Geotechnical Investigation Report F 1/2 Road Parkway and 24 1/2 Road Widening City of Grand Junction, Colorado RockSol Project No. 599.37 August 2, 2023



Prepared for:

City of Grand Junction Public Works Department 333 West Avenue, Building D Grand Junction, Colorado 81501

Attention: Brendan Hines, P.E., Project Engineer

Prepared by:



RockSol Consulting Group, Inc. 566 W Crete Circle, Unit 2 Grand Junction, Colorado 81505 (970) 822-4350

Geotechnical Investigation Report F 1/2 Road Parkway and 24 1/2 Road Widening City of Grand Junction, Colorado RockSol Project No. 599.37 August 2, 2023

Prepared for:

City of Grand Junction

Public Works Department 333 West Avenue, Building D Grand Junction, Colorado 81501

Attention: Brendan Hines, P.E., Project Engineer

Prepared by:



RockSol Consulting Group, Inc.

566 W Crete Circle, Unit 2 Grand Junction, Colorado 81505 (970) 822-4350

Madison Philips

Madison Philips, E.I.T.

Civil Engineering Associate

Jay Goldbaum, P.E. Senior Pavement Engineer

Donald G. Hunt, P.E. Senior Geotechnical Engineer



Table of Contents

1.0	PROJE	ECT OBJECTIVE AND DESCRIPTION	1
2.0	PROJE	ECT SITE CONDITIONS	2
3.0	GEOL	OGICAL CONDITIONS	3
4.0	SUBSU	JRFACE EXPLORATION	3
5.0	SURFA	ACE AND SUBSURFACE CONDITIONS	5
	5.2 F 5.3 N 5.4 S 5.5 O	Existing Asphalt Pavement Sections Fill Material Native Subgrade Soils Sedimentary Bedrock Groundwater	5 6 6 6
6.0		RATORY TESTING	
7.0		RADE CHARACTERIZATION	
8.0	7.2 S 7.3 \	Roadway Subgrade Soil Classification	8
9.0	8.2 F 8.3 F 8.3.1 8.3.2 8.3.3 8.3.4 8.4 S	Traffic Loading Pavement Subgrade Characterization. Pavement Section Recommendations, Flexible ME-Pavement Design Recommendations Rigid ME-Pavement Design Recommendations AASHTO 1993 Flexible Pavement Design AASHTO 1998 Rigid Pavement Design Subgrade Preparation (Prior to Pavement Construction) RETE BOX CULVERT EXTENSION DISCUSSION	12 13 14 15 16
10.0	EARTH	HWORK2	20
11.0	SEISM	IICITY DISCUSSION2	21
12.0	11.1 11.2 OTHE	General	21
13.0	LIMITA	ATIONS2	23
ATTAC	CHMEN	TS	
Figure Figure Figure Figure Figure	2: 3: 4:	F ½ Road Parkway Conceptual Layout (24 Road to 24 ½ Road) F ½ Road Parkway Conceptual Layout (24 ½ Road to 25 Road) F ½ Road Parkway Conceptual Layout (25 Road, F ½ Road to F/Patterson Roa F ½ Road Parkway Conceptual Layout (25 Road, Buchanan Drive to F ½ Road) F ½ Road Parkway Conceptual Layout (24 ½ Road from Brookwillow Loop to Tennis Courts)	



APPENDICIES

Appendix A: Legend and Individual Borehole Logs Appendix B: Summary of Laboratory Test Results

Appendix C: 20 and 30-Year Flexible ME-Pavement Design Output Sheets (F ½ Road)

Appendix C1: Rigid ME-Pavement Design Output Sheets (F ½ Road)

Appendix D: 20 and 30-Year Flexible ME-Pavement Design Output Sheets (24 ½ Road)

Appendix D1: Rigid ME-Pavement Design Output Sheets (24 ½ Road)

Appendix E: 20 and 30-Year Flexible ME-Pavement Design Output Sheets (24 ½ Road & F ½ Road Roundabout)

Appendix E1: Rigid ME-Pavement Design Output Sheets (24 ½ Road & F ½ Road Roundabout)

Appendix F: 20 and 30-Year Flexible ME-Pavement Design Output Sheets (25 Road)

Appendix F1: Rigid ME-Pavement Design Output Sheets (25 Road)

Appendix G: 20 and 30-Year Flexible ME-Pavement Design Output Sheets (25 Road & F ½ Road Intersection)

Appendix G1: Rigid ME-Pavement Design Output Sheets (25 Road & F ½ Road Intersection)

Appendix H: 20 and 30-Year Flexible ME-Pavement Design Output Sheets (Foresight Circle and F 1/4 Roads)

Appendix H1: Rigid ME-Pavement Design Output Sheets (Foresight Circle and F ¼ Roads)

Appendix I: 20 and 30-Year Flexible 1993 AASHTO Pavement Design Output Sheets (F ½ Road)

Appendix I1: Rigid 1998 AASHTO Pavement Design Output Sheets (F ½ Road)

Appendix J: 20 and 30-Year Flexible 1993 AASHTO Pavement Design Output Sheets (24 ½ Road)

Appendix J1: Rigid 1998 AASHTO Pavement Design Output Sheets (24 ½ Road)

Appendix K: 20 and 30-Year Flexible 1993 AASHTO Pavement Design Output Sheets (24 ½ Road & F ½ Road Roundabout)

Appendix K1: Rigid 1998 AASHTO Pavement Design Output Sheets (24 ½ Road & F ½ Road Roundabout)

Appendix L: 20 and 30-Year Flexible 1993 AASHTO Pavement Design Output Sheets (25 Road)

Appendix L1: Rigid 1998 AASHTO Pavement Design Output Sheets (25 Road)

Appendix M: 20 and 30-Year Flexible 1993 AASHTO Pavement Design Output Sheets (25 Road & F ½ Road Intersection)

Appendix M1: Rigid 1998 AASHTO Pavement Design Output Sheets (25 Road & F ½ Road Intersection)

Appendix N: 20 and 30-Year Flexible 1993 AASHTO Pavement Design Output Sheets (Foresight Circle and F 1/4 Roads)

Appendix N1: Rigid 1998 AASHTO Pavement Design Output Sheets (Foresight Circle and F 1/4 Roads)

i

Appendix O: Record Drawing CBC Structure (From Value Place Hotel Plan Set)

Appendix P: Slope Stability Models at NW Wall



1.0 PROJECT OBJECTIVE AND DESCRIPTION

This report documents the geotechnical engineering investigation performed by RockSol Consulting Group, Inc. (RockSol) for the F 1/2 Road Parkway and 24 1/2 Road Widening Project in the City of Grand Junction, Colorado (see Image 1, *Site Vicinity Map*).



Image 1 – Site Vicinity Map (Google Earth)

This project focuses on the design and construction of two sites for the City of Grand Junction. Site 1 includes new construction for F $\frac{1}{2}$ Road Parkway connecting 24 Road and 25 Road, as well as major improvements of existing adjacent roads/driveways, a new roundabout at the 24 $\frac{1}{2}$ Intersection, and a new realignment of the F $\frac{1}{2}$ Road and 25 Road intersection. F $\frac{1}{2}$ Road Parkway and 25 Road will be 4-lane roads with turn lanes and a center median.

In addition to the new parkway, major improvements will be made to 25 Road beginning at the intersection with F Road/Patterson Road, up to the intersection with Blichmann Avenue. North of Blichmann Avenue, 25 Road will be accessed by a new intersection off the diagonal portion of the parkway adjacent to the Heritage Heights development. In addition to the parkway and 25 Road work, improvements will be made to 25 Road north of F $\frac{1}{2}$ Road, as well as to F $\frac{1}{2}$ Road east of 25 Road.



Improvements are planned for F ¼ Road, Zenith Lane, and Flat Top Lane, which will continue east and connect with 25 Road. Lastly, the western leg of Foresight Circle will be modified at the connection to 25 Road.

Included in the new parkway construction will be an extension of the existing box culvert to the north that carries Leach Creek water under F ½ Road to accommodate the Parkway Widening.

Site 2 consists of widening and reconstruction of 24 $\frac{1}{2}$ Road, from F 3/8 Road north to Jack Creek Road (Canyon View Park), approximately 1.5 miles. Construction will include minor widening of the existing two lanes to incorporate a center turn lane, shoulder widening, and sidewalks to accommodate pedestrian and bike traffic. This construction will be completed in a separate project, but the City of Grand Junction would like to complete the Geotechnical Work at the same time as F $\frac{1}{2}$ Parkway.

The geotechnical investigation was conducted by RockSol for the City of Grand Junction. The scope of work for this geotechnical investigation included:

- Preparing a drilling/sampling program to perform a subsurface investigation and implementing the program to collect soil samples for laboratory testing.
- Performing laboratory tests and analyzing the data.
- Preparing a report that presents the field and laboratory data obtained, geological setting and conditions, geotechnical design parameters for the proposed structures, project site improvements, and roadway pavement thickness recommendations.

Surface and groundwater hydrology, hydraulic engineering, and environmental evaluation of site soils and groundwater for possible contaminant characterization were not included in RockSol's geotechnical scope of work.

Unless otherwise specified, all recommendations presented in this report are based on the Colorado Department of Transportation (CDOT) 2021 Standard Specifications for Road and Bridge Construction; the City of Grand Junction Standard Specifications for Road and Bridge Construction; and the City of Grand Junction Transportation Engineering Design Standards.

2.0 PROJECT SITE CONDITIONS

A combination of farm, commercial, residential, and undeveloped land immediately surrounds the project limits. The Colorado River is located approximately 0.5 miles southwest of the project site.

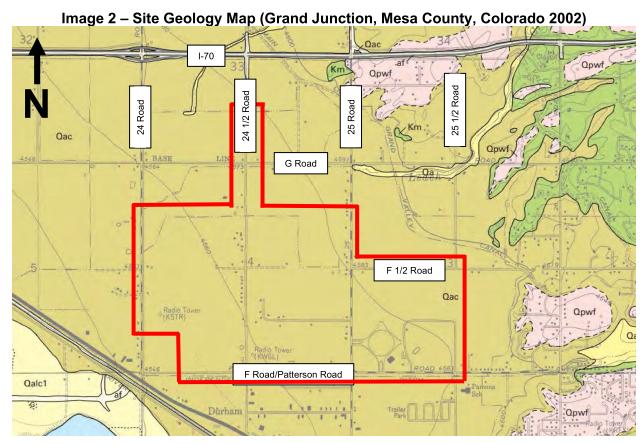
Currently, 24 $\frac{1}{2}$ Road consists of one travel lane in each direction within Site 2 project limits. 25 Road currently consists of two lanes, one in each direction and a center turn lane within the project vicinity. F $\frac{1}{2}$ Road consists of one travel lane in each direction with a center turn lane. The existing lanes are approximately 12 feet wide and surfaced with asphalt pavement throughout the project vicinity.

Topography throughout the project limits consist of nearly flat slopes in all directions. Within the project vicinity, Main Line Grand Valley Canal crosses 25 ½ Road between G road and F ½ Road, and North Leach Creek runs along the south side of G Road and then along the east side of 24 Road.



3.0 GEOLOGICAL CONDITIONS

Based on information presented in the United States Geological Survey (USGS) Geologic Map (See Image 2, *Site Geology Map*) of the Grand Junction Quadrangle, Mesa County, Colorado, by Roger B. Scott, Paul E. Carrara, William C. Hood, and Kyle E. Murray, dated 2002, alluvium and colluvium, undivided, (Holocene and late Pleistocene) (Qac) is mapped at the project site, as well as at the immediate surrounding areas. Alluvium generally consists of silt, sand and gravel and the colluvium generally consists of sandy silt, silty to clayey sand, and sandy clay. The materials identified by the USGS mapping were consistent with native soils encountered during our geotechnical investigation. Mancos Shale bedrock (Km) is mapped at or near the surface in two locations northeast of the project site. This correlates with the Claystone/shale bedrock identified at the bottom of Boreholes LC-2 and LC-3.



4.0 SUBSURFACE EXPLORATION

For this investigation, RockSol completed a total of 25 boreholes identified as B-1 through B-6, F-1 through F-16, and LC-1 through LC-3. (See Figures 1 through 5).

Boreholes F-1 through F-16 were drilled for the purpose of improvements, modifications, and new alignments within Site 1, including the design of the new F $\frac{1}{2}$ Road connecting 24 Road and 25 Road. Boreholes B-1 through B-6 were drilled along 24 $\frac{1}{2}$ Road for the purpose of rehabilitation and road widening within Site 2 (See Figures 1 through 4). Boreholes LC-1 through LC-3 were drilled at the intersection of 24 Road and F $\frac{1}{2}$ Road (See Figure 1). To assist with development of pavement thickness and structure foundation recommendations, "B" and "F" boreholes extended to approximate depths of 5 feet to 10 feet and "LC" boreholes extended to approximate



depths of 20 feet to 40 feet for characterization of subsurface conditions, including depths to bedrock and groundwater.

The locations of the geotechnical investigation boreholes are summarized below in Table 1. The boreholes were drilled between October 4, 2021, and October 20, 2021.

Table 1 – Borehole and Pavement Core Location Summary

Borehole ID	Borehole Location
B-1	24 ½ Road, at Tennis Court, southbound lane
B-2	24 ½ Road, just west of 6 Road, southbound lane
B-3	24 ½ Road, just south of roundabout, northbound lane
B-4	675 24 ½ Road, southbound shoulder
B-5	24 ½ Road, just north of Ajay Avenue, northbound lane
B-6	24 ½ Road at F 3/8 Road intersection, northbound lane
F-1	New F ½ Rd, ~240 feet east of existing F ½ Road and Market Street
F-2	Field along new proposed F ½ Road
F-3	Field near 24 ½ Road and new F ½ Road
F-4	Northeast side of 24 ½ Road and F ½ Road
F-5	24 ½ Road, ~135 feet north of F 3/8 Road
F-6	Southeast side of 24 ½ Road and F ½ Road
F-7	24 ¾ Road and west side of new F ½ Road
F-8	New F ½ Road alignment, vacant land
F-9	East end of proposed F ½ Road, west of 25 Road
F-10	653 25 Road (private property)
F-11	25 Road, front 645 25 Road, northbound lane
F-12	Corner of F 1/2 Road and 25 Road, ~18 feet off 25 Road
F-13	F ¼ Road, westbound lane
F-14	25 Road, ~320 feet south of F ¼ Road
F-15	Foresight Circle, ~250 feet east of 25 Road, eastbound lane
F-16	Field north of 6.5 Climb Gym (new road alignment)
LC-1	Northeast corner of 24 Road and F ½ Road (wingwall)
LC-2	Northeast corner of F ½ Road and 24 Road intersection
LC-3	Southeast corner of F ½ Road and 24 Road intersection

Boreholes were advanced with a truck mounted Simco 2800 drill rig using 4.25-inch outside diameter solid stem auger. The boreholes were logged in the field by a representative of RockSol with the depth to groundwater, if encountered, noted at the time of drilling. The boreholes were backfilled at the completion of drilling and groundwater level checks and patched with surface asphalt patch mix when drilled within existing pavement.

Subsurface materials were sampled and resistance of the soil to penetration of the sampler was performed using modified California barrel and standard split spoon samplers. Penetration Tests were performed using an automatic lift system and a hammer weighing 140 pounds falling 30 inches. The modified California barrel sampler has an outside diameter of approximately 2.5 inches and an inside diameter of 2 inches. The standard split spoon sampler used had an outside diameter of 2 inches and an inside diameter of 1%-inches. Brass tube liners were used with the



modified California barrel sampler. Brass tube liners are not used with the standard split spoon sampler.

The standard split spoon sampling method is the Standard Penetration Test (SPT) described by ASTM Method D-1586.

The modified California Barrel sampling method is similar to the SPT test with the difference being the sampler dimensions and the number of 6-inch intervals driven with the hammer per ASTM D-3550. It is RockSol's experience that blow counts obtained with the modified California sampler tend to be slightly greater than a standard split spoon sampler.

The boreholes were logged in general accordance with ASTM D-2488. Penetration resistance values (blow counts) were recorded for each sampling event. Blow counts, when properly evaluated, indicate the relative density or consistency of the soils. Depths at which the samples were taken, the type of sampler used, and the blow counts that were obtained are shown on the Borehole Logs (See Appendix A).

5.0 SURFACE AND SUBSURFACE CONDITIONS

The surface and subsurface materials encountered by RockSol at our borehole locations included asphaltic pavement, road base (aggregate base course/pit run material), topsoil, fill material, native soils, and sedimentary bedrock. A brief description of the materials encountered is presented below.

5.1 Existing Asphalt Pavement Sections

Asphalt pavement was encountered in Boreholes B-1, B-3, B-5, B-6, F-5, F-11, and F-13 through F-15. Asphalt pavement ranged in thickness from 2 to 7 inches and was underlain by 4 to 12 inches of aggregate base course (ABC). A summary of existing pavement section thickness encountered at each borehole location is presented in Table 2. Existing pavement section thicknesses are also shown on the individual borehole logs found in Appendix A.

Table 2 – Existing Pavement Sections

Borehole ID	HMA Pavement Thickness (in)	ABC Thickness (in)
B-1	6.0	11.0
B-3	5.0	12.0
B-5	7.0	11.0
B-6	5.0	11.0
F-5	6.0	6.0
F-11	6.0	6.0
F-13	2.0	10.0
F-14	6.0	4.0
F-15	3.0	9.0

HMA = Hot Mix Asphalt; ABC = Aggregate Base Course

5.2 Fill Material

Fill material was encountered in Boreholes B-6, F-5, F-11, F-14, and F-15 and extended to depths ranging from 2 feet to 4 feet below existing grades. Fill material generally consisted of a rocky and gravelly sand mixture and is locally described as pit-run material.



5.3 Native Subgrade Soils

Native soils were encountered at the ground surface of Boreholes B-2, B-4, F-1 through F-4, F-6 through F-10, F-12, F-16, and LC-1 through LC-3, and below existing pavement and fill materials at all other borehole locations. Native soils extended to maximum depths drilled at the borehole locations, except for Borehole LC-3. Native soils encountered generally consisted of very soft to very stiff, moist to wet, brown, sandy to silty clay to clay with sand or gravel. At Borehole LC-2, a medium stiff to very hard, brown to gray, very moist, sand with silt and gravel was encountered below the sandy clay layer, and at Borehole LC-3, a native sandy gravel was located at the ground surface. The native soils encountered by RockSol are generally consistent with the alluvium and colluvium materials identified on the USGS Geological Map (See Image 2) found in Section 3.0 of this report.

5.4 Sedimentary Bedrock

Claystone/shale bedrock was encountered in Boreholes LC-2 and LC-3 at depths of approximately 37 feet and 40 feet, respectively, below existing grades. Claystone/Shale was identified in the field as slightly moist, gray, and medium stiff to very hard, and is consistent with the Mancos Shale Formation mapped near the project site on the USGS Geological Map (Image 2). Bedrock was not encountered to the depth drilled at any other borehole locations for this project.

5.5 Groundwater

Groundwater was encountered during drilling/sampling activities at borehole locations B-2 and LC-1 through LC-3 at approximate depths ranging from 7 feet to 10 feet below existing grades at the time of drilling operations. Additionally, piezometers were installed in Boreholes LC-2 and LC-3 for continued groundwater monitoring. Depth to groundwater where encountered is recorded in Table 3, *Approximate Depths to Groundwater* and presented on individual borehole logs in Appendix A. Depth to sedimentary bedrock, if encountered is included in Table 3.

Table 3 – Approximate Depths to Groundwater

Borehole I.D.	Depth to Bedrock (feet)	Depth to Groundwater at time of drilling, (feet)	Depth to Groundwater 11/1/2021, (feet)	Depth to Groundwater 11/30/2021, (feet)	Depth to Groundwater 12/30/2021, (feet)
B-2	-	7.0	-	-	-
LC-1	-	7.0	-	-	-
LC-2	37.0	7.0	5.1	4.8	7.0
LC-3	40.0	10.0	10.3	10.6	10.0

Depth to groundwater is subject to change depending on climatic conditions, water flows in North Leach Creek and Main Line Grand Valley Canal, local irrigation practices, changes in local topography, and changes in surface storm water management. Long-term monitoring of groundwater elevations is required to establish groundwater fluctuations.



6.0 LABORATORY TESTING

Soil samples retrieved from the borehole locations were examined by the project geotechnical engineer in the RockSol laboratory. Selected samples were tested and classified per the Unified Soil Classification System (USCS). The following laboratory tests were performed in accordance with the American Society for Testing and Materials (ASTM), American Association of State Highway and Transportation Officials (AASHTO), and current local practices:

- Natural Moisture Content (ASTM D-2216)
- Percent Passing No. 200 Sieve (ASTM D-1140)
- Liquid and Plastic Limits (ASTM D-4318)
- Dry Density (ASTM D-2937)
- Gradation (ASTM D 6913)
- Water-Soluble Sulfates (CDOT CP-L 2103)
- Water-Soluble Chloride Content (CDOT CP-L 2104)
- Standard Test Method for pH of Soils (ASTM D4972-01)
- Soil Resistivity (ASTM G187 Soil Box)
- Soil Classification (ASTM D-2487 and AASHTO M145)
- Swell Test (Denver Swell Test, modified from ASTM D-4546)
- Resistance Value (AASHTO T-190)

R-Values (Resistance Values) were tested by Cesare, Inc. and water-soluble chlorides were tested by Colorado Analytical Laboratories. All other laboratory tests were performed by RockSol. Laboratory test results are presented in Appendix B and are also summarized on the Borehole Logs presented in Appendix A.

7.0 SUBGRADE CHARACTERIZATION

Laboratory test results were used to characterize the engineering properties of the subsurface material encountered. For soil classification, RockSol conducted sieve analyses and Atterberg Limits tests. Swell tests were used to determine the swell or consolidation characteristics of the subsurface materials. Lab testing was also performed on selected samples to determine the water-soluble sulfate content of subsurface materials to assist with cement type recommendations. A summary of physical and chemical test results is included in Appendix B.

7.1 Roadway Subgrade Soil Classification

Subgrade bulk samples of existing roadway grades were obtained at various depths from each pavement borehole location and were tested for AASHTO soil classification. The subgrade soils tested generally varied between A-4 and A-6 AASHTO soil types. A summary of the roadway subgrade soil classifications is presented in Table 4 and summarized by group index in Table 5.



Table 4 – Roadway Subgrade Soil Classifications

Borehole Location	Depth (feet)	AASHTO Classification
B-1	2-10	A-6 (9)
B-2	0-7	A-6 (7)
B-3	2-9	A-6 (8)
B-5	3-10	A-6 (16)
B-6	4-10	A-4 (0)
F-1	0-5	A-6 (17)
F-2	0-6	A-6 (17)
F-3	0-4	A-6 (13)
F-4	0-5	A-6 (10)
F-5	2-10	A-6 (8)
F-6	0-7	A-6 (10)
F-7	0-5	A-6 (8)
F-8	0-5	A-4 (3)
F-9	0-3	A-6 (13)
F-10	0-5	A-4 (7)
F-16	0-10	A-6 (8)
LC-1	0-5	A-6 (7)
LC-2	0-5	A-4 (4)
LC-3	2-4	A-6 (7)

Table 5 – Soil Classifications by Group Index Range

AASHTO Soil Type	Group Index Range	Number of Tests
A-4	0 – 7	4
A-6	7 – 10	10
A-6	11 – 17	6

7.2 Swell/Consolidation Potential of Subgrade Soils

Based on swell test results and plasticity index (PI) testing, the subgrade soils encountered within the upper 3 to 10 feet of the pavement surface exhibit low consolidation potential and no swell potential (-1.7 percent consolidation to 0.0 percent swell under 500 pounds per square foot (psf) surcharge pressure).

Based on the swell test results and subgrade soil classifications obtained, special mitigation methods for expansive soil are not deemed necessary for new pavement construction or for the proposed improvements planned for this project.

However, based on consolidation and penetration data obtained from the boreholes drilled, special mitigation is recommended for design and construction of shallow foundation systems being considered (See Section 9) due to settlement potential and constructability. Mitigation may consist of over excavation and replacement with coarse, granular material with geosynthetic fabrics and geogrids to help stabilize shallow foundation soils.

7.3 Water-Soluble Sulfate Content

Cementitious material requirements for concrete in contact with soils or groundwater are based on the percentage of water-soluble sulfate. Mix design requirements for concrete exposed to water-soluble sulfates in soils or water is considered by the Colorado Department of Transportation (CDOT) as shown in Table 6 and in the CDOT Standard Specifications for Road and Bridge Construction, dated 2022. Water-soluble Sulfate Testing Results are summarized in Table 7.



Table 6: Concrete Sulfate Exposure Class

Water-Soluble Sulfate (SO ₄) in Dry Soil, (%)	Sulfate (SO₄) In Water, ppm	Cementitious Material Requirements
0.00 to 0.10	0 to 150	Class 0
0.11 to 0.20	151 to 1,500	Class 1
0.21 to 2.0	1,500 to 10,000	Class 2
2.01 or greater	10,001 or greater	Class 3

Table 7 – Water-Soluble Sulfate Testing Summary

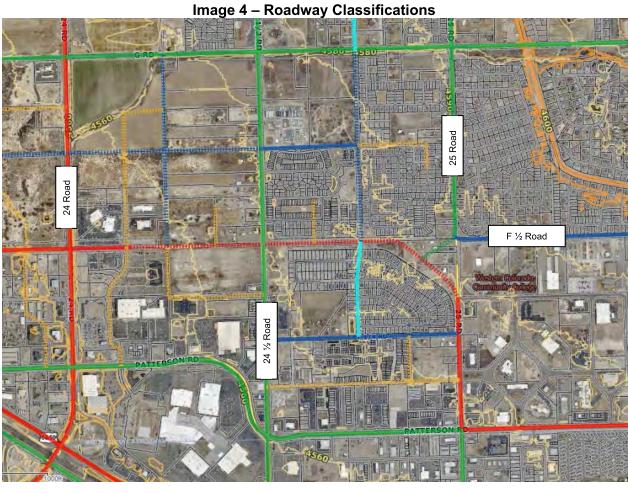
Borehole I.D.	Sample Depth (Feet)	Water-Soluble Sulfate (SO ₄) in dry soil, percent	Cementitious Material Requirements
F-1	0-5	0.38	Class 2
F-4	0-5	0.16	Class 1
F-5	2-10	0.26	Class 2
F-8	0-5	0.28	Class 2
F-10	0-5	1.04	Class 2
F-16	0-10	0.14	Class 1
LC-1	0-5	0.51	Class 2
LC-2	20	0.47	Class 2
LC-3	20	0.19	Class 1
LC-3	30	0.15	Class 1

The concentration of water-soluble sulfates measured in soil samples obtained from RockSol's exploratory boreholes ranged from 0.14 percent to 1.04 percent by weight. Based on the results of the water-soluble sulfate testing, **Class 2** cementitious material mix design requirements for concrete exposed to water soluble sulfates in soils is recommended. Refer to CDOT's current *Standard Specifications for Road and Bridge Construction Section 601* for concrete mixtures that satisfy appropriate sulfate exposure *Class* requirements.



8.0 PAVEMENT DESIGN RECOMMENDATIONS

24 Road and F ½ Road are classified as principal arterials, 24 ½ Road and F Road/Patterson Road are classified as minor arterials. All other roadways applicable to Sites 1 and 2 are classified as minor collector or unclassified roadways by the City of Grand Junction. The roadway classification for this project were found on the website for the City of Grand Junction's Transportation Map as shown in Image 4.



- Interstate 70
- III Interstate 70 Proposed
- Principal Arterial
- III Principal Arterial Proposed
- Minor Arterial
- III Minor Arterial Proposed

- Major Collector
- III Major Collector Proposed
- Minor Collector
- Minor Collector Proposed
- **III** Unclassified



New pavement is planned for the New F $\frac{1}{2}$ Road connecting 24 Road and 25 Road, as well as the reconstruction of 24 $\frac{1}{2}$ Road from F $\frac{3}{8}$ Road to Jack Creek, and a new F $\frac{1}{2}$ Road and 24 $\frac{1}{2}$ Road roundabout. New pavement is also planned for 25 Road and the new 25 Road and F $\frac{1}{2}$ Road intersection, as well as for the reconstruction of Foresight Circle and F $\frac{1}{2}$ Road. In this report Hot Mix Asphalt (HMA) pavement is identified as flexible pavement. Portland Cement Concrete (PCC) pavement is identified as rigid pavement.

Pavement thickness evaluation for the development of flexible and rigid pavement design recommendations within the City of Grand Junction right of way were performed in accordance with CDOT's 2021 M-E Pavement Design Manual as modified in 2022 which uses Version 2.3.1 of AASHTO's Pavement Mechanistic-Empirical Design (PMED) software, *Subsection 29.32 – Pavements and Truck Routes* in the City of Grand Junction Municipal Code as passed in Ordinance 5136 on March 15, 2023, and a spreadsheet developed by RockSol to replicate the 1993 AASHTO flexible pavement design as recommended in 29.32.040(a).

The correlation of subgrade soil R-Value to Resilient Modulus for this report was performed using equation 4-1 from CDOT's 2021 Mechanistic-Empirical Pavement Design Manual.

8.1 Traffic Loading

Traffic loading was estimated for a 30-year flexible pavement design life and 30-year rigid pavement design life in accordance with the City of Grand Junction Municipal Code (Subsection 29.32.030). RockSol included the estimated traffic loading for a 20-year flexible pavement design life since it is recommended in CDOT's Pavement Design Manual for reconstruction using flexible pavement. The current average daily traffic (ADT) for 24 ½ Road was supplied to RockSol by the Transportation Engineer from the City of Grand Junction. The ADT for 24 Road and 25 Road were obtained from the traffic counts found on the website for the City of Grand Junction's Transportation Map. The ADT for F ½ Road was estimated to be 16,000 by the City of Grand Junction. Since this project will close the gap between 24 and 25 Roads, it was estimated by the Transportation Engineer for the City of Grand Junction that 24 ½ Road, Foresight Circle and F ¼ Roads, as well as the 24 ½ Road and F ½ Road roundabout within this area will have an increase of approximately 10 percent above the current ADT. The Average Annual Daily Truck Traffic (AADTT) has a significant effect on the predicted pavement performance as compared to cars and pick-up trucks. For this project, predominately Class 5 vehicles when using the Federal Highway vehicle type classification system were noted on 24 ½ Road. Based on the ADT from 24 ½ Road, an average of 12.9 percent trucks will be used for this project. The AADTT used for the pavement designs of roadway segments is shown in Table 9. A compound growth rate of 2.2 percent over a 20-year and 30-year design life was used to develop the 18,000-pound equivalent single axle loads (ESAL's) from the PMED calculated value. Based on CDOT's Pavement Design Manual, Cluster 1 truck percentages will be used to model the truck traffic in the PMED software. Traffic data and projections are summarized in Table 9.



Table 9 – Summary of Traffic Load	dina	l oa		ffic	Traff	of '	ımarv	- Sun	9	Table	
-----------------------------------	------	------	--	------	-------	------	-------	-------	---	-------	--

Pavement Section	Estimated Truck Traffic	20-Year Flexible Design Life 18k ESALS	30-Year Flexible Design Life 18k ESALS	30-Year Rigid Design Life 18k ESALs
F 1/2 Road (Site 1)	2,100	5,510,000	9,300,000	12,020,000
24 1/2 Road (Site 2)	1,078	3,770,000	6,360,000	8,230,000
24 ½ Road & F ½ Road Roundabout (Site 1)	3,178	8,330,000	14,070,000	18,190,000
25 Road (Site 1)	850	2,970,000	5,020,000	6,490,000
25 Road & F ½ Road Intersection (Site 1)	2,950	7,730,000	13,060,000	16,890,000
Foresight Circle & F 1/4 Road (Site 1)	231	810,000	1,360,000	1,760,000

8.2 Pavement Subgrade Characterization

Subgrade bulk samples within the upper 5 to 10 feet of existing roadway grades were obtained at each borehole location and were tested for AASHTO soil classification. The subgrade soils tested were AASHTO classified as A-1-a, A-4, and A-6 soil types (See Sections 5.2 and 5.3).

Based on R-Value testing, a conservative R-Value of 5 with a corresponding subgrade resilient modulus value of 5,356 psi was used by RockSol as the design R-value for evaluation of new pavement constructed on the existing soils at 24 $\frac{1}{2}$ Road, F $\frac{1}{2}$ Road, and F $\frac{1}{2}$ Road, and Foresight Circle.

An R-Value of 10 with a corresponding subgrade resilient modulus value of 6,482 psi was used by RockSol as the design R-value for evaluation of new pavement constructed on the existing soils at 25 Road, and the F $\frac{1}{2}$ Road and 25 Road intersection.

To provide an appropriate structural layer for Hot Mix Asphalt (HMA), RockSol recommends 12 inches of a subbase layer of non-stabilized A-1-b Pit Run (Class 3) material be included as part of the pavement design section in addition to 8 inches of Aggregate Base Course (ABC) directly underlying the pavement. A structural coefficient of 0.12 was used for Class 6 Aggregate Base Course (ABC), 0.11 for Class 3 ABC, and 0.44 for HMA. The Class 3 material must have an R-Value of at least 40 and the Class 6 material must have an R-Value of at least 78 when tested in accordance with AASHTO T 190.

8.3 Pavement Section Recommendations,

Three pavement thickness design procedures were developed for new flexible and rigid pavement. The first procedure used for flexible and rigid pavement design was performed in accordance with the 2021 Colorado Department of Transportation M-E Pavement Design Manual as modified in 2022 and the PMED software, Version 2.3.1. The second procedure used a spreadsheet developed by RockSol to replicate the 1993 AASHTO flexible pavement design since the AASHTOWare DARWin version 3.1 Pavement Design and Analysis System recommended in subsection 29.32.040(a) of the City of Grand Junction Transportation Engineering Design Standards is no longer available. The third procedure used the 1998 version of the AASHTO Guide for the Design of Pavement Structures for rigid pavement in accordance with subsection 29.32.040 (b) of the City of Grand Junction Transportation Engineering Design Standards. The thicknesses of ABC Class 3 and Class 6 were taken from the typical sections supplied to RockSol by the City of Grand Junction. Class 2 ABC may be used in lieu of Class 3 ABC.



8.3.1 Flexible ME-Pavement Design Recommendations

A summary of the PMED recommended pavement section thicknesses for the 20 and 30-year design life of flexible pavement Site 1 and Site 2 are presented in Table 10 and the pavement design output sheets are included in Appendices C through H.

Table 10 - PMED Flexible Pavement Section Thickness Recommendations

Pavement Section	Material Type HMA SX(100) PG 64-28	20-year Pavement Design Thickness (inches)	30-year Pavement Design Thickness (inches)	Appendix
F ½ Road	HMA SX(100) PG 64-22	5.5	6.5	0
(Site 1)	ABC Class 6	8.0	8.0	С
	ABC Class 2 or 3	14.0	14.0	
	HMA SX(100) PG 64-28	2.0	2.0	
24 ½ Road	HMA SX(100) PG 64-22	5.0	6.0	D
(Site 2)	ABC Class 6	8.0	8.0	D
	ABC Class 2 or 3	10.0	10.0	
24 1/2 Road & F 1/2	HMA SX(100) PG 64-28	2.0	2.0	
Road	HMA SX(100) PG 64-22	8.0	9.0	Е
Roundabout	ABC Class 6	8.0	8.0	<u> </u>
(Site 1)	ABC Class 2 or 3	16.0	16.0	
	SX(100) PG 64-28	2.0	2.0	
25 Road	SX(100) PG 64-22	5.0	6.0	F
(Site 1)	ABC Class 6	8.0	8.0	'
	ABC Class 2 or 3	10.0	10.0	
25 Road & F ½ Road	HMA SX(100) PG 64-28	2.0	2.0	
Intersection	HMA SX(100) PG 64-22	7.0	9.0	G
(Site 1)	ABC Class 6	8.0	8.0	
(Sito 1)	ABC Class 2 or 3	12.0	12.0	
Foresight Circle	HMA SX(75) PG 64-28	2.0	2.0	
and	HMA SX(75) PG 64-22	4.0	5.0	н
F ¼ Road	ABC Class 6	8.0	8.0	''
(Site 1)	ABC Class 2 or 3	12.0	12.0	

HMA = Hot Mix Asphalt; ABC = Aggregate Base Course



8.3.2 Rigid ME-Pavement Design Recommendations

A summary of the PMED recommended pavement section thicknesses for the 30-year design life of rigid pavement Site 1 and Site 2 are presented in Table 11 and the pavement design output sheets are included in Appendices C1 through H1.

Table 11 – PMED Rigid Pavement Section Thickness Recommendations

Pavement Section	Material Type	Thickness (inches)	Appendix
F 1/ Dood	PCC	9.0	
F ½ Road (Site 1)	ABC Class 6	8.0	C1
(Site 1)	ABC Class 2 or 3	12.0	
04.1/ Dood	PCC	9.0	
24 ½ Road (Site 2)	ABC Class 6	8.0	D1
(Site 2)	ABC Class 2 or 3	12.0	
24 1/2 Road & F 1/2	PCC	9.0	
Road	ABC Class 6	8.0	E1
Roundabout (Site 1)	ABC Class 2 or 3	16.0	
OF Dood	PCC	9.0	
25 Road (Site 1)	ABC Class 6	8.0	F1
(Site 1)	ABC Class 2 or 3	12.0	
25 Road & F 1/2 Road	PCC	9.0	
Intersection	ABC Class 6	8.0	G1
(Site 1)	ABC Class 2 or 3	12.0	
Foresight Circle	PCC	8.0	
and	ABC Class 6	8.0	H1
F ¼ Road (Site 1)	ABC Class 2 or 3	12.0	

PCC = Portland Cement Concrete; ABC = Aggregate Base Course



8.3.3 AASHTO 1993 Flexible Pavement Design

A summary of the AASHTO 1993 Pavement Design recommended pavement section thicknesses for the 20 and 30-year design life of flexible pavement Site 1 and Site 2 are presented in Table 12 and the pavement design output sheets are included in Appendices I through N.

Table 12 - AASHTO 1993 Flexible Pavement Section Thickness Recommendations

Pavement Section	Material Type	20-year Pavement Design Thickness (inches)	30-year Pavement Design Thickness (inches)	Appendix	
	HMA SX(100) PG 64-28	2.0	2.0		
F ½ Road	HMA SX(100) PG 64-22	3.0	4.0	1	
(Site 1)	ABC Class 6	8.0	8.0	'	
	ABC Class 2 or 3	14.0	14.0		
	HMA SX(100) PG 64-28	2.0	2.0		
24 ½ Road	HMA SX(100) PG 64-22	3.5	4.0	J	
(Site 2)	ABC Class 6	8.0	8.0	J	
	ABC Class 2 or 3	10.0	10.0		
24 ½ Road & F	HMA SX(100) PG 64-28	2.0	2.0		
½ Road	HMA SX(100) PG 64-22	3.0	5.0	K	
Roundabout	ABC Class 6	8.0	8.0	K	
(Site 1)	ABC Class 2 or 3	16.0	16.0		
	HMA SX(100) PG 64-28	2.0	2.0		
25 Road	HMA SX(100) PG 64-22	2.5	3.0		
(Site 1)	ABC Class 6	8.0	8.0	L	
	ABC Class 2 or 3	10.0	10.0		
25 Road & F ½	HMA SX(100) PG 64-28	2.0	2.0		
Road	HMA SX(100) PG 64-22	3.5	4.0	M	
Intersection	ABC Class 6	0.8	8.0	IVI	
(Site 1)	ABC Class 2 or 3	12.0	12.0		
Foresight Circle	HMA SX(75) PG 64-28	2.0	2.0		
and	HMA SX(75) PG 64-22	1.0	1.5		
F ¼ Road	ABC Class 6	8.0	8.0	N	
(Site 1)	ABC Class 2 or 3	12.0	12.0		

HMA = Hot Mix Asphalt; ABC = Aggregate Base Course



8.3.4 AASHTO 1998 Rigid Pavement Design

A summary of the AASHTO 1998 Pavement Design recommended pavement section thicknesses for the 30-year design life of rigid pavement Site 1 and Site 2 are presented in Table 13 and the pavement design output sheets are included in Appendices I1 through N1.

Table 13 – AASHTO 1998 Rigid Pavement Section Thickness Recommendations

Pavement Section	Material Type	Thickness (inches)	Appendix
F 1/ Dood	PCC	9.5	
F ½ Road (Site 1)	ABC Class 6	8.0	I1
(Oite 1)	ABC Class 2 or 3	12.0	
04.1/ Dood	PCC	8.5	
24 ½ Road (Site 2)	ABC Class 6	8.0	J1
(Site 2)	ABC Class 2 or 3	12.0	
24 1/2 Road & F 1/2	PCC	10.0	
Road	ABC Class 6	8.0	K1
Roundabout (Site 1)	ABC Class 2 or 3	12.0	
OF Dood	PCC	8.5	
25 Road (Site 1)	ABC Class 6	8.0	L1
(Site 1)	ABC Class 2 or 3	10.0	
25 Road & F 1/2 Road	PCC	10.0	
Intersection	ABC Class 6	8.0	M1
(Site 1)	ABC Class 2 or 3	12.0	
Foresight Circle	PCC	7.0 (Note 1)	
and	ABC Class 6	8.0	N1
F ¼ Road (Site 1)	ABC Class 2 or 3	12.0	111

Note 1: Minimum recommended thickness by AASHTO and CDOT is 7.0 inches for rigid pavement design.

RockSol recommends the pavement thicknesses shown in Table 10 for the 20-year design life or Table 11 be used since the PMED software accounts for site specific variables that AASHTO 1993 and 1998 do not. The 20-year design life is recommended since the top layer of most HMA pavements will require rehabilitation within 20 years after construction that should remove the topdown fatigue cracking along with other surface defects and there is no significant difference between the 20 and 30-year design lives for the predicted rutting and bottom-up fatigue cracking. HMA or Rigid pavement shall consist of CDOT-approved mix designs. The bottom layers of HMA should consist of Grading S or SX(100) PG 64-22 for all roads except Foresight Circle and F 1/4 Road. Grading SX(75) PG 64-22 is recommended on Foresight Circle and F 1/4 Road since the 20-year design traffic is less than 3,000,000 18k ESAL's. To resist rutting and thermal cracking damage, the top two inches of HMA should consist of Grading SX(100) PG 64-28 material. Grading SX(75) PG 64-28 is recommended for the top two inches of Foresight Circle and F 1/4 Road. Grading SX(75) may be feasible and the top layer for all roads but will decrease the resistance to rutting. ABC should consist of material meeting CDOT Class 6 Aggregate Base Course and pit run should consist of material meeting CDOT Class 2 or 3 Aggregate Base Course per CDOT 703.03.



8.4 Subgrade Preparation (Prior to Pavement Construction)

Prior to construction of new pavements on subgrade soils, the underlying subgrade should be properly prepared by removal of all organic matter (topsoil), debris, loose material, and any deleterious material identified by the Project Engineer followed by scarification, moisture conditioning and re-compaction. The minimum depth of scarification, moisture conditioning and re-compaction in all cases shall be 6 inches. Based on the results of our field and laboratory tests, A-1-a, A-4, and A-6 soils are anticipated to be encountered at existing pavement subgrade elevations within the project limits.

Materials classified as AASHTO A-1, A-2-4, A-2-5, and A-3 soils shall be compacted at plus or minus 2 percent of Optimum Moisture Content (OMC) and to at least 95 percent of maximum dry density determined in accordance with AASHTO T 180 as modified by CDOT CP 23. All other soil types shall be compacted to 95 percent of the maximum dry density determined in accordance with AASHTO T 99 as modified by CDOT CP 23. Soils with 35 percent fines or less shall be compacted at plus or minus 2 percent of OMC. Soils with greater than 35 percent fines shall be compacted at a moisture content equal to or above OMC to achieve stability of the compacted lift. Stability is defined as the absence of rutting or pumping as observed and documented by the Contractor's Process Control Representative and as approved by the Project Engineer. If the soils cannot be compacted and prove to be unstable at a moisture content equal to or above OMC, then the required moisture content for compaction may be reduced below OMC if approved by the Engineer.

Where areas of unstable, wet subgrade soils are encountered, overexcavation and replacement with Class 3 Aggregate Base Course meeting the following requirements:

Maximum Particle Dimension: 8-inches
Percent passing No. 4 sieve: 20% min.
Minus 200 Screen Size: 20% max.
Plasticity Index (PI): 7 maximum

Prior to pavement section construction, subgrade proof rolling with pneumatic tire equipment shall be performed using a minimum axle load of 18 kips per axle after specified subgrade compaction has been obtained. Areas found to be weak and those areas which exhibit soft spots, non-uniform deflection or excessive deflection as determined by the project engineer shall be ripped, scarified, wetted, or dried if necessary, and re-compacted to the requirements for density and moisture. Complete coverage of the proof roller will be required.



9.0 CONCRETE BOX CULVERT EXTENSION DISCUSSION

As part of this project, the existing three-cell concrete box culvert (CBC) structure that carries Leach Creek water under F ½ Road will be extended to the North to accommodate the parkway widening (See Image 3). RockSol anticipates the CBC extensions will be performed in a phased approach. RockSol understands the extensions will be with precast CBC components.

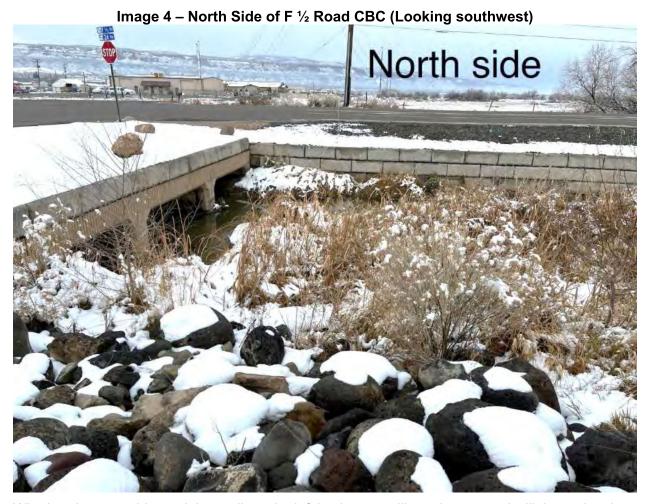


The CBC extensions will require removal of accumulated soil and vegetation and control of the water flow in Leach Creek during construction. Currently, block retaining walls are in place on the north side of the CBC structure, as well as on the south side. The walls on the west side of Leach Creek are roughly parallel with 24 Road for significant distances while the walls on the east side are relatively short in length and constructed as typical wingwalls. The wall blocks appear to be consistent with the "Redi-Rock" type of blocks. Design information and as-built plans of the retaining walls were not available from the City, so the wall backfill type and bottom of wall elevations are not confirmed. Several construction-phase images of the wall construction appear to show some type of granular material was placed behind the retaining wall on the south side of F ½ Road. A plan sheet identified as a "Record Drawing" showing an end view of the existing CBC structure and a typical detail of a RediRock Wall are shown in Appendix O.

The short, existing block retaining wall on the northeast side of the CBC structure will need to be reconstructed as part of the CBC extension. The existing block retaining wall on the northwest



side of the CBC will require consideration as to whether it is left in place or modified to allow the CBC extension. An image of the west wall on the north side of the CBC is shown in Image 4.



Whether the west side retaining wall can be left in place or will require removal will depend on how the CBC will be extended. If a portion of the existing retaining wall is to be removed, RockSol anticipates temporary shoring will be required.

RockSol anticipates soft, yielding subgrade conditions will be encountered within the Leach Creek channel that will require stabilization to allow placement of the CBC extensions and wingwalls. The amount, or degree, of stabilization will depend on whether heavy equipment will need to access the bottom of the Leach Creek channel during construction or if all heavy equipment can stay out of the channel and work from the sides. It will be important that the stabilization of the CBC subgrade soils does not adversely impact, or otherwise destabilize, the existing retaining wall. Modifications to the existing retaining walls will also require continuation of the proper "behind the wall" drainage systems.

At a minimum, RockSol recommends the following subgrade stabilization and subgrade improvements for proper support of the CBC extensions. RockSol recommends ground improvement consisting of overexcavation of subgrade soils to a minimum depth of 5 feet below the bottom of the CBC bottom slab and replacement with at least 2-feet of a Class 3 Aggregate Base Course to provide a stable working platform. Over the Class 3 material, a minimum of 3 feet of crushed aggregate material meeting CDOT No. 57 Concrete Aggregate which is fully



wrapped every 12-inches with a CDOT approved Class 1 stabilization/separator geotextile. The crushed aggregate and geotextile shall extend horizontally beyond the limits of the CBC a minimum of 1 foot in each direction (north/south and east/west). Placement of the aggregate material should be in horizonal lifts with a maximum lift thickness of 6 inches. Compaction of each lift with vibratory methods using lightweight equipment is recommended.

RockSol evaluated three scenarios to illustrate the issues associated with subgrade stabilization for the CBC extension in front of the existing west side retaining wall and removal of a portion of the existing wall to allow CBC extension. Each scenario was modeled with RocScience Slide program. The scenarios are identified as Case 1, Case 2, and Case 3. A summary output of each model is included in Appendix P of this report.

Case 1 was our model which simulates the existing condition of the channel and existing wall. Our model is not intended to be a precise representation of the existing conditions but a reasonable approximation. We created this model to be the basis of Cases 2 and 3. The Factor of Safety (FOS) of Case 1 was 1.48 which indicates a satisfactory FOS. The observed conditions at the existing wall would indicate satisfactory wall performance, suggesting our model is appropriate.

Case 2 was prepared to model a scenario where the existing retaining wall is left in place and a limited subexcavation is performed adjacent to the wall to remove unstable channel soils prior to replacement with suitable materials and construction of the CBC extension. For our model we assumed the subexcavation extended 3.5 feet below the bottom of the blocks placed for the wall. We also assumed the water in the channel was controlled and kept at the bottom of the excavation. In this model a FOS of 0.961 was obtained indicating movement of the wall is likely unless the bottom of the wall is stabilized with some form of temporary, or permanent, shoring. Another consideration if the existing retaining wall is left in place is the compatibility of the edge of the CBC extension with the outside edge of the wall blocks.

Case 3 was prepared to model a scenario where a portion of the existing retaining wall is removed to allow extension of the CBC structure. Our model assumed a cut slope that extended to the same subexcavation elevation noted in Case 2. The cut slope extended to the back of the existing curb and gutter of 24 Road and did not remove any of the existing roadway structure. The cut slope obtained was approximately 1H:1.25V. With traffic loading considered in the roadway the resulting FOS was 0.996, indicating slope movement is likely without temporary, or permanent, shoring or flattening the cut slope. To flatten the cut slope a portion of the existing roadway of 24 Road would need to be removed and a temporary traffic detour condition created.

10.0 EARTHWORK

New Embankment

To accommodate the new F ½ Road and widening of 24 Road, new embankment may be required along the roadway alignments. At some locations minor cuts may be required. Materials used to construct embankments, roadway side slopes, structure backfill, and aggregate base course materials should meet the material and moisture density control requirements specified Section 8.4 of this report.

At a minimum, the ground surface underlying all embankment fills should be carefully prepared by removing all organic matter (topsoil), scarification to a minimum depth of 6 inches and recompacting to the requirements for maximum dry density/compaction and moisture content presented in Section 8.4 of this report prior to fill placement.

Where fill material is to be placed on existing slopes steeper than 4 (H):1 (V), benching must be performed to tie the new fill into the existing slope. Benching into the existing slopes shall allow



sufficient bench width to accommodate placing and compaction equipment to operate in a horizontal orientation.

Broken concrete, broken asphalt, or other solid materials more than 6 inches in greatest dimension shall not be placed within embankment areas supporting the roadway shoulders and pavement structure. Claystone/shale materials shall not be used for construction of new embankment. Imported fill material used for embankment construction shall be compatible with designed side slopes. Material excavated from utility trenches may be used for backfilling provided it does not contain unsuitable material. Unsuitable material includes, but is limited to, topsoil, vegetation, brush, sod, trash, and other deleterious substances.

11.0 SEISMICITY DISCUSSION

11.1 General

The City of Grand Junction uses the 2018 International Building Code (IBC-2018) for development of seismic design parameters. The IBC-2018 references the American Society of Civil Engineers 7-16 (ASCE 7-16) seismic design code. Based on the subsurface conditions encountered, it is our opinion that the subject site meets criteria for Seismic Site Class D. Shear wave velocity testing was not performed by RockSol. Seismic design parameters for Seismic Site Class D are discussed below.

For final design, RockSol recommends performing shear wave velocity testing or performing penetration tests to a depth of 100 feet if determination of Seismic Site Class C conditions is necessary, otherwise Seismic Site Class D may be used for final design. Seismic design parameters for Seismic Site Class D are discussed below.

11.2 Seismic Design Parameters

Seismic design parameters were obtained from the United States Geological Survey (USGS) Earthquake Design Maps using the 2018 International Building Code specifications which reference ASCE 7-16. Values were obtained using the USGS site: https://seismicmaps.org. Since the proposed grandstands are structures, whose primary occupancy is public assembly with an occupant load greater than 300, the grandstands qualify as risk category III per Table 1604.5 of the IBC-2018. Interpolated values for Peak Ground Acceleration Coefficient (PGA), Spectral Acceleration Coefficient at Period 0.2 sec (S_s), and Spectral Acceleration Coefficient at Period 1.0 sec (S_1) were obtained using the latitude and longitude for the site. The seismic acceleration coefficients obtained (data based on 0.05-degree grid spacing) are presented in Table 14.

Table 14 – Seismic Acceleration Coefficients

F 1/2 Road and 24 Road (Latitude°/Longitude°)	Peak Ground Acceleration (PGA)	Spectral Acceleration Coefficient - S _s (Period 0.2 sec)	Spectral Acceleration Coefficient - S ₁ (Period 1.0 sec)
(39° 05' 56.69"/ -108° 36' 29.08")	0.13	0.236	0.065

The acceleration coefficients are then used to obtain Site Factors F_a , and F_v based on the defined Site Class as shown in Tables 1613.2.3(1) and 1613.2.3(2) of the *IBC-2018*. A summary of the Site Factor values obtained are shown in Table 15.



Tahla	15_	Spien	nic	Sita	Factor	Values
Iable	13-	Jeisii	1116	JILE	Iacioi	values

F 1/2 Road and 2/1 Road	F_{pga}	Fa	F _v		
F 1/2 Road and 24 Road (Latitude°/Longitude°) (39° 05' 56.69"/ -108° 36' 29.08")	(at zero-period on	(for short period range of	(for long period range of		
(Editidae /Eorigitade)	acceleration spectrum)	acceleration spectrum)	acceleration spectrum)		
(39° 05' 56.69"/ -108° 36' 29.08")	1.54	1.6	2.4		

Table 16 summarizes the Seismic Zone determination and horizontal response spectral Acceleration Coefficients (S_{D1}) and (S_{DS}) obtained for the proposed structures. Seismic Performance Zone determination is based on the value of the horizontal response spectral Acceleration Coefficient at 1.0 Seconds, S_{D1} , as determined by Eq.~16-39 of the IBC-2018 and the horizontal response spectral Acceleration Coefficient at 0.2 Seconds, S_{DS} , as determined by Eq.~16-38. Values for S_1 and S_2 0 are presented in Tables 14 and 15, shown above. The seismic performance zone was determined S_2 1 S_2 2 S_3 3 S_3 4 S_3 5 S_3 5 S_3 5 S_3 6 S_3 6 S_3 7 S_3 8 S_3 8 S_3 9 S_3

Table 16 - Seismic Performance Zone

F 1/2 Road and 24 Road (Latitude°/Longitude°)	l Coefficient I		Seismic Design Category		
(39° 05' 56.69"/ -108° 36' 29.08")	0.105	0.252	В		

Note: Seismic Design Category B (For Risk Category II) is assigned when 0.167g ≤ S_{DS} < 0.33g

12.0 OTHER DESIGN AND CONSTRUCTION CONSIDERATIONS

Proper construction practices, in accordance with the Colorado Department of Transportation (CDOT) 2021 Standard Specifications for Road and Bridge Construction; the City of Grand Junction Standard Specifications for Road and Bridge Construction; and the City of Grand Junction Transportation Engineering Design Standards, should be followed during site preparation, earthwork, excavations, roadway and bridge construction, and embankment and retaining wall construction for the suitable long-term performance of the proposed improvements. Excavation support should be provided to maintain onsite safety and the stability of excavations and slopes. Excavations shall be constructed in accordance with local, state, and federal regulations including OSHA guidelines. The contractor must provide a competent person to determine compliance with OSHA excavation requirements. For preliminary planning, existing fill material and native soils may be considered as OSHA Type C soils.

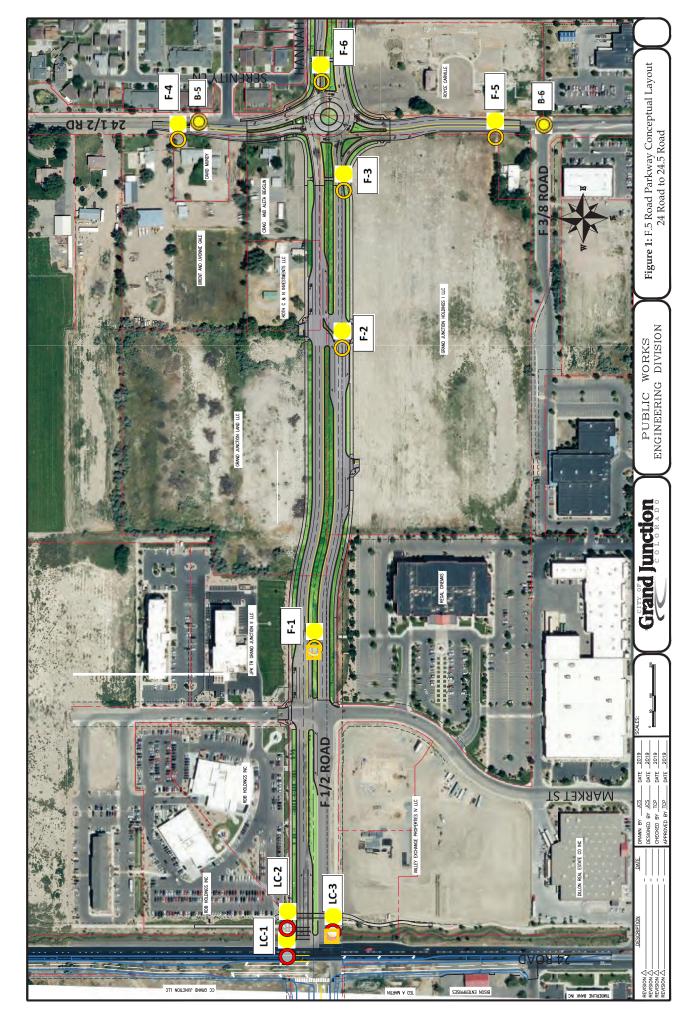
Surface drainage patterns may be altered during construction and local landscape irrigation (if any) must be controlled to prevent excessive moisture infiltration into the subgrade soils during and after construction.

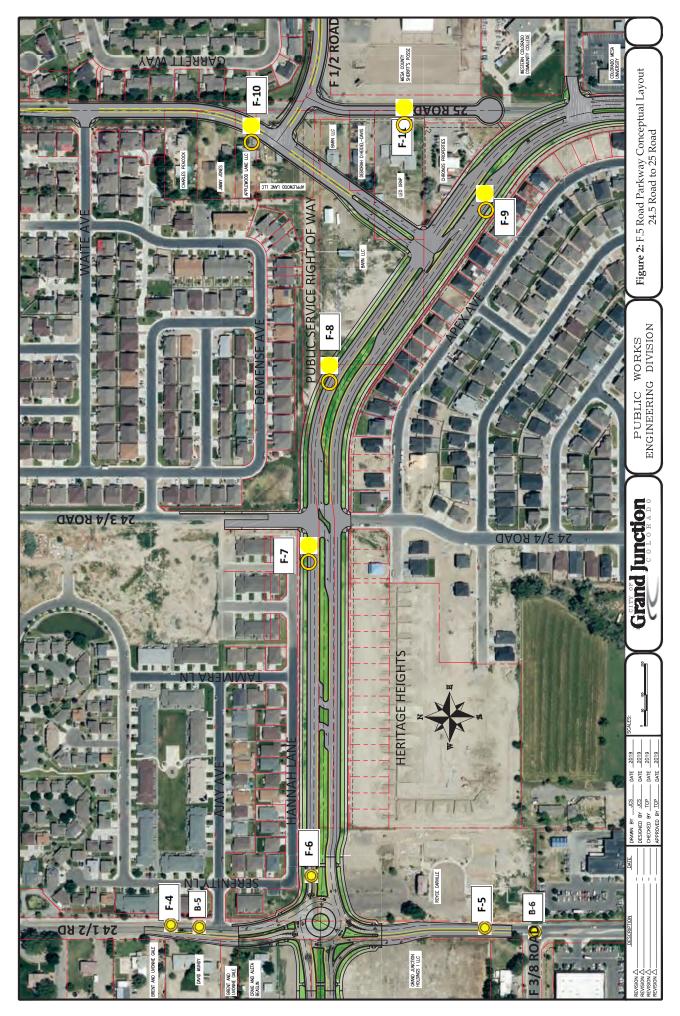
Environmentally contaminated material, if encountered, should be characterized, and removed under the direction of the project environmental consultant. Design and construction plans should be reviewed, and onsite construction should be observed by the professional engineers.

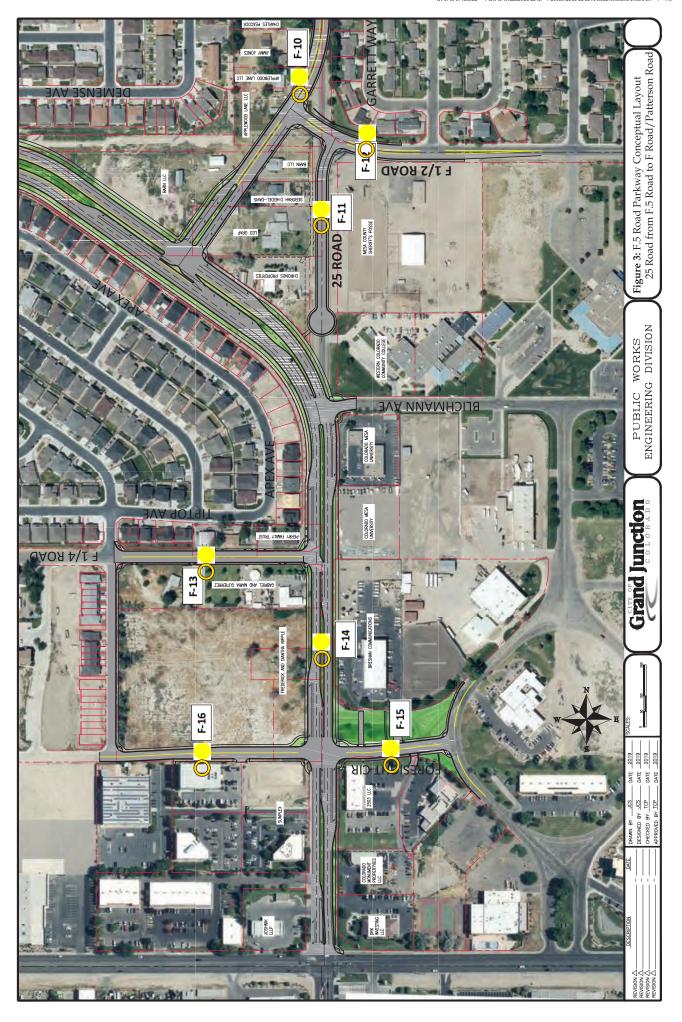


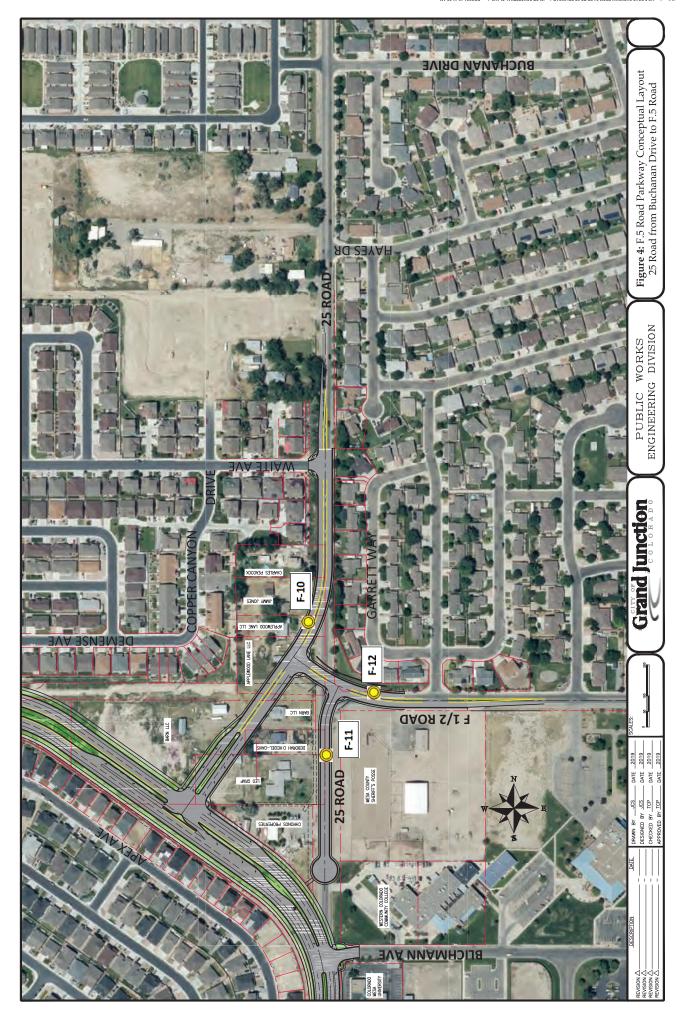
13.0 LIMITATIONS

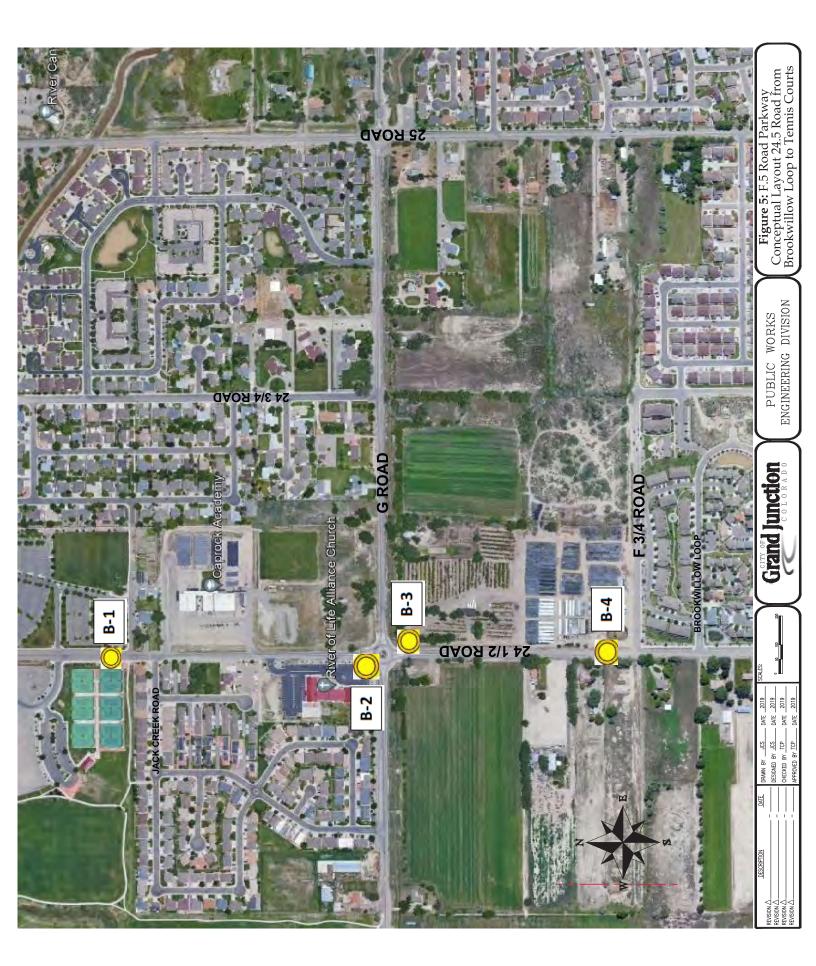
This geotechnical investigation was conducted in general accordance with the scope of work. RockSol's geotechnical practices are similar to those used in Colorado with similar soil conditions and based on our understanding of the proposed work. This report has been prepared for use by the City of Grand Junction for the project described in this report. The report is based on our exploratory boreholes and does not consider variations in the subsurface conditions that may exist between boreholes. Additional investigation is required to address such variation. If during construction activities, materials or water conditions appear to be different from those described herein, RockSol should be advised at once so that a re-evaluation of the recommendations presented in this report can be made. RockSol is not responsible for liability associated with interpretation of subsurface data by others.













APPENDIX A

LEGEND AND INDIVIDUAL BOREHOLE LOGS



CLIENT City of Grand Junction

PROJECT NAME F.5 Road Parkway and 24.5 Road Widening

PROJECT NUMBER 599.37

PROJECT LOCATION Grand Junction, Colorado

LITHOLOGY



Asphalt Pavement



Fill - SAND, gravelly



Fill - CLAY



Native - CLAY



Native - CLAY, sandy



Bedrock - SHALE

0

Fill - Aggregate Base Course



Fill - SAND, clayey to silty



Native - SAND



Native - CLAY, silty



Native - GRAVEL, silty

SAMPLE TYPE



Bulk Sample (Auger Cuttings)



MODIFIED CALIFORNIA SAMPLER 2.5" O.D. AND 2" I.D. WITH BRASS LINERS INCLUDED



SPLIT SPOON SAMPLER 2" O.D. AND 1 3/8" I.D. NO LINERS

Fines Content indicates amount of material, by weight, passing the US No 200 Sieve (%)

15/12 Indicates 15 blows of a 140 pound hammer falling 30 inches was required to drive the sampler 12 inches.

50/11 Indicates 50 blows of a 140 pound hammer falling 30 inches was required to drive the sampler 11 inches.

5,5,5 Indicates 5 blows, 5 blows, 5 blows of a 140 pound hammer falling 30 inches was required to drive the sampler 18 inches.

- ▼ GROUND WATER LEVEL AT TIME OF DRILLING
- ▼ GROUND WATER LEVEL AT 2ND MEASUREMENT
- **▼** GROUND WATER LEVEL AT 3RD MEASUREMENT

BORING: B-1

PAGE 1 OF 1

Consulting Group, Inc. CLIENT City of Grand Junction PROJECT NAME F.5 Road Parkway and 24.5 Road Widening PROJECT NUMBER 599.37 PROJECT LOCATION Grand Junction, Colorado DATE STARTED 10/20/21 __ COMPLETED _10/20/21 GROUND ELEVATION _____ STATION NO. **DRILLING CONTRACTOR** Colorado Drilling and Sampling LATITUDE 39.1 LONGITUDE 108.6 DRILLING METHOD Solid Stem Auger HOLE SIZE 4.25" BORING LOCATION: 24.5 Rd., SB lane, at Tennis Court LOGGED BY _D. Compton HAMMER TYPE _Automatic **GROUND WATER LEVELS:** NOTES WATER DEPTH None Encountered on 10/20/21 ATTERBERG FINES CONTENT (%) SWELL POTENTIAL (%) SAMPLE TYPE DRY UNIT WT. (pcf) MOISTURE CONTENT (%) ELEVATION (ft) LIMITS SULFATE (%) GRAPHIC LOG BLOW COUNTS PLASTICITY INDEX DEPTH (ft) PLASTIC LIMIT LIQUID LIMIT MATERIAL DESCRIPTION 0.0 Asphalt pavement, approximately 6 inches thick Aggregate Base Course, approximately 11 inches thick BBULK (Native) CLAY, with sand, moist to very moist, brown, medium stiff MC 6/12 103.7 18.9 5.0 **Approximate Bulk Depth 2-10** Liquid Limit= 27 BULK 27 13 83.3 14 Plastic Limit= 13 Plasticity Index= 14 Fines Content= 83.3 LOG - STANDARD 599.37_CITY OF GJ PARKWAY PROJECT.GPJ 11/16/21 7.5 10.0 Bottom of hole at 10.0 feet.

BORING : B-2
PAGE 1 OF 1

RockSol Consulting Group, Inc.	BORING : B-2 PAGE 1 OF 1
CLIENT City of Grand Junction	PROJECT NAME F.5 Road Parkway and 24.5 Road Widening
PROJECT NUMBER 599.37	PROJECT LOCATION Grand Junction, Colorado
DATE STARTED 10/20/21 COMPLETED 10/20/21	GROUND ELEVATION STATION NO
DRILLING CONTRACTOR Colorado Drilling and Sampling	LATITUDE 39.1 LONGITUDE 108.6
DRILLING METHOD Solid Stem Auger HOLE SIZE 4.25"	BORING LOCATION: 24.5 Rd. SB Shoulder, just west of 6 Rd.
LOGGED BY D. Compton HAMMER TYPE Automatic	ODOUND WATER LEVELO

	BY D. Co	mpton HAMMER TYPE Automatic			R LEVELS:								
NOTES _			▼ WA	TER DEP	TH 7.0 ft	on 10/	20/21						_
ELEVATION (ff)		MATERIAL DESCRIPTION		SAMPLE TYPE	BLOW	SWELL POTENTIAL (%)	SULFATE (%)	DRY UNIT WT. (pcf)	MOISTURE CONTENT (%)	LIQUID	PLASTIC WINT LIMIT	PLASTICITY SA	FINES CONTENT
	5	(Native) CLAY, sandy, very moist, brown, very stiff Approximate Bulk Depth 0-7 Liquid Limit= 28 Plastic Limit= 13 Plasticity Index= 15 Fines Content= 68.9 Bottom of hole at 7.0 feet.		()						28	13	15	68

BORING: B-3
PAGE 1 OF 1



LOG - STANDARD 599.37 CITY OF GJ PARKWAY PROJECT.GPJ 11/16/21

CLIENT City of Grand Junction PROJECT NAME F.5 Road Parkway and 24.5 Road Widening PROJECT NUMBER 599.37 PROJECT LOCATION Grand Junction, Colorado DATE STARTED 10/20/21 __ COMPLETED _10/20/21 GROUND ELEVATION _____ STATION NO. **DRILLING CONTRACTOR** McCracken Drilling LATITUDE 39.1 LONGITUDE 108.6 DRILLING METHOD Solid Stem Auger HOLE SIZE 4.25" BORING LOCATION: 24.5 Rd. NB lane, just south of roundabout LOGGED BY _D. Compton HAMMER TYPE _Automatic **GROUND WATER LEVELS:** NOTES WATER DEPTH None Encountered on 10/20/21 ATTERBERG FINES CONTENT (%) SWELL POTENTIAL (%) DRY UNIT WT. (pcf) SAMPLE TYPE MOISTURE CONTENT (%) LIMITS ELEVATION (ft) SULFATE (%) GRAPHIC LOG BLOW COUNTS DEPTH (ft) PLASTICITY PLASTIC LIMIT LIQUID LIMIT MATERIAL DESCRIPTION 0.0 Asphalt pavement, approximately 5 inches thick Aggregate Base Course, approximately 12 inches thick BULK (Native) CLAY, sandy, very moist, brown, medium stiff MC 5/12 105.8 19.6 Approximate Bulk Depth 2-9 Liquid Limit= 28 Plastic Limit= 12 BULK 28 12 16 66.6 Plasticity Index= 16 Fines Content= 66.6 Bottom of hole at 9.0 feet.

N/			ockSol onsulting Group, Inc.							В	OR	PAGE			
CLIE	NT Cit	y of Gr	and Junction	PROJECT NAME _F.5 Road Parkway and 24.5 Road Widening											
PRO.	JECT N	UMBE	R 599.37	PROJECT LOCATION Grand Junction, Colorado											
DATE	STAR	TED _	10/20/21 COMPLETED 10/20/21	GROUND ELEVATION STATION NO											
DRIL	LING C	ONTRA	ACTOR Colorado Drilling and Sampling	LATITUDE <u>39.1</u> LONGITUDE <u>108.6</u>											
DRIL	LING M	ETHOI	Solid Stem Auger HOLE SIZE 4.25"	BORING	LOCAT	I ON : <u>675</u>	24.5 R	d., SB	should	der					
LOGG	GED BY	_ <u>D. C</u>	Compton HAMMER TYPE _Automatic	GROUND WATER LEVELS:											
NOTE	ES			WA	TER DEP	TH None	Encou	ntered	d on 10	/20/21					
ELEVATION (ff)	O DEPTH (ft)	GRAPHIC LOG	MATERIAL DESCRIPTION		SAMPLE TYPE	BLOW	SWELL POTENTIAL (%)	SULFATE (%)	DRY UNIT WT. (pcf)	MOISTURE CONTENT (%)	1	PLASTIC HIMIT LIMIT		FINES CONTENT (%)	
			(Native) CLAY, silty, very wet, brown, very stiff												

Large rock @ 2'-3' 5.0 LOG - STANDARD 599.37_CITY OF GJ PARKWAY PROJECT.GPJ 11/12/21 | ||BULK 7.5 10.0 Bottom of hole at 10.0 feet.

BORING: B-5
PAGE 1 OF 1



LOG - STANDARD 599.37_CITY OF GJ PARKWAY PROJECT.GPJ 11/16/21

CLIENT City of Grand Junction PROJECT NAME F.5 Road Parkway and 24.5 Road Widening PROJECT NUMBER 599.37 PROJECT LOCATION Grand Junction, Colorado DATE STARTED 10/20/21 ___ COMPLETED _10/20/21 GROUND ELEVATION _____ STATION NO. **DRILLING CONTRACTOR** Colorado Drilling and Sampling LATITUDE 39.1 LONGITUDE 108.6 DRILLING METHOD Solid Stem Auger HOLE SIZE 4.25" BORING LOCATION: 24.5 Rd., NB lane, just north of Ajay Ave LOGGED BY D. Compton HAMMER TYPE Automatic **GROUND WATER LEVELS:** NOTES WATER DEPTH None Encountered on 10/20/21 ATTERBERG FINES CONTENT (%) SWELL POTENTIAL (%) DRY UNIT WT. (pcf) SAMPLE TYPE MOISTURE CONTENT (%) ELEVATION (ft) LIMITS SULFATE (%) GRAPHIC LOG BLOW COUNTS PLASTICITY INDEX DEPTH (ft) PLASTIC LIMIT LIQUID LIMIT MATERIAL DESCRIPTION 0.0 Asphalt pavement, approximately 7 inches thick Aggregate Base Course, approximatley 11 inches thick (Native) CLAY, very moist, brown, soft 2.5 5.0 MC 3/12 98.3 24.9 Approximate Bulk Depth 3-10 Liquid Limit= 33 Plastic Limit= 14 BULK 33 19 88.6 Plasticity Index= 19 Fines Content= 88.6 7.5 10.0 Bottom of hole at 10.0 feet.

BORING: B-6

PAGE 1 OF 1

PROJECT NAME F.5 Road Parkway and 24.5 Road Widening
PROJECT LOCATION Grand Junction, Colorado
GROUND ELEVATION STATION NO.
LATITUDE 39.1 LONGITUDE 108.6

DRILLING METHOD Solid Stem Auger HOLE SIZE 4.25" BORING LOCATION: 24.5 Rd. NB lane, @ F 3/8 Rd LOGGED BY D. Compton HAMMER TYPE Automatic **GROUND WATER LEVELS:**

Pock Sol

LOG - STANDARD 599.37 CITY OF GJ PARKWAY PROJECT.GPJ 12/9/21

NOTES WATER DEPTH None Encountered on 10/20/21 ATTERBERG FINES CONTENT (%) SWELL POTENTIAL (%) DRY UNIT WT. (pcf) MOISTURE CONTENT (%) SAMPLE TYPE LIMITS ELEVATION (ft) SULFATE (%) GRAPHIC LOG BLOW COUNTS PLASTICITY INDEX DEPTH (ft) PLASTIC LIMIT LIQUID LIMIT MATERIAL DESCRIPTION 0.0 Asphalt pavement, approximately 5 inches thick Aggregate Base Course (Fill) SAND, gravelly (Native) CLAY, silty, with sand, very moist, brown, very 5.0 Approximate Bulk Depth 4-10 Liquid Limit= 19 BULK 73.1 19 15 4 Plastic Limit= 15 Plasticity Index= 4 7.5 Fines Content= 73.1 10.0 Bottom of hole at 10.0 feet.





LOG - STANDARD 599.37_CITY OF GJ PARKWAY PROJECT.GPJ 11/16/21

CLIENT City of Grand Junction PROJECT NAME F.5 Road Parkway and 24.5 Road Widening PROJECT NUMBER 599.37 PROJECT LOCATION Grand Junction, Colorado **DATE STARTED** <u>10/4/21</u> **COMPLETED** <u>10/4/21</u> GROUND ELEVATION _____ STATION NO. DRILLING CONTRACTOR Colorado Drilling and Sampling ___ **LATITUDE** <u>39.1</u> LONGITUDE 108.6 DRILLING METHOD Solid Stem Auger HOLE SIZE 4.25" BORING LOCATION: LOGGED BY D. Compton HAMMER TYPE Automatic **GROUND WATER LEVELS:** NOTES WATER DEPTH None Encountered on 10/4/21 ATTERBERG FINES CONTENT (%) SWELL POTENTIAL (%) DRY UNIT WT. (pcf) SAMPLE TYPE MOISTURE CONTENT (%) ELEVATION (ft) LIMITS SULFATE (%) GRAPHIC LOG BLOW COUNTS PLASTICITY INDEX DEPTH (ft) PLASTIC LIMIT LIQUID LIMIT MATERIAL DESCRIPTION 0.0 (Native) CLAY, moist to very moist, brown, soft Approximate Bulk Depth 0-5 2.5 Liquid Limit= 38 BULK 0.38 38 19 88.8 19 Plastic Limit= 19 Plasticity Index= 19 Fines Content= 88.8 Sulfate= 0.38 MC 3/12 0.0 97.9 19.5 5.0 7.5 10.0 Bottom of hole at 10.0 feet.





LOG - STANDARD 599.37_CITY OF GJ PARKWAY PROJECT.GPJ 11/12/21

CLIEN	NT Cit	y of Gr	and Junction											
PROJ	ECT N	UMBEI	R 599.37											
DATE	STAR	TED _	10/5/21 COMPLETED 10/5/21	GROUN	D ELEVA	TION			STATIO	ON NO)			
DRILL	ING C	ONTRA	ACTOR Colorado Drilling and Sampling	LATITUI	DE <u>39.1</u>				LON	GITUE	DE _10	8.6		_
DRILL	ING M	ETHO	Solid Stem Auger HOLE SIZE 4.25"	BORING	LOCATI	ON: Field	l along	new p	oropose	ed F.5	Rd			
			Compton HAMMER TYPE Automatic	GROUN	D WATE	R LEVELS:								
NOTE	:s			_ WA	TER DEP	TH None	Encou	ntered	d on 10	/5/21				
_					Й		(%)	<u>(0</u>	l _E	(9)	ATT	ERBE	RG	INT:
ELEVATION (ft)	돈	GRAPHIC LOG			SAMPLE TYPE	» M	AL (SULFATE (%)	DRY UNIT WT. (pcf)	MOISTURE CONTENT (%)			≽	FINES CONTENT (%)
¥ €	DEPTH (ft)	%P LOC	MATERIAL DESCRIPTION		PLE	BLOW	WE	FAT	N S	IST TEN	LIQUID	STIC		00%
		9			WA.		SWELL POTENTIAL (SUL	JR Y	≥ S	S=	PLASTIC LIMIT	PLASTICITY INDEX	NES
	0.0	/////	(1) (1) (2) (2) (3)		1 (1		_						립	표
			(Native) CLAY, moist, brown, stiff		{}									
	-				J}									
					}}									
					{									
					{[]									
					{}									
	-				J}									
	2.5]}									
					{}									
	-		Approximate Bulk Depth 0-6 Liquid Limit= 37		BULK		1				37	19	18	92.3
	L _		Plastic Limit= 19 Plasticity Index= 18		мс	9/12			105.9	16.0				
			Fines Content= 92.3		\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \	9/12			103.9	10.9				
					{[
	-				{[]									
	5.0				[]									
					J}									
	-				}}									
	_				{									
	_													
	7.5													
	-													
	L -													
	-													
	L _													
	10.0		Bottom of hole at 10.0 feet.											
			251.51. 51. 1.51.5 41. 15.0 1501.											
	1	1					1		I	1	I	I	1	

BORING: F-3
PAGE 1 OF 1



LOG - STANDARD 599.37_CITY OF GJ PARKWAY PROJECT.GPJ 11/16/21

CLIENT City of Grand Junction PROJECT NAME F.5 Road Parkway and 24.5 Road Widening PROJECT NUMBER 599.37 PROJECT LOCATION Grand Junction, Colorado DATE STARTED 10/5/21 __ COMPLETED 10/5/21 GROUND ELEVATION _____ STATION NO. **DRILLING CONTRACTOR** Colorado Drilling and Sampling LATITUDE 39.1 LONGITUDE 108.6 DRILLING METHOD Solid Stem Auger HOLE SIZE 4.25" BORING LOCATION: Field near 24.5 Rd and new F.5 Rd LOGGED BY D. Compton HAMMER TYPE Automatic **GROUND WATER LEVELS:** NOTES WATER DEPTH None Encountered on 10/5/21 ATTERBERG FINES CONTENT (%) SWELL POTENTIAL (%) DRY UNIT WT. (pcf) MOISTURE CONTENT (%) SAMPLE TYPE ELEVATION (ft) LIMITS SULFATE (%) GRAPHIC LOG BLOW COUNTS PLASTICITY INDEX DEPTH (ft) PLASTIC LIMIT LIQUID LIMIT MATERIAL DESCRIPTION 0.0 (Native) CLAY, moist, brown, soft Approximate Bulk Depth 0-4 Liquid Limit= 33 Plastic Limit= 18 BULK 33 18 15 92.2 Plasticity Index= 15 Fines Content= 92.2 2.5 MC 3/12 103.3 | 13.1 5.0 7.5 10.0 Bottom of hole at 10.0 feet.





LOG - STANDARD 599.37_CITY OF GJ PARKWAY PROJECT.GPJ 11/16/21

CLIENT City of Grand Junction PROJECT NAME F.5 Road Parkway and 24.5 Road Widening PROJECT NUMBER 599.37 PROJECT LOCATION Grand Junction, Colorado DATE STARTED 10/5/21 __ COMPLETED _10/5/21 GROUND ELEVATION _____ STATION NO. **DRILLING CONTRACTOR** Colorado Drilling and Sampling LATITUDE 39.1 LONGITUDE 108.6 DRILLING METHOD Solid Stem Auger HOLE SIZE 4.25" BORING LOCATION: NE side of 24.5 Rd. and F.5 Rd LOGGED BY D. Compton HAMMER TYPE Automatic **GROUND WATER LEVELS:** NOTES WATER DEPTH None Encountered on 10/5/21 ATTERBERG FINES CONTENT (%) SWELL POTENTIAL (%) DRY UNIT WT. (pcf) SAMPLE TYPE MOISTURE CONTENT (%) ELEVATION (ft) LIMITS SULFATE (%) GRAPHIC LOG BLOW COUNTS PLASTICITY INDEX DEPTH (ft) PLASTIC LIMIT LIQUID LIMIT MATERIAL DESCRIPTION (Native) CLAY, with sand, moist, brown, soft Approximate Bulk Depth 0-5 Liquid Limit= 37 BULK 0.16 37 21 72.2 16 Plastic Limit= 21 Plasticity Index= 16 Fines Content= 72.2 Sulfate= 0.16 5.0 (Native) CLAY, silty, very moist, brown, soft 7.5 10.0 Bottom of hole at 10.0 feet.





LOG - STANDARD 599.37_CITY OF GJ PARKWAY PROJECT.GPJ

CLIENT City of Grand Junction PROJECT NAME F.5 Road Parkway and 24.5 Road Widening PROJECT NUMBER 599.37 PROJECT LOCATION Grand Junction, Colorado GROUND ELEVATION STATION NO. DATE STARTED 10/20/21 __ COMPLETED _10/20/21 **DRILLING CONTRACTOR** Colorado Drilling and Sampling LATITUDE 39.1 LONGITUDE 108.6 DRILLING METHOD Solid Stem Auger HOLE SIZE 4.25" **BORING LOCATION:** LOGGED BY D. Compton HAMMER TYPE Automatic **GROUND WATER LEVELS:** NOTES WATER DEPTH None Encountered on 10/20/21 ATTERBERG FINES CONTENT (%) SWELL POTENTIAL (%) DRY UNIT WT. (pcf) SAMPLE TYPE MOISTURE CONTENT (%) LIMITS ELEVATION (ft) SULFATE (%) GRAPHIC LOG BLOW COUNTS PLASTICITY INDEX DEPTH (ft) PLASTIC LIMIT LIQUID LIMIT MATERIAL DESCRIPTION 0.0 Asphalt pavement, approximately 6 inches thick Aggregate Base Course, approximately 6 inches thick (Fill) SAND, gravelly (Native) CLAY, with sand, very moist, brown, very stiff 5.0 Approximate Bulk Depth 2-10 Liquid Limit= 27 Plastic Limit= 14 BULK 0.26 27 13 81.3 14 Plasticity Index= 13 Fines Content= 81.3 Sulfate= 0.26 7.5 10.0 Bottom of hole at 10.0 feet.

BORING: F-6
PAGE 1 OF 1



LOG - STANDARD 599.37_CITY OF GJ PARKWAY PROJECT.GPJ 11/16/21

CLIENT City of Grand Junction PROJECT NAME F.5 Road Parkway and 24.5 Road Widening PROJECT NUMBER 599.37 PROJECT LOCATION Grand Junction, Colorado DATE STARTED 10/5/21 __ COMPLETED 10/5/21 GROUND ELEVATION _____ STATION NO. **DRILLING CONTRACTOR** Colorado Drilling and Sampling LATITUDE 39.1 LONGITUDE 108.6 DRILLING METHOD Solid Stem Auger HOLE SIZE 4.25" BORING LOCATION: SE side of 24.5 Rd and F.5 Rd LOGGED BY D. Compton HAMMER TYPE Automatic **GROUND WATER LEVELS:** NOTES WATER DEPTH None Encountered on 10/5/21 ATTERBERG FINES CONTENT (%) SWELL POTENTIAL (%) DRY UNIT WT. (pcf) SAMPLE TYPE MOISTURE CONTENT (%) ELEVATION (ft) LIMITS SULFATE (%) GRAPHIC LOG BLOW COUNTS PLASTICITY INDEX DEPTH (ft) PLASTIC LIMIT LIQUID LIMIT MATERIAL DESCRIPTION (Native) CLAY, with gravel, moist to very moist, brown, МС 103.0 21.1 11/12 Approximate Bulk Depth 0-7 Liquid Limit= 32 Plastic Limit= 18 BULK 32 18 14 79.9 Plasticity Index= 14 Fines Content= 79.9 5.0 7.5 10.0 Bottom of hole at 10.0 feet.

BORING: F-7
PAGE 1 OF 1



LOG - STANDARD 599.37_CITY OF GJ PARKWAY PROJECT.GPJ 11/16/21

CLIENT City of Grand Junction PROJECT NAME F.5 Road Parkway and 24.5 Road Widening PROJECT NUMBER 599.37 PROJECT LOCATION Grand Junction, Colorado DATE STARTED 10/5/21 __ COMPLETED 10/5/21 GROUND ELEVATION _____ STATION NO. **DRILLING CONTRACTOR** Colorado Drilling and Sampling LATITUDE 39.1 LONGITUDE 108.6 DRILLING METHOD Solid Stem Auger HOLE SIZE 4.25" BORING LOCATION: 24 3/4 RD and new F.5 Rd (west side) LOGGED BY _D. Compton HAMMER TYPE _Automatic **GROUND WATER LEVELS:** NOTES WATER DEPTH None Encountered on 10/5/21 ATTERBERG FINES CONTENT (%) SWELL POTENTIAL (%) DRY UNIT WT. (pcf) MOISTURE CONTENT (%) SAMPLE TYPE ELEVATION (ft) LIMITS SULFATE (%) GRAPHIC LOG BLOW COUNTS PLASTICITY INDEX DEPTH (ft) PLASTIC LIMIT LIQUID LIMIT MATERIAL DESCRIPTION (Native) CLAY, with sand, slightly moist, brown, very stiff 2.5 Approximate Bulk Depth 0-5 BULK 79.6 30 18 12 Liquid Limit= 30 Plastic Limit= 18 Plasticity Index= 12 Fines Content= 79.6 MC 22/12 109.5 4.8 73.7 (Native) CLAY, silt, moist, brown, stiff 5.0 7.5 10.0 Bottom of hole at 10.0 feet.





LOG - STANDARD 599.37_CITY OF GJ PARKWAY PROJECT.GPJ 11/16/21

CLIENT City of Grand Junction PROJECT NAME F.5 Road Parkway and 24.5 Road Widening PROJECT NUMBER 599.37 PROJECT LOCATION Grand Junction, Colorado DATE STARTED 10/5/21 __ COMPLETED 10/5/21 GROUND ELEVATION _____ STATION NO. **DRILLING CONTRACTOR** Colorado Drilling and Sampling LATITUDE 39.1 LONGITUDE 108.6 DRILLING METHOD Solid Stem Auger HOLE SIZE 4.25" BORING LOCATION: New F.5 alignment, Vacant land LOGGED BY D. Compton HAMMER TYPE Automatic **GROUND WATER LEVELS:** NOTES WATER DEPTH None Encountered on 10/5/21 ATTERBERG FINES CONTENT (%) SWELL POTENTIAL (%) DRY UNIT WT. (pcf) SAMPLE TYPE MOISTURE CONTENT (%) ELEVATION (ft) LIMITS SULFATE (%) GRAPHIC LOG BLOW COUNTS PLASTICITY INDEX DEPTH (ft) PLASTIC LIMIT LIQUID LIMIT MATERIAL DESCRIPTION (Native) CLAY, silty with sand, slightly moist to moist, brown, medium stiff Approximate Bulk Depth 0-5 2.5 Liquid Limit= 26 BULK 0.28 26 7 75.4 19 Plastic Limit= 19 Plasticity Index= 7 Fines Content= 75.4 Sulfate= 0.28 5.0 MC 6/12 107.2 9.2 62.4 7.5 10.0 Bottom of hole at 10.0 feet.





LOG - STANDARD 599.37_CITY OF GJ PARKWAY PROJECT.GPJ 11/16/21

CLIENT City of Grand Junction PROJECT NAME F.5 Road Parkway and 24.5 Road Widening PROJECT NUMBER 599.37 PROJECT LOCATION Grand Junction, Colorado DATE STARTED 10/5/21 __ COMPLETED 10/5/21 GROUND ELEVATION _____ STATION NO. **DRILLING CONTRACTOR** Colorado Drilling and Sampling LATITUDE 39.1 LONGITUDE 108.6 DRILLING METHOD Solid Stem Auger HOLE SIZE 4.25" BORING LOCATION: _East end new proposed F.5, west of 25 Rd. LOGGED BY _D. Compton HAMMER TYPE _Automatic **GROUND WATER LEVELS:** NOTES WATER DEPTH None Encountered on 10/5/21 ATTERBERG FINES CONTENT (%) SWELL POTENTIAL (%) DRY UNIT WT. (pcf) MOISTURE CONTENT (%) SAMPLE TYPE ELEVATION (ft) LIMITS SULFATE (%) GRAPHIC LOG BLOW COUNTS PLASTICITY INDEX DEPTH (ft) PLASTIC LIMIT LIQUID LIMIT MATERIAL DESCRIPTION (Native) CLAY, moist, brown, soft Approximate Bulk Depth 0-3 Liquid Limit= 33 BULK 33 18 15 89.5 Plastic Limit= 18 Plasticity Index= 15 Fines Content= 89.5 5.0 (Native) CLAY, silty, very moist, brown, soft 7.5 10.0 Bottom of hole at 10.0 feet.

BORING: F-10

PAGE 1 OF 1

RockSol Consulting Group, Inc.		5
CLIENT City of Grand Junction	PROJECT NAME	F.5 Road Parkway and 24.5 Road

SAMPLE TYPE		SWELL POTENTIAL (%)	SULFATE (%)	DRY UNIT WT. (pcf)	MOISTURE CONTENT (%)	LIQUID	PLASTIC WIE	PLASTICITY %	FINES CONTENT
		SWELL POTENTIAL	SULFATE (DRY UNIT V (pcf)	MOISTUR CONTENT (LIQUID	PLASTIC LIMIT	PLASTICITY INDEX	NES CONT
BULK									ᄪ
MC			1.04	101.4	18.3	30	20	10	79
{									



RockSol
Consulting Group, Inc.

LOG - STANDARD 599.37_CITY OF GJ PARKWAY PROJECT.GPJ 12/9/21

CLIEN	IENT City of Grand Junction					PROJECT NAME _F.5 Road Parkway and 24.5 Road Widening											
PROJ	ECT N	UMBER	599.37			PROJECT LOCATION Grand Junction, Colorado											
DATE	STAR	TED _10	0/20/21	COMPLETE	D 10/20/21	GROUN	D ELEV	ATION			STATI	ON NC)				
DRILL	ING C	ONTRA	CTOR Colorad	lo Drilling and Sa	ampling	_ LATITU	DE 39.1			LON	NGITU	DE _10	08.6				
					ZE <u>4.25"</u>			ON: 25 R									
LOGG	ED BY	D. Cc	ompton	_ HAMMER T	YPE Automatic	GROUN	D WATE	R LEVELS:									
NOTE	:s					WA	TER DEP	TH None	Encou	nterec	on 10	/20/21					
_							Щ		(%)		<u>.</u> :	<u> </u>	ATT	TERBE LIMITS	RG	F	
ELEVATION (ft)	O DEPTH	GRAPHIC LOG		MATERIAL DE	ESCRIPTION		SAMPLE TYPE	BLOW	SWELL POTENTIAL (SULFATE (%)	DRY UNIT WT. (pcf)	MOISTURE CONTENT (%)	LIQUID		PLASTICITY INDEX	FINES CONTENT (%)	
	0.0		Asphalt pave	ement, approxim	ately 6 inches thick												
		0	Aggregate B	ase Course, app	proximately 6 inches	s thick											
	2.5 		(Fill) SAND,	gravelly	oist, brown, stiff		BULK										
	 10.0			Bottom of ho	le at 10.0 feet.		{										

PAGE 1 OF 1

RockSol
Consulting Group, Inc.

LOG - STANDARD 599.37_CITY OF GJ PARKWAY PROJECT.GPJ 11/16/21

CLIENT _City of Grand Junction PROJECT NAME F.5 Road Parkway and 24.5 Road Widening PROJECT NUMBER 599.37 PROJECT LOCATION Grand Junction, Colorado GROUND ELEVATION _____ STATION NO. DATE STARTED 10/20/21 ___ COMPLETED 10/20/21 **DRILLING CONTRACTOR** Colorado Drilling and Sampling _ **LATITUDE** <u>39.1</u> LONGITUDE 108.6 DRILLING METHOD Solid Stem Auger HOLE SIZE 4.25" BORING LOCATION: Corner of F.5 and 25 Rd, ~18' off 25 Rd LOGGED BY D. Compton HAMMER TYPE Automatic **GROUND WATER LEVELS:** NOTES WATER DEPTH None Encountered on 10/20/21 ATTERBERG LIMITS FINES CONTENT (%) SWELL POTENTIAL (%) DRY UNIT WT. (pcf) MOISTURE CONTENT (%) SAMPLE TYPE ELEVATION (ft) SULFATE (%) GRAPHIC LOG BLOW COUNTS PLASTICITY INDEX DEPTH (ft) PLASTIC LIMIT LIQUID LIMIT MATERIAL DESCRIPTION (Native) CLAY, sandy, very moist, brown, very soft BULK Bottom of hole at 10.0 feet.

RockSol
Consulting Group, Inc.

LOG - STANDARD 599.37_CITY OF GJ PARKWAY PROJECT.GPJ 11/16/21

	_		risuling Group, mo.			_				_				
		-		PROJECT NAME F.5 Road Parkway and 24.5 Road Widening PROJECT LOCATION Grand Junction, Colorado										
			R _599.37 COMPLETED 10/20/21								<u> </u>			
			ACTOR Colorado Drilling and Sampling											
						ION: _F 1/4						08.6		
						R LEVELS:		v D iai	ie					_
						TH None		ntered	d on 10.	/20/21				
					ш		(9)					ERBE		È
ELEVATION (ft)	 <u>_</u>	일			SAMPLE TYPE	s > L	.L \(\)	SULFATE (%)	DRY UNIT WT. (pcf)	MOISTURE CONTENT (%)		LIMITS		FINES CONTENT (%)
TA E	DEPTH (ft)	GRAPHIC LOG	MATERIAL DESCRIPTION		E	BLOW	SWELL POTENTIAL (-ATE	(pcf)	ST EN	⊖ ⊑	PLASTIC LIMIT	PLASTICITY INDEX	Š8
		GR			AMF		STE	SULF	잝	Ø N	LIQUID	LIN LIN	ASTICI'	ZES
	0.0				<u> </u>		<u> </u>			0		<u> </u>	4	듄
		0	Asphalt pavement, approximately 2 inches thick Aggregate Base Course, approximately 10 inches t	hick										
	-	6.0	riggregate Base source, approximately to mones t	inor										
);												
			(Native) CLAY, silty, very moist, brown, very stiff											
	-													
				-										
	2.5			ľ	!(
					[]									
	-													
					}									
					}									
	-				}									
	L.			(
				ľ	il 💮									
	5.0			ŀ	¦[
	L .			ŀ	[[
	-				BULK									
					}									
				ľ	}									
	_			(
	7.5			(j]									
				(
				ŀ	[[
	-													
	L.													
					}									
	-			ľ	}									
	10.0													
			Bottom of hole at 10.0 feet.											
												[

RockSol
Consulting Group, Inc.

LOG - STANDARD 599.37_CITY OF GJ PARKWAY PROJECT.GPJ 12/9/21

OI :=:	T 0"		and have the	DDC 153	T 11457		LD. I		1015	D	.			
			and Junction R 599.37	PROJECT NAME F.5 Road Parkway and 24.5 Road Widening PROJECT LOCATION Grand Junction, Colorado										
			0/20/21 COMPLETED _10/20/21			ATION GIA).			
						<u> </u>								
			Solid Stem Auger HOLE SIZE 4.25"	BORING					01100	<u> </u>	0.0			_
LOGG	ED BY	D. C	ompton HAMMER TYPE Automatic	GROUN	O WATE	R LEVELS	:							
NOTE	s			WAT	ER DEP	TH None	Encou	nterec	d on 10/	20/21				
					ш		(%)	<u> </u>	Li.	(9)		ERBE		Z
ELEVATION (ft)	O DEPTH (ft)	GRAPHIC LOG	MATERIAL DESCRIPTION		SAMPLE TYPE	BLOW	SWELL POTENTIAL (SULFATE (%)	DRY UNIT WT. (pcf)	MOISTURE CONTENT (%)	LIQUID	PLASTIC	PLASTICITY INDEX	FINES CONTENT (%)
	0.0		Asphalt pavement, approximately 6 inches thick											
		. <u> </u>	Aggregate Base Course, approximately 4 inches th	nick										
			(Fill) CLAY, silty, slightly moist to moist, brown, har											
			(,											
			(Fill) SAND, gavelly		МС	24/12			114.2	10.8				
		\$.							
	2.5	\$ \$												
		* * * *												
			(Native) CLAY, silty, very moist, brown, stiff		3									
	5.0 5.0 7.5				BBULK BBULK ABOVE AND ADDRESS AND ADDRES									
			Bottom of hole at 10.0 feet.											

Consulting Group, Inc.

CLIEN	City of Grand Junction			PROJECT NAME _F.5 Road Parkway and 24.5 Road Widening										
PROJ	ECT N	UMBE	R _599.37	PROJECT LOCATION Grand Junction, Colorado										
DATE	STAR	TED _	10/20/21 COMPLETED 10/20/21	GROUN	ID ELEV	ATION			STATI	ON NO	D			
DRILL	ING C	ONTR	ACTOR Colorado Drilling and Sampling	LATITU	DE 39.1	1		LON	GITUD	E 10	8.6			
DRILL	ING M	IETHO	D Solid Stem Auger HOLE SIZE 4.25"			ION: Fore								
LOGG	SED BY	/ <u>D. C</u>	Compton HAMMER TYPE Automatic			R LEVELS:								
NOTE	:s					TH None		ntered	d on 10	/20/21				
											AT	ΓERBE		<u> </u>
ELEVATION (ft)	DEPTH (ft)	GRAPHIC LOG	MATERIAL DESCRIPTION		SAMPLE TYPE	BLOW	SWELL POTENTIAL (%)	SULFATE (%)	DRY UNIT WT. (pcf)	MOISTURE CONTENT (%)	LIQUID	PLASTIC MI	>	FINES CONTENT
	0.0		Asphalt pavement, approximately 3 inches thick										-	-
		0 . O	Aggregate Base Course, approximately 9 inches to	hick										
). *A. *A. *A. *A. *A. *A. *A. *A.	(Fill) SAND, gravelly											
			(Native) CLAY, silty, very moist, brown, stiff		[]									
	2.5													
					}									
	5.0													
					$\left\{ ight\}$									
					 B BULK									
	7.5													
					$\left\ \left\{ \right\ $									
					$\left\{ ight\}$									
	10.0		Bottom of hole at 10.0 feet.		[]									

BORING: F-16

PAGE 1 OF 1

RockSol
Consulting Group, Inc.

LOG - STANDARD 599.37_CITY OF GJ PARKWAY PROJECT.GPJ 11/16/21

CLIENT City of Grand Junction PROJECT NAME F.5 Road Parkway and 24.5 Road Widening PROJECT NUMBER 599.37 PROJECT LOCATION Grand Junction, Colorado DATE STARTED 10/20/21 __ COMPLETED 10/20/21 GROUND ELEVATION _____ STATION NO. **DRILLING CONTRACTOR** Colorado Drilling and Sampling LATITUDE 39.1 LONGITUDE 108.6 DRILLING METHOD Solid Stem Auger HOLE SIZE 4.25" BORING LOCATION: Field N of 6.5 Climb Gym - new road LOGGED BY D. Compton HAMMER TYPE Automatic **GROUND WATER LEVELS:** NOTES WATER DEPTH None Encountered on 10/20/21 ATTERBERG FINES CONTENT (%) SWELL POTENTIAL (%) DRY UNIT WT. (pcf) SAMPLE TYPE MOISTURE CONTENT (%) ELEVATION (ft) LIMITS SULFATE (%) GRAPHIC LOG BLOW COUNTS PLASTICITY INDEX DEPTH (ft) PLASTIC LIMIT LIQUID LIMIT MATERIAL DESCRIPTION (Native) CLAY, with sand, slightly moist, brown, stiff МС 14/12 95.8 7.1 96.5 Approximate Bulk Depth 0-10 5.0 Liquid Limit= 28 BULK 0.14 28 16 12 84.7 Plastic Limit= 16 Plasticity Index= 12 Fines Content= 84.7 Sulfate= 0.14 7.5 10.0 Bottom of hole at 10.0 feet.



Consulting Group, Inc. PROJECT NAME F.5 Road Parkway and 24.5 Road Widening CLIENT City of Grand Junction PROJECT NUMBER 599.37 PROJECT LOCATION Grand Junction, Colorado

 DATE STARTED
 10/4/21
 COMPLETED
 10/4/21

DRILLING CONTRACTOR Colorado Drilling and Sampling LATITUDE 39.1 LONGITUDE 108.6

DRILLING METHOD Solid Stem Auger HOLE SIZE 4.25" BORING LOCATION: NE corner of 24 Rd and F.5 Rd - wingwall

GROUND ELEVATION _____ STATION NO.

LOGG		D. Co	ompton HAMMER TYPE Automatic	— GROUND WATER LEVELS: WATER DEPTH _7.0 ft on 10/4/21									
ELEVATION (ft)	O DEPTH (ft)	GRAPHIC LOG	MATERIAL DESCRIPTION	SAMPLE TYPE	BLOW	SWELL POTENTIAL (%)	SULFATE (%)	DRY UNIT WT. (pcf)	MOISTURE CONTENT (%)	LIMIT	PLASTIC LIMIT	S 	FINES CONTENT (%)
	5		(Native) CLAY, with sand, moist to wet, brown, soft Approximate Bulk Depth 0-5 Liquid Limit= 27 Plastic Limit= 15 Plasticity Index= 12 Fines Content= 76.6 Sulfate= 0.51	t }	K		0.51			27	15	12	76.6
	15			ss	1/2/2				28.5				84.1
			Bottom of hole at 21.5 feet.	ss	1/2/2				29.5				49.5

RockSol
Consulting Group, Inc.

			and Junction	PROJECT NAME F.5 Road Parkway and 24.5 Road Widening PROJECT LOCATION Grand Junction, Colorado										
			<u>\$ 599.37</u>											
			CTOR Colorado Drilling and Sampling			TION								
			Solid Stem Auger HOLE SIZE 4.25"							GITUE				
			pmpton HAMMER TYPE _Automatic			ON: NE							<u> </u>	
			Transier Transier Tree Automatic	0.100.		R LEVELS: 5.1 ft on 1							 11/30/	'21
	. <u> </u>				1	0.110111					ΔΤΊ	TERBE		1
ELEVATION (ft)	DEPTH (ft)	GRAPHIC LOG	MATERIAL DESCRIPTION		SAMPLE TYPE NUMBER	BLOW COUNTS (N VALUE)	SWELL POTENTIAL (%)	SULFATE (%)	DRY UNIT WT. (pcf)	MOISTURE CONTENT (%)	LIQUID	PLASTIC LIMIT		FINES CONTENT (%)
ш	0	/ % // %	(Native) CLAY, sandy, moist to wet, soft		% 13		8	S	<u> </u>	-8		<u> </u>	7	Z Z
	5		Approximate Bulk Depth 0-5 Liquid Limit= 25 Plastic Limit= 15 Plasticity Index= 10 Fines Content= 68.2		BULK						25	15	10	68.2
	10				M C		-0.2		87.9	25.0				55.1
	20				X ss	1/1/2		0.47		29.0				58.4
	30		(Native) SAND, with silt and gravel, slightly moist, to gray, medium stiff to very hard	brown	× ss	81/12				6.4	NP	NP	NP	7.7
	35		(Bedrock) Shale, very moist to slightly moist, gray medium stiff to very hard Bottom of hole at 40.3 feet.	,	SS	50/3				15.1				42.1

PAGE 1 OF 1

RockSol
Consulting Group, Inc.

CLIENT City of Grand Junction

PROJECT NAME F.5 Road Parkway and 24.5 Road Widening

PROJECT NUMBER 599.37

PROJECT LOCATION Grand Junction, Colorado

DATE STARTED 10/4/21 COMPLETED 10/4/21

GROUND ELEVATION STATION NO.

DRILLING CONTRACTOR Colorado Drilling and Sampling

DRILLING METHOD Solid Stem Auger HOLE SIZE 4.25"

BORING LOCATION: SE corner of F.5 Rd and 24 Rd underpass

LOGGED BY D. Compton HAMMER TYPE Automatic GROUND WATER LEVELS: 1st DEPTH 10.0 ft on 10/4/21

NOTES **Y2ND DEPTH** 10.3 ft on 11/1/21 **Y3RD DEPTH** 10.6 ft on 11/30/21 **ATTERBERG** FINES CONTENT (%) SAMPLE TYPE NUMBER DRY UNIT WT. (pcf) MOISTURE CONTENT (%) LIMITS ELEVATION (ft) SULFATE (%) BLOW COUNTS (N VALUE) GRAPHIC LOG SWELL POTENTIAL (DEPTH (ft) PLASTICITY PLASTIC LIMIT LIQUID MATERIAL DESCRIPTION (Native) GRAVEL, sandy, moist, brown, stiff 58.1 BULK (Native) CLAY, with sand, very moist to wet, brown, soft BULK 28 15 13 74.9 Approximate Bulk Depth 0-2 Fines Content= 58.1 MC 4/12 -1.7 102.2 19.6 Approximate Bulk Depth 2-4 Liquid Limit= 28 Plastic Limit= 15 Plasticity Index= 13 Fines Content= 74.9 SS 1/1/1 26.6 29 16 13 94.4 15 20 SS 1/1/1 0.19 34.4 83.7 25 (Native) CLAY, with sand, slightly moist to moist, brown, hard 30 × ss 71/10 0.15 6.2 40 14.8 53.2 (Bedrock) SHALE, slightly moist, gray, very hard \ SS / 50/1 Bottom of hole at 40.1 feet.

LOG - STANDARD - 2 H20 599.37 CITY OF GJ PARKWAY PROJECT.GPJ



APPENDIX B

SUMMARY OF LABORATORY TEST RESULTS



CLIENT City of Grand Junction

SUMMARY OF PHYSICAL & CHEMICAL TEST RESULTS

PAGE 1 OF

0

PROJECT NAME F.5 Road Parkway and 24.5 Road Widening

S/M Proctor S=Standard M=Modified OMC MDD Chlorides (%) 0.0159 0.1012 0.0054 0.0787 0.0332 0.0334 0.0157 PROJECT LOCATION Grand Junction, Colorado 8.0 8.0 8.2 8.0 8.1 တ H ζ. ∞ Resistivity (ohm-cm) 580 @ 26.4% 530 @ 19.6% 690 @ 19.0% 970 @ 19.8% 320 @ 25.3% 670 @ 25.2% 420 @ 28.2% Sulfate (%) 0.38 0.16 0.26 0.28 1.04 0.14 51 Unconfined Compressive Strength (psi) 103.3 109.5 105.8 105.9 103.0 107.2 Dry Density (pcf) 103.7 101.4 114.2 98.3 95.8 oj. 97. Water Content (%) 18.9 19.6 29.5 24.9 19.5 16.9 18.3 10.8 28.5 13.1 21.1 4.8 9.2 7.1 AASHTO A-6 (17) A-6 (10) A-6 (8) A-6 (13) A-4 (0) A-6 (17) A-6 (10) A-4 (7) A-6 (13) A-6 (9) A-6 (7) A-6 (8) A-6 (8) A-6 (8) 3 A-6 (7) A-4 Classification CL-ML CL-ML USCS 占 겅 겅 겅 占 겅 占 겅 占 占 겅 占 占 占 %<#200 Sieve 75 90 2 9/ 83 29 73 89 92 72 8 80 74 62 85 77 84 50 69 92 80 97 Swell Potential (%) 0.0 Plasticity Index 4 15 16 19 15 13 4 15 10 9 16 12 7 12 4 / Plastic Limit 13 13 12 19 19 9 4 8 20 15 2 8 9 18 16 5 Liquid Limit 19 28 28 38 26 27 27 33 30 28 37 33 37 32 30 27 PROJECT NUMBER 599.37 Depth (ft) 2-10 2-10 0-10 4-10 0-7 2-9 0-5 9-0 0-5 0-7 0-5 0-3 0-5 0-5 0-2 12 2 က 0-4 2 7 7 20 3 4 က 4 7 က Borehole F-10 F-10 F-14 F-16 F-16 <u>5</u> LC-1 7 B-3 B-5 B-6 F-3 F-5 F-6 F-6 F-8 F-9 **B-**2 B-3 F-2 F-2 F-3 F-8 <u>Р</u> <u>F</u> F-1 F-4 F-7 F-7

SUMMARY-STANDARD LANDSCAPE CDOT SPACING 599.37 CITY OF GJ PARKWAY PROJECT GPJ 12/9/21



SUMMARY OF PHYSICAL & CHEMICAL TEST RESULTS

PROJECT NAME F.5 Road Parkway and 24.5 Road Widening

PAGE 2 OF 2

CLIENT City of Grand Junction

	æ	S/M												
	Proctor	OMC S/M												
	Proctor S=Standard M=Modified	MDD												
rado	Chlorides													
n, Colo												8.1		
Grand Junctic		(w) (ohm-cm)												
ATION	Sulfate	(%)			0.47							0.19	0.15	
PROJECT LOCATION Grand Junction, Colorado	nconfined mpressive	strength (psi)												
	Dry Doneity	(pct)		87.9						102.2				
	Water	(%)		25.0	29.0	6.4	15.1			19.6	26.6	34.4	6.2	14.8
	Classification	AASHTO	A-4 (4)			A-1-a (0)			A-6 (7)		A-6 (11)			
	Classi	nscs	CL			SP-SM			CL		CL			
	%<#200	Sieve	89	22	28	8	42	28	75		94	84		53
	Swell	(%)		-0.2						-1.7				
	Plasticity	Limit Index (%)	10			NP			13		13			
	Plastic	Limit	15			NP			15		16			
9.37	Liquid	Limit	25			NP			28		29			
SER 599	Depth	Œ	0-5	10	20	30	40	0-2	2-4	2	10	20	30	40
PROJECT NUMBER 599.37	olodoro		LC-2	TC-5	LC-2	TC-5	TC-5	FC-3	FC-3	FC-3	FC-3	FC-3	FC-3	F-O7

SUMMARY-STANDARD LANDSCAPE CDOT SPACING 599.37_CITY OF GJ PARKWAY PROJECT.GPJ 12/9/21



GDT

FMPI ATE

GJ PARKWAY

4

ATTERBERG LIMITS RESULTS AASHTO T89 Method A/T90

PROJECT NAME F.5 Road Parkway and 24.5 Road Widening **CLIENT** City of Grand Junction PROJECT NUMBER 599.37 PROJECT LOCATION Grand Junction, Colorado (CL)(сн) 50 A S T 40 С 30 Т ı Ν 20 D O E **₽** 10 CL-ML (ML)(MH) 40 100 LIQUID LIMIT Specimen Identification LL PL PI Fines | Classification **B-1** 2.0-10.0 27 13 83.3 LEAN CLAY with SAND (CL) (A-6) lacktrian14 \blacksquare **B-2** 0.0 - 7.028 13 15 68.9 | SANDY LEAN CLAY (CL) (A-6) 12 66.6 SANDY LEAN CLAY (CL) (A-6) **B-3** 2.0-9.0 28 16 \star **B-5** 3.0-10.0 33 14 19 88.6 | LEAN CLAY (CL) (A-6) 4.0-10.0 19 15 73.1 SILTY CLAY with SAND (CL-ML) (A-4) ⊚ **B-6** 4 0.0 - 5.019 ٥l F-1 38 19 88.8 | LEAN CLAY (CL) (A-6) O F-2 0.0 - 6.037 19 18 92.3 | LEAN CLAY (CL) (A-6) 0.0-4.0 33 18 \triangle F-3 15 92.2 | LEAN CLAY (CL) (A-6) \otimes F-4 0.0-5.0 37 21 16 72.2 | LEAN CLAY with SAND (CL) (A-6) ⊕ F-5 2.0-10.0 14 27 13 81.3 | LEAN CLAY with SAND (CL) (A-6) F-6 0.0 - 7.032 18 14 79.9 LEAN CLAY with GRAVEL (CL) (A-6) **⊕** F-7 0.0-5.0 30 18 12 79.6 | LEAN CLAY with SAND (CL) (A-6) 19 7 **₽** F-8 0.0 - 5.026 75.4 | SILTY CLAY with SAND (CL-ML) (A-4) F-9 0.0 - 3.033 18 15 89.5 | LEAN CLAY (CL) (A-6) ☆ ස F-10 0.0-5.0 30 20 10 79.1 | LEAN CLAY with SAND (CL) (A-4) ■ F-16 0.0-10.0 28 16 12 84.7 | LEAN CLAY with SAND (CL) (A-6) ♦ LC-1 0.0-5.0 15 27 12 76.6 | LEAN CLAY with SAND (CL) (A-6) \Diamond LC-2 0.0 - 5.025 10 68.2 | SANDY LEAN CLAY (CL) (A-4) 15 LC-2 30.0 NP NP NP 7.7 POORLY GRADED SAND with SILT and GRAVEL (SP-SM) (A-1-a LC-3 2.0-4.0 28 15 74.9 LEAN CLAY with SAND (CL) (A-6) 13



ROCKSOL TEMPLATE.GDT 12/9/21

CITY OF GJ PARKWAY PROJECT.GPJ

599.37

ATTERBERG LIMITS - STANDARD

ATTERBERG LIMITS RESULTS AASHTO T89 Method A/T90

CLIENT City of Grand Junction PROJECT NAME F.5 Road Parkway and 24.5 Road Widening PROJECT NUMBER 599.37 PROJECT LOCATION Grand Junction, Colorado 60 (CL) (CH) 50 L A S T I 40 C 30 NDEX 20 10 CL-ML (ML) (MH)20 40 80 100 LIQUID LIMIT Specimen Identification LL PLPI Fines | Classification ● LC-3 10.0 29 16 94.4 LEAN CLAY (CL) (A-6) 13



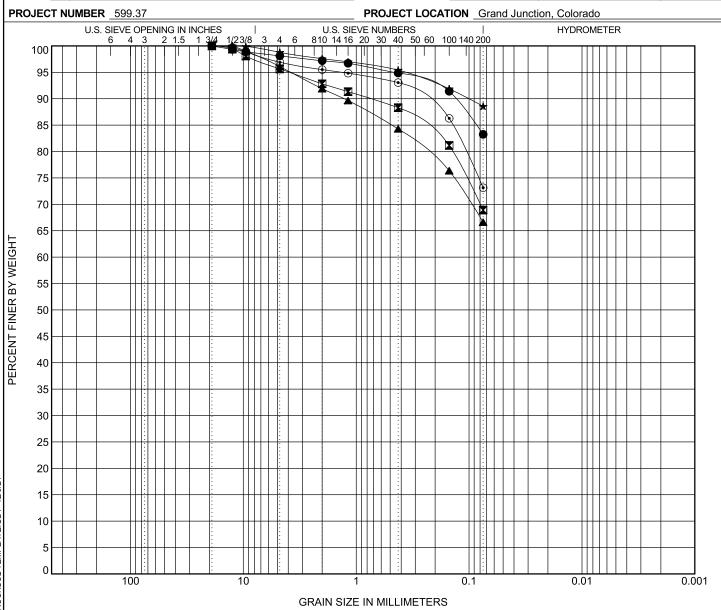
RockSol Consulting Group, Inc.

19

4.0-10.0

CLIENT City of Grand Junction

PROJECT NAME F.5 Road Parkway and 24.5 Road Widening



COBI	RIFS	GRA	VEL		SAND)	SILT OR CLAY
СОВ	DLES	coarse	fine	coarse	coarse medium fin		SILT OR CLAY

					<u>'</u>		,	•					
•	Specimen	Identification			(Classifica	ation		LL	PL	PI	Сс	Cu
•	B-1	2.0-10.0		LE	AN CLA	Y with S	AND (CL) (A	A-6)	27	13	14		
X	B-2	0.0-7.0		S	ANDY L	EAN CL	AY (CL) (A-	6)	28	13	15		
▲	B-3	2.0-9.0		S	ANDY L	EAN CL	AY (CL) (A-	6)	28	12	16		
*		3.0-10.0			LEA	VCLAY (CL) (A-6)		33	14	19		
⊙ •	B-6	4.0-10.0		SILT	Y CLAY	with SA	ND (CL-ML)	(A-4)	19	15	4		
	Specimen	Identification	D100	D60	D30	D10	%Gravel	%Coarse Sand	%Fine S	Sand	%Silt	%	Clay
•	B-1	2.0-10.0	19				2.8	2.3	11.6	;		33.3	
•	B-2	0.0-7.0	19				7.2	4.5	19.4			68.9	
▲	B-3	2.0-9.0	12.5				8.1	7.6	17.7	•	(66.6	
*	B-5	3.0-10.0	12.5				2.4	2.2	6.8			88.6	

4.5

2.5

19.9

73.1

I PARKWAY PROJECT.GPJ ROCKSOL TEMPLATE.GDT 12/9/21

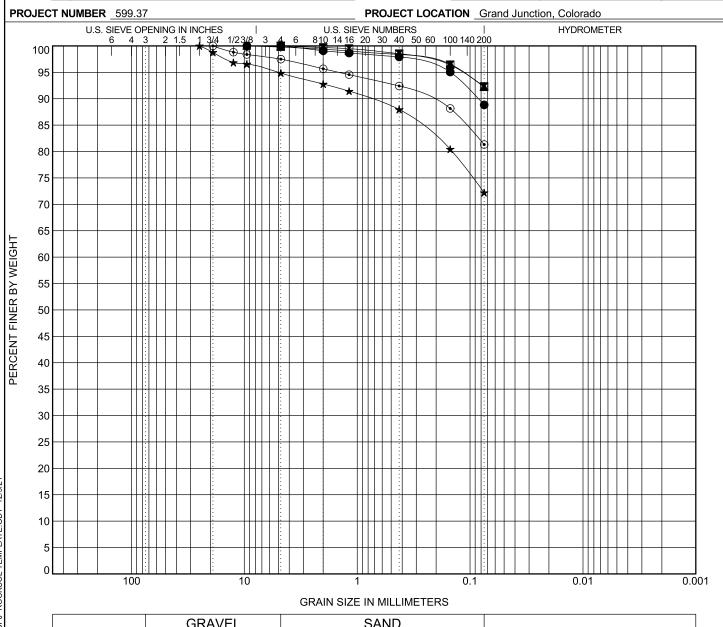
B-6



RockSol Consulting Group, Inc.

CLIENT City of Grand Junction

PROJECT NAME F.5 Road Parkway and 24.5 Road Widening



COBBLES	GRA	VEL		SAND)	SULTIORICIAY
COBBLES	coarse	fine	coarse	medium	fine	SILT OR CLAY

31		L				I .	I	l						·
7	Sp	ecimen lo	dentification			(Classifica	ation		LL	PL	PI	Сс	Cu
PAKKWA		F-1	0.0-5.0			LEAN	CLAY (CL) (A-6)		38	19	19		
		F-2	0.0-6.0			LEAN	CLAY (CL) (A-6)		37	19	18		
3 4	^	F-3	0.0-4.0			LEAN	CLAY (CL) (A-6)		33	18	15		
	- 1	F-4	0.0-5.0		LE	AN CLA	Y with S	AND (CL) (A	\-6)	37	21	16		
۶ľ (•	F-5	2.0-10.0		LE	AN CLA	Y with S	AND (CL) (A	\-6)	27	14	13		
660	Sp	ecimen la	dentification	D100	D60	D30	D10	%Gravel	%Coarse Sand	%Fine S	Sand	%Silt	%(Clay
ANDARD		F-1	0.0-5.0	9.5				0.9	1.2	9.1			38.8	
N N		F-2	0.0-6.0	4.75				0.3	1.2	6.2		9	92.3	
	A	F-3	0.0-4.0	9.5				0.6	1.0	6.2		9	92.2	
Ĭ,	*	F-4	0.0-5.0	25				7.2	4.8	15.7		-	72.2	

4.3

3.2

11.1

81.3

SRADATION - STANDARD 599.37_CITY OF GJ PARKWAY PROJECT.GPJ ROCKSOL TEMPLATE.GDT 12/9/21

⊙ F-5

19

2.0-10.0

73.7

75.4

62.4



RockSol Consulting Group, Inc.

0.075

19

0.075

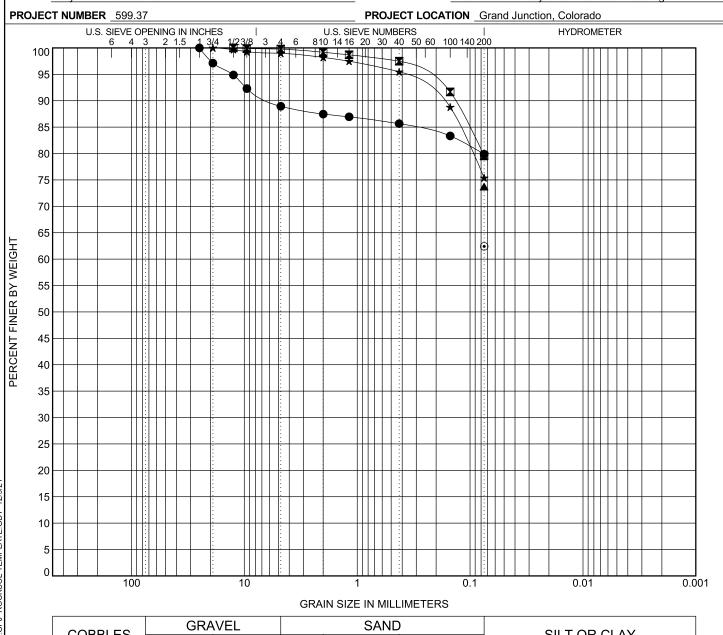
3.0

5.0

0.0-5.0

CLIENT City of Grand Junction

PROJECT NAME F.5 Road Parkway and 24.5 Road Widening



COBBLES	GRA	VEL		SAND)	SILT OR CLAY
COBBLES	coarse	fine	coarse	medium	fine	SILT OR CLAY

ŹΙ														
	Sp	oecimen Iden	tification			(Classifica	ation		LL	PL	PI	Сс	Cu
Ž V V	•	F-6	0.0-7.0		LEA	N CLAY	with GR	AVEL (CL)	(A-6)	32	18	14		
Ĭ	\blacksquare	F-7	0.0-5.0		LE	AN CLA	Y with S	30	18	12				
5[A	F-7	3.0		LE	AN CLA	Y with S	AND (CL) (A	\-6)					
- 1	*	F-8	0.0-5.0		SILT	Y CLAY	with SAN	ND (CL-ML)	(A-4)	26	19	7		
٠ <u>٠</u>	•	F-8	5.0		SILTY CLAY with SAND (CL-ML) (A-4)									
386	Sp	oecimen Iden	tification	D100	D60	D30	D10	%Gravel	%Coarse Sand	%Fine S	Sand	%Silt	%(Clay
DARD DARD	•	F-6	0.0-7.0	25				12.5	1.8	5.8		7	9.9	
NA I	×	F-7	0.0-5.0	12.5				0.8	1.7	17.9)	7	' 9.6	

1.8

2.7

20.1

GRADATION - STANDARD 599.37_CITY OF GJ PARKWAY PROJECT.GPJ ROCKSOL TEMPLATE.GDT 12/9/21

• F-8

F-7

F-8



RockSol Consulting Group, Inc.

CLIENT City of Grand Junction

PROJECT NAME F.5 Road Parkway and 24.5 Road Widening

PROJECT NUMBER 599.37 PROJECT LOCATION Grand Junction, Colorado U.S. SIEVE NUMBERS | 810 14 16 20 30 40 50 60 100 140 200 U.S. SIEVE OPENING IN INCHES 6 4 3 2 1.5 1 3/4 HYDROMETER 1/23/8 100 Ž 95 90 85 80 75 70 65 PERCENT FINER BY WEIGHT 60 55 50 45 40 35 30 25 20 RKWAY PROJECT.GPJ ROCKSOL TEMPLATE.GDT 12/9/21 15 10 5 0.01 0.001 **GRAIN SIZE IN MILLIMETERS**

CORRIES	GRA	VEL		SAND)	SILT OR CLAY
COBBLES	coarse	fine	coarse	medium	fine	SILT OR CLAT

ÄL	Specime	n Identification			Classifica	ation		LL	PL	PI	Сс	Cu
GJ PARKWAY PR	● F-9	0.0-3.0		LEA	N CLAY (CL) (A-6)		33	18	15		
PA	▼ F-10	0.0-5.0	LE	AN CLA	Y with S	AND (CL)	(A-4)	30	20	10		
9 F	▲ F-10	2.0	LE	AN CLA	Y with S	AND (CL)	(A-4)					
ŽĮ.	★ F-16	0.0-10.0	LE	AN CLA	Y with S	AND (CL)	(A-6)	28	16	12		
99.37_(2.0	LE	AN CLA	Y with S	AND (CL)	(A-6)					
\approx Γ												

		pecimen	identification	D100	D60	D30	D10	%Gravel	%Coarse Sand	%Fine Sand	%Silt	%Clay
DARD		F-9	0.0-3.0	9.5				0.5	1.1	8.9	89	9.5
STAND/	X	F-10	0.0-5.0	4.75				0.8	2.7	17.4	79	9.1
S-NOI	A	F-10	2.0	0.075							76	6.5
DATIC	*	F-16	0.0-10.0	4.75				0.3	1.1	13.9	84	4.7
GRAE	•	F-16	2.0	0.075							96	6.5

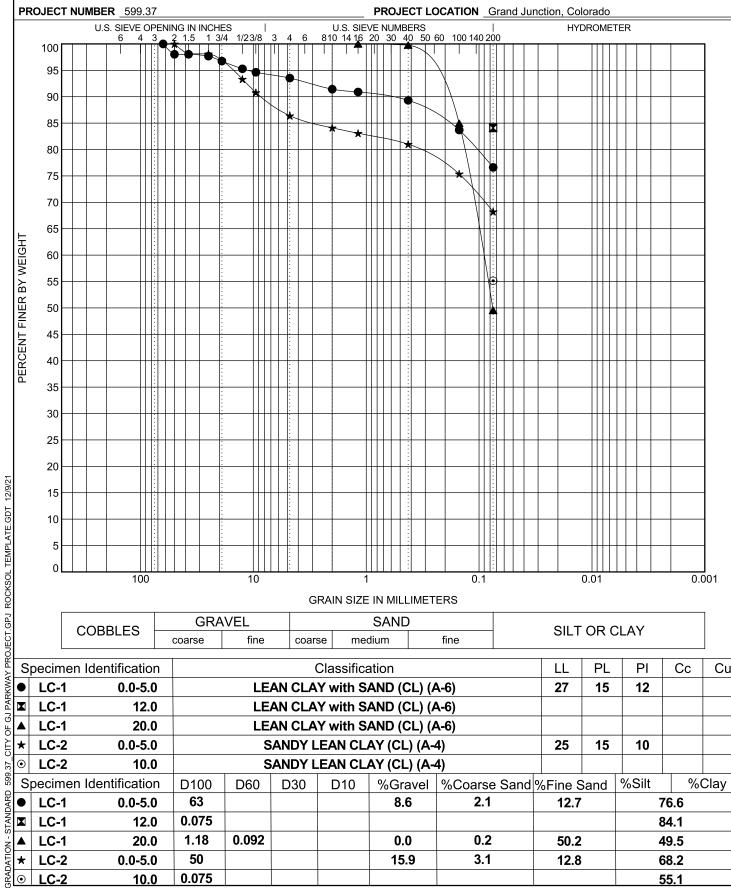


RockSol Consulting Group, Inc.

CLIENT City of Grand Junction

COBBLES

PROJECT NAME F.5 Road Parkway and 24.5 Road Widening



GRAVEL SAND SILT OR CLAY fine medium fine coarse

Z L														
<u>ا</u> خ	S	Specimen Identification Classification									PL	PI	Сс	Cu
\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \	•	LC-1	LC-1 0.0-5.0 LEAN CLAY with SAND (CL) (A-6)											
¥[X	LC-1 12.0 LEAN CLAY with SAND (CL) (A-6)												
5	▲	LC-1 20.0 LEAN CLAY with SAND (CL) (A-6)												
<u>`</u>	*	LC-2	0.0-5.0		S	ANDY L	EAN CL	AY (CL) (A-	4)	25	15	10		
نة م	⊙ LC-2 10.0 SANDY LEAN CLAY (CL) (A-4)													
		pecimen	Identification	D100	D100 D60 D30 D10 %Gravel %Coarse Sand %						Sand	%Silt	%(Clay
ᇫ	● LC-1 0.0-5.0 63 8.6 2.1								12.7	•		76.6		

coarse

0.075 LC-1 12.0 \blacksquare 84.1 20.0 1.18 0.092 0.2 LC-1 0.0 50.2 49.5 LC-2 0.0-5.0 50 15.9 3.1 12.8 68.2 0.075 • LC-2 10.0 55.1



RockSol Consulting Group, Inc.

CLIENT City of Grand Junction

PROJECT NAME F.5 Road Parkway and 24.5 Road Widening

PROJECT NUMBER 599.37 PROJECT LOCATION Grand Junction, Colorado U.S. SIEVE OPENING IN INCHES 6 4 3 2 1 5 1 3/4 U.S. SIEVE NUMBERS | 810 14 16 20 30 40 50 60 100 140 200 HYDROMETER 1/23/8 100 95 90 85 80 75 × 70 65 PERCENT FINER BY WEIGHT 60 55 50 45 \blacksquare 40 35 30 Ì 25 20 PROJECT.GPJ ROCKSOL TEMPLATE.GDT 12/9/21 15 10 5 0.01 0.001 **GRAIN SIZE IN MILLIMETERS**

COBBLES	GRA	VEL		SAND)	SILT OR CLAY
COBBLES	coarse	fine	coarse	medium	fine	SILT OR CLAT

31									l l					_
OF GU PARAWAI PROJ	S	pecimen	Identification			(Classifica	LL	PL	PI	Сс	Cu		
	•	LC-2	20.0		S	ANDY L	EAN CL							
	X	LC-2	30.0 PC	ORLY G	RADED	SAND	with SIL7	Γ and GRAV	/EL (SP-SM) (A-1	-a) NP	NP	NP	0.33	57.77
5 .	lack	LC-2	40.0	PC	ORLY G	RADED	SAND v	vith SILT ar	nd GRAVEL					
[.	*	LC-3	0.0-2.0			SA	ANDY GF	RAVEL						
	<u>⊙</u> S	LC-3	2.0-4.0		LE	AN CLA	Y with S	AND (CL) (A	A-6)	28	15	13		
		pecimen	Identification	D100	D60	D30	D10	%Gravel	%Coarse Sand	%Fine \$	Sand	%Silt %Cla		Clay
	•	LC-2	20.0	0.075								58.4		
	×	LC-2	30.0	37.5	37.5 6.442 0.484			53.3	18.7	20.3		7.7		
<u>.</u>	A	LC-2	40.0	0.075	.075							'	42.1	
ξ[.	<u>★</u>	LC-3	0.0-2.0	37.5	0.093			12.4		,	58.1			
[<u> </u>	LC-3	2.0-4.0	19				10.4	3.8	10.9		74.9		



RockSol Consulting Group, Inc.

CLIENT City of Grand Junction

PROJECT NAME F.5 Road Parkway and 24.5 Road Widening

PROJECT NUMBER 599.37 PROJECT LOCATION Grand Junction, Colorado U.S. SIEVE NUMBERS | 810 14 16 20 30 40 50 60 100 140 200 U.S. SIEVE OPENING IN INCHES 6 4 3 2 1.5 1 3/4 HYDROMETER 1/23/8 3 100 95 90 85 80 75 70 65 PERCENT FINER BY WEIGHT 60 55 50 45 40 35 30 25 20 CITY OF GJ PARKWAY PROJECT.GPJ ROCKSOL TEMPLATE.GDT 12/9/21 15 10 5 0.01 0.001 **GRAIN SIZE IN MILLIMETERS GRAVEL** SAND **COBBLES** SILT OR CLAY fine medium fine coarse coarse

시	Sp	oecimen l	dentification	Classification	LL	PL	PI	Сс	Cu
%X X	•	LC-3	dentification 10.0 20.0	LEAN CLAY (CL) (A-6)	29	16	13		
		LC-3	20.0	LEAN CLAY					
OF G	A	LC-3	40.0	LEAN CLAY					
ا≾									

.37												
299	S	pecimen Ide	entification	D100	D60	D30	D10	%Gravel	%Coarse Sand	%Fine Sand	%Silt	%Clay
DAR	•	LC-3	10.0	9.5				1.5	0.7	3.5	94	1.4
TAN	X	LC-3	20.0	0.075							83	3.7
S-N	A	LC-3	40.0	0.075							53	3.2
ATIO												
J.K.												



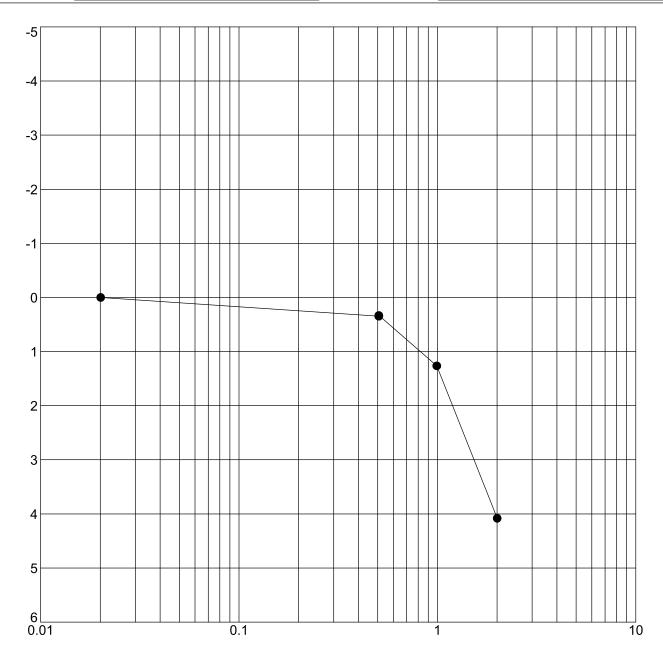
SWELL - CONSOLIDATION TEST

CLIENT City of Grand Junction

PROJECT NAME F.5 Road Parkway and 24.5 Road Widening

PROJECT NUMBER 599.37

PROJECT LOCATION Grand Junction, Colorado



STRESS, ksf

Specimen Ide	ntification	Classification	Swell/Consol. (%)	$\gamma_{d}(pcf)$	MC%
● F-1	3	CLAY	0.0	97.9	19.5

SWELL - STANDARD 599.37_CITY OF GJ PARKWAY PROJECT.GPJ ROCKSOL TEMPLATE.GDT 12/9/21

STRAIN, %



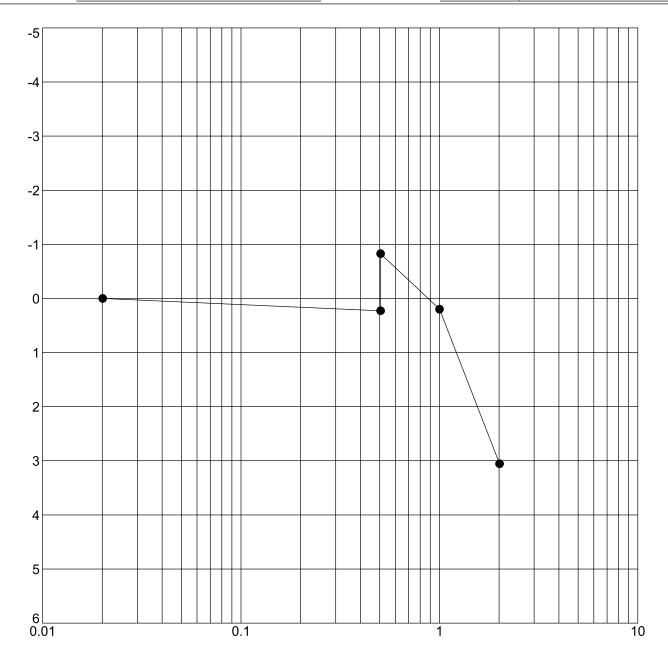
SWELL - CONSOLIDATION TEST

CLIENT City of Grand Junction

PROJECT NAME F.5 Road Parkway and 24.5 Road Widening

PROJECT NUMBER 599.37

PROJECT LOCATION Grand Junction, Colorado



STRESS, ksf

S	Specimen Ide	entification	Classification	Swell/Consol. (%)	γ _d (pcf)	MC%
•	F-3	4	CLAY		103.3	13.1

SWELL - STANDARD 599.37_CITY OF GJ PARKWAY PROJECT.GPJ ROCKSOL TEMPLATE.GDT 12/9/21

STRAIN, %



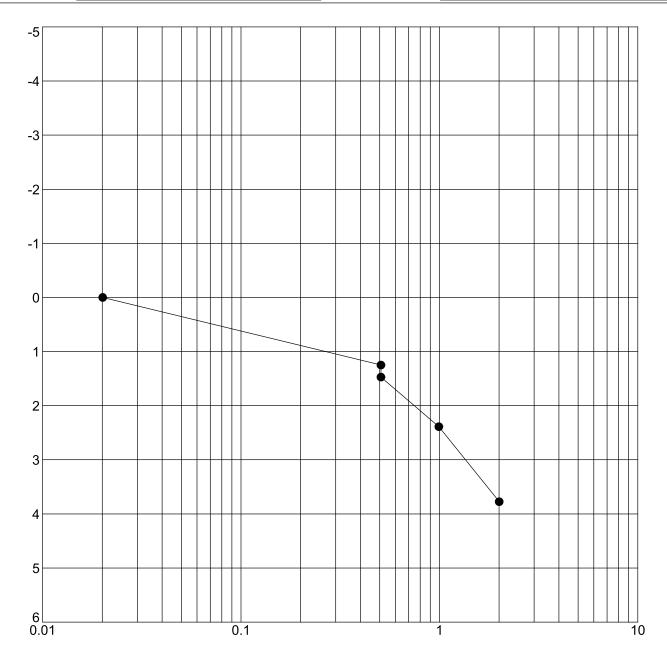
SWELL - CONSOLIDATION TEST

CLIENT City of Grand Junction

PROJECT NAME F.5 Road Parkway and 24.5 Road Widening

PROJECT NUMBER 599.37

PROJECT LOCATION Grand Junction, Colorado



STRESS, ksf

Specimen Identification Classification		Swell/Consol. (%)	$\gamma_{d}(pcf)$	MC%	
■ LC-2 10 SANDY LEAN CLAY (CL) (A-4)		-0.2	87.9	25.0	

SWELL - STANDARD 599.37_CITY OF GJ PARKWAY PROJECT.GPJ ROCKSOL TEMPLATE.GDT 12/9/21

STRAIN, %



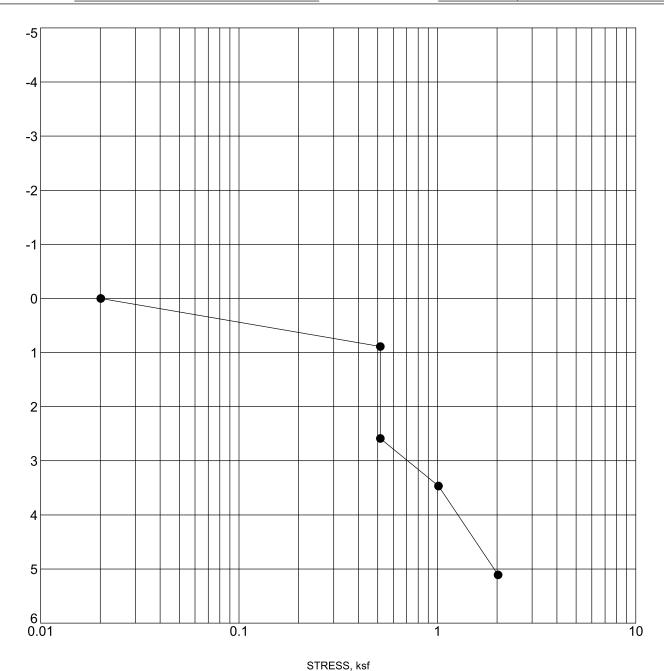
SWELL - CONSOLIDATION TEST

CLIENT City of Grand Junction

PROJECT NAME F.5 Road Parkway and 24.5 Road Widening

PROJECT NUMBER 599.37

PROJECT LOCATION Grand Junction, Colorado



Specimen Identification		Classification		$\gamma_{d}(pcf)$	MC%
● LC-3	5	CLAY, with SAND	-1.7	102.2	19.6

SWELL - STANDARD 599.37_CITY OF GJ PARKWAY PROJECT.GPJ ROCKSOL TEMPLATE.GDT 12/9/21

STRAIN, %



APPENDIX C

20 and 30-YEAR
FLEXIBLE ME-PAVEMENT DESIGN OUTPUT
SHEETS F ½ ROAD





Design Inputs

Design Life: 20 years Base construction: May, 2022 Climate Data 39.134, -108.538

Sources (Lat/Lon) Design Type: **FLEXIBLE** Pavement construction: June, 2022

> Traffic opening: September, 2022

Design Structure

Layer type	Material Type	Thickness (in)
Flexible	R3 Level 1 SX(100) PG 64-28	2.0
Flexible	R2 Level 1 SX(100) PG 64-22	5.5
NonStabilized	Crushed gravel	8.0
NonStabilized	A-1-b	14.0
Subgrade	A-6 (R-Value = 5)	Semi-infinite

Volumetric at Construction:			
Effective binder content (%)	10.7		
Air voids (%)	5.7		

Traffic

Age (year)	Heavy Trucks (cumulative)
2022 (initial)	2,100
2032 (10 years)	3,814,160
2042 (20 years)	8,555,580

Design Outputs

Distress Prediction Summary

Distress Type		Distress @ Specified Reliability		Reliability (%)		
	Target	Predicted	Target	Achieved	Satisfied?	
Terminal IRI (in/mile)	200.00	174.46	90.00	97.78	Pass	
Permanent deformation - total pavement (in)	0.80	0.68	90.00	98.99	Pass	
AC bottom-up fatigue cracking (% lane area)	25.00	21.26	90.00	94.31	Pass	
AC thermal cracking (ft/mile)	1500.00	151.56	90.00	100.00	Pass	
AC top-down fatigue cracking (ft/mile)	3000.00	382.11	90.00	100.00	Pass	
Permanent deformation - AC only (in)	0.65	0.49	90.00	99.70	Pass	

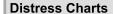
Report generated on: 7/12/2023 2:53 PM

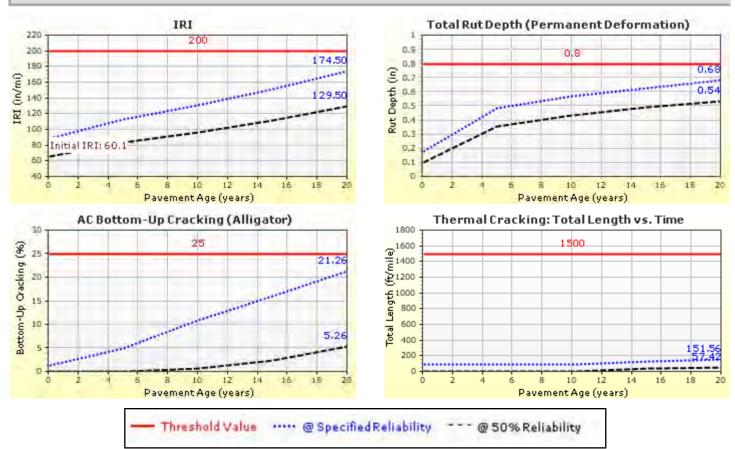
Version: 2.3.1+66

Created by: on: 8/26/2015 12:00 AM









Created^{by:} on: 8/26/2015 12:00 AM

Approved on: 8/26/2015 12:00 AM

Page 2 of 22



File Name: C:\Users\goldbaum\Documents\My PMED Designs\My ME Design\Projects\F.5 Road\F.5 Road (Updated).dgpx



Traffic Inputs

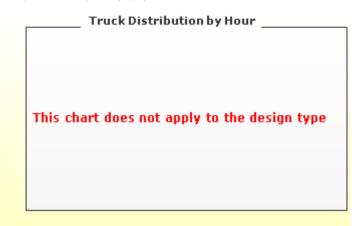
Graphical Representation of Traffic Inputs

Initial two-way AADTT: 2,100

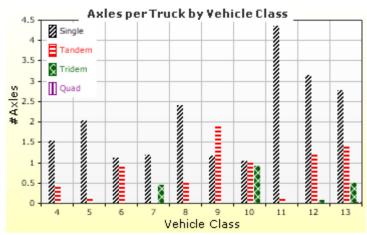
Number of lanes in design direction: 2



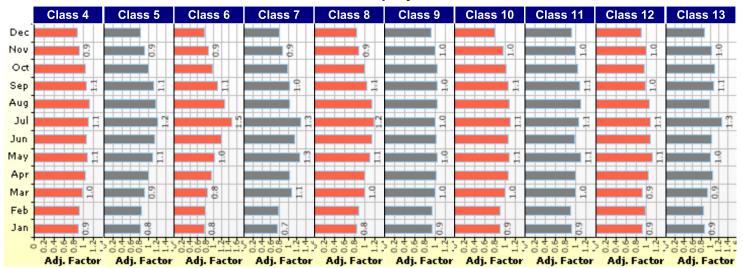
Percent of trucks in design direction (%): 50.0
Percent of trucks in design lane (%): 90.0
Operational speed (mph) 35.0



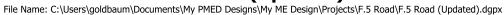




Traffic Volume Monthly Adjustment Factors









Tabular Representation of Traffic Inputs

Volume Monthly Adjustment Factors

Level 3: Default MAF

Month	Vehicle Class									
WIOTILIT	4	5	6	7	8	9	10	11	12	13
January	0.9	0.8	0.8	0.7	0.8	0.9	0.9	0.9	0.9	0.9
February	0.9	0.8	0.8	0.8	0.9	0.9	0.9	0.9	1.0	0.8
March	1.0	0.9	0.8	1.1	1.0	1.0	1.0	1.0	0.9	0.9
April	1.0	1.0	0.9	1.0	1.0	1.0	1.1	1.0	1.0	1.1
May	1.1	1.1	1.0	1.3	1.1	1.0	1.1	1.1	1.1	1.0
June	1.1	1.1	1.2	1.1	1.1	1.0	1.1	1.0	1.1	1.0
July	1.1	1.2	1.5	1.3	1.2	1.0	1.1	1.1	1.1	1.3
August	1.1	1.2	1.3	1.0	1.1	1.0	1.1	1.1	1.1	1.0
September	1.1	1.1	1.1	1.0	1.1	1.0	1.1	1.1	1.0	1.1
October	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	0.9	1.1
November	0.9	0.9	0.9	0.9	0.9	1.0	1.0	1.0	1.0	1.0
December	0.9	0.8	0.8	0.8	0.8	0.9	0.8	0.9	0.9	0.9

Distributions by Vehicle Class

Truck Distribution by Hour does not apply

Vehicle Class	AADTT Distribution (%)	Growth Factor		
	(Level 3) `	Rate (%)	Function	
Class 4	2.1%	2.2%	Compound	
Class 5	56.1%	2.2%	Compound	
Class 6	4.4%	2.2%	Compound	
Class 7	0.3%	2.2%	Compound	
Class 8	14.2%	2.2%	Compound	
Class 9	21.1%	2.2%	Compound	
Class 10	0.7%	2.2%	Compound	
Class 11	0.7%	2.2%	Compound	
Class 12	0.2%	2.2%	Compound	
Class 13	0.2%	2.2%	Compound	

Axle Configuration

Traffic Wander				
Mean wheel location (in)	18.0			
Traffic wander standard deviation (in)	10.0			
Design lane width (ft)	12.0			

Average axle width (ft)	8.5
Dual tire spacing (in)	12.0
Tire pressure (psi)	120.0

Axle Configuration

Wheelbase does not apply

Number of Axles per Truck

Vehicle Class	Single Axle	Tandem Axle	Tridem Axle	Quad Axle
Class 4	1.53	0.45	0	0
Class 5	2.02	0.16	0.02	0
Class 6	1.12	0.93	0	0
Class 7	1.19	0.07	0.45	0.02
Class 8	2.41	0.56	0.02	0
Class 9	1.16	1.88	0.01	0
Class 10	1.05	1.01	0.93	0.02
Class 11	4.35	0.13	0	0
Class 12	3.15	1.22	0.09	0
Class 13	2.77	1.4	0.51	0.04

Average Axle Spacing		
Tandem axle spacing (in)	51.6	
Tridem axle spacing (in)	49.2	
Quad axle spacing (in)	49.2	

Report generated on: 7/12/2023 2:53 PM

Version: 2.3.1+66

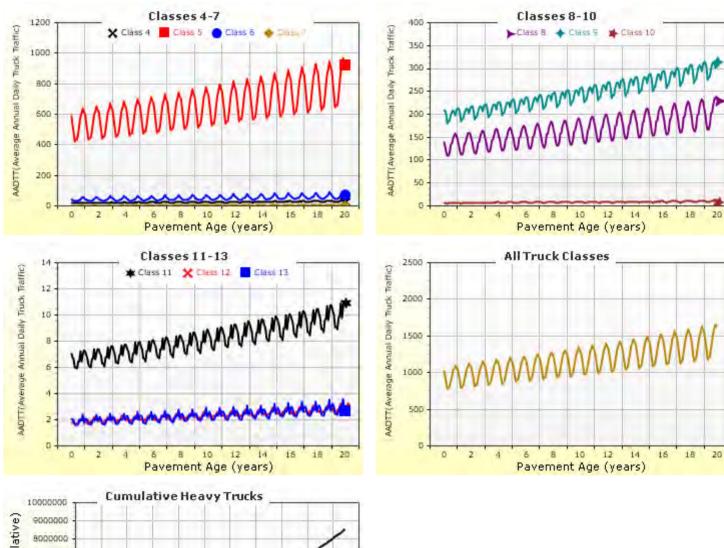
Created by: on: 8/26/2015 12:00 AM

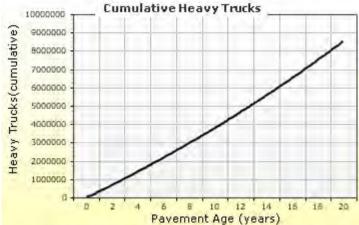
File Name: C:\Users\goldbaum\Documents\My PMED Designs\My ME Design\Projects\F.5 Road\F.5 Road (Updated).dgpx



AADTT (Average Annual Daily Truck Traffic) Growth

* Traffic cap is not enforced







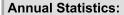
File Name: C:\Users\goldbaum\Documents\My PMED Designs\My ME Design\Projects\F.5 Road\F.5 Road (Updated).dgpx



Climate Inputs

Climate Data Sources:

Climate Station Cities: Location (lat lon elevation(ft))
GRAND JUNCTION, CO 39.13400 -108.53800 4839

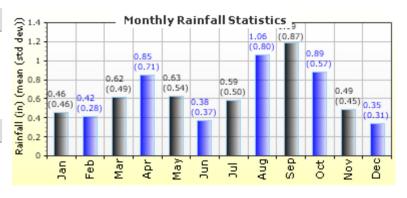


Mean annual air temperature (°F) 53.75

Mean annual precipitation (in) 7.96

Freezing index (°F - days) 360.58

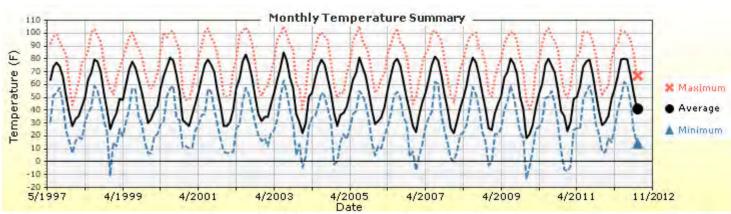
Average annual number of freeze/thaw cycles: 111.77

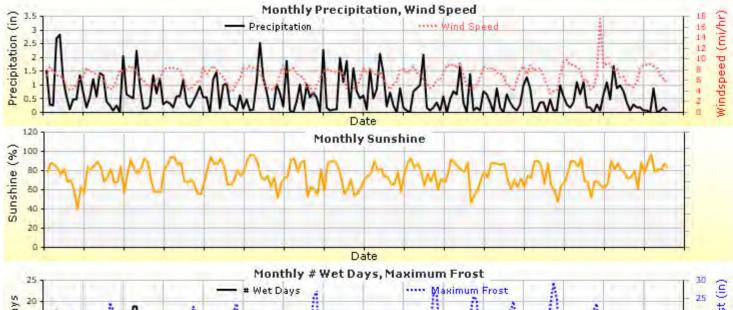


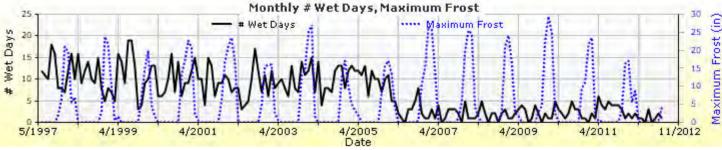
Water table depth (ft)

10.00

Monthly Climate Summary:



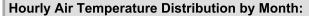


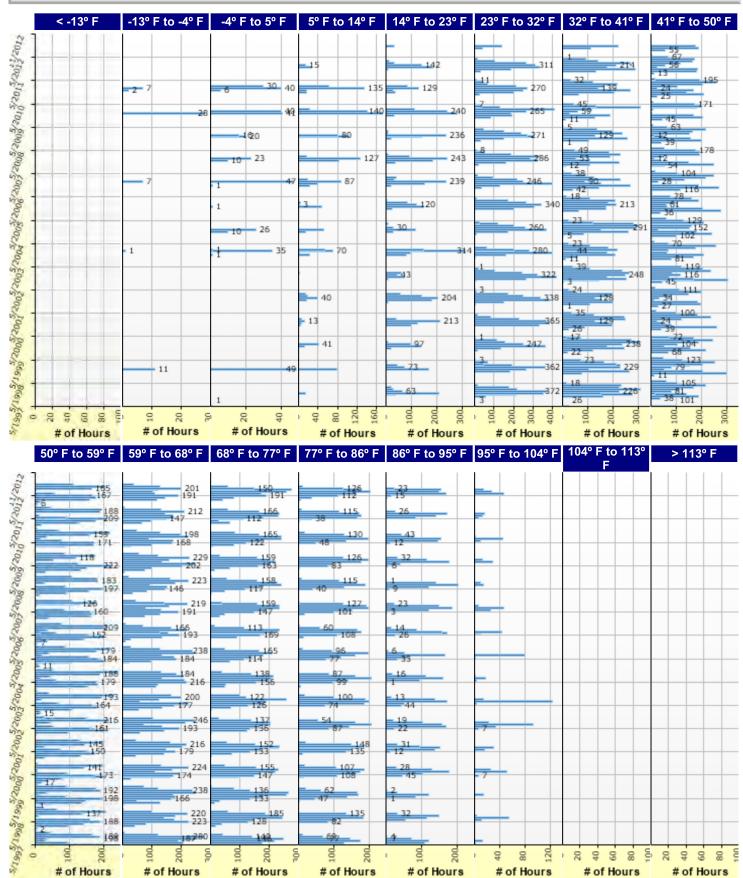


Created by: on: 8/26/2015 12:00 AM















Design Properties

HMA Design Properties

AC surface shortwave absorptivity

Use Multilayer Rutting Model	False
Using G* based model (not nationally calibrated)	False
Is NCHRP 1-37A HMA Rutting Model Coefficients	True
Endurance Limit	-
Use Reflective Cracking	True
	-
Structure - ICM Properties	

0.85

Layer Name	II avar Ivna	Interface Friction
Layer 1 Flexible : R3 Level 1 SX (100) PG 64-28	Flexible (1)	1.00
Layer 2 Flexible : R2 Level 1 SX (100) PG 64-22	Flexible (1)	1.00
Layer 3 Non-stabilized Base : Crushed gravel	Non-stabilized Base (4)	
Layer 4 Non-stabilized Base : A-1-b	Non-stabilized Base (4)	1.00
Layer 5 Subgrade : A-6 (R-Value = 5)	Subgrade (5)	-

Report generated on: 7/12/2023 2:53 PM

Version: 2.3.1+66 Created by: on: 8/26/2015 12:00 AM



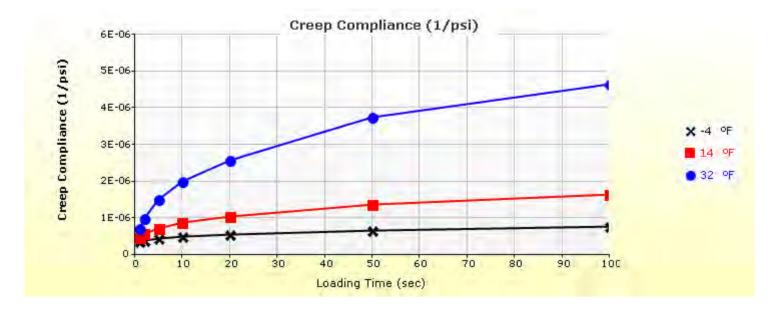




Thermal Cracking (Input Level: 1)

Indirect tensile strength at 14 °F (psi)	519.00
Thermal Contraction	
Is thermal contraction calculated?	True
Mix coefficient of thermal contraction (in/in/ºF)	-
Aggregate coefficient of thermal contraction (in/in/°F)	5.0e-006
Voids in Mineral Aggregate (%)	16.4

	Creep Compliance (1/psi)		
Loading time (sec)	-4 °F	14 °F	32 °F
1	3.61e-007	4.73e-007	7.12e-007
2	4.04e-007	5.74e-007	9.97e-007
5	4.51e-007	7.35e-007	1.52e-006
10	5.11e-007	8.78e-007	1.99e-006
20	5.67e-007	1.04e-006	2.59e-006
50	6.57e-007	1.37e-006	3.75e-006
100	7.68e-007	1.66e-006	4.66e-006



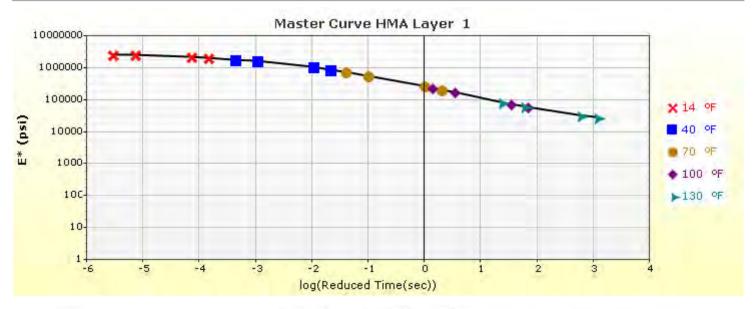
Report generated on: 7/12/2023 2:53 PM

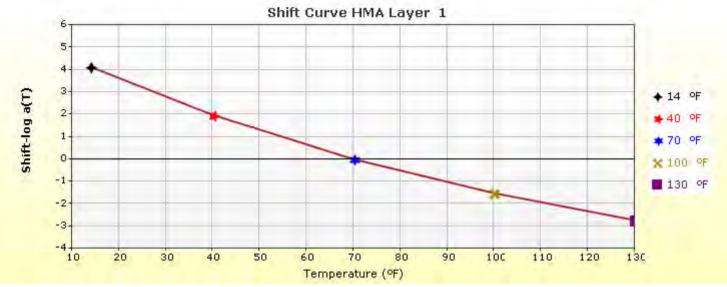
Version: 2.3.1+66 Created by: on: 8/26/2015 12:00 AM

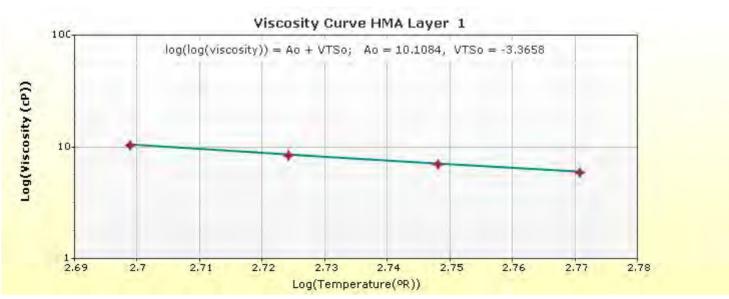




HMA Layer 1: Layer 1 Flexible: R3 Level 1 SX(100) PG 64-28



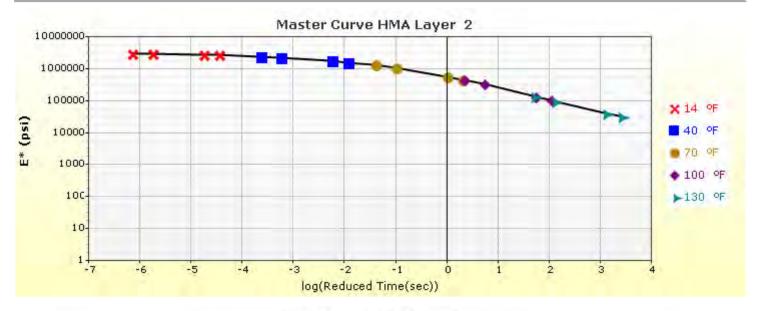


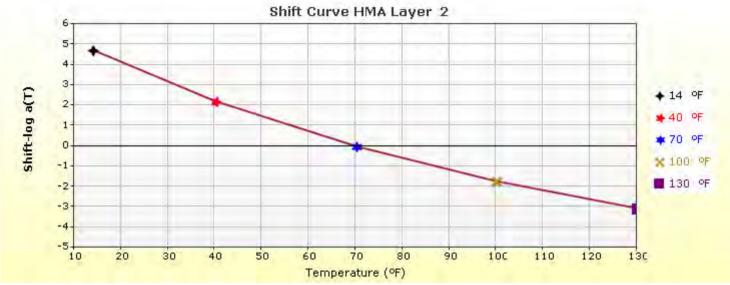


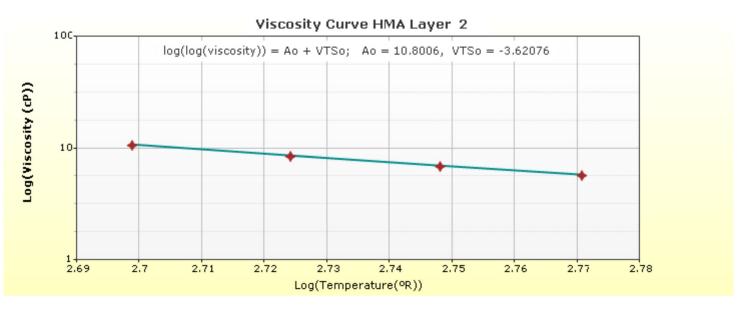




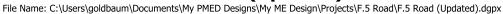
HMA Layer 2: Layer 2 Flexible: R2 Level 1 SX(100) PG 64-22





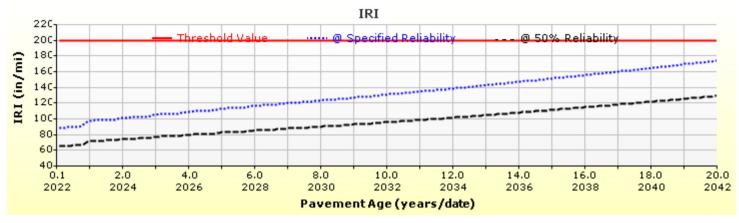


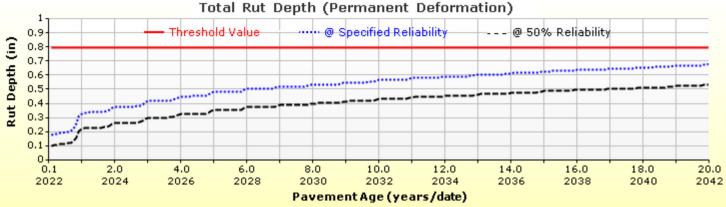


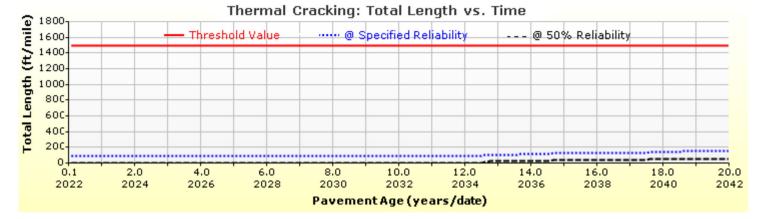




Analysis Output Charts







Created^{by:} on: 8/26/2015 12:00 AM

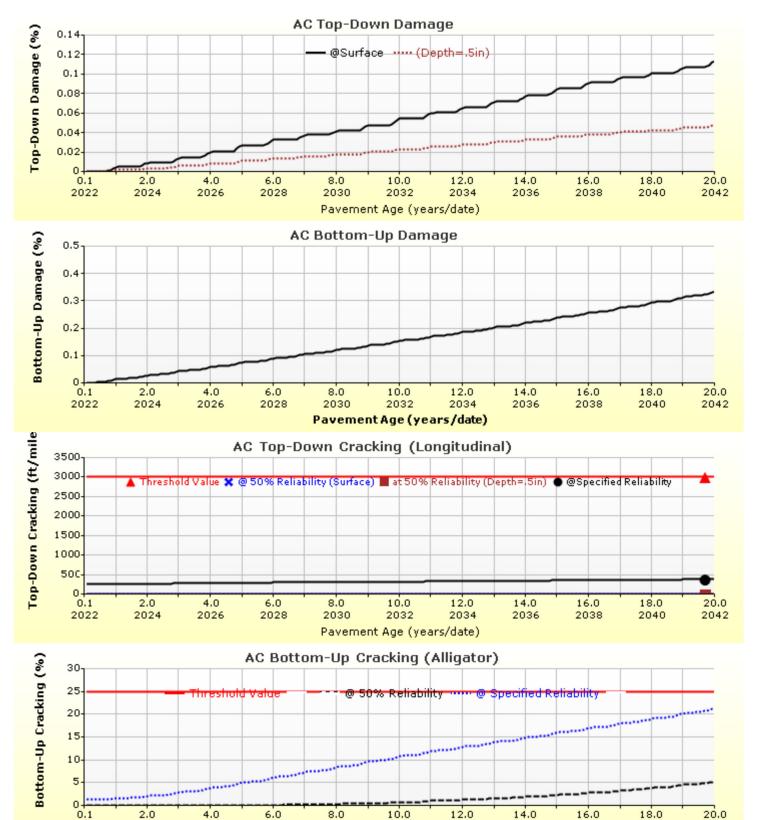
Approved by: on: 8/26/2015 12:00 AM

Page 12 of 22









2022

2026

2028

2024

2030

2032

Pavement Age (years/date)

2034

2036

2038

2040

2042





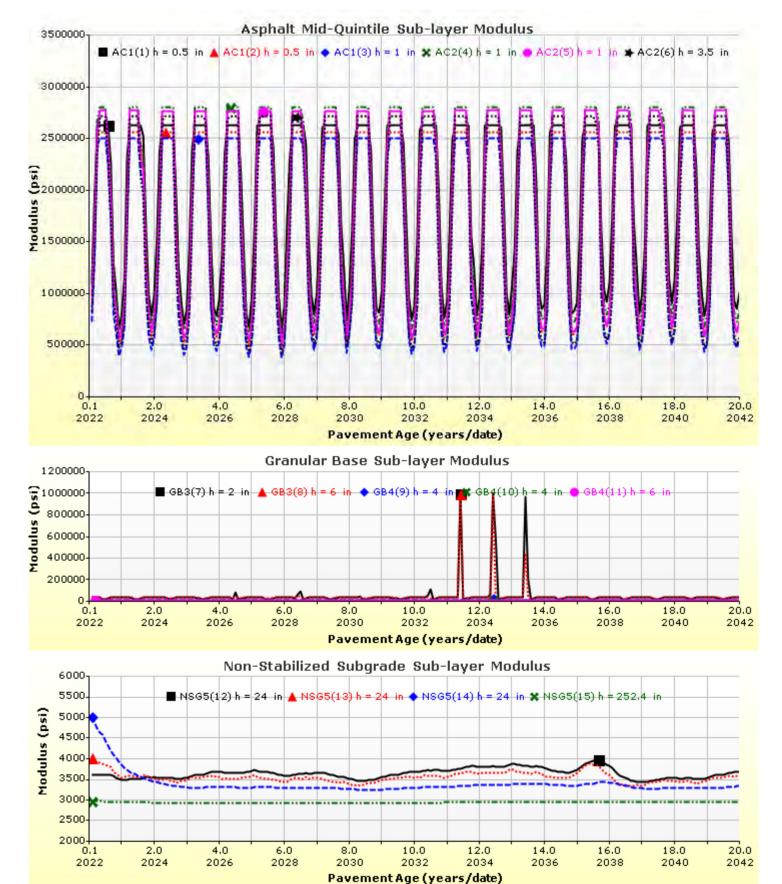


Created by: on: 8/26/2015 12:00 AM



File Name: C:\Users\goldbaum\Documents\My PMED Designs\My ME Design\Projects\F.5 Road\F.5 Road (Updated).dgpx











Layer Information

Layer 1 Flexible: R3 Level 1 SX(100) PG 64-28

Asphalt			
Thickness (in)	2.0		
Unit weight (pcf)	145.0		
Poisson's ratio	ls Calculated?	True	
	Ratio	-	
	Parameter A	-1.63	
	Parameter B	3.84E-06	

Asphalt Dynamic Modulus (Input Level: 1)

T (°F)	0.5 Hz	1 Hz	10 Hz	25 Hz
14	1687360	2134249	2493389	2608869
40	697463	1127680	1612900	1802220
70	173403	334774	616373	765125
100	54259	93163	175106	227742
130	27890	38645	60413	74657

Asphalt Binder

Temperature (°F)	Binder Gstar (Pa)	Phase angle (deg)
147.2	3051	81.6
158	1495	83.1
168.8	772	85

General Info

Name	Value
Reference temperature (°F)	70
Effective binder content (%)	10.7
Air voids (%)	5.7
Thermal conductivity (BTU/hr-ft-°F)	0.67
Heat capacity (BTU/lb-°F)	0.23

Identifiers

Field	Value
Display name/identifier	R3 Level 1 SX(100) PG 64-28
Description of object	Mix ID # FS1959
Author	CDOT
Date Created	4/3/2013 12:00:00 AM
Approver	CDOT
Date approved	4/3/2013 12:00:00 AM
State	Colorado
District	
County	
Highway	
Direction of Travel	
From station (miles)	
To station (miles)	
Province	
User defined field 1	sx
User defined field 2	
User defined field 3	
Revision Number	0

Report generated on: 7/12/2023 2:53 PM

Version: 2.3.1+66 Created by: on: 8/26/2015 12:00 AM







Layer 2 Flexible: R2 Level 1 SX(100) PG 64-22

Asphalt				
Thickness (in)	5.5			
Unit weight (pcf)	145.0	145.0		
Poisson's ratio	Is Calculated?	True		
	Ratio	-		
	Parameter A	-1.63		
	Parameter B	3.84E-06		

Asphalt Dynamic Modulus (Input Level: 1)

T (°F)	0.5 Hz	1 Hz	10 Hz	25 Hz
14	2333549	2642179	2861449	2927779
40	1309490	1791270	2219829	2365949
70	379514	695090	1127310	1318450
100	87238	174824	349546	452545
130	29326	49265	92795	122034

Asphalt Binder

Temperature (°F)	Binder Gstar (Pa)	Phase angle (deg)
147.2	1857	81.6
158	889	83.1
168.8	451	85

General Info

Name	Value
Reference temperature (°F)	70
Effective binder content (%)	11.2
Air voids (%)	5.1
Thermal conductivity (BTU/hr-ft-°F)	0.67
Heat capacity (BTU/lb-ºF)	0.23

Identifiers

Field	Value
Display name/identifier	R2 Level 1 SX(100) PG 64-22
Description of object	Mix ID # FS1938
Author	CDOT
Date Created	4/3/2013 12:00:00 AM
Approver	CDOT
Date approved	4/3/2013 12:00:00 AM
State	Colorado
District	
County	
Highway	
Direction of Travel	
From station (miles)	
To station (miles)	
Province	
User defined field 1	sx
User defined field 2	
User defined field 3	
Revision Number	2

Report generated on: 7/12/2023 2:53 PM

Version: 2.3.1+66

Created by: on: 8/26/2015 12:00 AM





Layer 3 Non-stabilized Base : Crushed gravel

Unbound	
Layer thickness (in)	8.0
Poisson's ratio	0.35
Coefficient of lateral earth pressure (k0)	0.5

Madulina	/122114	1 00/01	I. 2\
Modulus	IIIDUL	Leve	i. 31

Analysis Type:	Modify input values by temperature/moisture
Method:	Resilient Modulus (psi)

Resilient Modulus (psi)
25000.0

Use Correction factor for NDT modulus?	-
NDT Correction Factor:	-

Identifiers

Field	Value
Display name/identifier	Crushed gravel
Description of object	Default material
Author	AASHTO
Date Created	1/1/2011 12:00:00 AM
Approver	
Date approved	1/1/2011 12:00:00 AM
State	
District	
County	
Highway	
Direction of Travel	
From station (miles)	
To station (miles)	
Province	
User defined field 1	
User defined field 2	
User defined field 3	
Revision Number	41

Sieve

Liquid Limit	6.0
Plasticity Index	1.0
Is layer compacted?	True

	Is User Defined?	Value
Maximum dry unit weight (pcf)	False	127.7
Saturated hydraulic conductivity (ft/hr)	False	5.054e-02
Specific gravity of solids	False	2.7
Water Content (%)	False	7.4

User-defined Soil Water Characteristic Curve (SWCC)		
Is User Defined? False		
af	7.2555	
bf	1.3328	
cf	0.8242	
hr	117.4000	

Sieve Size	% Passing
0.001mm	
0.002mm	
0.020mm	
#200	8.7
#100	
#80	12.9
#60	
#50	
#40	20.0
#30	
#20	
#16	
#10	33.8
#8	
#4	44.7
3/8-in.	57.2
1/2-in.	63.1
3/4-in.	72.7
1-in.	78.8
1 1/2-in.	85.8
2-in.	91.6
2 1/2-in.	
3-in.	
3 1/2-in.	97.6







Layer 4 Non-stabilized Base : A-1-b

Unbound	
Layer thickness (in)	14.0
Poisson's ratio	0.35
Coefficient of lateral earth pressure (k0)	0.5

Modulus ((Input	Level:	3)
modulus (IIIPUL	LC V CI.	

Analysis Type:	Modify input values by temperature/moisture
Method:	Resilient Modulus (psi)

Resilient Modulus (psi)
9494.0

Use Correction factor for NDT modulus?	-
NDT Correction Factor:	-

Identifiers

Field	Value
Display name/identifier	A-1-b
Description of object	Default material
Author	AASHTO
Date Created	1/1/2011 12:00:00 AM
Approver	
Date approved	1/1/2011 12:00:00 AM
State	
District	
County	
Highway	
Direction of Travel	
From station (miles)	
To station (miles)	
Province	
User defined field 1	
User defined field 2	
User defined field 3	
Revision Number	0

Sieve

Liquid Limit	11.0
Plasticity Index	1.0
Is layer compacted?	True

	Is User Defined?	Value
Maximum dry unit weight (pcf)	False	124.2
Saturated hydraulic conductivity (ft/hr)	False	2.303e-03
Specific gravity of solids	False	2.7
Water Content (%)	False	9.1

User-defined Soil Water Characteristic Curve (SWCC)		
Is User Defined? False		
af	5.8206	
bf	0.4621	
cf	3.8497	
hr	126.8000	

Sieve Size	% Passing
0.001mm	
0.002mm	
0.020mm	
#200	13.4
#100	
#80	20.8
#60	
#50	
#40	37.6
#30	
#20	
#16	
#10	64.0
#8	
#4	74.2
3/8-in.	82.3
1/2-in.	85.8
3/4-in.	90.8
1-in.	93.6
1 1/2-in.	96.7
2-in.	98.4
2 1/2-in.	
3-in.	
3 1/2-in.	99.4

Report generated on: 7/12/2023 2:53 PM

Version: 2.3.1+66

Created by: on: 8/26/2015 12:00 AM







Layer 5 Subgrade : A-6 (R-Value = 5)

Unbound	
Layer thickness (in)	Semi-infinite
Poisson's ratio	0.35
Coefficient of lateral earth pressure (k0)	0.5

Modulus (Input Level: 3)

Analysis Type:	Modify input values by temperature/moisture
Method:	Resilient Modulus (psi)

Resilient Modulus (psi) 5355.0

Use Correction factor for NDT modulus?	-
NDT Correction Factor:	-

Identifiers

Field	Value
Display name/identifier	A-6 (R-Value = 5)
Description of object	Default material
Author	AASHTO
Date Created	1/1/2011 12:00:00 AM
Approver	
Date approved	1/1/2011 12:00:00 AM
State	
District	
County	
Highway	
Direction of Travel	
From station (miles)	
To station (miles)	
Province	
User defined field 1	
User defined field 2	
User defined field 3	
Revision Number	0

Sieve

Liquid Limit	33.0
Plasticity Index	16.0
Is layer compacted?	False

	Is User Defined?	Value
	False	107.9
Saturated hydraulic conductivity (ft/hr)	False	1.95e-05
Specific gravity of solids	False	2.7
Water Content (%)	False	17.1

User-defined Soil Water Characteristic Curve (SWCC)					
Is User Defined?	False				
af	108.4091				
bf	0.6801				
cf 0.2161					
hr	500.0000				

Sieve Size	% Passing
0.001mm	
0.002mm	
0.020mm	
#200	63.2
#100	
#80	73.5
#60	
#50	
#40	82.4
#30	
#20	
#16	
#10	90.2
#8	
#4	93.5
3/8-in.	96.4
1/2-in.	97.4
3/4-in.	98.4
1-in.	99.0
1 1/2-in.	99.5
2-in.	99.8
2 1/2-in.	
3-in.	
3 1/2-in.	100.0

Report generated on: 7/12/2023 2:53 PM

Version: 2.3.1+66 Created by: on: 8/26/2015 12:00 AM





Calibration Coefficients

AC Fatigue				
1 \k2\beta_1 \k3\beta_1	k1: 0.007566			
$N_{f} = 0.00432 * C * \beta_{f1} k_{1} \left(\frac{1}{\varepsilon_{1}}\right)^{k_{2}\beta_{f2}} \left(\frac{1}{E}\right)^{k_{3}\beta_{f3}}$	k2: 3.9492			
	k3: 1.281			
$1C = 10^{M}$	Bf1: 130.3674			
$M = 4.84 \left(\frac{V_b}{V_c + V_b} - 0.69 \right)$	Bf2: 1			
Ya I YB	Bf3: 1.217799			

AC Rutting

$$\begin{split} \frac{\varepsilon_p}{\varepsilon_r} &= k_z \beta_{r1} 10^{k_1} T^{k_2 \beta_{r2}} N^{k_8 B_{r8}} \\ k_z &= (C_1 + C_2 * depth) * 0.328196^{depth} \\ C_1 &= -0.1039 * H_\alpha^2 + 2.4868 * H_\alpha - 17.342 \\ C_2 &= 0.0172 * H_\alpha^2 - 1.7331 * H_\alpha + 27.428 \end{split}$$

 $\varepsilon_p = plastic strain(in/in)$ $\varepsilon_r = resilient strain (in/in)$ $T = layer temperature(^{\circ}F)$ N = number of load repetitions

 $H_{ac} = total\ AC\ thickness(in)$

AC Rutting Standard Deviation	0.1414 * Pow(RUT,0.25) + 0.001	
AC Layer	K1:-3.35412 K2:1.5606 K3:0.3791	Br1:4.3 Br2:1 Br3:1

Thermal Fracture

$$C_f = \text{400} * N(\frac{\log C/h_{ac}}{\sigma}) \\ \Delta C = (k*\beta t)^{n+1} * A*\Delta K^n \\ A = 10^{(4.389-2.52*log(E*\sigma_m*n))} \\ \text{Level 1 K: 6.3} \\ \text{Level 2 Standard Deviation: 0.3972 * THERMAL + 55.462} \\ \text{Level 3 K: 6.3} \\ C_f = \text{observed amount of the rmal cracking}(ft/500ft) \\ k = refression coefficient determined through field calibration \\ N() = \text{standard normal distribution evaluated at()} \\ \sigma = \text{standard deviation of the log of the depth of cracks in the payments} \\ C = \text{crack depth(in)} \\ h_{ac} = \text{thickness of asphalt layer(in)} \\ \Delta C = \text{Change in the crack depth due to a cooling cycle} \\ \Delta K = \text{Change in the stress intensity factor due to a cooling cycle} \\ A_n = \text{Fracture parameters for the asphalt mixture} \\ E = \text{mixture stif fness} \\ \sigma_M = \text{Undamaged mixture tensile strength} \\ \beta_t = \text{Calibration parameter} \\ \text{Level 3 K: 6.3} \\ \text{Level 3 Standard Deviation: 0.2841 * THERMAL + 55.462} \\ \text{Level 3 Standard Deviation: 0.3972 * THERMAL + 20.422} \\ \text{Level 3 Standard Deviation: 0.3972 * THERMAL + 20.422} \\ \text{Level 3 Standard Deviation: 0.3972 * THERMAL + 20.422} \\ \text{Level 3 Standard Deviation: 0.3972 * THERMAL + 20.422} \\ \text{Level 3 Standard Deviation: 0.3972 * THERMAL + 20.422} \\ \text{Level 3 Standard Deviation: 0.3972 * THERMAL + 20.422} \\ \text{Level 3 Standard Deviation: 0.3972 * THERMAL + 20.422} \\ \text{Level 3 Standard Deviation: 0.3972 * THERMAL + 20.422} \\ \text{Level 3 Standard Deviation: 0.3972 * THERMAL + 20.422} \\ \text{Level 3 Standard Deviation: 0.3972 * THERMAL + 20.422} \\ \text{Level 3 Standard Deviation: 0.3972 * THERMAL + 20.422} \\ \text{Level 3 Standard Deviation: 0.3972 * THERMAL + 20.422} \\ \text{Level 3 Standard Deviation: 0.3972 * THERMAL + 20.422} \\ \text{Level 3 Standard Deviation: 0.3972 * THERMAL + 20.422} \\ \text{Level 3 Standard Deviation: 0.3972 * THERMAL + 20.422} \\ \text{Level 3 Standard Deviation: 0.3972 * THERMAL + 20.422} \\ \text{Level 3 Standard Deviation: 0.3972 * THERMAL + 20.422} \\ \text{Level 3 Standard Deviation: 0.3972 * THERMAL + 20.422} \\ \text{Level 3 Standard Deviation: 0.3972 * THERMAL + 20.422} \\ \text{Level 3 Standard$$

CSM Fatigue

$$N_f = 10$$

$$\begin{pmatrix} k_1 \beta_{c1} \left(\frac{\sigma_s}{M_r} \right) & N_f = number \ of \ repetitions \ to \ fatigue \ cracking \ \sigma_s = Tensile \ stress(psi) \ M_r = modulus \ of \ rupture(psi)$$
k1: 1 | k2: 1 | Bc1: 0.75 | Bc2:1.1

Report generated on: 7/12/2023 2:53 PM

Version: 2.3.1 + 66 Created by: on: 8/26/2015 12:00 AM





Subgrade Rutting					
$\delta_a(N) = \beta_{s_1} k_1 \varepsilon_v h\left(\frac{\varepsilon_0}{\varepsilon_r}\right) \left e^{-\left(\frac{\rho}{N}\right)^{\beta}} \right \qquad \begin{cases} N \\ \varepsilon_v \\ \varepsilon_0 \end{cases}$		$\delta_a = permanent deformation for the layer N = number \ of \ repetitions \varepsilon_v = average \ veritcal \ strain(in/in) \varepsilon_0, \beta, \rho = material \ properties \varepsilon_r = resilient \ strain(in/in)$			
Granular			Fine		
k1: 2.03	Bs1: 0.22		k1: 1.35		Bs1: 0.37
Standard Deviation (BASERUT) 0.0104 * Pow(BASERUT,0.67) + 0.001		Standard Deviation (BASERUT) 0.0663 * Pow(SUBRUT,0.5) + 0.001			

AC Cracking						
AC Top Down Cracking				AC Bottom Up Cracking		
$FC_{top} = \left(\frac{C_4}{1 + e^{(C_1 - C_2 * log_{10}(Damage))}}\right) * 10.56$		$FC = \left(\frac{6000}{1 + e^{\left(C_1 * C_1' + C_2 * C_2' log_{10}(D * 100)\right)}}\right) * \left(\frac{1}{60}\right)$ $C_2' = -2.40874 - 39.748 * (1 + h_{ac})^{-2.856}$ $C_1' = -2 * C_2'$				
c1: 7	c2: 3.5	c3: 0	c4: 1000	c1: 0.021	c2: 2.35	c3: 6000
AC Cracking Top Standard Deviation		AC Cracking Bottom Standard Deviation				
200 + 2300/(1+exp(1.072-2.1654*LOG10 (TOP+0.0001)))		1 + 15/(1+exp(-3.1472-4.1349*LOG10 (BOTTOM+0.0001)))				

CSM Crac	king			IRI Flexible Pavements			
FC_{ctb}	$= C_1 + $	$\frac{C}{1+e^{C_3-C}}$	1 2 (4(Damage)	C1 - Rutt C2 - Fati;	ing gue Crack	C3 - Tran C4 - Site I	sverse Crack Factors
C1: 0	C2: 75	C3: 5	C4: 3	C1: 50	C2: 0.55	C3: 0.0111	C4: 0.02
CSM Standard Deviation							
CTB*1				1			

Report generated on: 7/12/2023 2:53 PM

Version: 2.3.1+66 Created by: on: 8/26/2015 12:00 AM





Design Inputs

Design Life: 30 years Base construction: May, 2022 Climate Data 39.134, -108.538

Sources (Lat/Lon) Design Type: **FLEXIBLE** Pavement construction: June, 2022

> September, 2022 Traffic opening:

Design Structure

Layer type	Layer type Material Type	
Flexible	R3 Level 1 SX(100) PG 64-28	2.0
Flexible	R2 Level 1 SX(100) PG 64-22	6.5
NonStabilized	Crushed gravel	8.0
NonStabilized	A-1-b	14.0
Subgrade	A-6 (R-Value = 5)	Semi-infinite

Volumetric at Construction:				
Effective binder content (%)	10.7			
Air voids (%)	5.7			

Traffic

Age (year)	Heavy Trucks (cumulative)
2022 (initial)	2,100
2037 (15 years)	6,056,020
2052 (30 years)	14,449,700

Design Outputs

Distress Prediction Summary

Distress Type		Distress @ Specified Reliability		Reliability (%)	
	Target	Predicted	Target	Achieved	Satisfied?
Terminal IRI (in/mile)	200.00	219.79	90.00	78.86	Fail
Permanent deformation - total pavement (in)	0.80	0.76	90.00	95.19	Pass
AC bottom-up fatigue cracking (% lane area)	25.00	19.48	90.00	95.94	Pass
AC thermal cracking (ft/mile)	1500.00	355.20	90.00	100.00	Pass
AC top-down fatigue cracking (ft/mile)	3000.00	315.18	90.00	100.00	Pass
Permanent deformation - AC only (in)	0.65	0.56	90.00	97.94	Pass

Report generated on: 7/8/2023 8:38 PM

Version: 2.3.1+66

Created by: on: 8/26/2015 12:00 AM

Approved by: on: 8/26/2015 12:00 AM

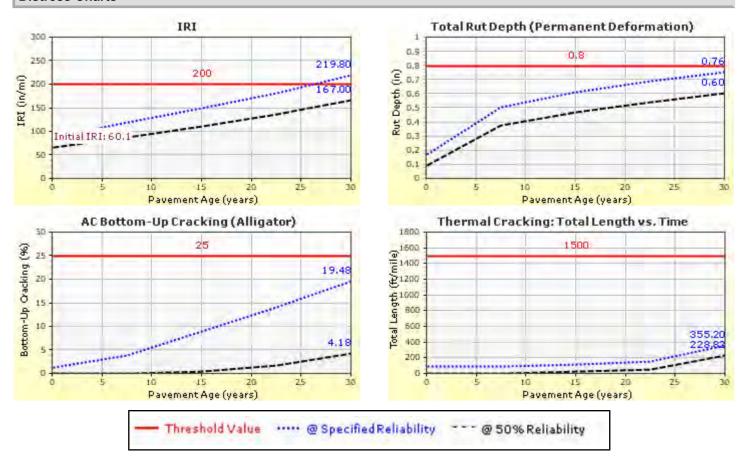
Page 1 of 22







Distress Charts









Traffic Inputs

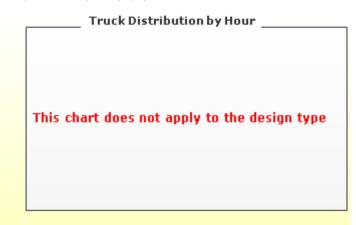
Graphical Representation of Traffic Inputs

Initial two-way AADTT: 2,100 Number of lanes in design direction: 2

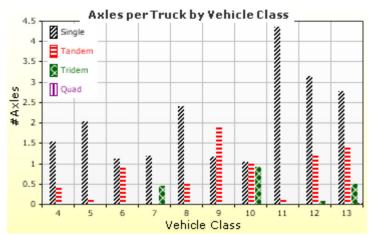


Vehicle Class

Percent of trucks in design direction (%): 50.0 Percent of trucks in design lane (%): 90.0 Operational speed (mph) 35.0







Traffic Volume Monthly Adjustment Factors

13









Tabular Representation of Traffic Inputs

Volume Monthly Adjustment Factors

Level 3: Default MAF

Month	Vehicle Class									
WIOTILIT	4	5	6	7	8	9	10	11	12	13
January	0.9	0.8	0.8	0.7	0.8	0.9	0.9	0.9	0.9	0.9
February	0.9	0.8	0.8	0.8	0.9	0.9	0.9	0.9	1.0	0.8
March	1.0	0.9	0.8	1.1	1.0	1.0	1.0	1.0	0.9	0.9
April	1.0	1.0	0.9	1.0	1.0	1.0	1.1	1.0	1.0	1.1
May	1.1	1.1	1.0	1.3	1.1	1.0	1.1	1.1	1.1	1.0
June	1.1	1.1	1.2	1.1	1.1	1.0	1.1	1.0	1.1	1.0
July	1.1	1.2	1.5	1.3	1.2	1.0	1.1	1.1	1.1	1.3
August	1.1	1.2	1.3	1.0	1.1	1.0	1.1	1.1	1.1	1.0
September	1.1	1.1	1.1	1.0	1.1	1.0	1.1	1.1	1.0	1.1
October	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	0.9	1.1
November	0.9	0.9	0.9	0.9	0.9	1.0	1.0	1.0	1.0	1.0
December	0.9	0.8	0.8	0.8	0.8	0.9	0.8	0.9	0.9	0.9

Distributions by Vehicle Class

Truck Distribution by Hour does not apply

Vehicle Class	AADTT Distribution (%)	Growth Factor		
	(Level 3) `´	Rate (%)	Function	
Class 4	2.1%	2.2%	Compound	
Class 5	56.1%	2.2%	Compound	
Class 6	4.4%	2.2%	Compound	
Class 7	0.3%	2.2%	Compound	
Class 8	14.2%	2.2%	Compound	
Class 9	21.1%	2.2%	Compound	
Class 10	0.7%	2.2%	Compound	
Class 11	0.7%	2.2%	Compound	
Class 12	0.2%	2.2%	Compound	
Class 13	0.2%	2.2%	Compound	

Axle Configuration

Traffic Wander				
Mean wheel location (in)	18.0			
Traffic wander standard deviation (in)	10.0			
Design lane width (ft)	12.0			

Wheelbase	does	not	apply

Axle Configuration	Vehic	
Average axle width (ft)	8.5	Clas
Dual tire spacing (in)	12.0	Class
Tiro prossuro (psi)	120.0	Class

Number of Axles per Truck

Vehicle Class	Single Axle	Tandem Axle	Tridem Axle	Quad Axle
Class 4	1.53	0.45	0	0
Class 5	2.02	0.16	0.02	0
Class 6	1.12	0.93	0	0
Class 7	1.19	0.07	0.45	0.02
Class 8	2.41	0.56	0.02	0
Class 9	1.16	1.88	0.01	0
Class 10	1.05	1.01	0.93	0.02
Class 11	4.35	0.13	0	0
Class 12	3.15	1.22	0.09	0
Class 13	2.77	1.4	0.51	0.04

Average Axle Spacing				
Tandem axle spacing (in)	51.6			
Tridem axle spacing (in)	49.2			
Quad axle spacing (in)	49.2			

Report generated on: 7/8/2023 8:38 PM

Version: 2.3.1+66

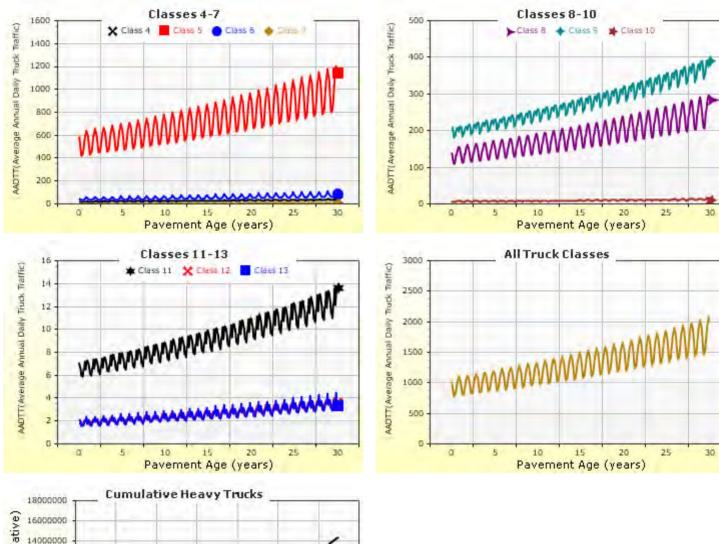
Created by: on: 8/26/2015 12:00 AM

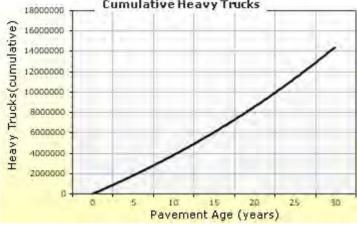




AADTT (Average Annual Daily Truck Traffic) Growth

* Traffic cap is not enforced





30



 $\textbf{F.5 Road (Updated)(30-year)} \\ \textbf{File Name: C:\Users\goldbaum\Documents\My PMED Designs\My ME Design\Projects\F.5 Road\GupdateGupdateG$



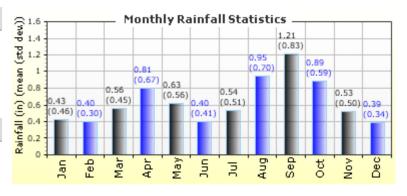
Climate Inputs

Climate Data Sources:

Climate Station Cities: Location (lat lon elevation(ft)) **GRAND JUNCTION, CO** 39.13400 -108.53800 4839



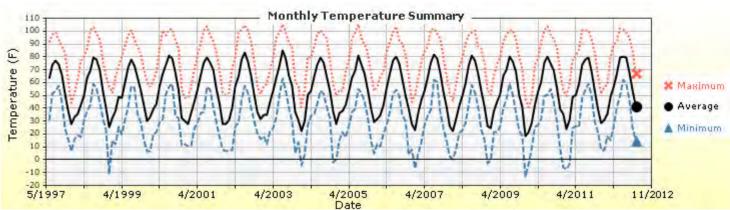
Mean annual air temperature (°F) 53.55 Mean annual precipitation (in) 7.76 Freezing index (°F - days) 398.73 Average annual number of freeze/thaw cycles: 111.77

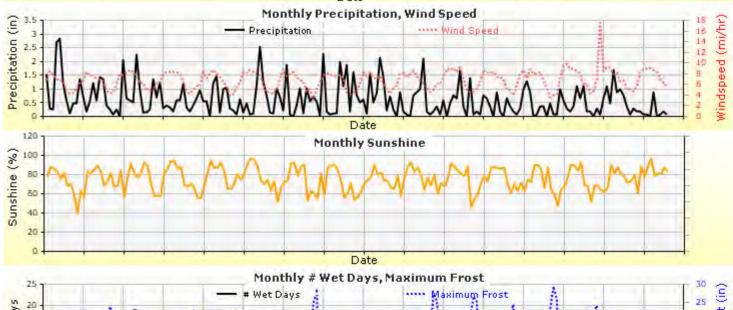


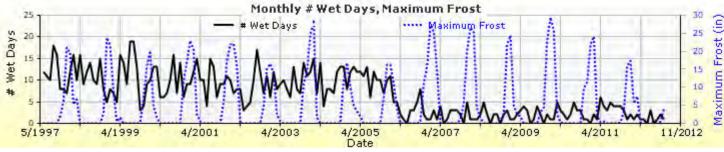
Water table depth (ft)

10.00

Monthly Climate Summary:

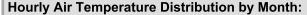


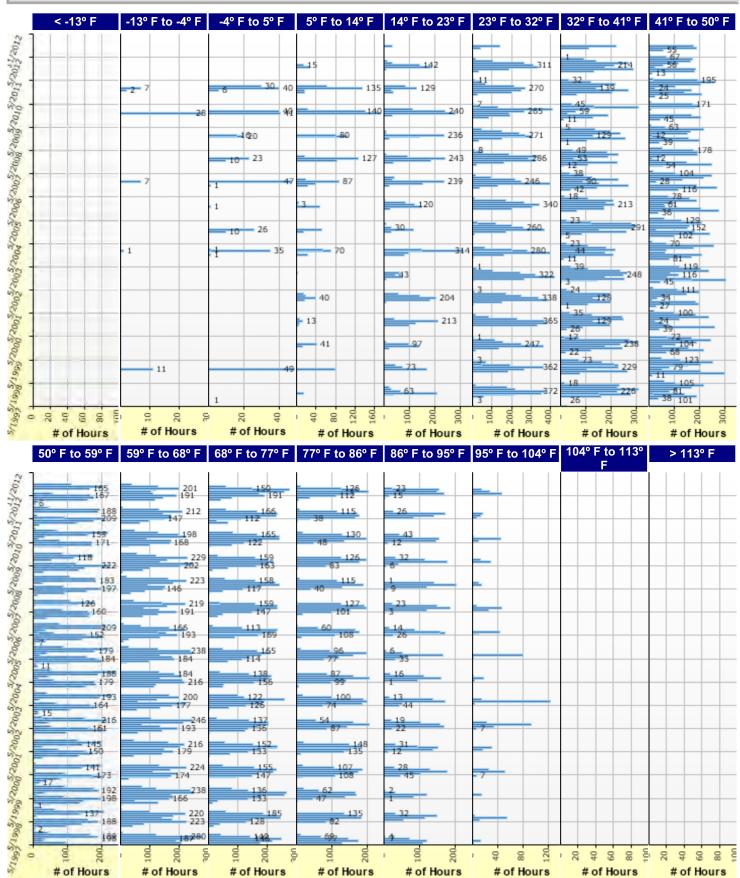














$\textbf{F.5 Road (Updated)(30-year)} \\ \textbf{File Name: C:\Users\goldbaum\Documents\My PMED Designs\My ME Design\Projects\F.5 Road\F.5 Road (Updated)(30-year).dgpx} \\ \textbf{File Name: C:\Users\goldbaum\Documents\My PMED Designs\My ME Design\Projects\F.5 Road\F.5 Road\Gupdated)(30-year).dgpx} \\ \textbf{File Name: C:\Users\goldbaum\Documents\My PMED Design\Nrojects\F.5 Road\Gupdated)(30-year).dgpx} \\ \textbf{File Name: C:\Users\goldbaum\Documents\My PMED Design\Nrojects\F.5 Road\Gupdated)(30-year).dgpx} \\ \textbf{File Name: C:\Users\goldbaum\Documents\My PMED Design\Nrojects\F.5 Road\Gupdated)(30-year).dgpx} \\ \textbf{File Name: C:\Users\goldbaum\Documents\My PMED Design\Nrojects\Nrojects\F.5 Road\Gupdated)(30-year).dgpx} \\ \textbf{File Name: C:\Users\goldbaum\Documents\My PMED Design\Nrojects\Nrojects\Gupdated)(30-year).dgpx} \\ \textbf{File Name: C:\Users\goldbaum\Documents\My PMED Design\Nrojects\Gupdated)(30-year).dgpx} \\ \textbf{File Name: C:\Users\goldbaum\Gupdated)(30-year).dgpx} \\ \textbf{File Name: C:\Users\goldbaum\Gupdated)(30-year).dgpx}$





Design Properties

HMA Design Properties

Use Multilayer Rutting Model	False
Using G* based model (not nationally calibrated)	False
Is NCHRP 1-37A HMA Rutting Model Coefficients	True
Endurance Limit	-
Use Reflective Cracking	True
Structure - ICM Properties	

Layer Name	Layer Type	Interface Friction
Layer 1 Flexible : R3 Level 1 SX (100) PG 64-28	Flexible (1)	1.00
Layer 2 Flexible : R2 Level 1 SX (100) PG 64-22	Flexible (1)	1.00
Layer 3 Non-stabilized Base : Crushed gravel		1.00
Layer 4 Non-stabilized Base : A-1-b	Non-stabilized Base (4)	1.00
Layer 5 Subgrade : A-6 (R-Value = 5)	Subgrade (5)	-

Ose Kellective Gracking	True
	-
Structure - ICM Properties	
AC surface shortwave absorptivity	0.85

Report generated on: 7/8/2023 8:38 PM

Version: 2.3.1+66

Created by: on: 8/26/2015 12:00 AM



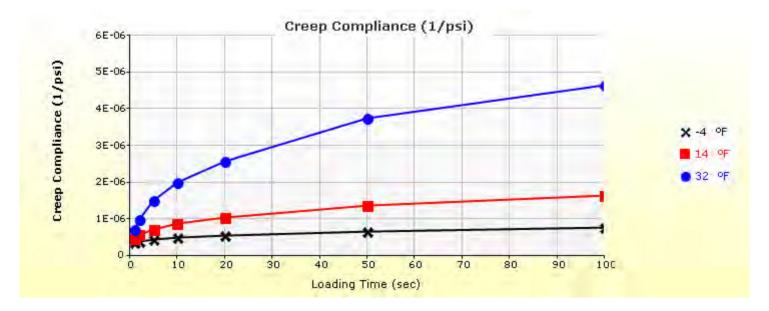




Thermal Cracking (Input Level: 1)

Indirect tensile strength at 14 °F (psi)	519.00	
Thermal Contraction		
Is thermal contraction calculated?	True	
Mix coefficient of thermal contraction (in/in/°F)	-	
Aggregate coefficient of thermal contraction (in/in/°F)	5.0e-006	
Voids in Mineral Aggregate (%)	16.4	

	Creep Compliance (1/psi)		
Loading time (sec)	-4 °F	14 °F	32 °F
1	3.61e-007	4.73e-007	7.12e-007
2	4.04e-007	5.74e-007	9.97e-007
5	4.51e-007	7.35e-007	1.52e-006
10	5.11e-007	8.78e-007	1.99e-006
20	5.67e-007	1.04e-006	2.59e-006
50	6.57e-007	1.37e-006	3.75e-006
100	7.68e-007	1.66e-006	4.66e-006



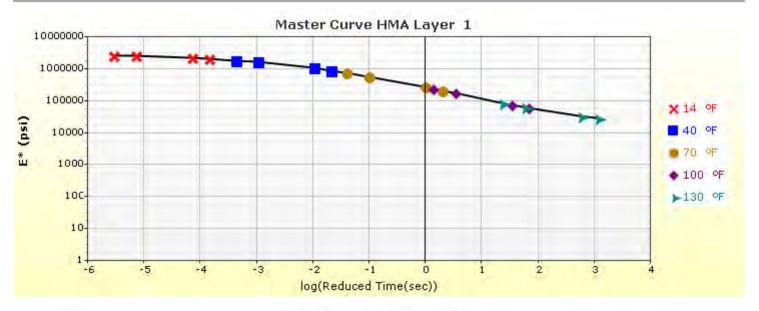
Report generated on: 7/8/2023 8:38 PM

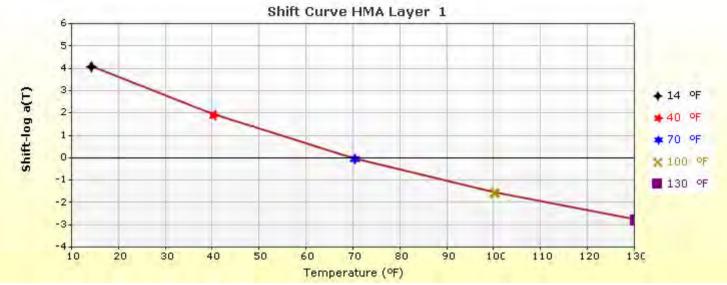
Version: 2.3.1+66 Created by: on: 8/26/2015 12:00 AM

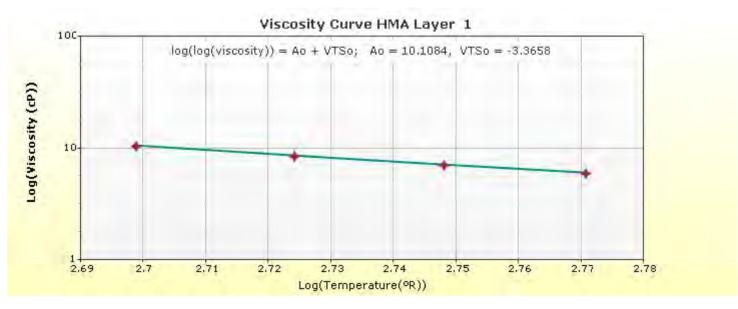




HMA Layer 1: Layer 1 Flexible: R3 Level 1 SX(100) PG 64-28





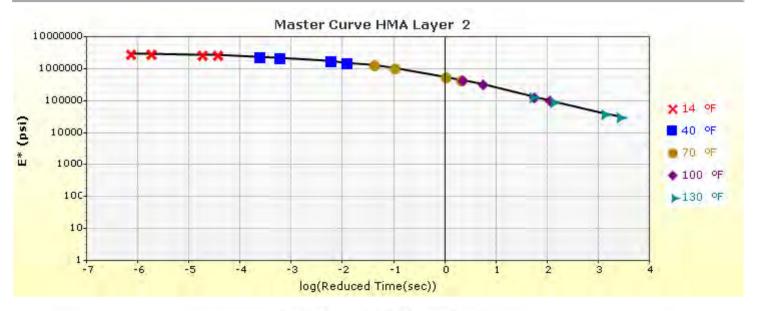


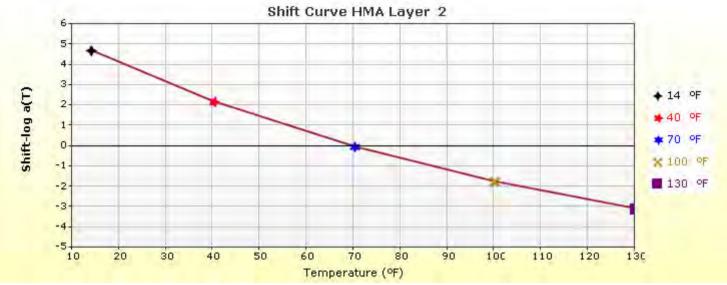


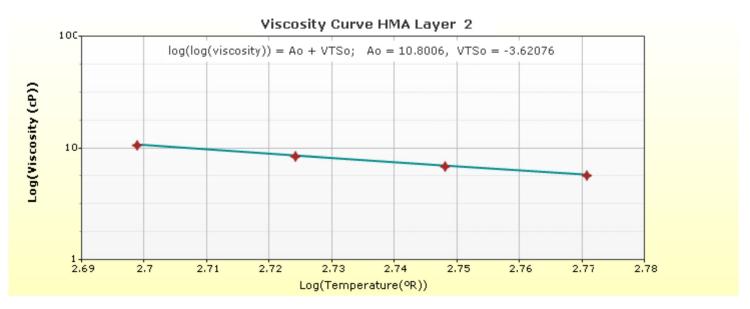
F.5 Road (Updated)(30-year)
File Name: C:\Users\goldbaum\Documents\My PMED Designs\My ME Design\Projects\F.5 Road\F.5 Road (Updated)(30-year).dgpx



HMA Layer 2: Layer 2 Flexible: R2 Level 1 SX(100) PG 64-22





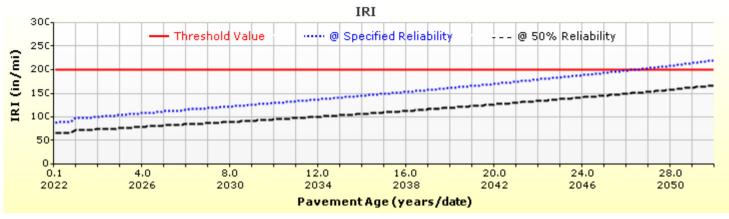


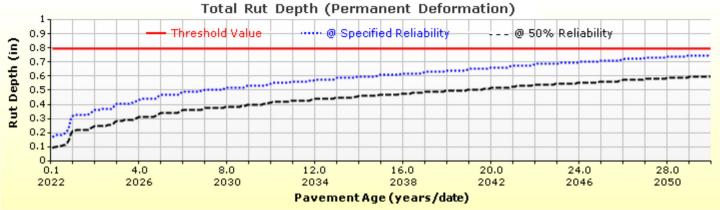


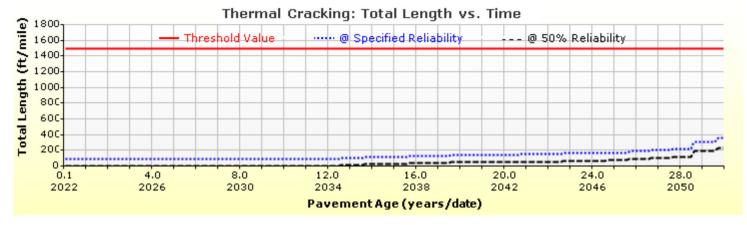




Analysis Output Charts





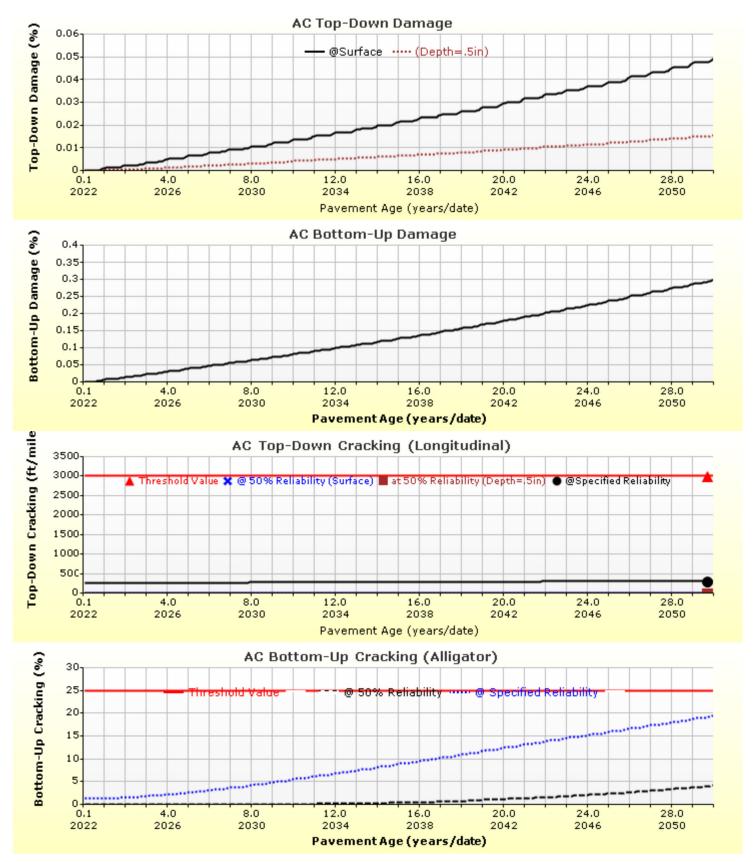




F.5 Road (Updated)(30-year)



File Name: C:\Users\goldbaum\Documents\My PMED Designs\My ME Design\Projects\F.5 Road\F.5 Road (Updated)(30-year).dgpx





F.5 Road (Updated)(30-year) File Name: C:\Users\goldbaum\Documents\My PMED Designs\My ME Design\Projects\F.5 Road\F.5 Road (Updated)(30-year).dgpx





Created by: on: 8/26/2015 12:00 AM

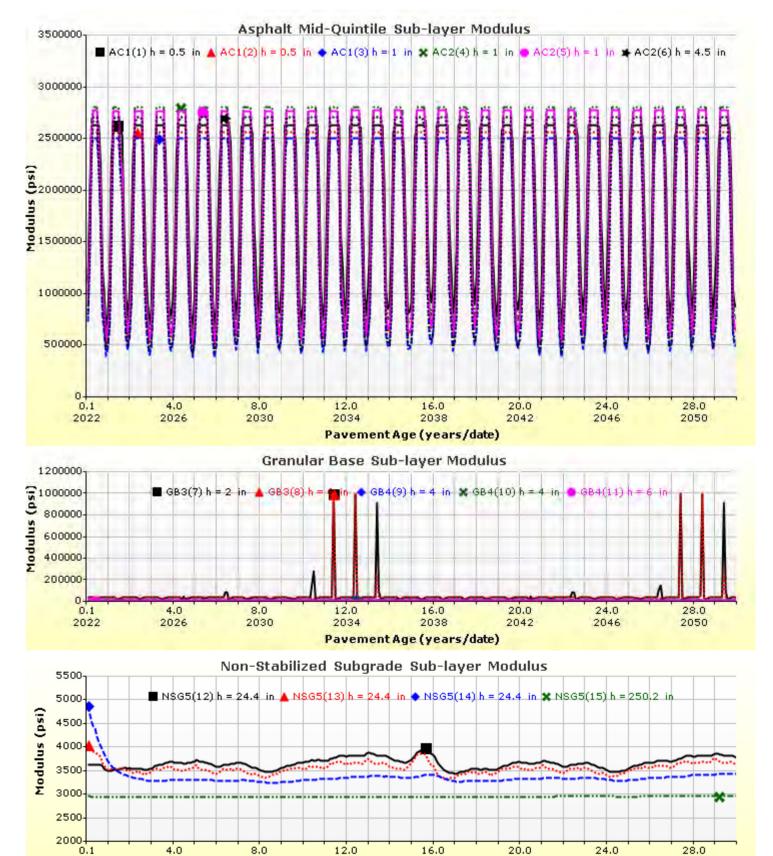
Approved by: on: 8/26/2015 12:00 AM

Page 14 of 22

F.5 Road (Updated)(30-year)



File Name: C:\Users\goldbaum\Documents\My PMED Designs\My ME Design\Projects\F.5 Road\F.5 Road (Updated)(30-year).dgpx



2022

2030

2026

2034

2038

Pavement Age (years/date)

2046

2042

2050







Layer Information

Layer 1 Flexible: R3 Level 1 SX(100) PG 64-28

Asphalt		
Thickness (in)	2.0	
Unit weight (pcf)	145.0	
Poisson's ratio	Is Calculated?	True
	Ratio	-
	Parameter A	-1.63
	Parameter B	3.84E-06

Asphalt Dynamic Modulus (Input Level: 1)

T (°F)	0.5 Hz	1 Hz	10 Hz	25 Hz
14	1687360	2134249	2493389	2608869
40	697463	1127680	1612900	1802220
70	173403	334774	616373	765125
100	54259	93163	175106	227742
130	27890	38645	60413	74657

Asphalt Binder

Temperature (°F)	Binder Gstar (Pa)	Phase angle (deg)
147.2	3051	81.6
158	1495	83.1
168.8	772	85

General Info

Name	Value
Reference temperature (°F)	70
Effective binder content (%)	10.7
Air voids (%)	5.7
Thermal conductivity (BTU/hr-ft-°F)	0.67
Heat capacity (BTU/lb-ºF)	0.23

Identifiers

Field	Value
Display name/identifier	R3 Level 1 SX(100) PG 64-28
Description of object	Mix ID # FS1959
Author	CDOT
Date Created	4/3/2013 12:00:00 AM
Approver	CDOT
Date approved	4/3/2013 12:00:00 AM
State	Colorado
District	
County	
Highway	
Direction of Travel	
From station (miles)	
To station (miles)	
Province	
User defined field 1	sx
User defined field 2	
User defined field 3	
Revision Number	0

Report generated on: 7/8/2023 8:38 PM

Version: 2.3.1+66

Created by: on: 8/26/2015 12:00 AM



F.5 Road (Updated)(30-year) File Name: C:\Users\goldbaum\Documents\My PMED Designs\My ME Design\Projects\F.5 Road\F.5 Road (Updated)(30-year).dgpx





Layer 2 Flexible: R2 Level 1 SX(100) PG 64-22

Asphalt		
Thickness (in)	6.5	
Unit weight (pcf)	145.0	
Poisson's ratio	Is Calculated?	True
	Ratio	-
	Parameter A	-1.63
	Parameter B	3.84E-06

Asphalt Dynamic Modulus (Input Level: 1)

T (°F)	0.5 Hz	1 Hz	10 Hz	25 Hz
14	2333549	2642179	2861449	2927779
40	1309490	1791270	2219829	2365949
70	379514	695090	1127310	1318450
100	87238	174824	349546	452545
130	29326	49265	92795	122034

Asphalt Binder

Temperature (°F)	Binder Gstar (Pa)	Phase angle (deg)
147.2	1857	81.6
158	889	83.1
168.8	451	85

General Info

Name	Value
Reference temperature (°F)	70
Effective binder content (%)	11.2
Air voids (%)	5.1
Thermal conductivity (BTU/hr-ft-°F)	0.67
Heat capacity (BTU/lb-ºF)	0.23

Identifiers

Field	Value
Display name/identifier	R2 Level 1 SX(100) PG 64-22
Description of object	Mix ID # FS1938
Author	CDOT
Date Created	4/3/2013 12:00:00 AM
Approver	CDOT
Date approved	4/3/2013 12:00:00 AM
State	Colorado
District	
County	
Highway	
Direction of Travel	
From station (miles)	
To station (miles)	
Province	
User defined field 1	SX
User defined field 2	
User defined field 3	
Revision Number	2

Report generated on: 7/8/2023 8:38 PM

Version: 2.3.1+66

Created by: on: 8/26/2015 12:00 AM



$\textbf{F.5 Road (Updated)(30-year)} \\ \textbf{File Name: C:\Users\goldbaum\Documents\My PMED Designs\My ME Design\Projects\F.5 Road\F.5 Road\(Updated)(30-year).dgpx} \\ \textbf{Topology Projects\F.5 Road\F.5 Road\GupdateGupdateGupdat$





Layer 3 Non-stabilized Base : Crushed gravel

Unbound	
Layer thickness (in)	8.0
Poisson's ratio	0.35
Coefficient of lateral earth pressure (k0)	0.5

Analysis Type:	Modify input values by temperature/moisture
Method:	Resilient Modulus (psi)

Resilient Modulus (psi)
25000.0

Use Correction factor for NDT modulus?	-
NDT Correction Factor:	-

Identifiers

Field	Value
Display name/identifier	Crushed gravel
Description of object	Default material
Author	AASHTO
Date Created	1/1/2011 12:00:00 AM
Approver	
Date approved	1/1/2011 12:00:00 AM
State	
District	
County	
Highway	
Direction of Travel	
From station (miles)	
To station (miles)	
Province	
User defined field 1	
User defined field 2	
User defined field 3	
Revision Number	41

Sieve

Liquid Limit	6.0
Plasticity Index	1.0
Is layer compacted?	True

	Is User Defined?	Value
Maximum dry unit weight (pcf)	False	127.7
Saturated hydraulic conductivity (ft/hr)	False	5.054e-02
Specific gravity of solids	False	2.7
Water Content (%)	False	7.4

User-defined Soil Water Characteristic Curve (SWCC)		
Is User Defined?	False	
af	7.2555	
bf	1.3328	
cf	0.8242	
hr	117.4000	

Sieve Size	% Passing
0.001mm	
0.002mm	
0.020mm	
#200	8.7
#100	
#80	12.9
#60	
#50	
#40	20.0
#30	
#20	
#16	
#10	33.8
#8	
#4	44.7
3/8-in.	57.2
1/2-in.	63.1
3/4-in.	72.7
1-in.	78.8
1 1/2-in.	85.8
2-in.	91.6
2 1/2-in.	
3-in.	
3 1/2-in.	97.6

Report generated on: 7/8/2023 8:38 PM

Version: 2.3.1+66 Created by: on: 8/26/2015 12:00 AM



F.5 Road (Updated)(30-year) File Name: C:\Users\goldbaum\Documents\My PMED Designs\My ME Design\Projects\F.5 Road\F.5 Road (Updated)(30-year).dgpx





Layer 4 Non-stabilized Base : A-1-b

Unbound	
Layer thickness (in)	14.0
Poisson's ratio	0.35
Coefficient of lateral earth pressure (k0)	0.5

Modulus ((Input	Level:	3)
modulus (IIIPUL	LC V CI.	

Analysis Type:	Modify input values by temperature/moisture
Method:	Resilient Modulus (psi)

Resilient Modulus (psi)	
9494.0	

Use Correction factor for NDT modulus?	-
NDT Correction Factor:	-

Identifiers

Field	Value
Display name/identifier	A-1-b
Description of object	Default material
Author	AASHTO
Date Created	1/1/2011 12:00:00 AM
Approver	
Date approved	1/1/2011 12:00:00 AM
State	
District	
County	
Highway	
Direction of Travel	
From station (miles)	
To station (miles)	
Province	
User defined field 1	
User defined field 2	
User defined field 3	
Revision Number	0

Sieve

Liquid Limit	11.0
Plasticity Index	1.0
Is layer compacted?	True

	Is User Defined?	Value
, , ,	False	124.2
Saturated hydraulic conductivity (ft/hr)	False	2.303e-03
Specific gravity of solids	False	2.7
Water Content (%)	False	9.1

User-defined Soil Water Characteristic Curve (SWCC)	
Is User Defined?	False
af	5.8206
bf	0.4621
cf	3.8497
hr	126.8000

Sieve Size	% Passing
0.001mm	
0.002mm	
0.020mm	
#200	13.4
#100	
#80	20.8
#60	
#50	
#40	37.6
#30	
#20	
#16	
#10	64.0
#8	
#4	74.2
3/8-in.	82.3
1/2-in.	85.8
3/4-in.	90.8
1-in.	93.6
1 1/2-in.	96.7
2-in.	98.4
2 1/2-in.	
3-in.	
3 1/2-in.	99.4

Report generated on: 7/8/2023 8:38 PM

Version: 2.3.1+66

Created by: on: 8/26/2015 12:00 AM

Approved on: 8/26/2015 12:00 AM

Page 19 of 22



$\textbf{F.5 Road (Updated)(30-year)} \\ \textbf{File Name: C:\Users\goldbaum\Documents\My PMED Designs\My ME Design\Projects\F.5 Road\F.5 Road\(Updated)(30-year).dgpx} \\ \textbf{Topology Projects\F.5 Road\F.5 Road\GupdateGupdateGupdat$





Layer 5 Subgrade : A-6 (R-Value = 5)

Unbound	
Layer thickness (in)	Semi-infinite
Poisson's ratio	0.35
Coefficient of lateral earth pressure (k0)	0.5

Modulus ((Inpi	ıt Lo	evel	: 3)
inoaaiao j				. •	

Analysis Type:	Modify input values by temperature/moisture
Method:	Resilient Modulus (psi)

Resilient Modulus (psi)	
5355.0	

Use Correction factor for NDT modulus?	-
NDT Correction Factor:	-

Identifiers

Field	Value
Display name/identifier	A-6 (R-Value = 5)
Description of object	Default material
Author	AASHTO
Date Created	1/1/2011 12:00:00 AM
Approver	
Date approved	1/1/2011 12:00:00 AM
State	
District	
County	
Highway	
Direction of Travel	
From station (miles)	
To station (miles)	
Province	
User defined field 1	
User defined field 2	
User defined field 3	
Revision Number	0

Sieve

Liquid Limit	33.0
Plasticity Index	16.0
Is layer compacted?	False

	Is User Defined?	Value
, , ,	False	107.9
Saturated hydraulic conductivity (ft/hr)	False	1.95e-05
Specific gravity of solids	False	2.7
Water Content (%)	False	17.1

User-defined Soil Water Characteristic Curve (SWCC)			
Is User Defined?	False		
af	108.4091		
bf 0.6801			
cf	0.2161		
hr	500.0000		

Sieve Size	% Passing
0.001mm	
0.002mm	
0.020mm	
#200	63.2
#100	
#80	73.5
#60	
#50	
#40	82.4
#30	
#20	
#16	
#10	90.2
#8	
#4	93.5
3/8-in.	96.4
1/2-in.	97.4
3/4-in.	98.4
1-in.	99.0
1 1/2-in.	99.5
2-in.	99.8
2 1/2-in.	
3-in.	
3 1/2-in.	100.0

Report generated on: 7/8/2023 8:38 PM

Version: 2.3.1+66 Created by: on: 8/26/2015 12:00 AM

F.5 Road (Updated)(30-year) File Name: C:\Users\goldbaum\Documents\My PMED Designs\My ME Design\Projects\F.5 Road\(Updated)(30-year).dgpx



Calibration Coefficients

AC Fatigue	
$N_f = 0.00432 * C * \beta_{f1} k_1 \left(\frac{1}{\varepsilon_1}\right)^{k_2 \beta_{f2}} \left(\frac{1}{E}\right)^{k_3 \beta_{f3}}$	k1: 0.007566
$N_f = 0.00432 * C * \beta_{f1} k_1 \left(\frac{1}{c}\right)$	k2: 3.9492
	k3: 1.281
$C = 10^M$	Bf1: 130.3674
$M = 4.84 \left(\frac{V_b}{V_a + V_b} - 0.69 \right)$	Bf2: 1
Ya I Yb	Bf3: 1.217799

AC Rutting

$$\begin{split} \frac{\varepsilon_p}{\varepsilon_r} &= k_z \beta_{r1} 10^{k_1} T^{k_2 \beta_{r2}} N^{k_3 B_{r3}} \\ k_z &= (C_1 + C_2 * depth) * 0.328196^{depth} \\ C_1 &= -0.1039 * H_\alpha^2 + 2.4868 * H_\alpha - 17.342 \\ C_2 &= 0.0172 * H_\alpha^2 - 1.7331 * H_\alpha + 27.428 \end{split}$$

 $\varepsilon_p = plastic strain(in/in)$ $\varepsilon_r = resilient strain (in/in)$ T = layer temperature(°F)N = number of load repetitions

 $H_{aa} = total AC thickness(in)$

uc	· /	
AC Rutting Standard Deviation	0.1414 * Pow(RUT,0.25) + 0.001	
AC Layer	K1:-3.35412 K2:1.5606 K3:0.3791	Br1:4.3 Br2:1 Br3:1

Thermal Fracture

$$C_f = \text{doo} * N(\frac{\log C/h_{ac}}{\sigma}) \\ \Delta C = (k*\beta t)^{n+1}*A*\Delta K^n \\ A = 10^{(4.389-2.52*\log(E*\sigma_m*n))} \\ \text{Level 1 K: 6.3} \\ \text{Level 2 Standard Deviation: } 0.2841* \text{ THERMAL} + 65.027 \\ \text{Level 3 K: 6.3} \\ \text{Level 3 Standard Deviation: } 0.66 \text{ ficient determined through field calibration} \\ N() = \text{standard normal distribution evaluated at ()} \\ n() = \text{standard deviation of the log of the depth of cracks in the payments} \\ n() = \text{standard deviation of the log of the depth of cracks in the payments} \\ n() = \text{standard deviation of the log of the depth of cracks in the payments} \\ n() = \text{standard deviation of the log of the depth of cracks in the payments} \\ n() = \text{standard deviation of the log of the depth of cracks in the payments} \\ n() = \text{standard deviation of the log of the depth of cracks in the payments} \\ n() = \text{standard deviation of the log of the depth of cracks in the payments} \\ n() = \text{standard deviation of the log of the depth of cracks in the payments} \\ n() = \text{standard deviation of the log of the depth of cracks in the payments} \\ n() = \text{standard deviation of the log of the depth of cracks in the payments} \\ n() = \text{standard deviation of the log of the depth of cracks in the payments} \\ n() = \text{standard deviation of the log of the depth of cracks in the payments} \\ n() = \text{standard deviation of the log of the depth of cracks in the payments} \\ n() = \text{standard deviation of the log of the depth of cracks in the payments} \\ n() = \text{standard deviation of the log of the depth of cracks in the payments} \\ n() = \text{standard deviation of the log of the depth of cracks in the payments} \\ n() = \text{standard deviation of the log of the depth of cracks in the payments} \\ n() = \text{standard deviation of the log of the depth of cracks in the payments} \\ n() = \text{standard deviation of the log of the depth of cracks in the payments} \\ n() = \text{standard deviation of the log of the depth of crack depth of cracks in the payments} \\ n() = \text{standard deviation of the log of the depth of crack depth of crack depth$$

CSM Fatigue

$$N_f = 10^{\left(rac{k_1 eta_{c1}\left(rac{\sigma_s}{M_r}
ight)}{k_2 eta_{c2}}
ight)} egin{array}{c} N_f = number\ of\ repetitions\ to\ fatigue\ cracking\ \sigma_s = Tensile\ stress(psi)\ M_r = modulus\ of\ rupture(psi) \ \end{array}$$

Report generated on: 7/8/2023 8:38 PM

Version: 2.3.1 + 66 Created by: on: 8/26/2015 12:00 AM





F.5 Road (Updated)(30-year)
File Name: C:\Users\goldbaum\Documents\My PMED Designs\My ME Design\Projects\F.5 Road\F.5 Road (Updated)(30-year).dgpx

Subgrade Rutt	ing				
$\delta_a(N) = \beta_s$	$\left k_1 \varepsilon_v h \left(\frac{\varepsilon_0}{\varepsilon_r} \right) \right e^{-\left(\frac{\rho}{N} \right)^{\beta}} \right $	$N = \varepsilon_v = \varepsilon_0, \beta$	= permanent de : number of rep = average verito 3, ρ = material γ = resilient strai	etitions cal strain properti	es
Granular		F	ine		
k1: 2.03	Bs1: 0.22	k	(1: 1.35		Bs1: 0.37
	tion (BASERUT) BASERUT,0.67) + 0.001		Standard Devia).0663 * Pow(S		

AC Cracki	AC Cracking					
AC Top Dov	vn Cracking			AC Bottom Up C	racking	
$FC_{top} = \left(\frac{C_4}{1 + e^{\left(C_1 - C_2 * log_{10}(Damage)\right)}}\right) * 10.56$		$FC = \left(\frac{6000}{1 + e^{\left(C_1 * C_1' + C_2 * C_2' \log_{10}(D * 100)\right)}}\right) * \left(\frac{1}{60}\right)$ $C_2' = -2.40874 - 39.748 * (1 + h_{ac})^{-2.856}$ $C_1' = -2 * C_2'$				
c1: 7	c2: 3.5	c3: 0	c4: 1000	c1: 0.021	c2: 2.35	c3: 6000
AC Cracking Top Standard Deviation		AC Cracking Bottom Standard Deviation		eviation		
200 + 2300 (TOP+0.00	/(1+exp(1.07 01)))	72-2.1654*L0	OG10	1 + 15/(1+exp(-3 (BOTTOM+0.00		.OG10

CSM Cracking		IRI Flexible Pavements					
FC_{ctb}	$C_{Ctb} = C_1 + \frac{C_2}{1 + e^{C_3 - C_4(Damage)}}$		C1 - Rutting C3 - Transvers C2 - Fatigue Crack C4 - Site Facto				
C1: 0	C2: 75	C3: 5	C4: 3	C1: 50	C2: 0.55	C3: 0.0111	C4: 0.02
CSM Standa	ard Deviation						
CTB*1				1			

Report generated on: 7/8/2023 8:38 PM

Version: 2.3.1+66 Created by: on: 8/26/2015 12:00 AM



APPENDIX C1

RIGID ME-PAVEMENT DESIGN OUTPUT SHEETS F 1/2 ROAD



File Name: C:\Users\RSPavement\Documents\PMED Designs\My ME Design\Projects\F.5 Road\PCCP F.5 Road.dgpx



Design Inputs

Design Life: 30 years Existing construction: Climate Data 39.134, -108.538

Sources (Lat/Lon) Design Type: **JPCP** Pavement construction: May, 2022

> Traffic opening: August, 2022

Design Structure

Layer type	Material Type	Thickness (in)
PCC	R4 Level 1 Lawson	9.0
NonStabilized	Crushed stone	8.0
Subgrade	A-1-b (Pit run) R value 40	12.0
Subgrade	A-6	Semi-infinite

Joint Design:	
Joint spacing (ft)	12.0
Dowel diameter (in)	1.25
Slab width (ft)	12.0

Traffic

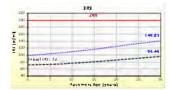
Age (year)	Heavy Trucks (cumulative)
2022 (initial)	2,100
2037 (15 years)	6,056,020
2052 (30 years)	14,449,700

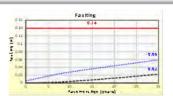
Design Outputs

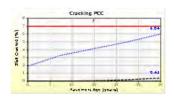
Distress Prediction Summary

Distress Type		Specified bility	Reliability (%)		Criterion Satisfied?	
	Target	Predicted	Target	Achieved	Satisfied?	
Terminal IRI (in/mile)	200.00	140.85	90.00	99.86	Pass	
Mean joint faulting (in)	0.14	0.06	90.00	100.00	Pass	
JPCP transverse cracking (percent slabs)	7.00	6.04	90.00	93.34	Pass	

Distress Charts







Threshold Value @ Specified Reliability --- @ 50% Reliability

Report generated on: 1/5/2022 12:55 PM

Version: 2.3.1+66

Created by: on: 8/5/2016 12:00 AM





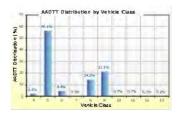


Traffic Inputs

Graphical Representation of Traffic Inputs

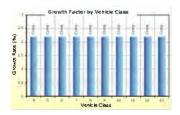
Initial two-way AADTT: 2,100

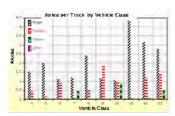
Number of lanes in design direction: 2



Percent of trucks in design direction (%): 50.0
Percent of trucks in design lane (%): 90.0
Operational speed (mph) 35.0







Traffic Volume Monthly Adjustment Factors

Class 4	Class 5	Class 6	Class 7	Class 8	Class 9	Class 10	Class 11	Class 12	Class 13
Dec									
Har-	a a	Su Control	2	2	2	9	2	2	4
On I									
Asq.			3			2		3	
7-1									
1	7						1		
Uay Table		9	12		3				9
As-									
u 9	3	**************************************	F	2	2	2	2	2	2
Te b									
3	8	a d	G G	3	2	21112	2	3	3
○ 23 23 + 11. Adj. Per tor	2333-23: Adj. Pec los	2333-2331 Adj. Per tor	Adj. Pector	Adj. Per tor	2333-11 Adj. Nactor	2333-11 Adj. Nactor	Adj. Pertor	2333-11 Adj. Nactor	2333-233 Adj. Pertor

Report generated on: 1/5/2022 12:55 PM

Version: 2.3.1+66

Created by: on: 8/5/2016 12:00 AM

Α







Tabular Representation of Traffic Inputs

Volume Monthly Adjustment Factors

Level 3: Default MAF

Month		Vehicle Class								
WIOTILIT	4	5	6	7	8	9	10	11	12	13
January	0.9	0.8	0.8	0.7	0.8	0.9	0.9	0.9	0.9	0.9
February	0.9	0.8	0.8	0.8	0.9	0.9	0.9	0.9	1.0	0.8
March	1.0	0.9	0.8	1.1	1.0	1.0	1.0	1.0	0.9	0.9
April	1.0	1.0	0.9	1.0	1.0	1.0	1.1	1.0	1.0	1.1
May	1.1	1.1	1.0	1.3	1.1	1.0	1.1	1.1	1.1	1.0
June	1.1	1.1	1.2	1.1	1.1	1.0	1.1	1.0	1.1	1.0
July	1.1	1.2	1.5	1.3	1.2	1.0	1.1	1.1	1.1	1.3
August	1.1	1.2	1.3	1.0	1.1	1.0	1.1	1.1	1.1	1.0
September	1.1	1.1	1.1	1.0	1.1	1.0	1.1	1.1	1.0	1.1
October	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	0.9	1.1
November	0.9	0.9	0.9	0.9	0.9	1.0	1.0	1.0	1.0	1.0
December	0.9	0.8	0.8	0.8	0.8	0.9	0.8	0.9	0.9	0.9

Distributions by Vehicle Class

Vehicle Class	AADTT Distribution (%)	Growt	h Factor	
	(Level 3) `´	Rate (%) Function		
Class 4	2.1%	2.2%	Compound	
Class 5	56.1%	2.2%	Compound	
Class 6	4.4%	2.2%	Compound	
Class 7	0.3%	2.2%	Compound	
Class 8	14.2%	2.2%	Compound	
Class 9	21.1%	2.2%	Compound	
Class 10	0.7%	2.2%	Compound	
Class 11	0.7%	2.2%	Compound	
Class 12	0.2%	2.2%	Compound	
Class 13	0.2%	2.2%	Compound	

Truck Distribution by Hour

Hour	Distribution (%)	Hour	Distribution (%)
12 AM	1.65%	12 PM	6.75%
1 AM	1.37%	1 PM	6.81%
2 AM	1.28%	2 PM	6.83%
3 AM	1.36%	3 PM	6.56%
4 AM	1.66%	4 PM	6.02%
5 AM	2.32%	5 PM	5.23%
6 AM	3.8%	6 PM	4.35%
7 AM	4.95%	7 PM	3.59%
8 AM	5.9%	8 PM	2.98%
9 AM	6.48%	9 PM	2.56%
10 AM	6.83%	10 PM	2.12%
11 AM	6.85%	11 PM	1.75%
		Total	100%

Axle Configuration

Traffic Wander				
Mean wheel location (in)	18.0			
Traffic wander standard deviation (in)	10.0			
Design lane width (ft)	12.0			

Axle Configuration				
Average axle width (ft)	8.5			
Dual tire spacing (in)	12.0			
Tire pressure (psi)	120.0			

Average Axle Spacing				
51.6				
49.2				
49.2				

Wheelbase						
Value Type	Axle Type	Short	Medium	Long		
Average spacing of axles (ft)		12.0	15.0	18.0		
Percent of Trucks (%)		17.0	22.0	61.0		

Number of Axles per Truck

Vehicle Class	Single Axle	Tandem Axle	Tridem Axle	Quad Axle
Class 4	1.53	0.45	0	0
Class 5	2.02	0.16	0.02	0
Class 6	1.12	0.93	0	0
Class 7	1.19	0.07	0.45	0.02
Class 8	2.41	0.56	0.02	0
Class 9	1.16	1.88	0.01	0
Class 10	1.05	1.01	0.93	0.02
Class 11	4.35	0.13	0	0
Class 12	3.15	1.22	0.09	0
Class 13	2.77	1.4	0.51	0.04

Report generated on: 1/5/2022 12:55 PM

Version: 2.3.1+66

Created by: on: 8/5/2016 12:00 AM

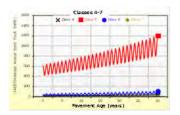


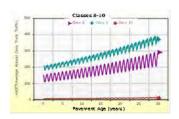
File Name: C:\Users\RSPavement\Documents\PMED Designs\My ME Design\Projects\F.5 Road\PCCP F.5 Road.dgpx

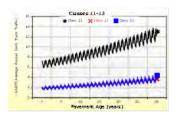


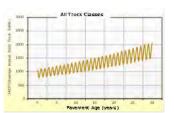
AADTT (Average Annual Daily Truck Traffic) Growth

* Traffic cap is not enforced











Created by: on: 8/5/2016 12:00 AM





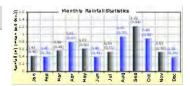


Climate Inputs

Climate Data Sources:

Climate Station Cities: **GRAND JUNCTION, CO** Location (lat lon elevation(ft))

39.13400 -108.53800 4839

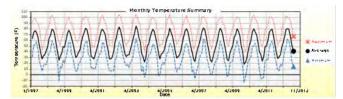


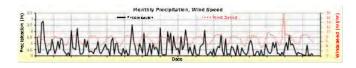
Annual Statistics:

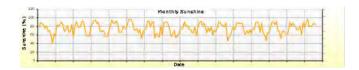
Mean annual air temperature (°F) 53.51 Mean annual precipitation (in) 7.75 Freezing index (°F - days) 399.81 Average annual number of freeze/thaw cycles: 111.77

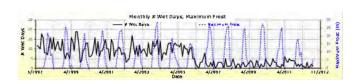
Water table depth 10.00 (ft)

Monthly Climate Summary:









Report generated on: 1/5/2022 12:55 PM

Version: 2.3.1+66

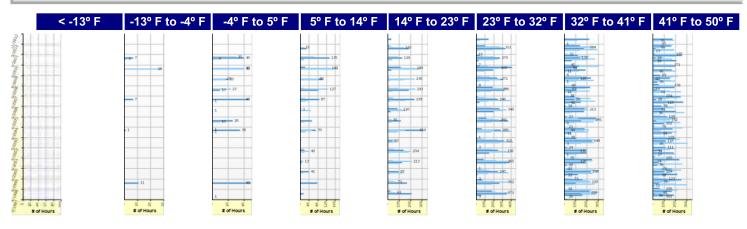
Created^{by}: on: 8/5/2016 12:00 AM

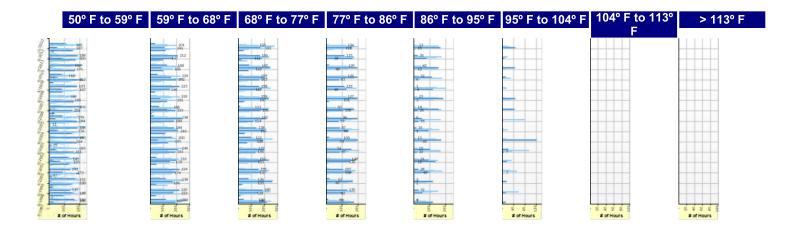


File Name: C:\Users\RSPavement\Documents\PMED Designs\My ME Design\Projects\F.5 Road\PCCP F.5 Road.dgpx



Hourly Air Temperature Distribution by Month:





Created by: on: 8/5/2016 12:00 AM







Design Properties

JPCP Design Properties

Structure - ICM Properties					
PCC surface shortwave absorptivity	0.85				

PCC joint spacing (ft)				
Is joint spacing random ?	False			
Joint spacing (ft)	12.00			

Doweled Joints	
Is joint doweled?	True
Dowel diameter (in)	1.25
Dowel spacing (in)	12.00

Widened Slab	
Is slab widened ?	False
Slab width (ft)	12.00

Sealant type	Other(Including No Sealant Liquid Silicone)
--------------	---

Tied Shoulders	
Tied shoulders	True
Load transfer efficiency (%)	50.00

PCC-Base Contact Friction	
PCC-Base full friction contact	True
Months until friction loss	360.00

Erodibility index	4

Permanent curl/warp effective temperature difference (°F)	-10.00
---	--------

Report generated on: 1/5/2022 12:55 PM

Version: 2.3.1+66

Created by: on: 8/5/2016 12:00 AM

Approved by: on: 8/5/2016 12:00 AM

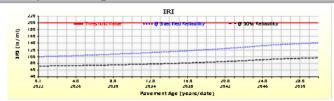
Page 7 of 15

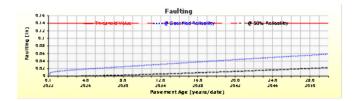






Analysis Output Charts





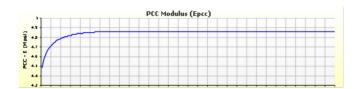


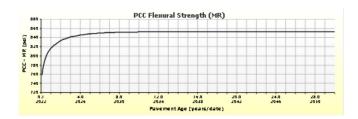
Created by: on: 8/5/2016 12:00 AM

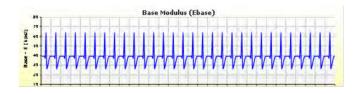


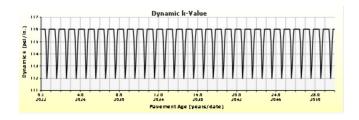










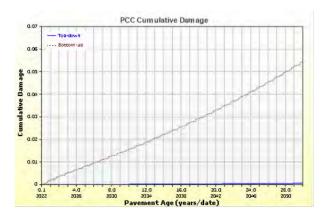


Created by: on: 8/5/2016 12:00 AM











Created by: on: 8/5/2016 12:00 AM







Layer Information

Layer 1 PCC : R4 Level 1 Lawson

PCC	
Thickness (in)	9.0
Unit weight (pcf)	140.6
Poisson's ratio	0.2

Thermal	
PCC coefficient of thermal expansion (in/in/°F x 10^-6)	4.86
PCC thermal conductivity (BTU/hr-ft-°F)	1.25
PCC heat capacity (BTU/lb-°F)	0.28

Mix		
Cement type		Type I (1)
Cementitious material co	ontent (lb/yd^3)	563
Water to cement ratio		0.36
Aggregate type		Dolomite (2)
PCC zero-stress	Calculated Internally?	True
temperature (°F)	User Value	-
	Calculated Value	90.7
Ultimate shrinkage	Calculated Internally?	True
(microstrain)	User Value	-
	Calculated Value	516.0
Reversible shrinkage (%)		50
Time to develop 50% of ultimate shrinkage (days)		35
Curing method		Curing Compound

PCC strength and modulus (Input Level: 1)

Time	Modulus of rupture (psi)	Elastic modulus (psi)
7-day	560	3230000
14-day	620	3500000
28-day	710	4030000
90-day	730	4240000
20-year/28-day	1.2	1.2

Identifiers

Field	Value
Display name/identifier	R4 Level 1 Lawson
Description of object	Mix ID # 2009105
Author	CDOT
Date Created	4/3/2013 12:00:00 AM
Approver	CDOT
Date approved	4/3/2013 12:00:00 AM
State	Colorado
District	
County	
Highway	
Direction of Travel	
From station (miles)	
To station (miles)	
Province	
User defined field 1	Region 4/1/6
User defined field 2	
User defined field 3	
Revision Number	0

Report generated on: 1/5/2022 12:55 PM

Version: 2.3.1+66

Created by: on: 8/5/2016 12:00 AM







Layer 2 Non-stabilized Base : Crushed stone

Unbound	
Layer thickness (in)	8.0
Poisson's ratio	0.35
Coefficient of lateral earth pressure (k0)	0.5

NAI	l /l		1	- 21
Modu	lus (Ir	ıbut L	evel	: 3)

Analysis Type:	Modify input values by temperature/moisture
Method:	Resilient Modulus (psi)

Resilient Modulus (psi) 25000.0

Use Correction factor for NDT modulus?	-
NDT Correction Factor:	-

Identifiers

Field	Value
Display name/identifier	Crushed stone
Description of object	Default material
Author	AASHTO
Date Created	1/1/2011 12:00:00 AM
Approver	
Date approved	1/1/2011 12:00:00 AM
State	
District	
County	
Highway	
Direction of Travel	
From station (miles)	
To station (miles)	
Province	
User defined field 1	
User defined field 2	
User defined field 3	
Revision Number	20

Sieve

Liquid Limit	6.0
Plasticity Index	1.0
Is layer compacted?	True

	Is User Defined?	Value
Maximum dry unit weight (pcf)	False	127.7
Saturated hydraulic conductivity (ft/hr)	False	5.054e-02
Specific gravity of solids	False	2.7
Water Content (%)	False	7.4

User-defined Soil Water Characteristic Curve (SWCC)		
Is User Defined?	False	
af	7.2555	
bf	1.3328	
cf	0.8242	
hr	117.4000	

Sieve Size	% Passing
0.001mm	
0.002mm	
0.020mm	
#200	8.7
#100	
#80	12.9
#60	
#50	
#40	20.0
#30	
#20	
#16	
#10	33.8
#8	
#4	44.7
3/8-in.	57.2
1/2-in.	63.1
3/4-in.	72.7
1-in.	78.8
1 1/2-in.	85.8
2-in.	91.6
2 1/2-in.	
3-in.	
3 1/2-in.	97.6

Report generated on: 1/5/2022 12:55 PM

Version: 2.3.1+66

Created by: on: 8/5/2016 12:00 AM







Layer 3 Subgrade : A-1-b (Pit run) R value 40

Unbound	
Layer thickness (in)	12.0
Poisson's ratio	0.35
Coefficient of lateral earth pressure (k0)	0.5

Modulus	(Input	Level:	3)
inoaaiao j	Jude		

Analysis Type:	Modify input values by temperature/moisture
Method:	Resilient Modulus (psi)

Resilient Modulus (psi	
9494.0	

Use Correction factor for NDT modulus?	-
NDT Correction Factor:	-

Identifiers

Field	Value
Display name/identifier	A-1-b (Pit run) R value 40
Description of object	Default material
Author	AASHTO
Date Created	1/1/2011 12:00:00 AM
Approver	
Date approved	1/1/2011 12:00:00 AM
State	
District	
County	
Highway	
Direction of Travel	
From station (miles)	
To station (miles)	
Province	
User defined field 1	
User defined field 2	
User defined field 3	
Revision Number	0

Sieve

Liquid Limit	11.0
Plasticity Index	1.0
Is layer compacted?	True

	Is User Defined?	Value
Maximum dry unit weight (pcf)	False	124.2
Saturated hydraulic conductivity (ft/hr)	False	2.303e-03
Specific gravity of solids	False	2.7
Water Content (%)	False	9.1

User-defined Soil Water Characteristic Curve (SWCC)		
Is User Defined? False		
af	5.8206	
bf 0.4621		
cf 3.8497		
hr 126.8000		

Sieve Size	% Passing
0.001mm	
0.002mm	
0.020mm	
#200	13.4
#100	
#80	20.8
#60	
#50	
#40	37.6
#30	
#20	
#16	
#10	64.0
#8	
#4	74.2
3/8-in.	82.3
1/2-in.	85.8
3/4-in.	90.8
1-in.	93.6
1 1/2-in.	96.7
2-in.	98.4
2 1/2-in.	
3-in.	
3 1/2-in.	99.4

Report generated on: 1/5/2022 12:55 PM

Version: 2.3.1+66

Created by: on: 8/5/2016 12:00 AM







Layer 4 Subgrade : A-6

Unbound	
Layer thickness (in)	Semi-infinite
Poisson's ratio	0.35
Coefficient of lateral earth pressure (k0)	0.5

Modulus (Input Level: 3)

Analysis Type: Modify input values by temperature/moisture		
Method:	Resilient Modulus (psi)	

Resilient Modulus (psi) 5355.0

Use Correction factor for NDT modulus?	-
NDT Correction Factor:	-

Identifiers

Field	Value
Display name/identifier	A-6
Description of object	Default material
Author	AASHTO
Date Created	1/1/2011 12:00:00 AM
Approver	
Date approved	1/1/2011 12:00:00 AM
State	
District	
County	
Highway	
Direction of Travel	
From station (miles)	
To station (miles)	
Province	
User defined field 1	
User defined field 2	
User defined field 3	
Revision Number	0

Sieve

Liquid Limit	33.0
Plasticity Index	16.0
Is layer compacted?	True

	Is User Defined?	Value
,	False	108.6
Saturated hydraulic conductivity (ft/hr)	False	1.856e-05
Specific gravity of solids	False	2.7
Water Content (%)	False	17.1

User-defined Soil Water Characteristic Curve (SWCC)			
Is User Defined?			
af	108.4091		
bf 0.6801			
cf	0.2161		
hr	500.0000		

Sieve Size	% Passing
0.001mm	-
0.002mm	
0.020mm	
#200	63.2
#100	
#80	73.5
#60	
#50	
#40	82.4
#30	
#20	
#16	
#10	90.2
#8	
#4	93.5
3/8-in.	96.4
1/2-in.	97.4
3/4-in.	98.4
1-in.	99.0
1 1/2-in.	99.5
2-in.	99.8
2 1/2-in.	
3-in.	
3 1/2-in.	100.0

Report generated on: 1/5/2022 12:55 PM

Version: 2.3.1+66

Created by: on: 8/5/2016 12:00 AM





Calibration Coefficients

PCC Faulting						
$C_{12} = C_1 + (C_2)$						
$C_{34} = C_3 + (C_3)$	•	,	147-4 D \ 2 ^C 6			
$FaultMax_0 =$	$FaultMax_0 = C_{12} * \delta_{curling} * \left[\log(1 + C_5 * 5.0^{EROD}) * \log\left(P_{200} * \frac{WetDays}{p_S}\right) \right]^{C_6}$					
$FaultMax_i =$	$FaultMax_0 + C_7 * \sum_{j=1}^{m}$	$DE_j * \log(1 + C_5 * 5.0^E)$	ROD)C ₆			
$\Delta Fault_i = C_{34}$	$*(FaultMax_{i-1} - Fa$	$ult_{i-1})^2 * DE_i$				
$C_8 = DowelDe$	$C_8 = DowelDeterioration$					
C1: 0.5104	C1: 0.5104					
C5: 5999 C6: 0.8404 C7: 5.9293 C8: 400						
PCC Reliability Faulting Standard Deviation						
0.0831*Pow(FAULT,0.3426) + 0.00521						

IRI-jpcp		
C1 - Cracking	C1: 0.8203	C2: 0.4417
C2 - Spalling	C3: 1.4929	C4: 25.24
C3 - Faulting	Reliability Stan	dard Deviation
C4 - Site Factor	5.4	

PCC Cracking					
MD	Fatigue Coefficients		Cracking Coefficients		
$\log(N) = C1 \cdot (\frac{MR}{R})^{C2}$	C1: 2	C2: 1.22	C4: 0.6	C5: -2.05	
σ	PCC Reliability Cr	acking Standard D	eviation		
$CRK = \frac{100}{1 + C4 FD^{C5}}$	Pow(57.08*CRA0	CK,0.33) + 1.5			
$\frac{CRR - \frac{1}{1 + C4 FD^{CS}}}{1 + C4 FD^{CS}}$					

Report generated on: 1/5/2022 12:55 PM

Version: 2.3.1+66 Created by: on: 8/5/2016 12:00 AM



APPENDIX D

20 and 30-YEAR
FLEXIBLE ME-PAVEMENT DESIGN OUTPUT
SHEETS 24 ½ ROAD



24.5 Road (Updated)(20-year)File Name: C:\Users\goldbaum\Documents\My PMED Design\My ME Design\Projects\F.5 Road\24.5 Road (Updated)(20-year).dgpx



Design Inputs

Design Life: 20 years Base construction: May, 2022 Climate Data 39.134, -108.538

Sources (Lat/Lon) Design Type: **FLEXIBLE** Pavement construction: June, 2022

> September, 2022 Traffic opening:

Design Structure

Layer type	Material Type	Thickness (in)	
Flexible	R3 Level 1 SX(100) PG 64-28	2.0	
Flexible	R2 Level 1 SX(100) PG 64-22	5.0	
NonStabilized	Crushed gravel	8.0	
NonStabilized	A-1-b	10.0	
Subgrade	A-6 (R-Value = 5)	Semi-infinite	

Volumetric at Construction:		
Effective binder content (%)	10.7	
Air voids (%)	5.7	

Traffic

Age (year)	Heavy Trucks (cumulative)	
2022 (initial)	1,078	
2032 (10 years)	2,610,580	
2042 (20 years)	5,855,820	

Design Outputs

Distress Prediction Summary

Distress Type		Distress @ Specified Reliability		Reliability (%)	
	Target	Predicted	Target	Achieved	Satisfied?
Terminal IRI (in/mile)	200.00	176.69	90.00	97.38	Pass
Permanent deformation - total pavement (in)	0.80	0.70	90.00	98.40	Pass
AC bottom-up fatigue cracking (% lane area)	25.00	22.69	90.00	92.80	Pass
AC thermal cracking (ft/mile)	1500.00	190.41	90.00	100.00	Pass
AC top-down fatigue cracking (ft/mile)	3000.00	445.43	90.00	100.00	Pass
Permanent deformation - AC only (in)	0.65	0.51	90.00	99.52	Pass

Report generated on: 7/12/2023 3:42 PM

Version: 2.3.1+66

Created by: on: 8/26/2015 12:00 AM



