.474 | 14.43 | 3.39 | 94 | 417 | 3988 | 191 |
| 0.5824 | 1.479 | 14.48 | 3.39 | 94 | 416 | 3977 | 190 |
| 0.5844 | 1.484 | 14.53 | 3.39 | 93 | 413 | 3946 | 189 |
| 0.5865 | 1.490 | 14.59 | 3.39 | 93 | 413 | 3940 | 189 |
| 0.5889 | 1.496 | 14.65 | 3.40 | 92 | 411 | 3917 | 188 |
| 0.5910 | 1.501 | 14.70 | 3.40 | 92 | 409 | 3895 | 187 |
| 0.5932 | 1.507 | 14.75 | 3.40 | 91 | 407 | 3872 | 185 |
| 0.5956 | 1.513 | 14.81 | 3.40 | 91 | 405 | 3850 | 184 |
| 0.5977 | 1.518 | 14.86 | 3.40 | 90 | 402 | 3822 | 183 |
| 0.5999 | 1.524 | 14.92 | 3.41 | 90 | 399 | 3791 | 181 |
| 0.6020 | 1.529 | 14.97 | 3.41 | 89 | 398 | 3778 | 181 |