	C	$\tilde{(0)}$	RAN
City of Grand Ju Community Dev Planning ! Zor 250 North 5th S Grand Junction	relopment Department ing ! Code Enforcement treet CO 81501-2668	Phone: (970) 244-1430 FAX: (970) 256-4031	
FAX TRANSMITTAL			
DATE:	7-16-03	21 	
то:	Liz Wright		
FAX NUMBER:	245, - 9538		
PHONE NUMBER:	245-1600		
Dakota (Get amo	West 2 - Disbursem unt from DIA)	ent Agreement	
FROM:	haura Lambert	3	
FAX NUMBER:			
PHONE NUMBER:	256-4155	12.2	
THIS FAX CONSISTS	DF 5 PAGES (INCLUDING COV	/ER SHEET)	

K)

Wendy Spurr - Dakota West

From:	John Shaver		
To:	Lori Bowers		
Date:	7/2/03 10:47AM		
Subject:	Dakota West		

Page 1

Lori,

I write in response to your request for an opinion on the June 27, 2003 letter from the Grand Junction Drainage District concerning the Dakota West subdivision, FP 2003-079.

It appears from that letter and the attached deed and aerial photograph that the drainage district has a legal interest in, on, along and across a portion of the property that is the subject of this application. While the District's letter does not state the width of access required for the District's facilities, the request and supporting documentation reasonably appear to be valid. I would advise that you request that the Developer meet with the District and clarify what width the district reasonably requires and that the same be memorialized on the plat as a "irrigation and drainage easement."

If you have questions or if I may otherwise be of assistance to you on this or any other matter, please let me know. Please enter this e-mail message as "review agency comments" on the development application.

From:	Peter Krick
To:	Lori Bowers
Date:	6/18/03 2:25PM
Subject:	Dakota West Subdivision

 $\bigcirc$ 

Lori,

I have reviewed the revised Title Commitment for this project. I have no additional comments. I am forwarding the revised Commitment to John Shaver for his use. Peter

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Pag

From:	Peter Krick
To:	Lori Bowers
Date:	6/17/03 4:04PM
Subject:	Dakota West

Lori,

I spoke with John Shaver concerning some title issues (problems) with the current Title Commitment. I had a conference with Dennis Shellhorn with Thompson Langford Corp. and he has called the Title Company. The Title Company will be issuing a new, updated and revised commitment for this project. It should take about 1 or 2 days for this to happen. When I get the new Policy, I will review it with our legal department and everything should be ready for signing of the Mylar. However, I do not know at this time if the Mylar will change between now and then. The client will be taking a chance if they get all signatures now.

0

Peter

To: Rob + Gina

 $\bigcirc$ 

Lori Bowers - Re: Dakota West Subdivision Irrigation

From:	John Shaver
To:	Lori Bowers
Date:	6/6/03 2:02PM
Subject:	Re: Dakota West Subdivision Irrigation

Lori,

As much as they want to drag you in, don't let them. Our issue pertains to the easement and the relocation/conveyance of that vis a vis developability; as you know we don't have a dog in the fight over who gets water, how much water they get (or don't get) etc. The neighbors have civil remedies that I will be pleased to explain to them/encourage them to pursue.

>>> Lori Bowers 06/05/03 09:09AM >>> John.

I'm not sure how to handle the numerous phone calls I am receiving regarding Dakota West and the irrigation issues on this property. I sent a letter yesterday to the Cantrells asking them to give me an update as to the irrigation issues on this property, but until I hear from them I'm not sure what to do. I have received numerous phone calls and have had several people come to the counter complaining about the Cantrell's and how they have interrupted/shut-off irrigation water to neighboring properties; have crossed driveways without permission; are building headgates on other people's property without permission; and it is rumored that they are not going to provide irrigation water to the subdivision because it is so much trouble. Laura Lamberty has been fielding most of the irrigation issues but she is out of the office this week. I am aware that they were planning a blanket easement for irrigation over the property until these issues are resolved. Is this a civil matter or do I need to do something other than what I have done? Thanks for any input you can give me.

CC: Dan Wilson

Pag

appreciate it. I'm not sure how to answer some of the questions that the neighbors are asking me because I'm not really sure what has been done and what has not. Thanks for your cooperation in this matter.

Sincerely,

20. 1. 1.

City of Grand Junction

Jui V. Bonen

Lori V. Bowers, Senior Planner Community Development Department



THOMPSON - LANGFORD CORPORATION ENGINEERS AND LAND SURVEYORS tic@ticwest.com Feosimile (970) 241-2845 Telephone: (970) 243-6067

529 25 1/2 Rd, Grand Function, CO 81505

		TRAN	ISM	ITTAL	DE
To: From: Date: Re:	Lori Bowers Jeff Mace 05/06/03 Dakota West	Subdivision Fil	ing 2	COM	RECEIVED MAY 0 6 2003 MUNITY DEVELOPMENT DEPT.
We are	sending you:	Attached	Unde	r separate cover	
Via: [	JUSPS	FedEx	8	Delivery	
□ Origir	nals 🛛 Prin	ts 🛛 Cop	oies	D,	
Copies	i	ltem		De	escription and Remarks
2	Plat for the a	above referenced	l project		
COMME	ENTS:				
These a	re transmitted a	s checked below:			
Ger A	pproval	⊠For	your Use		As Requested
SFor R	leview and Com	ment			

IF ENCLOSURES ARE NOT AS NOTED, PLEASE NOTIFY US IMMEDIATELY

9-25-03; 7:41AM;Elam Const., Inc.

# SUPERPAVE METHOD ASPHALTIC CONCRETE JOB MIX FORMULA GRADING "SX", 75 DESIGN GYRATIONS, PG 64-22 ASPHALT CEMENT

## Elam Construction, Inc. Mule Farm Pit 2003 House Mix

Prepared For:

Elem Construction, Inc. 1225 S. 7<sup>th</sup> Street Grand Junction, Colorado 81501

Prepared by:

Western Colorado Testing, Inc. 529 25½ Road, Suite B-101 Grand Junction, Colorado 81505 (970) 241-7700

> Date: May 8, 2003 Job No.: 102303A

9-25-03; 7:4:AM;Elam Const., Inc.





# 3/ 14

# SUPERPAVE METHOD ASPHALTIC CONCRETE JOB MIX FORMULA GRADING "SX", 75 Design Gyrations, PG 64-22 ASPHALT CEMENT

Elam Construction, Inc. Mule Farm Pit 2003 House Mix

**Prepared** For:

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. Prepared by:

Western Colorado Testing, Inc. 529 25 1/2 Road, Suite B101 Grand Junction, Colorado 81505 (970) 241-7700

> Date: May 8, 2003 Job No.: 102303A

:970 245 7716

Elam Construction, Inc. SUPERPAVE Method Mix Design Grading "SX", 75 Gyrations, PG 64-22 Binder Mule Farm Pit - 2003 House Mix May 8, 2003; WCT #102303A

#### Mixture Aggregate Qualities and Moisture Susceptibility

Specific gravities and absorption properties of the individual aggregate stockpiles and composite mixture blend are:

- and - Test	5/8	3/8*	Grushed	Natural	Comp.
Fine Addresate (CE-2 4102)	Rock	Recat	Eines	Fines	
Builly Days Co. C	0.004	0 501	2.506	0.565	0.505
Bulk Dry Sp.G., g/cc	2.604	2.591	2.596	2.505	2.595
Bulk SSD Sp.G., g/cc	2.637	2.630	2.633	2.607	2.631
Effective Sp.G., g/cc	-	-	-	-	2.666
Apparent Sp.G., g/cc	2.694	2.696	2.696	2.676	2.693
Absorption, % Water	1.30	1.50	1.43	1.61	1.41
Absorption, % AC (Pba)	-			-	1.06

Supplemental aggregate quality tests required by the project specifications for the composite material include:

				115 6 2		<u></u>	
L.A. Abrasion, % Loss, (@500rev)			1	5	45 1	Max.	AASHTO T-96
Fractured Faces, % (2 or more)			9	5	70 Min. C		CP-45
Fine Aggregate Angularity		48 45 Min.		CP-L 5113			
Sand Equivalent Value		7	2		-	AASHTO T-176	
Liquid Limit	Cr. F.	Naturals	N/V	N/V		_	AASHTO T-89
Pl. Index	Cr. F.	Naturals	N/P	N/P	N/P	N/P	AASHTO T-90

Moisture susceptibility testing was performed during the final phase of the mixture development. The Resistance of Compacted Bituminous Mixture to Moisture Induced Damage "Lottman" test was performed to assess the stripping potential of the mixture. The result of the testing is summarized below with complete data located in Appendix C of this report.

den 1. 1997, de margin de la destructura destructura de la destructura de la destructura de la destruc	Rasult	
Dry Tensile Strength, kpa (psi)	720 (104)	205 (30) Min.
Wet Tensile Strength, kPa (psi)	599 (87)	
Tensile Strength Retained, %	83	80 Minimum

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Elam Construction, Inc. SUPERPAVE Method Mix Design Grading "SX", 75 Gyrations, PG 64-22 Binder Mule Farm Pit - 2003 House Mix May 8, 2003; WCT #102303A

dentral a		Steve Size -		Sumportive	Induction	
		Contraction of the	(S)	S PAR	CONTRACTOR -	
5/8" Crushed Rock	30	37.5	1 1/2	100	(100)	
3/8" Crushed Rock	10	25.0	1	100	(100)	
Crushed Fines	50	19.0	34	100	(100)	
Natural Fines	10	12.5	4	96	(90-100)	
		9.5	3/8	84	(6)	
Contraction and the second		4.75	No.4	54	(5)	
Comb. Agg. Bulk Sp.Gr. (Gab)	2.595	2.36	No.8	37	(5)	
Fine Agg. (-)#4 Bulk Sp.Gr.	2.593	1.18	No.15	27	(-)	
Mix Effective Sp.Gr. (Gse)	2.666	0.600	No.30	21	(4)	
Agg. Apparent Sp.Gr. (Gsa)	2.693	0.300	No.50	15	(-)	
Asphalt Absorption, % (Pba)	1.06	0.150	No.100	9	(-)	
Sp. Gr. of AC (Gb) (est.)	1.03	0.075	No.200	5.7	(2)	

The recommended optimum asphalt content is 6.3 percent by total weight of mixture (based on 4.0% voids). The project specifications allow for a production asphalt content tolerance of (+/-) 0.3% of this value. The properties of the asphaltic concrete at this oil content and design gyrations (except where noted) are:

- Destor Mik Property	Found	Specification	Printing C
HVEEM Stabilometer Value	32	28 Minimum	CP-L 5106
Compacted Modure Sp.Gr., g/cc (Gmb)	2.326	٠	CP-L5115, 5103
Compacted Mixture Unit Wt., pcf	144.8	-	62.24 Conv.
Maxdmum Theo. Sp.Gr., g/cc (Gmm)	2.423	*	CP-51
Maximum Theoretical Density, pcf	150.8	-	62.24 Conv.
Effective Voids, % N(ini) (Va)	12.6	(For info)	CP-L 5115
Effective Voids, % N(des)(Va)	4.0	3.5-4.5	CP-L 5115
Voids in Min. Agg.,% N(des)(VMA)	16.0	14.0 Minimum	CP-48
Voids Filled, % N(des) (VFA)	75	65-80	Al, SP-2
Effective AC Content, % (Pbe)	5.3	-	AI, SP-2
Dust to Asphalt Ratio (DP)	1.1	0.8-1.6 (For info)	CP-50

Elam Construction, Inc. SUPERPAVE Method Mix Design Grading "SX", 75 Gyrations, PG 64-22 Binder Mule Farm Pit - 2003 House Mix May 8, 2003; WCT #102303A

#### Limitations

The asphaltic concrete job mix formula and recommendations given herein are based upon specific materials, gradations and design procedures. Variations in test results for laboratory prepared mixes due to multi-laboratory precision, variations in materials, gradations and design procedures are to be expected. All of these factors should be considered when job mix verification of laboratory mixes are performed.

All of the physical properties of the mix should be retested and re-evaluated for hot plant produced material. It is often necessary to make adjustments to the job mix formula due to the variations between the laboratory tested and field produced material. Should the source or physical characteristics of the materials change substantially, the development of a new or revised job mix formula is recommended.

The information presented in this report is specific to the subject project only. Any re-use of the information should not be considered without the knowledge and written consent of WCT.

If there are any questions or additional information needed, please feel free to contact our office, 970-241-7700.

Respectfully Submitte WESTERN COLORADO 2475 John E. Vasey, P. Construction Servi

JEV/mh F/jobs2003/1023 A Mix Design

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Elam Construction, Inc. SUPERPAVE Method Mix Design Grading "SX", 75 Gyrations, PG 64-22 Binder Mule Farm Pit - 2003 House Mix May 8, 2003; WCT #102303A

# Appendices

A	Superpave Summary - Varying AC Mix Properties
B	Varying AC Mixture Property Graphs
С	Detailed Lottman Test Results
D	Composite Gradation Summary Stockpile Data
E	Composite Gradation 0.45 Sieve Power Graph

Elam Construction SUPERPAVE Method JMF Grading "SX", 75 Design Gyrations

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# Appendix A

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SUPERPAVE VOLUMETRIC	SUMMAR	Y		8 6 8
Varying Asphalt Content Physi	ical Prop	pertie	8	
Mixture Grading Type:	"SX	•, 1/2•	Max. Nomi	nal
SUPERPAVE Gyration Data:	N(ini)-	7	N(das)=	75
Measured Individual Mixture Properties	Var	ying Ad	t Resul	lts
Asphalt Content by Total Wt. of Mix, % (Fb)	5.8	6.3	6.8	7.3
Specimen Height- N(ini), mm	71.7	70.6	68.9	67.5
specimen Height- N(des), mm	65.2	64.3	62.B	61.4
Max. Theoretical Sp. Gr., g/cc (Gmm)	2.441	2.423	2.406	2.389
Max. Theoretical Unit Wt., pcf	151.9	150.8	149.7	148.7
Compacted Mix Bulk Sp Gr- N(des), g/cc (Gmb)	2.294	2.326	2.349	2.363
Compacted Mix Unit Wt N(des), pcf	142.8	144.8	146.2	147.1
Calc. Mix Bulk SpGr N(ini), g/cc (Gmb)	2.086	2.118	2.141	2.149
Calc. Mix Unit Wt N(ini), pcf	129.8	131.9	133.3	133.8
Calculated Air Voids- N(ini), % (Va)	14.5	12.6	11.0	10.0
Calculated Air Voids- N(des), % (Va)	6.0	4.0	2.4	1.1
Calc. Voids in Min. Agg N(des), + (VNA)	16.7	16.0	15.6	15.6
Calculated Voids Filled- N(des), & (VFA)	64	75	85	93
Effective Asphalt Content of Mix, % (Pbe)	4.8	5,3	5.8	6.3
Dust to Effective AC Proportion (DP)	0.9	0.8	0.8	0.7
Hveem Stability Index	31	32	34	35

Data Used For Volumetric Calculations							
Trial Max. Theo. Sp. Gr., g/cc 2.389 AT	7.3 \$ AC						
Combined Aggregate Bulk Sp. Gr., g/cc (Gsb)	2.595						
Fine Aggregate Bulk Specific Gravity, g/cc	2.593						
Composite Aggregate Blend Pass #200 Sieve, #	5.7						
Calculated Mix Effective Sp. Gr., g/cc (Gse)	2.666						
Calculated Asphalt Absorption, & (Pba)	1.06						
Asphalt Cement Estimated Sp. Gr., g/cc (Gb)	1.03						

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Mule Farm Pit - House Mix

WCT Job No. 102303A

May 8, 2003

Elant Construction SUPERPAVE Method JMF Grading "SX", 75 Design Gyrations



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Elam Construction SUPERPAVE Method JMF Grading "SX", 75 Design Gyrations

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Mule Farm Pit - House Mix WCT Job No. 102303A May 8, 2003

# Appendix C RESISTANCE OF COMPACTED BITUMINOUS MIXTURE TO MOISTURE INDUCED DAMAGE

Mixture Moisture Suseptability - Lottman Test Results

Test Procedure: CDOT CL-L 5109, Method B (5 minute saturation)

Mix Data

Mix Type:	75 Design	Gyration Superpav	e Method (CDOT	CP-L 5115}	
Grading:	"SX"	1/2" Maximum Non	minal Mixture		
Grade of Aspha	lt Cement Gra	de Used: PG	64-22		
Asphalt Cement	Supplier:	Koch Performance	Asphalt		
Asphalt Mixing	Temp. (C):	163 Asphalt Co	mpaction Temp.	(C) :	149
Asphalt Conten	t of Specimen	s by Total Wt. Of :	Mix, 4:	-	6.3
Max. Theo. Sp.	Gr. (Gmm) of	Mix at AC Content	, g/cc: .		2.423
Antistripping	agent Used in	the Mixture:	Liquid Amin	e (Agrigrij	a)
			the second se		

Compacted Specimen Test Data

		bi	RY SUBSI	48		WET SUBSET				
	Compacted Specimens		Total Load	otal Tensile Load Strength		Compacted Specimens		Total Load	Tensile Strength	
	Sp. Gr., g/cc	Air Voids,	Lbs.	kPa	psi	Sp. Gr., g/cc	Air Voids,	Lbs.	kPa	psi
1	2.270	6.3	1658	732	106	2.273	6.2	1304	574	83
2	2.269	6.4	1796	793	115	2.268	6.4	1372	605	88
3	2.254	7.0	1440	634	92	2.254	7.0	1400	617	90
Ave.	2.264	6.5	1631	720	104	2.265	6.5	1359	599	87

pegimen Compagied Height Data							
	Dry Sul	bset	Wet Subset				
1	2.524	in	2.532	in			
2	2.526	in	2.529	in			
3	2.532	in	2.529	in			
Ave.	2.527	in	2.530	in			

Wet Subset Saturation Data	
Average Saturation, 8:	74
Average Swell, %:	(-)0.3

Tensile Strength Ratio (TSR)

83

Test Specimen Obervations Noted:

Elam Construction SUPERPAVE Method JMF Grading "SX", 75 Gyrations

Mule Farm Pit - House Mix WCT Job No. 102303A May 8, 2003

# Appendix D

MIXTURE GRADATION SUMMARY

## Individual Stockpiles and Combined Mixture

Test Procedure Used: CDOT CP 31a and 31b Max. Nominal Particle Size: Grading Specification of Mix: CDOT "SX" 1/2 Individual Stockpiles Blend % 30.0 10.0 50.0 10.0 Job Mix Grading Sieve Size B C D E F Composite A Tolerances Specification 37.5mm/1 1/2" 100 100 100 100 100 100 100 31.0mm/1 1/4" 100 100 100 100 100 100 100 100 25,0mm/1" 100 100 100 100 100 100 100 100 19.0mm/3/4" 100 100 100 100 100 100 100 90 minimum 12.5mm/1/2" 86 100 96 90-100 9.5mm/3/8" 86 100 98 51 84 78-90 -4.75mm/No.4 4 5 88 83 54 49-59 2 76 2.36mm/No.8 1 57 37 27-37 28-58 1.18mm/No.16 1 1 38 72 27 --1 1 27 69 21 0.600mm/No.30 17-25 \_ 15 0.300mm/No.50 1 1 20 43 --13 19 0.150mm/No.100 1 1 9 white -10.6 0.075mm/No.200 0.6 0.8 8.8 5.7 3.7-7.7 2 - 10Stockpiles Blend & 5/8" Crushed Rock 30.0 A, B 4 C Ind. Stockpile results were A= 8= 3/8" Crushed Rock 10.0 provided by the client from crusher 50.0 C= **Crushed Fines** control data (design batched to targets). Natural Fines D =10.0 OR 0.0 E= D Ind. Stockpile results 0.0 F= tested by the mix design lab.

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Elam Construction SUPERPAVE Method JMF Grading "SX", 75 Gyrations

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Mule Farm Pit - House Mbr WCT Job No. 102303A May 8, 2003 1 . 1



Appendix E

Location: 🧾	3088 D'12 Rd	Project Name: Da Kota West	ItI
STEP	ACTIVITY	SUBMITTAL ITEMS	SSID RE
1	Pre-construction	<ul> <li>City Approval of Construction Drawings</li> <li>Pre-construction Notice</li> <li>Work within Public ROW Permit</li> <li>NPDES Permit</li> <li>Improvements Agreement/Guarantee</li> </ul>	VII-5 VII-5 VII-5 VII-5 VII-2,3
2	Grading Street Rough Cut Sanitary Sewer Water Irrigation Other Utilities Sub cmda	<ul> <li>Construction Report: Grading and Pipeline Phase</li> <li>Construction Report: Concrete and Pavement Prep.</li> <li>Revised Asphalt Design (if necessary) Alex</li> <li>Request City Lamping of Sewerline G</li> <li>Complete Compaction Tests for all utilities, subgrade, and base course under concrete. All at</li> </ul>	X-4 X-3 VII-6
Aun ( (hu Sign and date	Sub-grade Base Course Concrete Placement 9/23/03 OKAY FOR CONCRETE	<ul> <li>A Letter from water purveyor stating passage of pressure and disinfection tests</li> <li>A Sanitary sewer pressure test after wet utility installation.</li> <li>C Redlined Sanitation Sewer As-Builts</li> <li>C Redlined Storm Sewer As-Builts</li> <li>C Complete CompactionTests for base course under asphalt. All at once just prior to pavement.</li> </ul>	VII-5 VII-6 VII-6 VII-6
Sign and date	OKAY FOR PAVEMENT	°	
3	Asphalt Pavement Dry Utilities Traffic Control Facilities Monumentation Permanent On-Site Benchmark (Subdivisions Only)	<ul> <li>Complete QA Reports for asphalt and concrete.</li> <li>Construction Report: Concrete and Pavement Placement</li> <li>Complete Set of As-Built Drawings</li> <li>Request for City Initial Inspection</li> <li>Letter from PE stating passage of sanitary sewer pressure test after dry utility installation.</li> </ul>	X-2 IX-3 to IX-7 VII-6 VII-6
Λ	Warranty Period	O Request for City Final Inspection	VII-6

of reproducible drawings. A copy of this form, which has approval, City Engineering will st Post-It\* Fax Note been completed for the specific pi 7671 Date preconstruction meeting. To # of pages 2. From vill make every effort to City Engineering approval of sub Co./Dept.

provide timely approvals in order construction proceeds, then City

3. The "OKAY FOR CONCRETE' Fax # Development Engineer prior to 1 THE DEVELOPER'S KEDI VI.

a Co. Phone # Phone # Fax #

in a timely manner as

pector or the

signatures. IT IS LS.

Distribution for Signatures: Construction Inspector and Development Engineer May 2002

Final Drainage Report

1.

# **Dakota West Subdivision**

February 27, 2003

Prepared for:

G & R West, LLC Mr. Rob Cantrell 2650 El Corona Dr. Grand Junction, CO 81501

Prepared by:

THOMPSON-LANGFORD CORPORATION 529 251/2 RD., SUITE B-210 Grand Junction, CO 81505 PH. 243-6067

Job No. 0543-001

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Engin	eer's Certification	3
I,	GENERAL LOCATION AND DESCRIPTION A. Site and Major Basin Location B. Site and Major Basin Description	4 4 4
II.	EXISTING DRAINAGE CONDITIONS A. Major Basin B. Site	4 4 5
Π.	PROPOSED DRAINAGE CONDITIONS A. Changes in Drainage Patterns B. Maintenance Issues	5 5 5
IV.	DESIGN CRITERIA AND APPROACH A. General Considerations B. Hydrology C. Hydraulics	6 6 7
V.	RESULTS AND CONCLUSIONS A. Retention Volume B. Runoff Rates for 2 and 100 Year Storms C. Overall Compliance	7 7 8 8

# APPENDIX

1.

Time of Concentration, Rainfall Intensities and Runoff Rate -Basin H1 Time of Concentration, Rainfall Intensities and Runoff Rate -Basin H2 Time of Concentration, Rainfall Intensities and Runoff Rate -Basin OS1 Time of Concentration, Rainfall Intensities and Runoff Rate -Basin D1 Time of Concentration, Rainfall Intensities and Runoff Rate -Basin D2 Retention Pond Calculations Rational Runoff Coefficients for Historical and Developed Conditions SCS Soils Map and narrative Hydrologic Soils Group Reference Historical Drainage Conditions – Figure 1 Proposed Drainage Conditions – Figure 2

# Engineer's Certification

۱." •

I hereby certify that this report was prepared by me or under my direct supervision for the Owner's hereof.

Jeffrey W. Mace, P.E.

Reg. No. 37343



#### I. GENERAL LOCATION AND DESCRIPTION:

#### A. Site and Major Basin Location:

The proposed Dakota West Subdivision is located east of 30 <sup>3</sup>/<sub>4</sub> Road and north of D <sup>1</sup>/<sub>2</sub> Road. In more legal terms, it lies within the Southeast <sup>1</sup>/<sub>4</sub> of the Northeast <sup>1</sup>/<sub>4</sub> of Section 16, Township 1 South, Range 1 East of the Ute Meridian.

#### B. Site and Major Basin Description:

The proposed development is adjacent to an area wide basin known as the Lewis Wash Watershed. This basin originates in the Bookcliffs area and drains from the northeast to the southwest ultimately discharging into the Colorado River.

The site is made up of three separate parcels all of which are included within a sub basin that contributes to the Lewis Wash Watershed. There are existing features that define this sub basin. There is a topographical ridge along the northern edge separating it from the development adjacent to Gunnison Avenue. To the east, 31 Road forms the watershed boundary and 30 <sup>3</sup>/<sub>4</sub> Road to the west. The southern boundary is formed by D <sup>1</sup>/<sub>2</sub> Road between 30 <sup>3</sup>/<sub>4</sub> Road and 31 Road. The western portion of this sub basin drains into a storm sewer that crosses under D <sup>1</sup>/<sub>2</sub> Road, runs approximately 1,000 feet to the south and then east into Lewis Wash. A culvert under D <sup>1</sup>/<sub>2</sub> Road, at the access point of the proposed development, conveys flows from the eastern portion into an irrigation ditch that flows south and into the same storm sewer.

The project site is 11.06 acres with approximately 0.9 acres being an existing home site and the remainder previously undeveloped ground covered by natural vegetation. According to the Soil Survey, Series 1940, No. 19, performed by the U.S. Department of Agriculture's Soil Conservation Service for the Grand Junction area, the soils present at the site are a combination of Billings Silty Clay ( $B_A$ ) and Billings Silty Clay Loam ( $B_C$ ). Billings Silty Clay Loam is predominate throughout the Grand Valley with areas of Billings Silty Clay occurring toward the Colorado River south and southeast of Grand Junction. Both soil types are derived from alluvial deposits that came mostly from Mancos Shale with the Billings Silty Clay being harder and in most places darker. Surface runoff is slow to very slow, especially in areas with slopes less than one percent. Due to the massive subsoil and low permeability, internal drainage is also slow to very slow. A pre-development basin map has been included in the Appendix.

#### **II. EXISTING DRAINAGE CONDITIONS:**

#### A. Major Basin:

The predominant drainage pattern for the Lewis Wash area is characterized by overland flow sloping towards the Colorado River at varying grades. Channels and ditches intermittently cross the sloping ground surface collecting surface runoff as well as ground water and

typically flow from northeast to southwest. The construction of major arternal roads such as D Road and 31 Road also serves to intercept and collect surface water runoff. Consideration of these parameters led to the watershed boundary definitions of the major basin.

The existing drainage conditions adjacent to the project site are defined predominately by rural residential characteristics. There is a lack of drainage ways or any other formal stormwater conveyance along D ½ Road aside from the storm sewer crossing approximately 450 feet west. The only existing outfall adjacent to the proposed site is a 12" corrugated metal pipe under D ½ Road.

#### **B.** Site:

The project site is gradually sloping from northeast to southwest with approximate grades varying from zero to one percent. Currently, runoff from the western two parcels, Basin H-1, sheet flows across the site and collects in abandoned irrigation ditches. These ditches flow toward D  $\frac{1}{2}$  Road to a 12" CMP at the entrance to the site. The 12" CMP conveys flows under D  $\frac{1}{2}$  Road and into an irrigation waste ditch along the eastern boundary of the parcel south of D  $\frac{1}{2}$  Road. The eastern parcel, Basin H-2, and the adjacent property to the north, Basin OS-1, flow to a low point at the southern boundary where it appears to pond.

#### III PROPOSED DRAINAGE CONDITIONS:

#### A. Changes in Drainage Patterns

Historic drainage patterns will remain intact, where possible, in an effort to minimize the impact of the development of this parcel on surrounding properties. At a minimum, the fronts of the proposed lots will drain toward the street with an effort to drain as much of the lots to the street as grades will allow. Runoff from the majority of the site, Basin D-1, and the off site flows, Basin OS-1, will be collected in concrete curb and gutters and conveyed to a low point near the proposed entrance at D ½ Road and into inlets. Here storm water will be retained without release. The remaining area, Basin D-2, will be collected in curb and gutter and discharged at less than historic rates at the low point where run off currently collects.

#### **B.** Maintenance Issues:

Maintenance of the on-site collection and conveyance facilities within the right of way will be the responsibility of the City. Facilities outside of the right of way will be maintained by the Homeowners Association.

## IV DESIGN CRITERIA AND APPROACH:

#### A. General Considerations:

+ 8

Storm water runoff for the 2-year and 100-year events will be quantified using the Rational Method as detailed in Section VI "Hydrology" of the Storm water Management Manual for the City of Grand Junction and Mesa County dated May 1996.

The overall drainage patterns for the major basin are not being significantly altered. Notable differences in drainage will occur in the area of the proposed subdivision and these differences will be reflected in the runoff characteristics of the historic conditions versus those of the new development. The rate at which storm water runoff is drained from the project site will be increased due to the developed conditions. However, due to detention the cumulative effect of adding these flows to those of the other undeveloped areas in the major basin will not appreciably increase the 2-year or 100-year flows for the major drainage basin.

The 2-year and the 100-year design storms will be considered when sizing all proposed drainage features. On-site inlets, pipes, gutters, and swales will be sized to carry the 2-year storm water flows at a minimum. For events with flows greater than the 2-year storm, excess flow will be conveyed by the remainder of the street section. For areas where storm sewer pipe crosses through private property, or within easements, the storm sewer will be designed to carry the 100-year runoff volume while flowing 80% full.

The analysis and design procedures as outlined in the Storm water Management Manual for the City of Grand Junction and Mesa County (SWMM) will be adhered to during the design of all on-site collection and storm conveyance facilities proposed for the subdivision.

#### B. Hydrology:

According to the Soil Conservation Service soil survey for the Grand Junction Area, the dominant soil type is Billings Silty Clay (B<sub>A</sub>) and Billings Silty Clay Loam (B<sub>C</sub>) having a hydrologic soil group index of "B".

The maximum times of concentration used by the Modified Rational Method to determine maximum flow quantities for individual sub-basins will be a cumulative result of overland, curb and gutter, asphalt sheeting and storm sewer flow times.

For the determination of maximum flows, the total area of each sub-basin with its corresponding runoff coefficient will be used in the calculations. For the existing condition, the "natural" sub-basin will have uniform coefficients related to the hydrologic soil group. The affects of landscaping will be accounted for in the calculation of the composite "C" values for the developed area.

### C. Hydraulics:

Flow capacity of concrete pans, curb and gutter, and underground conduits will be calculated using Manning's Equation with the required flow resistance coefficients taken from appendices "G" and "H" of the SWWM.

### D. Retention Basin:

The total retention volume was determined per the procedure described in Section VIII.E.3 on page 13 of the SWMM. The 100-year developed runoff coefficient used in the equation for total retention volume was the same value as was used in the calculations for storm water runoff and sizing of the hydraulic features of the project and was derived from representative values given in Appendix B of the SWMM. The total precipitation value used in the equation was taken from Appendix A of the SWMM and the developed area in the equation was the total area of the watershed contributing to the retention basin.

A pumping system will be utilized to assure dissipation of the retention volume within the allowable 48 hour time period. The pump will be designed to discharge at a rate which will evacuate the pond within the 48 hours without exceeding the historic discharge.

#### V RESULTS AND CONCLUSIONS:

#### A. Retention Volume

The values used to determine the total retention volume have been reproduced in the following table.

Developed Runoff	Area Acres $(ft^2)$	Precipitation, P <sub>100, 24hr</sub>	Volume
Coefficient, C <sub>100d</sub>		in (ft)	(ft <sup>3</sup> )
0.39	11.55 (503,118)	2.01 (.1675)	32,866

#### **Total Retention Volume Calculation**

The rate required to drain the 24 hour, 100 year storm water runoff out of the retention pond within 48 hours is approximately 85 gpm or 0.19 cfs, well below the historic rate of 3.37 cfs. The parameters used in this estimation are reproduced in the table below.

Potention Volume	Allowable Time	Minimum Dequired	Minimum Paquirad
$(ft^3)$	(hours)	Pump Rate	Pump Rate
1		(gpm)	(cfs)
32,866	48	85.4	0.19

#### Soil Percolation Time, 24 Hour, 100 Year Storm Event

## B. Runoff Rates for 2 and 100 Year Storms

Each step of the calculations necessary for the Rational Method – Composite Runoff Coefficients, Time of Concentration and Rainfall Intensities, and Runoff Rates - have been incorporated into spreadsheets and attached to the Appendix of this report. These results were utilized to develop storm water runoff quantities at specific locations in the project site. Conveyance values for these points were compared to these results. The drainage plan drawings for the proposed conditions attached to this report show the locations isolated and analyzed for flow quantities.

Design Point No.	Developed Runoff (ft <sup>3</sup> /sec)	Allowable Runoff (ft <sup>3</sup> /sec)
1	7.2	7.2 (street capacity)
2	1.8	4.0 (Historic)
3	<3.4	3.4 (Historic)

Tabulated Runoff Rates at Specific Design Points for the 100-Year Storm Event

#### C. Overall Compliance

In conclusion, the retention volume designed on the project drawings has sufficient volume to retain total runoff for the 24 hour, 100 year storm event. Additionally, the 100-year storm water flow quantities conveyed by the curb, gutter and inlets are within allowable values.



Basin H1		L	S	Nor <i>N</i> *	V <sub>2</sub>	V100	Tt2	Tt100	Tc2	Tc100	i,	i <sub>100</sub>
	Descrip.	Length	Slope		Vel.	Vel.	Travel	Travel	Time of		Inter	nsity
	of Flow						Time	Time	Concer	ntration	Grd.	Jctn.
		ft.	%	coel.	fps	fps	min.	min.	min.	min.	Cu	ves
							Pg E-2	SWMM				
Basin H1												
	Overland Flow*	290.80	1.62%	0.120			44.78	26.43	62.5	43.2	0.33	1.69
Shallow (	Concentrated Flow**	669.00	0.56%	0.120	0.75	0.75	14.87	14.87				
	Channel Flow***	427.50	1.15%	0.025	2.50	3.73	2.85	1.91				

#### TIME OF CONCENTRATION and RAINFALL INTENSITIES For: Dakota West

\* N = Mannings n for Open Channel Flow calculations, N = Overland Flow Resistance Factor taken from Table "E-1" page E-5 of the SWMM.

\*\* Figure "E-3", Pg. E-9, Storm Water Management Manual was used for shallow flows.

\*\*\* Mannings Equa. was used to determine gutter and natural swale velocities. Mannings n=0.016 was used for curb and gutter, and n=0.050 was used for natural swales. For natural swales a flow of .25 cfs/AC was assumed for a 2 Year Storm and a flow of 1.25 cfs/AC was assumed for 100 Year Storm

#### RATIONAL CALCULATION OF DESIGN FLOWS

	С	Cf	*	A	Q
	Composite	Antecedent	Rainfall	Basin	Volume
	Coefficient	Precip. Fac.	Intensity	Area	
	n/a	n/a	in/hr	acres	cfs
Basin "H1"					
2-year	0.18	1.00	0.33	8.29	0.49 <<<<<<<<<<
100-year	0.24	1.00	1.69	8.29	3.37 <<<<<<<<<

\*The rainfall intensity is based on the formula presented on Table A-3 of the SWMM

#### TIME OF CONCENTRATION and RAINFALL INTENSITIES For: Dakota West

Basin H	2	L	S	NorN *	V <sub>2</sub>	V <sub>100</sub>	Tt2	Tt100	Tc2	Tc100	i,	i <sub>lco</sub>
	Descrip.	Length	Slope		Vel.	Vel.	Travel	Travel	Time of		Intens	ity
	of Flow						Time	Time	Concer	ntration	Grd. Jc	tn.
		ft.	%	coef.	fps	fps	min.	min.	min.	min.	Curve	S
							Pg E-2	SWMM				
Basin H2												
	Historic overland*	300	0.85%	0.030			19.60	11.57	29.3	21.2	0.55	2.E2
	Shallow Concentrated Flow**	161	0.74%	0.255	0.92	0.92	2.92	2.92				
	Shallow Concentrated Flow**	373	0.79%	0.255	0.92	0.92	6.76	6.76				

\* N = Mannings n for Open Channel Flow calculations, N = Overland Flow Resistance Factor taken from Table "E-1" page E-5 of the SWMM.

\*\* Figure "E-3", Pg. E-9, Storm Water Management Manual was used for shallow flows.

\*\*\* Mannings Equa. was used to determine gutter and natural swale velocities. Mannings n=0.016 was used for curb and gutter, and n=0.050 was used for natural swales. For natural swales a flow of .25 cfs/AC was assumed for a 2 Year Storm and a flow of 1.25 cfs/AC was assumed for 100 Year Storm

#### RATIONAL CALCULATION OF DESIGN FLOWS

	С	Cf	<b>I</b> *	Α	Q
	Composite	Antecedent	Rainfall	Basin	Volume
	Coefficient	Precip, Fac.	Intensity	Area	
	n/a	n/a	in/hr	acres	cfs
Basin "H2"					
2-year	0.18	1.00	0.55	6.36	0.63 <<<<<<<<<<<<<
100-year	0.24	1.00	2.62	6.36	4.00 <<<<<<<<<<<<<<

\*The rainfall intensity is based on the formula presented on Table A-3 of the SWMM

TIME O	F CONCENTRATION an	d RAINFA	LL INTENSI	TIES								
For: Da	ikota West											
Basin OS	1	L	S	NorN *	$V_2$	V100	Tt2	Tt100	Tc2	Tc100	1 <sub>2</sub>	i100
	Descrip.	Length	Slope		Vel.	Vel.	Travel	Travel	Time of		Intensi	ity
	of Flow						Time	Time	Concer	ntration	Grd. Jc	tn.
		ft.	%	coef.	fps	fps	min.	min.	min.	min.	Curve	S
							Pg E-2	SWMM				
Basin OSI	L,											
	Historic overland*	300	0.74%	0.030			20.72	12.23	23.6	15.1	0.63	3.0
5	shallow Concentrated Flow**	161	0.74%	0.255	0.92	0.92	2.92	2.92			· • • • • • • • • • • • • • • • • • • •	the factors

\* N = Mannings n for Open Channel Flow calculations, N = Overland Flow Resistance Factor taken from Table "E-1" page E-5 of the SWMM.

\*\* Figure "E-3", Pg. E-9, Storm Water Management Manual was used for shallow flows.

\*\*\* Mannings Equa. was used to determine gutter and natural swale velocities. Mannings n=0.016 was used for curb and gutter, and n=0.050 was used for natural swales. For natural swales a flow of .25 cfs/AC was assumed for a 2 Year Storm and a flow of 1.25 cfs/AC was assumed for 100 Year Storm

#### RATIONAL CALCULATION OF DESIGN FLOWS

	C	Cf	1*	A	Q
	Composite	Antecedent	Rainfall	Basin	Volume
	Coefficient	Precip. Fac.	Intensity	Area	
	n/a	n/a	in/hr	acres	cfs
Basin "OS1"					
2-year	0.18	1.00	0.63	3.69	0.42 <<<<<<<<<<
100-year	0.24	1.00	3.09	3.69	2.74 <<<<<<<<<<

\*The rainfall intensity is based on the formula presented on Table A-3 of the SWMM

#### TIME OF CONCENTRATION and RAINFALL INTENSITIES For: Dakota West BASIN D1

	L	S	N*	V <sub>2</sub>
Descrip. of Flow	Length	Slope	Mannings	Vel.
	ft.	%	coel.	fps
Overland*	300	0.74%	0.120	
Shallow Concentrated Flow**	159	0.74%	0.255	0.92
Curb and Gutter Flow	75.00	2.00%	0.016	2.68
(from SDSK calculator - d=	=2" for 2-`	Yr. & d=5'	' for 100-Yr.)	
Curb and Gutter Flow	318.60	0.50%	0.016	1.34
(from SDSK calculator - d=	=2" for 2-'	Yr. & d=5'	' for 100-Yr.)	
Curb and Gutter Flow	593.10	0.50%	0.016	1.34
(from SDSK calculator - d=	=2" for 2-'	Yr. & d=5'	' for 100-Yr.)	

					2-Year	100-**ear	
V <sub>100</sub>	Tt <sub>2</sub>	Tt100	Tc <sub>2</sub>	Tc100	ì	ī	
Vel.	Travel	Travel	Time of		Intensity	Intensity	
	Time	Time	Concentra	tion	Grd. Jctn.	Grd ctn.	
fps	min,	min.	min.	min.	Curves	Curves	
	62.81	37.07	77.5	46.6	0.28	1.61	
0.92	2.88	2.88			UILO		
1.78	0.47	0.26					
סר ל	3.05	2 22					
6.00	5.50	6.66					
2.39	7.38	4.14					

\* T<sub>0</sub> based on SCS formula pg. E-2 Storm Water Management Manual

\*\* Figure "E-3", Pg. E-9, Storm Water Management Manual was used for shallow flows. \*\*\* Mannings Equation was used to determine gutter and concrete pan flow velocities an N value of 0.016 was used for conrete gutters and pans

RUNOFF RATES (Q)

For: Unaweep Heights USING RATIONAL METHOD O=CxCfxIxA

BASIN D1	Q	C	Cf	Ι*	A
	Volume	Composite	Antecedent	Rainfall	Basin
		Coefficient	Precip. Fac.	Intensity	Area
	cfs	n/a	n/a	in/hr	acres
2-Yr	0.96	0.30	1	0.28	11.55
100-Yr	7.23	0.39	l	1.61	11.55

#### TIME OF CONCENTRATION and RAINFALL INTENSITIES For: Dakota West BASIN D2

	L	S	N*	V <sub>2</sub>	$V_{100}$	Tt <sub>2</sub>	Tt <sub>100</sub>	Tc <sub>2</sub>	Tc100	i	i
Descrip.	Length	Slope	Mannings	Vel.	Vel.	Travel	Travel	Time of		Intensity	Intensity
01 Flow	ft.	•⁄/s	coef.	fps	fps	Time min.	Time min,	Concentra min.	ition min.	Grd. Jctn. Curves	Grd. Jetn. Curves
Overland*	300	0.74%	0.120			62.81	37.07	69.9	42.3	0.30	1.72
Shallow Concentrated Flow**	161.1	0.74%	0.255	0.92	0.92	2.92	2.92				
Curb and Gutter Flow	75.00	2.00%	0.016	2.68	4.78	0.47	0.26	5			
(from SDSK calculator - d	=2" for 2-	-Yr. & d=5	" for 100-Yr.)			FOLLAR THE					
Curb and Gutter Flow (from SDSK calculator - d	295.40 =2" for 2-	0.50% -Yr.&d=5	0.016 " for 100-Yr.)	1.34	2.39	3.67	2.06				

\* T<sub>0</sub> based on SCS formula pg. E-2 Storm Water Management Manual

\*\* Figure "E-3", Pg. E-9, Storm Water Management Manual was used for shallow flows.

\*\*\* Mannings Equation was used to determine gutter and concrete pan flow velocities an N value of 0.016 was used for conrete gutters and pans

RUNOFF RATES (Q)

For: Dakota West USING RATIONAL METHOD Q=CxCfxIxA

BASIN D2	Q	C	Cf	I*	A
	Volume	Composite	Antecedent	Rainfall	Basin
		Coefficient	Precip. Fac.	Intensity	Area
	cfs	n/a	n/a	in/hr	acres
2-Yr	0.24	0.26	1	0.30	3.12
100-Yr	1.77	0.33	1	1.72	3.12

.

2-Year

100-Year

STORMWATER RETENTION (Within Grand Valley only) For: Dakota West Date: 1/6/2003 Job. No.0543-001

Total Retention (without overflow)

12

= 32866.18 Ft<sup>3</sup>

 $V = P_{10024hr} \times A \times C_{100d}$   $P_{10024hr} = 2.01 (see Table A-2, Pg A-4, SWM Area = 11.55 Ac. = 503118.00 Ft<sup>2</sup>$   $C_{100d} = 0.39 (see Table B-1, Pg B-3, SWM V(FT<sup>3</sup>) = P_{10024hr} (inches) \times AREA (FT<sup>2</sup>) x C_{100d}$ 

10:27 AM, 1/8/2003

Retention.xls

#### COMPOSITE RUNOFF COEFICIENTS

#### For: DAKOTA WEST

#### USING

GRAND JUNCTION RECOMME	NDED RUN	OFF COEFICIE	NTS		BASIN		BASIN		BASIN	
					OS		Dl		D2	
	Hydro.	Slope 2-6%			Devel.		Devel.		Devel.	
Description	Soils	Runoff	Sel.		Unit	Wt'd	Unit	Wt'd	Unit	Wt'd
Surface Area	Group	Coeff.'s	Coeff.		Area	Value	Area	Value	Area	Value
Pavement and Roofs	B	0.94	0.94	2-Yr.	0.00	0.00	0.00	0.00	0,00	0.00
	В	0.96	0.96	100-Yr.	0.00	0.00	0.00	0.00	0.00	0.00
Residential Areas	В	0.29 to 0.37	0.33	2-Yr.	0.00	0.00	9.39	3.10	1.58	0.52
1/4 acre per unit	в	0.38 to 0.46	0.42	100-Yr.	0.00	0.00	9.39	3.94	1.58	0.66
Bare Ground	В	0.14 to 0.37	0.18	2-Yr.	3.69	0.66	2.16	0.39	1.54	0.28
		0.20 to 0.28	0.24	100-Yr.	3.69	0.89	2.16	0.52	1.54	0.37

Cotal Basin Area:	3.69		11.55	[	3.12	
COMPOSITE "C" VALUE (2-year)		0,18		0.30		0.26
COMPOSITE "C" VALUE (100-year)		0.24		0.39	1	0.33

Provide and the second s	The second s	-											
LAND USE OR	SCS HYDROLOGIC SOIL GROUP (SEE							APPENDIX "C" FOR DESCRIPTIONS)					
CHARACTERISTICS	Α			В			С			D			
	0-2%	2-6%	6%+	0-2%	2-6%	6%+	0-2%	2-6%	6%+	0-2%	2-6%	6%+	
UNDEVELOPED AREAS Bare ground 0.18 0.24	.1020 .1424	.1626 .2232	.2535 .3040	(14 · 22 20 · 28)	.2230 .2836	.3038 .3745	.2028	.2836	.3644	2432	.3038	.4048	
Cultivated/Agricultural	.0818 .1424	.1323 .1828	.1626 .2232	11 - 19 16 - 24	.1523 .2129	.2129 .2836	.1422	.1927	.2634	18 - 26	.2331	.3139	
Pasture	.1222 .1525	.2030 .2535	.3040 .3747	.1826	.2836	.3745	.2432	.3442	.4452	.3038	.4048	.4149	
Meadow	.1020 .1424	.1626 .2232	.2535 .3040	.1422 .2028	.2230	.3038	.2028	.2836	.3644	24 - 32	.5058	.6270	
Forest	.0515 0818	.0818 .1121	.1121	08 - 16	.1119	.1422	.1018	.1321	.1624	12 - 20	.1624	.5058	
RESIDENTIAL AREAS 1/8 acre per unit	.4050 .4858	.4353 .5262	.4656 .5565	.42 - 50 50 - 58	.4553	.5058	.4553	.4856	.5361	.4856	.5159	.5765	
1/4 acre per unit	.2737 .3545	.3141 .3949	.3444 .4252	29 - 37 38 - 46	.3442 .4250	.3846 .4755	.3240 .4149	.3644	.4149	35-43	.3947	.4553	
1/3 acre per unit	.2232 .3141	.2636 .3545	.2939 .3848	.25 - 33 .33 - 41	.2937 .3846	.3341 .4250	.2836 .3644	.3240	.3745	31 - 39	.3543	.4250	
1/2 acre per unit	1626 .2535	.2030 .2939	.2434 .3242	.1927 .2836	.2331 .3240	.2836	.2230 .3139	.2735	.3240	.2634	.3038	.3745	
1 acre per unit	.1424 .2232	.1929 .2636	.22 • .32 .2939	.17 - 25 .2432	.2129 .2836	.2634	20 - 28	.2533	.3139	2432	.2937	.3543	
MISC, SURFACES Pavement and roofs	.93 .95	.94 .96	.95 .97	.93 .95	.94 .96	.95	.93	.94	.95	.93	.3343	.95	
Traffic areas (soil and gravel)	.5565 .6570	.6070 .7075	.6474 .7479	.6068 .6876	.6472 .7280	.6775 .7583	64 - 72 72 - 80	.6775	.6977	.7280	.7583	.7785	
Green landscaping (lawns, parks)	.1020 .1424	.1626 .2232	.2535 .3040	.1422 ,2028	.2230 .2836	.3038 .3745	.2028 .2634	.2836	.3644	24 - 32	.3038	.4048	
Non-green and gravel landscaping	.3040 .3444	.3646 .4252	.4555 .5060	.4555 .5060	.4250 .4856	.5058 .5765	.4048	.4856	.5664	.4452	.5058	.6068	
Cemeteries, playgrounds	.2030 .2434	.2636 .3242	.3545 .4050	.35 - 45 .4050	.3240 .3846	.4048 .4755	30 · .38 .3644	.3844	.4654	34 . 42	.4048	.5058	
<ul> <li>NOTES: 1. Values above and below pertain to the 2-year and 100-year storms, respectively.</li> <li>2. The range of values provided allows for engineering judgement of site conditions such as basic shape, homogeneity of surface type, surface depression storage, and for longer duration. In general, during shorter duration storms (Te ≤ 10 minutes), infiltration capacity is higher, allowing use of a "C" value in the low range. Conversely, For residential development at less than 1/8 are per unit or greater than 1 are per unit, and also for commercial and industrial areas, use values under MISC</li> </ul>													
R	ATIONAL	L METHO	OD RUN	DEF COF	FEICIEN	TC				and the second	all the second		

TABLE "B-1"

t

B-L

DEC 1994


<u>Hillings silty clay loam, 0 to 2 percent slopes (Bc).</u>—This soil, locally called adobe, is one of the most important and extensive in the Grand Valley. It covers nearly one-fifth of the Grand Junction Area. The areas occur on the broad flood plains and very gently sloping coalescing alluvial fans along streams. Many large areas are nor h of the Colorado River.

The soil is derived from deep alluvial deposits that came mainly from Mancos shale but in a few places from fine-grained sandstone materials. The deposits ordinarily range from 4 to 40 feet deep but in places exceed 40 feet. The deposits have been built up from thin sediments brought in by the streams that have formed the coalescing alluvial fans or have been dropped by the broad washes that have no drainage channel. The thickest deposit, near Grand Junction, was built up by Indian Wash.

The color and texture of the soil profile vary from place to place. The 8- to 10-inch surface soil normally consists of gray, light-gray, light olive-gray, or light brownish-gray silty elay loam. This layer grades into material of similar color and texture that extends to dep hs of 3 or 4 feet. Below this depth the successive depositional layers show more variation. Although the dominant texture is silty elay loam, the profile may have a loam, clay loam, fine sandy loam, or a very fine sandy loam texture.

Where there are fairly uniform beds of Mancos shale and where the soil is not influenced by materials deposited by adjoining drainage courses, the profile varies only slightly within the upper 3 or 4 feet. In treas bordering drainage courses, however, the soil varies more in texture and color from the surface downward.

One small area about 1½ miles southeast of Loma consists of light gravish-brown or pale-brown heavy silty clay loam that shows only slight variation in texture to depths of 4 to 6 feet. The underlying soil material is more variable. Below depths of 6 to 10 feet the layers generally are somewhat thicker and have a higher percentage of coarse soil material.

Also included with this soil are several small areas totaling about 3 scuare miles that are dominantly pale yellow. These are located 2½ 50 3½ miles northeast of Fruita, 5 miles north of Fruita, 2½ miles northeast of Loma, 3 to 5 miles north of Loma, 1½ miles northwest of Loma, and 4 miles northwest of Mack. In these areas the 8- or 10-inch surface soil is pale-yellow silty clay loam, and the subsoil is a relatively uniform pale-yellow silty clay loam to depths of 4 to 8 feet. The accumulated alluvial layers are difficult to distinguish, but in a few places transitional to Fruita soils there are small areas having a pale-brown to light-yellowish brown color. These transitional areas are included with Billings silty clay loam because they have a finer textured subsoil than is characteristic of the Ravola soils.

Although moderately fine textured, this Billings soil permits successful growth of deep-rooted crops such as alfalfa and tree fruits. Its permeability is normally not so favorable as that of the Mesa, Fru.ta, and Ravola soils. Its tilth and workability are fair, but it puddles so quickly when wet and bakes so hard when dry that good tilth can be maintained only by proper irrigation and special cultural practices. Runoff is slow and internal drainage is very slow.

Like all other soils in the area, this one has a low organic-matter

tration of salts derived from the parent rock (Mancos slate). In places, however, it contains so much salt that good yields cannot be obtained. Some large areas are so strongly saline they cannot be used for crops. Generally, this soil is without visible lime, but it is calcareous. In many places small white flecks or indistinct lightcolored streaks or seams indicate that lime, gypsum, or sults are present.

Use and management.—About 80 percent of this soil is cultivated. The chief irrigated crops are alfalfa, corn, dry beans, sugar beets, small grains, and tomatees and other truck crops. Where the soil is located so as to avoid frost damage, tree fruits are grown.

Most of the field crops are grown in the central and westen parts of the valley, or from Grand Junction westward. The entire acreage in tree fruits-approximately 3 square miles-lies betweer Grand Junction and Palisade. Because the climate is more favorable near Palisade, the acreage in orchard fruits is greater there. A few small orchards are located northeast of Grand Junction in the direction of Clifton. The main fruit acreage is between Clifton and Palisade. Peach orchards predominate, but a considerable acreage is in pears, especially near Clifton. Yields depend on the age of the trees and other factors, including management, but the estimated potential yield is somewhat less on this soil than on Mesa soils. This takes into account the slower internal drainage of this soil and its susceptibility to salinity if overirrigated. Yields of other crops vary according to the length of time the land has been irrigated, internal drainage or subdrainage, salt content of the soil, management practices, and local climate.

The uncultivated areas of this soil are mostly inaccessible places adjoining the larger washes, which occur mainly in the western part of the area, and those places that cannot be cropped profitably because they have inadequate drainage and a harmful concentration of salts. The uncultivated land supports a sparse growth of greasewood, saltbush, shadscale, rabbitbrush, ryegrass, peppergrass, and saltgrass. From 70 to 90 acres are required to pasture on a ninual during a season.

A number of places shown on the map by small marsh symbols are low and seepy. They could be ditched, but their acreage is I kely too small to justify the expense. Left as they are, their salt content makes them worthless for any use except pasture.

Sizeable acreages of this soil apparently were overirrigated in the past. Irrigation water applied at higher levels to the north seeps upward in this soil where it occurs in low areas toward the river. Even now, new saline areas are appearing, and existing treas are getting larger. The total acreage affected by salts has remained more or less the same for the last two decades, but affected treas will continue to change in size and shape because of seepage.

Most fields are ditched where necessary. Some uncultivated areas require both leveling and ditching. In places subdrainage is inadequate because irregularities in the underlying shale tend to create pockets and prevent underground water from flowing into the drainage ditches. Also, in some areas where the alluvial mantle is 30 to 40 feet thick, the ditches are not always deep enough to drain the soi. Some areas are seeny because there are no ditches running in an cost-west irrighted, permeable, medium-textured, stratified soils on the upper parts of the fan to the north. After being leveled, uncultivated areas would have to be cropped for 3 years before their salt content would be reduced enough to permit good yields.

Farmers can increase the organic-matter content of this soil by applying manure liberally and by growing alfalfa or clovers at least part of the time. A combination field crop and livestock type of farming favors improvement of this soil. Many of the small imperfectly drained areas may be kept in pasture. Strawberry clover and sweetclover are well suited, and mixtures of pasture grasses grow well.

Billings sifty clay loam, 2 to 5 percent slopes (Bp).—This soil covers a relatively small acreage in the Grand Valley. The areas are widely scattered. Except for its stronger slope, the soil is almost the same as Billings silty clay loam, 0 to 2 percent slopes. In a few places, notably moth of Loma, there are areas having a pale-yellow color rather than the gray typical of the Billings soils.

Use and management.—Only about 15 percent of this soil is cultivated. Many of the areas lie along large drainageways or washes where they are difficult to reach. Even a larger number have such an uneven surface that considerable leveling would have to be done before they could be cropped. The cost of leveling, together with the expense of controlling erosion and gullying, discourages farmers from using them.

Many of the uncultivated areas have moderate concentrations of salts, but they are not particularly difficult to reclaim because they border natural ditches or washes which afford free disposal of irrigation water. Furthermore, for the most part, they have a porous substratum.

About the same crops are grown on this soil as on Billings silty day loam,  $\theta$  to 2 percent slopes. The average yields are approximately the same.

Billings\_silty\_clay, 0 to 2 percent slopes (BA).—This soil, locally called heavy adobe, occurs well toward the Colorado River. It is on alluzial materials—4 to about 40 feet thick—that largely came from Marcos shale. Most of this soil lies east and southeast of Grand Junction and along the railroad between Grand Junction and Fruita.

The 8- or 10-inch surface soil consists of light brownish-gray, gray, or onive-gray silty clay. The layer is similar to the surface layer of Billings silty clay learn soils but it is harder and, in many places, darker. The subsoil consists of similarly colored layers of silty clay learn, silt learn, and silty clay. In places the soil is silty clay to depths exceeding 4 feet.

The entire profile is firm when moist and has a massive structure. The subsoil has many small irregularly shaped light-gray specks or indistinct mottles. Poorly defined light-colored streaks indicate the presence of lime, gypsum, or salts. The surface soil and subsoil are calcareous, the lime being well distributed. The fine texture of the soil greatly retards penetration of roots, moisture, and air.

Surface runoff is very slow to slow where the slope is less than 1 percent. Internal drainage is very slow because the subsoil is massive and very slowly permeable. Even with ample drainage ditches, the disc nurse of interation water is show Tilth and workability are not good, because the soil has a fine texture and a low content of organic matter. Moreover, some fields contain areas 20 to 60 feet across that have excessive amounts of salts. Slick spots also occur. These salty areas and slick spots produce low or negligible yields of most crops and are extremely difficult to eliminate.

Use and management.—About 75 percent of this soil is cultivated. Most of the rest is affected by salts. Snull grains, bears, sugar beets, and alfalfa are the chief crops. They yield less than or Billings silty elay loam, 0 to 2 percent slopes. Ordinarily, newly broken fields are cropped to oats or other small grains the first few seasons so that excess salts can be removed. Afterwards, if drainage is adequate, they may be planted to pinto beans, sugar beets, corn, or alfalfa. The very slow permeability of this soil makes it unsuitable for orchard crops. Also, it is located mainly in areas where the frost hazard is great. Probably the greater part of the irrigable acreage is used for sugar beets. Small grains, alfalfa, and pinto beans usually follow in the order named.

Billings silty clay, 2 to 5 percent slopes (BB).—This soil is similar to Billings silty clay, 0 to 2 percent slopes. It differs mainly in having greater slopes and a slightly finer textured and darker gray surface soil. In places, below depths of 3 or 4 feet, the silty clay or clay material is light olive gray.

The tilth and workability are poor. Surface runoff is medium, and internal drainage is very slow. The soil is better suited to urigation than most of the larger nearly level areas of Billings silky cla7, 0 to 2 percent slopes, many of which are affected by salts. Approximately 12 acres of this soil is in peach orchards. All the rest is normally used for cultivated crops, principally corn, pinto beans, and alfalfa. This soil is suited to about the same crops as Billings silty clay, 0 to 2 percent slopes, but it generally produces better yields.

Billings silty clay, moderately deep over Green River soil material, 0 to 2 percent slopes (Br).—This soil occurs on the outer margin of coalescing alluvial fans where 1 to 4% feet of fine-textured deposits derived from shale overlies Green River soil materials.

Except for a few strips only a few rods wide that adjoin low-lying areas of Green River soils, this soil has not been altered by high overflows from the Colorado River. It is not likely that the main part of the soil will be covered by floodwaters from the Colorado River, as it lies well above the level of normal overflow.

Use and management.—About 85 percent of this soil is cultivated. The principal crops are alfalfa, corn, sugar beels, and pinte beans. A few peach orchards are on this soil near Clifton. Because the underlying strata are coarser, crops produce better on this soil than on most areas of the other Billings silty clay soils. Draininge and saline conditions have to be corrected before the soil will produce well.

Uncultivated accenges of this soil northwest of Grand Junction are saline, imperfectly drained, or both. Their tilth and workability are poor because they have a fine texture and a low content of organic matter.

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Exhibit A-1, continued: Hydrologic soil groups for United States soils

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BENFIELD	C	BEULAH	BI	BIRCHFIELD	0	I ELAKENEI	~	BI IM	C
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RENSIEY	B	I BICE	9 1	BISBET	A	ELANKET			-
DENERN	n	I BICKERDYST	D I	BISCARD	D	SLANTON	A 1	BUDIFIL	
DENADN	-	1 BACKETT	n 1	RISCAY	8/D	BLANTON.	5 1	BDBTDPH	D
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BEDT14	B	I SIDDEFORD	0 1	BISHARCE	D	BLASDELL		OUCKER ABZEGRAN	8
BEAULUE		B TOOL FHAN	B	3 ISOCDI	D	BLASE	C 1	BUCKSTON	~
DEDEVEC	-		e 1	BISPING	2	BLASINGAME	C I	BODE	P
BEDUINH		1 BIDARA		BICCFII	8	BLAYDEN	C	BODECKER	A
BERCUMB	8	BIDAEFC	2 1	OT SE DUNE I	<b>D</b>	BLAZBIRD	DI	BODELL	D
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BERRYLAND	8/0	BICAINDED	5 1	B LAC X MAMMER	C 1	NUMBER PERSONNELLY	0 1	BOISTFORT	
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# GEOTECHNICAL INVESTIGATION Dakota West Subdivision, Phases 1, 2 and 3 North and West of D ½ Road and 31 Road Grand Junction, Colorado

**Prepared For:** 

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Attention: Mr. Robert Cantrell

Job No. 1,288

February 17, 2003

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#### SCOPE

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This report presents the results of a Geotechnical Investigation for the proposed Dakota West Subdivision, Phases 1, 2 and 3 to be located north and west of D 1/2 Road and 31 Road, in Grand Junction, Colorado. Our investigation subsurface conditions, provide conducted to explore pavement was recommendations and provide foundation recommendations for the proposed The report includes descriptions of subsoil and groundwater residences. conditions found in thirteen exploratory test pits, recommended pavement sections, recommended foundation systems and allowable design soil pressures, and design and construction criteria for details influenced by the subsurface conditions. This investigation was performed in general conformance with our Proposal No. 03-011 dated January 14, 2003.

The report was prepared from data developed during our field exploration, laboratory testing, engineering analysis and experience with similar conditions. A brief summary of our conclusions and recommendations follows. Detailed criteria are presented within the report.

#### SUMMARY OF CONCLUSIONS

- Subsoils found in the thirteen exploratory test pits consisted of silty, sandy clay to the maximum depths explored of 5 to 10 feet below the ground surface. Groundwater was not encountered to the maximum depth explored the day of observation or when checked one day later.
- We believe shallow footing foundations can perform satisfactorily for the proposed residences. A discussion, including detailed design and construction criteria are included in the text of the report.
- We believe slab-on-grade construction supported by the soils encountered has low potential for movement. We recommend structurally supported floors in all finished living areas. Nonstructural, slab-on-grade construction should be limited to flatwork and garage areas.
- 4. An asphalt thickness of 5.25 inches or 3.0 inches asphalt over 7.25 inches base course supported by stabilized / well compacted subgrade soils are recommended for interior residential streets, ESAL = 54,750. Additional pavement section alternatives and design and construction criteria are presented in the text of the report.
- 5. Surface drainage should be designed for rapid runoff of surface water away from the proposed residences and pavements.

## SITE CONDITIONS

The subject site was located north and west of D ½ Road and 31 Road in Grand Junction, Colorado. A vicinity map is included as Fig. 1. The subject site was a basically flat and nearly level, grass covered pasture. We noted areas

where the vegetation was stripped. The ground surface sloped down towards the south at 1 percent or less (estimated with hand held Brunton and pacing). An abandoned / remnant, north south oriented irrigation ditch was noted in the east central portion of the site. Single family residences and a vacant parcel were north. Single family residences, fenced pasture and outbuildings were east. Single family residences were west beyond a vacant parcel. Single family residences were south beyond D ½ Road. The vicinity sloped down toward the south, towards the Colorado River at slopes of approximately 1 percent (USGS Clifton, Colorado topographical quadrangle, 1962, photorevised 1973).

#### PROPOSED CONSTRUCTION

We understand the subject site is proposed for development and construction of approximately 45 lots for single family residential construction. Residences will be wood framed, single story structures with no below grade construction. Shallow footing type foundations are desired. There will be no site grading changes. There will be about 2,200 lineal feet of paving for interior streets. There will be a turn lane and deceleration lane addition to D ½ Road. There will be no storm water retention/detention area soil testing required. We anticipate foundation loads may range from 1,000 to 2,000 pounds per lineal foot of foundation wall. If proposed construction is different than what is described above,

we should be notified so that we can re-evaluate the recommendations presented in this report in light of the differences.

#### SUBSURFACE CONDITIONS

Subsurface conditions at the site were investigated by observing and sampling thirteen (13) exploratory test pits. Locations of test pits are shown on Fig. 2. Replacement of test pit excavations as a well compacted fill should be confirmed at the time of construction. Graphic logs of the soils found in the exploratory test pits and field penetration resistance tests are presented on Figs. 3 through 7. Subsurface conditions encountered in the exploratory test pits consisted of silty, sandy clay to the maximum depths explored of 5 to 10 feet below the ground surface.

The silty, sandy clay was very soft to very stiff, dry to very moist, brown and tan with sulfates noted and a scattered porous fabric noted in the upper 3 feet. Clay samples tested had moisture contents of 5.0 percent to 22.4 percent and dry densities of 87 pcf to 103 pcf. Six samples were tested for Atterberg limits. These samples ranged from exhibiting liquid limits of 22 to 33, plasticity indices of 2 to 15 and 65 to 92 percent passing the No. 200 sieve (silt and clay sized particles). Seven clay samples were tested for one-dimensional swell / consolidation

characteristics. These samples ranged from compressing 0.5 percent to swelling 1.1 percent when wetted under a confining pressure of 500 or 1,000 psf. Groundwater was not encountered to the maximum depths explored or when checked one day later. Results of laboratory testing are included in Figs. 8 through 12 and summarized on Table I.

#### SITE DEVELOPMENT

We understand there will be no site grading changes. We believe utility installation in the silty, sandy clay soils may be accomplished using conventional excavation equipment to the depths investigated. Utility trenches should be sloped or shored to meet local, State and Federal safety regulations. Based on our investigation, we believe soils at this site may be classified as either Type A, Type B and / or Type C, based on OSHA standards. Excavation slopes specified by OSHA are dependent upon types of soils and groundwater conditions encountered. Contractors should identify the conditions encountered in the excavation and refer to OSHA standards to determine appropriate slopes.

Water and sewer lines will be constructed beneath pavements. Compaction of trench backfill can have a significant effect on the life and serviceability of pavements. We recommend trench backfill be placed in thin, loose lifts, moisture conditioned to within 2 percent of optimum moisture content

and compacted to at least 95 percent of standard Proctor maximum dry density (ASTM D 698). The placement and compaction of utility trench backfill should be observed and tested by a geotechnical engineer during construction.

We did not identify groundwater during this investigation to depths of 5 to 10 feet below the ground surface. We anticipate groundwater levels may rise during irrigation season. As a result, there may be groundwater concerns during construction, which were not identified by this investigation. Soft and very soft soils were identified in the central and east portions of the site at depths of 3 to 6 feet. Utility trench bottom areas may require stabilization if soft conditions are encountered at the time of excavation. Our representative should be called to observe recommendations for stabilization at that time.

#### **RESIDENCE FOUNDATIONS**

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This investigation indicates subsurface conditions at anticipated foundation levels consist of soft to very stiff, silty, sandy clay soils. The soft / very soft soils identified may be due in part to recent irrigation on the subject site. These soils may become less soft over time with the discontinuation of irrigation. We recommended no further irrigation on the subject site. One method of support to help reduce settlement concerns is the use of deep foundations such as drilled or helical piers bedded in an underlying competent stratum. This investigation did not identify an underlying competent bearing stratum. Additional investigation would be required to provide deep foundation recommendations, as requested. We understand shallow footing foundations are desired. In our experience, shallow foundations have been used in this area with satisfactory performance for conditions similar to those identified at this site. We recommend that shallow foundations bear as shallow as practical (12-inches to 24-inches maximum depth). To provide a more uniform foundation subgrade, we recommend the subgrade be well compacted. Areas of soft to very soft conditions were encountered and stabilization may be necessary across the site. We also recommend the subgrade be "proof rolled" using a heavy, pneumatic tired vehicle to identify soft areas.

We present design and construction criteria for spread footing foundations below. These criteria were developed from analysis of field and laboratory data and our experience. The additional requirements (if any) of the structural engineer and structural warrantor should also be considered.

## Spread Footing Foundations

 Spread footing foundations, bearing on well compacted native soils, can be designed for a maximum soils bearing pressure of 1,000 psf. Footings should bottom as shallow as practical and no deeper than 24-inches below the existing ground surface. Loose soils should be completely removed from foundation bearing areas, prior to placing concrete.

- 2. The completed excavation, within 2 feet horizontally of bearing areas, should be scarified 10 inches, moisture conditioned to within 2 percent of optimum moisture content and compacted to at least 95 percent of standard Proctor maximum dry density (ASTM D698). Our representative should be called to test compaction of subgrade soils and observe a proof roll of entire subgrade, performed by a heavy pneumatic tired vehicle such as a 10-wheeled, loaded dump truck prior to forming. If soft or yielding conditions are encountered then stabilization may be required. Our representative should make specific stabilization recommendations depending on conditions encountered, at the time of our site visit. If porous fabric is noted up to 2 feet of soil removal beneath foundations may be required, replaced with a well compacted structural fill.
- 3. We recommend a minimum width of 18 inches for continuous footings. Isolated pads should be at least 30 inches by 30 inches. Foundation walls should be well reinforced top and bottom. We recommend reinforcement sufficient to span an unsupported distance of at least 12 feet. Reinforcement should be designed by the structural engineer.
- 4. Exterior walls must be protected from frost action. We understand 2 feet for frost cover is typically assumed in the Mesa County area.
- The completed foundation excavation should be observed by our representative prior to placing forms, to verify the foundation bearing conditions and test compaction.

#### FLOOR SYSTEMS

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1.1

We believe the near-surface soils which will support slab-on-grade floors exhibited low movement potential. Some movement must be assumed from an increase in moisture by residential development and associated landscaping and irrigation. To our knowledge, the only reliable solution to control floor movement is the construction of a structurally supported floor with at least a 12-inch air space between the floor and subgrade. In our opinion, structural floors should be used in all finished living areas. Structurally supported floors are normally not used in garage areas. A slab-on-grade floor can be used in garages provided the builder and owner is aware of and accepts risk of potential movement. Driveways, sidewalks and exterior patio slabs are also constructed as slabs-on-grade.

We recommend the following precautions for construction of slabs-on-grade at this site. These precautions will not prevent movement in the event the underlying soils become wetted; they tend to reduce damage if movement occurs.

- 1. Slab-on-grade construction should be limited to areas such as garage and exterior flatwork.
- Slab subgrade areas should be scarified, moisture conditioned and compacted as described earlier in the "RESIDENCE FOUNDATION" section of this report.
- Slabs should be separated from exterior walls and interior bearing members with a slip joint which allows for free vertical movement of slabs.
- 4. The use of slab-bearing partitions should be minimized. Where such partitions are necessary, a slip joint allowing at least 1.5 inches of free vertical slab movement should be used. The home owner should be advised of potential movement and re-establish this void if it closes. Doorways and stairwells should also be designed for this movement. Sheetrock should not extend to slab-on-grade floors.



- 6. Plumbing and utilities which pass through slabs should be isolated from the slabs. Heating and air conditioning systems supported by the slabs should be provided with flexible connections capable of at least 1.5 inches of vertical movement so that slab movement is not transmitted to the duct work.
- 7. Frequent control joints should be provided to reduce problems associated with shrinkage and curling. The American Concrete Institute (ACI) and Portland Cement Association (PCA) recommend a maximum panel size of 8 to 15 feet depending upon concrete thickness and slump, and the maximum aggregate size. We advocate additional control joints 3 feet off and parallel to grade beams and foundation walls.
- Exterior patio and porch slabs should be designed to function as independent units. Movement of slabs-on-grade should not be transmitted directly to the residence foundations. Stucco finish (if any) should terminate at least 6 inches above any flatwork.

#### BELOW-GRADE CONSTRUCTION

No below-grade construction is anticipated at this site. Typically, foundation drains are not required for construction of this type. Crawl space areas should be sloped so that potential moisture will not collect in these areas, but flow out of the crawl space. Crawl space areas (where applicable) should also be well ventilated to mitigate potential musty odors. We can provide foundation drain details if requested.

#### PAVEMENT

The pavement subgrade soils include stiff to very stiff, silty, sandy clay. We visually classified each sample obtained from the test pits and tested samples in our laboratory. We tested a combined sample from exploratory test pits, TP-1 through TP-6 at 0 to 5 feet for pavement design purposes. The sample was tested for Atterberg limits, gradation, standard Proctor, and California Bearing Ratio (CBR). The sample tested exhibited a maximum dry density of 111.0 pcf, optimum moisture of 15.0 percent and a California Bearing Ratio (CBR) of 9.1. We used a design CBR value of 5.0. The results of laboratory testing are shown on Table I and included in Figs. A-1 and A-2.

Our design utilized the computer program WinPAS, based on the 1993 AASHTO Guide for Design of Pavements Structures, 30 year design period, and our experience. We understand pavements will be used to for interior residential streets and acceleration / deceleration lane improvements. We used a 30 year Equivalent Single Axle Load (ESAL) of 54,750 for the interior streets (converted from an equivalent daily load application, EDLA=5) for interior streets. We obtained an average daily traffic (ADT) of 3786 for D ½ Road west of 31 Road from the City of Grand Junction. We used this ADT to calculate a 30 year ESAL for flexible and rigid pavements for the turn lane and deceleration lane addition. We calculated an ESAL of 1,204,500 for flexible pavements and an ESAL of 1,806,750 for rigid pavements for these D ½ Road improvements. A non-linear relationship developed by CDOT to relate the CBR value to the subgrade resilient modulus (Mr) was used for flexible pavement. Using this relationship, we calculated a Mr value of 6,607 psi. We converted the subgrade resilient modulus (Mr) to the modulus of subgrade reaction (k) using the relationship K = Mr / 19.4, for rigid pavements. Using this equation, we calculated a k value of 340 psi / in. We used a regional factor of 2.0 and a design serviceability index of 2.0 (interior streets) and 2.5 (D ½ Road improvements). Pavement design calculations are included in Appendix A. Table A below shows our recommendations.

TABLE A SUMMARY OF RECOMMENDED PAVEMENT SECTIONS

Anticipated Traffic Type	Asphaltic Concrete	Asphalt and Aggregate Base Course	Asphalt, Aggregate Base Course and Aggregate Sub Base Course	Portland Cement Concrete
Interior Streets (ESAL = 54,750)	5.25"	3.0" +7.25" 4.0" + 4.0"		5.0"
D ½ Road Improvements ESAL=1,806,750 or ESAL=1,204,500	8.5"	3.0" + 18.25" 4.0" + 15.0"	4.0" + 6.0" + 10.75"	8.0"

The pavement subgrade should be scarified a depth of 10-inches, moisture conditioned to within 2 percent of optimum moisture content and compacted to at least 95 percent of standard Proctor (ASTM D698) maximum dry density. Soft

areas that require stabilization may be encountered. A Geotechnical Engineering Group, Inc. representative should be called to observe a "proof roll" of the completed subgrade, made by a heavy pneumatic tired vehicle. Soft subgrade conditions that require stabilization may be identified. Care should be taken to avoid excessive construction traffic.

Our experience indicates asphalt pavement in areas which will be subjected to heavy trucks stopping and turning does not perform satisfactorily. On residential interior streets, (ESAL = 54,750), we recommend placing a 5 inch thick Portland cement concrete pavement in all areas where this heavy truck traffic may occur, including access aprons and trash dumpster locations. On turn lane / deceleration lane improvements (ESAL=1,806,750), we recommend placing an 8.0-inch thick Portland cement concrete pavement in all areas where this heavy truck traffic occur.

The design of a pavement system is as much a function of paving materials as supporting characteristics of the subgrade. The quality of each construction material is reflected by the strength coefficient used in the calculations. If the pavement system is constructed of inferior material, then the life and serviceability of the pavement will be substantially reduced.

Dakota West Subdivision, Phases 1, 2 and 3 North and West of D ½ Road and 31 Road GEG Job No. 1,288 The asphalt component of the pavement was designed assuming at least 1,650 pounds Marshall stability. Normally, an asphaltic concrete should be relatively impermeable to moisture and should be designed with a well-graded sand/gravel mix. The oil content, void ratio, flow and gradation need to be considered in the design. We recommend a job mix design be performed and periodic checks are made to verify compliance with these specifications.

If construction materials cannot meet the above requirements, then the pavement design should be evaluated based upon available materials. We recommend the materials and placement methods conform to the requirements listed in the Colorado Department of Transportation "Standard Specifications for Road and Bridge Construction". All materials planned for construction should be submitted and tested to confirm their compliance with these specifications.

A primary cause of early pavement deterioration is water infiltration into the pavement system. The addition of moisture usually results in softening of untreated base course and subgrade and eventual failure of the pavement. We recommend drainage be designed for rapid removal of surface runoff. Curb and gutter should be backfilled and the backfill compacted to reduce ponding adjacent to pavements. Final grading of the subgrade should be carefully controlled so that design cross-slope is maintained and low spots in the subgrade which could trap water are eliminated. Seals should be provided between curb and pavement and

Dakota West Subdivision, Phases 1, 2 and 3 North and West of D ½ Road and 31 Road GEG Job No. 1,288

at all joints to reduce moisture infiltration. Landscaped areas and detention ponds in pavements should be avoided.

We have included construction recommendations for flexible and rigid pavement construction in Appendix B. Routine maintenance, such as sealing and repair of cracks annually and overlays at 5 to 7-year intervals, are necessary to achieve the long-term life of an asphalt pavement system. If the design and construction recommendations cannot be followed or anticipated traffic loads change considerably, we should be contacted to review our recommendations.

#### CONCRETE

One soil sample (TP-1 through TP-6 at 0 to 5 feet depth bulk combined) was tested in the laboratory for water soluble sulfate content. Test results indicate that the sample had a water soluble sulfate concentration of 6,500 ppm. Sulfate concentrations in this range are considered to have a severe effect on concrete which comes into contact with the soils. We recommend a Type V cement be used for concrete that comes into contact with the subsoils. We understand a locally available Type I / II modified cement is typically used for similar conditions as Type V. In addition, concrete should have a maximum water-cement ratio of 0.45.

Dakota West Subdivision, Phases 1, 2 and 3 North and West of D ½ Road and 31 Road GEG Job No. 1,288

#### SURFACE DRAINAGE

Performance of foundations and concrete flatwork is influenced by surface moisture conditions. Risk of wetting foundation soils can be reduced by carefully planned and maintained surface drainage. Surface drainage should be designed to provide rapid runoff of surface water away from the proposed residences. We recommend the following precautions be observed during construction and maintained at all times after the construction is completed.

- The ground surface surrounding the exterior of the residences should be sloped to drain away from the residence in all directions. We recommend a slope of at least 12 inches in the first 10 feet around the residences, where possible. In no case should the slope be less than 6 inches in the first 5 feet. The ground surface should be sloped so that water will not pond adjacent to the residences.
- 2. Backfill around foundation walls should be moistened and compacted.
- Roof downspouts and drains should discharge well beyond the limits of all backfill. Splash blocks and downspout extenders should be provided at all discharge points.
- 4. Landscaping should be carefully designed to minimize irrigation. Plants used close to foundation walls should be limited to those with low moisture requirements; irrigated grass should not be located within 5 feet of the foundation. Sprinklers should not discharge within 5 feet of foundations. Irrigation should be limited to the minimum amount sufficient to maintain vegetation; application of more water will increase likelihood of slab and foundation movements.

5. Impervious plastic membranes should not be used to cover the ground surface immediately surrounding the residences. These membranes tend to trap moisture and prevent normal evaporation from occurring. Geotextile fabrics can be used to limit the weed growth and allow for evaporation.

#### CONSTRUCTION MONITORING

Geotechnical Engineering Group, Inc. should be retained to provide general review of construction plans for compliance with our recommendations. Geotechnical Engineering Group, Inc. should be retained to provide construction monitoring services during all earthwork and foundation construction phases of the work. This is to observe the construction with respect to the geotechnical recommendations, to enable design changes in the event that subsurface conditions differ from those anticipated prior to start of construction and to give the owner a greater degree of confidence that the proposed construction is constructed in accordance with the geotechnical recommendations.

Dakota West Subdivision, Phases 1, 2 and 3 North and West of D ½ Road and 31 Road GEG Job No. 1,288

## LIMITATIONS

Thirteen exploratory test pits were observed; seven in proposed residence areas and six in proposed pavement areas. The test pits are representative of conditions encountered only at the exact test pit locations. Variations in the subsoil conditions not indicated by the exploratory test pits are always possible. Our representative should observe open foundation excavations and test subgrade and fill compaction to confirm soils are as anticipated from the test pits and foundation soils are prepared as recommended herein.

We believe this investigation was conducted in a manner consistent with that level of care and skill ordinarily used by geotechnical engineers practicing in this area at this time. No other warranty, express or implied, is made. If we can be of further service in discussing the contents of this report or the analysis of the influence of the subsurface conditions on the design of the proposed construction, please call.

Dakota West Subdivision, Phases 1, 2 and 3 North and West of D ½ Road and 31 Road GEG Job No. 1,288

Sincerely, GEOTECHNICAL ENGINEERING GROUP, INC. 36618 Gregory G oettgei Project Engineer

**Reviewed by:** 

John P. Withers, P.E. Principal Engineer

GGP:JPW:cb (2 copies sent)

1 cc: Thompson Langford Corp. Mr. Jeff Mace 529 25 ½ Road, Suite B210 Grand Junction, CO 81505

Dakota West Subdivision, Phases 1, 2 and 3 North and West of D ½ Road and 31 Road GEG Job No. 1,288

Geotechnical Investigation Dakota West Subdivision, Phase 1, 2 and 3 North and West of D 1/2 Road and 31 Road Grand Junction, Colorado F TELLER AVE NCNULLIN ANUOU TECO HELDON HOULIGH HILL AVE DRI CT TECO S 5 SELAN MITN BROO UNNISON AVE 0 3/4 RD ))§ MOHAWK AVE *UEADOW* COLOROW H R08-DR CREDHLEAF 8 ANMNESSA CT REN 1/4 SENECA 0 5/8 RD SUN CT OURAY RY C AVE AZTEC CREEK DR COLOROW 28 AVE EAGLE WOOD CHOCTAW MEADOW LN ROOD 1/4 AVE DEVON CT CHESHIRE Subject Site 2 0 1/4 RD SAXON CT COLORADO EDARWOOD CT IRONWOOD SAND-COLORADO SINCK -HEID AVE 3 CHICK N TEAL CT SIVE ROVE DR CIREST TRA RISTOL S TEAL CK TANCISTER SILVER-CI OFY FORK CT

Job No. 1,288

Vicinity Map

Fig. 1

No Scal



Job No. 1,288 Location of Exploratory Test Pits Fig. 2



Fig. 3



Fig. 4





# Legend

Ø

Clay, silty, sandy, very soft to very stiff, dry to very moist, brown, tan, scattered porous fabric in upper 3 feet, sulfates noted (CL)

Indicates location of penetration test. The symbol 28/12 indicates that 28 blows of a 15 pound hammer falling 26 inches were required to drive a 1.0 inch diameter penetrometer 12 inches. The symbol HD indicates hand drive using modified California (2.0-inch O.D.) liner.

Indicates location of bulk sample collected from test pits.

# **Notes**

- 1. Test pits were observed and sampled on January 15, 2003.
- Elevations of borings were determined using an automatic level and the temporary benchmark (TBM) shown on Fig. 2.
- These logs are subject to the explanations, limitations and conclusions as contained in this report.

Legend of Logs of Exploratory Test Pits

Job No. 1,288

Fig. 7








Job No. 1,288

Swell Consolidation Test Results

Fig. 11





### TABLE I

# SUMMARY OF LABORATORY TEST RESULTS

				Attert	perg Limits	Swell / Co	onsolidation	PASSING	WATER		
HOLE	DEPTH	NATURAL	DRY	LIQUID	PLASTICITY		CONFINING	NO. 200	SOLUBLE	SOIL TYPE	0
		MOISTURE	DENSITY	LIMIT	INDEX	SWELL	PRESSURE	SIEVE	SULFATES		
	(FEET)	(%)	(PCF)	(%)	(%)	(%)	(PSF)	(%)	(ppm)		
			4			6					
TP-1 through 6 bulk ccmbined	0°-5°	6.1		29	9			92	6,500	Clay, silty, sandy (CL)	
TP-7	3	84	87		······	-0.5	500		<u> </u>	Clay silty sandy (CL)	
	5	59	95	26	6	0.0		91		Clay silty sandy (CL)	
		0.0								Oldy, Silly, Salidy (OL)	
TP-8	3	9.7		33	15			91		Clay, sandy (CL)	
	6	9.7	92			-0.4	1,000			Clay, silty, sandy (CL)	
											R
TP-9	3	8.0	103	27	11			65		Clay, silly, sandy (CL)	
	5	12.0	96			-0.5	1,000			Clay, silty, sandy (CL)	
											0
TP-10	3	11.2	95			+1.1	500			Clay, silty, sandy (CL)	
TP-11	0	14.7	101					79		Clay, silty, sandy (CL)	
	3	18.3	100			+0.4	500			Clay, silty, sandy (CL)	
	5	16.9	97	26	8			78		Clay, silty, sandy (CL)	
	8	22.4	94							Clay, silty, sandy (CL)	
<u>TP-12</u>	3	5.0	95	22	2			84		Clay, silty, sandy (CL)	
	6	9.1	99			+0.2	1,000			Clay, silty, sandy (CL)	
70.10			ļ								
IP-13	3	9.0	92			-0.1	500			Clay, silty, sandy (CL)	
L			1		1						

### APPENDIX A

### **PAVEMENT DESIGN CALCULATIONS**

## Geotechnical Engineering Group, Inc. Moistur - Density Relationship



Geotechnical Engineering Group, Inc.



CBR @ 0.1" Penetration	9.1
CBR @ 0.2" Penetration	10.6
Maximum Dry Density (pcf)	111.0
Optimum Moisture Content (%)	15.0
Dry Density (pcf)	109.5
Dry Density (% Maximum)	98.6
Surcharge Weight (Ibs)	10.0
Swell (%)	
Before Soaking Moisture Content	15.0
After Soaking Moisture Content:	
Top Inch	20.2
Average	17.6

#### Pavement Thickness Design According to 1993 AASHTO Guide for Design of Pavements Structures American Concrete Pavement Association

#### Flexible Design Inputs

Agency: Company: GEG Job No. 1,288 Contractor: Project Description: Dakota West Subdivision, Accel / Decel Lane Location: N & W D ½ Road and 31 Road

#### Flexible Pavement Design/Evaluation

Structural Number3.39Design ESALs1,204,500.00Reliability80.00Overall Deviation0.45	percent	Soil Resilient Modulus Initial Serviceability Terminal Serviceability	6,607.00 4.50 2.50	psi
--	---------	---	--------------------------	-----

#### Layer Pavement Design/Evaluation

Layer Material	Layer Coefficient	Drainage Coefficient	Layer Thickness	Layer SN
Asphalt Cement Concrete	0.40	1.00	8.47	3.39
Crushed Stone Base	0.12	1.00	0.00	0.00
	0.00	0.00	0.00	0.00
	0.00	0.00	0.00	0.00
	0.00	0.00	0.00	0.00
	0.00	0.00	0.00	0.00
			ΣSN	3 39

Job No. 1,288

Pavement Design Calculations

#### Pavement Thickness Design According to 1993 AASHTO Guide for Design of Pavements Structures American Concrete Pavement Association

### Flexible Design Inputs

Agency: Company: Contractor: Project Description: Location: N & W of D ½ Road and 31 Road

#### Flexible Pavement Design/Evaluation

Structural Number3.39Design ESALs1,204,500.00Reliability80.00Overall Deviation0.45	percent	Soil Resilient Modulus Initial Serviceability Terminal Serviceability	6,607.00 4.50 2.50	psi
--	---------	---	--------------------------	-----

#### Layer Pavement Design/Evaluation

Layer Material	Layer Coefficient	Drainage Coefficient	Layer Thickness	Layer SN
Asphalt Cement Concrete	0.40	1.00	3.00	1.20
Crushed Stone Base	0.12	1.00	18.22	2.19
Granular Subbase	0.10	0.00	0.00	0.00
	0.00	0.00	0.00	0.00
	0.00	0.00	0.00	0.00
	0.00	0.00	0.00	0.00
			ΣSN	3.39

Job No. 1,288

Pavement Design Calculations

#### Pavement Thickness Design According to 1993 AASHTO Guide for Design of Pavements Structures American Concrete Pavement Association

### Flexible Design Inputs

Agency: Company: GEG Job No. 1,288 Contractor: Project Description: Dakota West Subdivision, Accel / Decel Lane Location: N & W of D ½ Road and 31 Road

#### Flexible Pavement Design/Evaluation

Structural Number3.39Design ESALs1,204,500.00Reliability80.00Overall Deviation0.45	) ) percent	Soil Resilient Modulus Initial Serviceability Terminal Serviceability	6,607.00 4.50 2.50	psi
--	-------------------	---	--------------------------	-----

#### Layer Pavement Design/Evaluation

Layer Material	Layer Coefficient	Drainage Coefficient	Layer Thickness	Layer SN
Asphalt Cement Concrete	0.40	1.00	4.00	1.60
Crushed Stone Base	0.12	1.00	14.89	1.79
Granular Subbase	0.10	1.00	0.00	0.00
	0.00	0.00	0.00	0.00
	0.00	0.00	0.00	0.00
	0.00	0.00	0.00	0.00
			ΣSN	3 39

Job No. 1,288

Pavement Design Calculations

#### Pavement Thickness Design According to 1993 AASHTO Guide for Design of Pavements Structures American Concrete Pavement Association

### **Flexible Design Inputs**

Agency: Company: GEG Job No. 1,288 Contractor: Project Description: Dakota West Subdivision, Accel / Decel Lane Location: N & W of D ½ Road and 31 Road

#### Flexible Pavement Design/Evaluation

Structural Number Design ESALs Reliability Overall Deviation	3.39 1,204,500.00 80.00 0.45	percent	Soil Resilient Modulus Initial Serviceability Terminal Serviceability	6,607.00 4.50 2.50	psi
Reliability Overall Deviation	1,204,500.00 80.00 0.45	percent	Terminal Serviceability	4.50 2.50	

#### Layer Pavement Design/Evaluation

Layer Material	Layer Coefficient	Drainage Coefficient	Layer Thickness	Layer SN
Asphalt Cement Concrete	0.40	1.00	4.00	1.60
Crushed Stone Base	0.12	1.00	6.00	0.72
Granular Subbase	0.10	1.00	10.66	1.07
	0.00	0.00	0.00	0.00
	0.00	0.00	0.00	0.00
	0.00	0.00	0.00	0.00
			ΣSN	3 39

Job No. 1,288

Pavement Design Calculations

### Pavement Thickness Design According to 1993 AASHTO Guide for Design of Pavements Structures American Concrete Pavement Association

### **Rigid Design Inputs**

Agency: Company: Job No. 1,288 Contractor: Project Description: Dakota West Subdivision, Accel / Decel Lane Location: N & W of D ½ Road and 31 Road

#### Rigid Pavement Design/Evaluation

PCC Thickness Design ESALs	7.68 1,806,750.00	inches	Load Transfer, J Mod. Subgrade Reaction, k	3.20 340	psi/in
Reliability Overall Deviation	80.00 0.35	percent	Drainage Coefficient, Cd Initial Serviceability	1.00 4.50	
Modulus of Rupture Modulus of Elasticity	500 3,375,000	psi psi	Terminal Serviceability	2.50	

Modulus of Subgrade Reaction	145.00	psi/in	
Loss of Support Value (0,1,2,3)	0.00		
Depth to Rigid Foundation	0.00	feet	
Subbase Thickness	0.00	inches	
Resilient Modulus of the Subbase	0.00	psi	
Resilient Modulus of the Subgrade	6,607.00	psi	
Wodulus of Subgrade Reaction (K-value	<u>Determinatio</u>	<u>n</u>	

Job No. 1,288

Pavement Design Calculations

#### Pavement Thickness Design According to 1993 AASHTO Guide for Design of Pavements Structures American Concrete Pavement Association

### Flexible Design Inputs

Agency: Company: GEG Job No. 1,288 Contractor: Project Description: Dakota West Subdivision, Interior Streets Location: N & W of D ½ Road and 31 Road

#### Flexible Pavement Design/Evaluation

Structural Number Design ESALs 5 Reliability Overall Deviation	2.05 54,750.00 80.00 0.45	percent	Soil Resilient Modulus Initial Serviceability Terminal Serviceability	6,607.00 4.50 2.00	psi
			5		

#### Layer Pavement Design/Evaluation

Layer Material	Layer Coefficient	Drainage Coefficient	Layer Thickness	Layer SN	
Asphalt Cement Concrete	0.40	1.00	5.13	2.05	
Crushed Stone Base	0.12	1.00	0.00	0.00	
Granular Subbase	0.10	1.00	0.00	0.00	
V 0	0.00	0.00	0.00	0.00	
	0.00	0.00	0.00	0.00	
	0.00	0.00	0.00	0.00	
			ΣSN	2 05	

Job No. 1,288

Pavement Design Calculations

# DAKOTA WEST SUBDIVISION PHASE 2 A REPLAT OF LOTS 10 AND 12, BLOCK 1 OF DAKOTA WEST SUBDIVISION CITY OF GRAND JUNCTION, MESA COUNTY, COLORADO

YICINITY MAP



NOTES

\* Intestion assument located on the north boundary of subdivision to be granted by supersite instrument.



#### STATEMENT OF OWNERSHIP AND DEDICATION

KNOW ALL MEN BY THESE PRESENTS:

That the undereigned, G&R West, LLC, a Colorado Linited Linitely Company, is the same of that null property in the County of Mean, State of Colorado, described at Reception Moi 2005/052, 2009007, and 2004/750 of the recent of the Mean County Clark and Recorder, and are shown on the accompanying plats, said property being more particularly described as thoses.

Lot 10 Block 1, Debote West Sub-Melon

Let 12 Black 1, Datata Host Subdivision, according to the plat thereof recorded at Reception No.\_\_\_\_\_ In the office of the Mesea Country Cart and Recorder

That sold Owner has by these presents lold cut, platted and sublished the above learning read property as shown herean, and designates the same as DALDTA WEBT SUBDIVISION FINARE 2, a subdivision of the Obje of Grand Junction, Mess County, Johnson, and does hereby make the following dedications and granter.

<sup>4</sup> All structs and roads shown hencer, being Alexidson Lane, Diemarck Otreer, and Weehum Struct to the full width of their platted rights-of-new are hereby dedicated to the City of Crand Junction for the use of the public forever as public structs, and for drainage and underground utility purposes.

\*All makin-purposes examinants dedicated to the Oily of Orand Junction for the use of Oily approved public utilities as perpetual essenants for the installation, operation, matricence and repair of utilities and appurtementes thereto including but not invited to dedictic lines, could Villes, externing as profiles, earliering search has, writer less, talaphone lines, irrigation lines, draining, and also for the installation and matricence of tranfile countries fastings, stream fasting, these and grade originates.

\*Al drainage assemants are to be granted by separate instrument to the Delote West Homeoward Association as perpetual assemants for consumance of runoff water which originates if from the property hereby platead, subjects to the terms, conditions and relations est forth in said grant. Grant recorded in Book \_\_\_\_\_ at Page \_\_\_\_\_

All brigation assements are to be granted by expensive instrument to the Debute West Homeowners Association as perpetiple sections for the buildstice, operation, resistances and reperior of brigation systems and to supply and drain brigation peter. Grant recorded in Book \_\_\_\_\_\_ at Page \_\_\_\_\_.

\*All assessments include the right of ingress and agrees on, stong, over, under, through and aprove by the beneficiaries, their successors, or anyon, together with the right to form or reverse interfering trace and insuits provided however, there the beneficiaries/ private shall utilize the same is a resecrable and prudeit memory. Furthermore, the more of each its is store by patital shall not burden or overhurden each essentiate by practing or placing any improvements therean ishibit may prevent resecrable ingress and agrees to and from the assessment.

Sold owners further certify that all Retholders are represented hereon.

IN WITNESS WHEREOF asid owners have asured their names to be hereunto autoordinal.

G & R West, LL.C., a Colorado Limited Liebility Company.

		By Henaging Parts
State of	2	
Courts of	<u> </u>	

The foreactive Statement of Commission and Dedication was acknowledged before me

y \_\_\_\_\_\_ an Managing Partner of G & R Wart, LLC

its \_\_\_\_\_\_ day of \_\_\_\_\_\_\_, 2005 for the atorementioned purposed

Natary Public

As any statements of the section of

DECLARATION OF COVENANTS

This property is subject to the terms of the parameter, conditions, and restrictions contained in an instrument recorded in Book \_\_\_\_\_\_ at Page \_\_\_\_\_\_

#### TITLE CERTIFICATION

HILD CECK IT PARTIAGENT THE Company, a title insurance company, as ally learned in the Starte of Colorade, knowly cantify that we have examined that the Starte of Colorade, knowly cantify that we have examined that the Starte of Colorade, and the Starte of Colorade, the Starte of the Starte of Colorade, the Starte of the Starte of Colorade, the Starte of Colorade the Starte of Colorade, the Starte of Colorade the Starte

BYL NAME AND TITLE Plast American Hertiage This Compary

CITY APPROVAL

Othe Manager

Manar

CLERK AND RECORDERS CERTIFICATE

Otate of Colorado )

County of Mess

This plat was accepted for filing in the office of the Clark and Recordsr of

Mease County, Colorado, at \_\_\_\_ of slook \_\_ M, on this \_\_\_\_\_ day of

ia.\_\_\_\_\_, in First Dook\_\_\_\_ at Page \_\_\_\_\_, Drawer No.

Clerk and Recorder Deputy

#### SURVEYING STATEMENT

I. Denvite R. Shallhorn, a registranul Professional Land Surveyor In the State of Colonado, do humby state their the accompanying plate of DARDTA WEST SUBDIVISION PHASE 2, a subdivision of a part of the City of Grand Junction, Colonado, has have program by mean/or under my direct supervision and improvements a field survey of the same. This plate conforms to the regularization for autoinvision plate expecting in the City of Drand Junction Development Code and the applicable same of the Detect of Colonado to the heart of my Interladge and shall. This statement is only applicable to the survey data hemotic and shall not represent a warranty or option as to constanting, Berholders, or quality of this.

Dennie R. Shelhorn, Colorado PLS 18478

This survey does not constitute a title earnch by this survey does not constitute a title earnch by this survey or "hompson-Langford Corporation. All information regarding ownership, rights-of-way, earnormet or incard, adjointerna, and other adsources that may afflex the quality of this to this property is from a title commitment program by Prex American Nettoge Title Company, No. CON40702, datad Morris 25, 2002, Meriden Land This, LLC, No. 50610, datad Morris 20, 2002, and Meriden Land Title, LLC, No. D62445, datad Morris 2002.

#### NOTE

A foundation observation report by a licensed Engineer is required for indicing construction.









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# **DAKOTA WEST SUBDIVISION PHASE 2** A REPLAT OF LOTS 10 AND 12, BLOCK 1 OF DAKOTA WEST SUBDIVISION **CITY OF GRAND JUNCTION, MESA COUNTY, COLORADO**





NOTES

Intention assement located on the north boundary of subdivision to be granted by



STATEMENT OF OWNERSHIP AND DEDICATION KNOW ALL MEN BY THESE PRESENTS

That the undersigned, GSR Wost, LLC, a Colorado Linutad Lishibity Company, is the owner of that real property in the County of Mese, State of Colorado, described at Reception Nor's 2008/087, 2006/087, 2004/788 and 21/22/48 of the records of the Mese County Cark and Recorder, and as shown on the accompanying plat, seld proper boing more particularly described as billows:

Lot 10 Block L Daketa West Subdivision ANY Lot 12 Block I, Dakota West BubdMalon, according to the plat thereor recorded at Recorder Clerk and Recorder

That sold Owner has by these presents laid out, platted and subdivided the above described real property as shown hereon, and designates the same as DAKDTA WEDT SUBDYISHON PHABE 2, a subdivideo of the City of Grand Jurotion, Mess County, Colorado, and does handly make the following dedications and granter

<sup>4</sup> All streats and roads shown hereon, being Aberalam Lans, Biemarck Streat, and Weakhum Streat to the full water of their platted rights-of-way are hereby dedicat to the CDy of Grand Junction for the use of the public forever as public streats, an for drainings and underground utility purposes.

pee peepents dedicated to the City of Grand J I public utilities as perpetual essemantic for the hert and repear of utilities and appartenentoes thereto in total and the safe TV here, netural gas pipetnes, and the here, interfer to the drain age, and also for the her of traffic control facilities, utrain lighting, traves and the frames.

s assements are to be granted by separate instrument to the Dakota West Association se perpetual essements for convegence of runoff water which on the property hereby platted, subject to the terms, conditions and set forth in said grant. Grant recorded in Book <u>3395</u> at Page <u>983</u>.

ved by the owners for the benefit of adjoining properties.

Include this right of ingreese and agreese on, slong, over, under, through he beneficiance, their successors, or asset together with the right withorforing trans and brunk provided however, thus the beneficiants flas the same in a reasonable and prudent manner. Furthermore, the oth hardsy platted shall not burden or overkunder and assements by f anid lots he n which may pro

Seld owners further cartify that all lienholders are represented herson.

THESS WHEREOF eacl among have caused their names to be he

State of Country of The foregoing St. w Kohert G. Cantrell as Managing Partner of G & K West, LLC the 23'd word Jules Santte & anth ty commission againer 02117/04

#### LIENHOLDERS RATIFICATION OF PLAT

densigned hereby contribut the sholder of a security interset upon operty hereon described and does hereby join in and consent to the tion of the land described in addiadization by the current thereof and just for executivy interset which is recorded in Book 5571 at Fage 654 of gree that Ite ado shall be subordinated to the dee

(Thicken ) Und-For: Bank of Colorade

State of Colorados Country of Meso.)

Notary Public

notion expires: 01-25-00

The foregoing Lienholder's Ratification of Flat was by Michael Mast, Vice Ausident of Bank of Colorada,

Vice Aresident on 2310 and Stuly for the effortmentioned purposes,

TITLE CEITIFICATION We, Martelen Land Thie, LL.C., a this insurance company, as duly licensed in the State of Colorado, handy cartly that we have auamited the State of the hencon described property. that we find the title to the property is vested to G&R West, LLC, a Colorado Limitad Labitity Company that the current tense have been paid; that all nontagepen not activities or cales and or record nor otherwise terming to law one others hence be that the them are not set means and the to are are of in hencen and that there are no o mb That all paperments, res etions and rights of say of record an shown hereon.

BY DEA LAWRENCE D. YENT PATE JULY 23, 2003 Heridian Land Title LLC

CITY APPEROVAL

Otate of Colorado )

July \_\_\_\_. 2000. A.D., and was recorded at Reception No. 2138663 In Flat Book 9 at Page 375 Drawer No. 00-19 -- \$20.00+ \$1.00

Clerk and Keconse

alts a title search by this surveyor or The tion. All information regarding ownership, rights-of-way, one, adjoiners, and other documents that may affect the quality many is from a title commitment memory is that Amount of title t m a title commitment prepared by First Am 10146173, deted March 20, 2002, Meridian I ad March 20, 2002, and Maridian Land Title, LLC

NOTE

FP-2003-079 RMF-5 SIF 292.00 500.00 TCP

DECLARATION OF ODVENANTS

This property is subject to the terms of the covenants, conditions, and r contained in an instrument recorded in Dock  $\underline{3395}$  at Page  $\underline{970}$ 

This plat of DAKOTA WEST SUBDIVISION PHASE 2, a subdivision of the City of Grand lunction, County of Mess. State of Colorado, was approved

this 24th day of Th 1hAn glarry 5 Bulli

CLERK AND RECORDERS OPENINGATE

County of Mesa

This plat was accepted for filing in the office of the Clerk and Recorder of Mose County, Colorado, at 15 dock B.M. on this 24th day of

SURVEYOR'S STATEMENT

L Dermie E. Shallhort, a registered Professional Land Burveyor in the State of Colorado, do hereby state that the accompanying plat of DAKOTA WEST SUDDIVISION PHASE 2, a subsidiation of a part of the City of Grand Junction Colorado, has been prepared by ma analor under my direct supervision and represente a field survey of the same. This plat confirms to the regularement for sub-Mission plate specified in the City of Grand Junction Development Col and the applicate large of the State of Colorado to the beet of my browkedge and beier. Indeed Tables, is endy specification to plate survey and thereon, and beier. Indeed Tables of the State of Colorado to the beet of my browkedge and beier. Indeed Tables is endy specification to the specific specific to a substance of the State of Colorado to the servery date bereon, and does of the specific the menty or opinion as to ownership, Berholders,

A foundation observation report by a licensed Engineer is required for building construction.







COMMUNITY DEVELOPMENT

June 15, 2004

FP-2003-079

. 6 .....

Rob and Gina Cantrell G & R West, LLC

RE: Fencing in dedicated right-of-way / Fences over the allowed height in the front-yard setback

Dear Rob & Gina:

For permission to allow the current illegal fencing to remain in the Dakota West, Subdivision, two permits will need to be applied for: 1) A Revocable Permit for the fencing to remain in and across dedicated rights-of-way; 2) a variance to allow over height fencing to remain in the front-yard setback until the fencing in the right-of-way is removed. I am enclosing both checklists that are required for these processes.

The first process will be the Variance, which will be reviewed by the Planning Commission. If the variance is granted, Staff will recommend that it be conditioned. When the fences in the right-of-way are to be removed, the fences in the front-yard setback will have to be removed or lowered to meet the current Code requirements for fencing in the front-yard setback.

The second process will be the Revocable Permit, which will be reviewed by the City Council. You can submit the materials for review at the same time, but they will be two separate processes.

As I mentioned to you earlier, there is no precedent for issuing a Revocable Permit for fencing across a dedicated right-of-way. If the Variance for the fence in the front-yard setback is denied by the Planning Commission, the process will stop there and the Revocable Permit will not proceed to the City Council.

Should you have any further questions regarding this process please feel free to contact me at 256-4033.

Sincerely.

Lori V. Bowers, Senior Planner Community Development Department

FEE \$10.00	PERMIT #	12211
GRAND JUNCTION COMMUNITY DEVELOPMEN		
PROPERTY ADDRESS 308 8 D 2 Rd	A PLOT PLAN	
TAX SCHEDULE NO 2943-161-00-187		
PROPERTY OWNER GIAG + ROD Control		<u> </u>
OWNER'S PHONE (970) 255-8164	л. Ал — И	0.
OWNER'S ADDRESS	the	fla
CONTRACTOR CHRIS'S LANDSCADING	NOR	·
CONTRACTOR'S PHONE (970) 640-0244	Be	÷
CONTRACTOR'S ADDRESS 528N26H st.		
FENCE MATERIAL Cedur Fonce		
FENCE HEIGHT 6Ft /30" in pront		
Plot plan must show property lines and property dimensions, all ease all setbacks from property lines, & fence height(s). NOTE: PROPER BEHIND THE SIDEWALK.	ements, all rights-of-way, all TY LINE IS LIKELY ONE FO	structures, OT OR MORE
A THIS SECTION TO BE COMPLETED BY COMMUNITY DEVELO	PMENT DEPARTMENT STA	FF =

D.

ZONE KMF-S SET	TBACKS: Front from property line (PL) or
special conditions pront 20' will be	from center of ROW, whichever is greater.
30" then le grom then back. side	e <u>Ol</u> from PL Rear <u>Oc</u> from PL

Fences exceeding six feet in height require a separate permit from the City/County Building Department. A fence constructed on a corner lot that extends past the rear of the house along the side yard or abuts an alley requires approval from the City Engineer (Section 4.1.J of the Grand Junction Zoning and Development Code).

The owner/applicant must correctly identify all property lines, easements, and rights-of-way and ensure the fence is located within the property's boundaries. Covenants, conditions, restrictions, easements and/or rights-of-way may restrict or prohibit the placement of fence(s). The owner/applicant is responsible for compliance with covenants, conditions, and restrictions which may apply. Fences built in easements may be subject to removal at the property owner's sole and absolute expense. Any modification of design and/or material as approved in this fence permit must be approved, in writing, by the Community Development Department Director.

I hereby acknowledge that I have read this application and the information and plot plan are correct; I agree to comply with any and all codes, ordinances, laws, regulations, or restrictions which apply. I understand that failure to comply shall result in legal action, which may include but not necessarily be limited to removal of the (fence(s) at the owner's cost.

include but not necessarily be limited to temoval or menerate(s) at the owner's cost.	
Applicant's Signature Chow he law he AMGR	Date
Community Development's Approval C. tay Adam	Date 2/12/03
City Engineer's Approval (if required)	Date



# **DAKOTA WEST SUBDIVISION PHASE 2**



# FP-200 **DAKOTA WEST SUBDIVISION** OF PARCELS SITUATED IN THE SE1/4 NE1/4 S.16, T.1 S., R.1 E., UTE MERII CITY OF GRAND JUNCTION, MESA COUNTY, COLORADO

VICINITY MAP



NOTES

ement located on the north boundary of sublivielon to be granted by ment.





a survey does not constitute a title search by this surveyor or Thempson-igford Corporation. All Information regarding ownership, righte-of-way, emonts of record, adjoiners, and other documents thats may affact the quality title to this property is from a title constituent property by First American fuega Title Comparty. No. 64405, databal June 12, 2008. Langford of title to

NOTE tion observation report by a loan for building construction. relate

5

ADITCE: According to Coldroom law you must commence any legal action based upon any defect in this survey within three years after you first discover defect. In no event eavy any action based upon any defect in this survey be commenced each bank ban year year from the date of the cartification atomin here

LAND USE SUMMARY LOTS TRACTS STREETS 80.1% 2.7% 12.2% 0.301 gcres 1.353 gcres TOTAL 11.061 ocms 100%

STATEMENT OF OWNERSHIP AND DEDICATION

KNOW ALL MEN BY THESE PRESENTS 

Beginning at a point which bears West 496 fast from the East Quarter Corrier of Bection 18, Ternship 1 Bouch, Range 1 East of the Ute Meridien, thence West 125 feet; thence East 125 feet; thence East 125 feet; thence East 126 feet; to the Point of Beginning. EXCEPT road right of way on the Bouth. AND Beginning 485.0 feat East of the Southwest Corner of the SEI/4 of the NEV4 of said Sector 15 thereos North COTBTON East 1932.01 fast to the North Bre of said BEI/4 of the 1 EU4 of Sector 16 thereos Booth S71.82 feat thereos Booth S71.82 feat thereos Booth S71.82 feat thereos Booth S71.82 feat thereos Booth S71.84 feat S71.84 feat S71.84 feat S72.85 feat there Bouch 340.40 freq there Bouch 340.40 freq EXC2PT Depriving as the Bouchwest Conter of and BE1/4 of the NE1/4, whose Bouch Net Networks South 907000° East with all bearings container herein to be relative thereta; there Bouch 9070000° East 4406.0 field there Bouch 9070000° East 4406.0 field there Bouch 00° BOOC° East 4406.0 field there Bouch 00° BOOC° East 440.70 field there Bouch 00° BOOC° East 447.70 field there Bouch 00° BOOC° East 447.70 field there Bouch 00° BOOC° Meet 154.70 field there North 80° COOOC° West 47.70 field the true Point of Depinning AND Regiming at a point being 567,00 feet NOC'O/O/CE and 188,00 feet NBC/DO/O/W of the 65 corner of the NEVA Section 16, 115, NT2, LIM, and considering the East line of the NEVA Section 16, 115, NT2, LIM, Earlier 1 Early, LIM, to lear NOC'O/D/CE and all bestinge contained here to be determine the common section.

Eastly (July to Pair Net of the most northerly NEcomer og the lend s00°00'00° 87.20 fæst to the most northerly NEcomer og the lend al n Dok 1202 at Page 826; N80°00'00° 870.00 fæst N80°00'00° 870.00 fæst S00°00°00° 870.00 fæst 500°00°00° 500.00 fæst 500°00°00° 500.00 fæst

AND Deginning at the Boutinevet corner of a parcel of land described in a warranty deex recorded in Book 3192 at Fage 514 of the Mess County

In any series (section) to both the both 2012 as I age both the three to being series along the extension of the Bouth line of that percel described eadl Book 3212 at Page B14, North 88°067467 West, a distance of 2.01 set to the East line of a percel of land described in a warparity deed recorded Dook 3216 at Pages B5/1569. Hence storing the East line of thiss percel described in and Dook 3246 at second any the East line of thiss percel described in and Dook 3246 at second any the East line of thiss percel described in and Dook 3246 at second any the Bouth line of this percel described in and Book 3246 at second any the Bouth line of this percel described in setal Book 22266 at second any the Bouth line of this percel described in setal Book 22266 at second any the Bouth line of this percel described in setal Book 22266 at second any the Bouth line of this percel described in setal Book 22266 at second any the Bouth line of this percel described in setal Book 2266 at second line to the Second line at Book 5025 at Fage 574; second any set West line, South CO°0314° West, a distance of 365.55

That acid Owner has by these presents laid out, platted and subdivided the shows described real property as shown hereon, and designates the same as DAKOTA WEST SUBDYNSON, a widebase of the Dry of Grand Jumston, Neas County, Colorado, and does hereby mats the following dedications and grantes

<sup>6</sup> All etrests and roads shown haraon, being Alamiaan Lana, Bienterck Streen, and D-V2 Read to the full width of their platted rights-of-way are hereby dedicated to City of Grand Junction for the use of the public forever as public streats, and for drainage and underground utility purposes.

<sup>4</sup> All multi-purpose segments deallested to the City of Grand Junction for the use of City a purpose public stiffeties as perpectual estematics for the installation; operation, matricians and repair of utilities and appurtaments thereto including but, for brothed to deterio less, cable TV lines, instand are pholines, sentiary server lines, with mask, todephone lives, instantion and instant setting operation lines, instanda, and also for the installation and instant setting operation lines, instanda, and also for the installation and instant setting operation lines, instanda, and also for the installation and instant setting operation lines, instanda, and also for the installation and instant setting operation lines, instanda, and also for the installation and

<sup>6</sup> Utility assemants dedicated to the City of Grand Junction for the use of City approved public utilities as perpetual severants for the installation, operation maintenance and report of utilities and appurtenances thereto including just not instants to select to inse, calle TV insex, natural gas pipelines, santiary sever inse, water lines, and telephone insex.

• All drainage seguments are to be granted by separate instrument to the Datota We Homeowner Association as perpetual essenants for conveyance of runsft water which originates in from the property hereby platted, subject to the terms, conditions and representations are freth in and grants. Charts recorded in Book 3395 rr Page 9.70

Tract A is to be conveyed by departed instrument to the Debate Wast Homeomen secondation, for the purpose of retaining runoff matter which orginates from the proper entry platted, or from operations means, through natural or man-made facilities and anautomal and asythetic purposes as determined appropriate by said owners, subject parms estimations and asythetic burgers and subject to the Convention and constitutions for Children West. Deed of convegiance recorded in Boot 2355 st Page 970

\* All essentible in tude the right of ingress and agrees or, along, over, under, through and across by the isonaliciaries, their successors, or assigna, together with the right to strin or remove interfering trease and investig provided however, that the isoniciciaries owners of add tother the sense in a reasonable and prudent memore. Furthermore, the amounting or plends, ary improvements therean which muy prevent responsible ingress and agrees to and from the assessment.

Said owners fath -- certify that all fienholders are represented hereon.

IN WITNESS WHERE OF and memory have druged their n

G & R West, LLC. & Colorado Limited Liability Company

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State of ) os County of )	a corone			
W Robert Contre	10	enaging Farther o	I G & K Wort, LLC	
Panetti Kan	ott			
My commission expires: O	2/17/06	_		
DECLARATION OF COVENAN This property is subject to t contained in an instrument r	ns he terms of the cover scorded in Book 314	santa, conditional, 15 at Page 97	and restrictions	
LIENHOLDIERS KATIFICATIO	OFPLAT			
The undersigned hereby certi- interest upon the property in join in and concerts to the de dedication by the owners the interest which is recorded in public records of Messe Court	flee that it is a holde aroun described and a dication of the lend a woof and agree that i Book 3371 at Page 5 by, Colorado shall be s	r of a security loss handry lescribed in seld to security 54 of the security		
to the dedications shown he in witness whereof, the said to be signed by its <u>(156); (cf</u> sutherity of its Board of Din	rean. separation has cause His climit of actors, this 197 d	d these presents , with the law of 2003.		8+ T-4
man Strate Muller	For Bank of	Colorado		
TITLE CERTIFICATION	a title House com	Denv. at the		
Boarneed in the State of Colo examined the title to the her title to the property is vesta Liability Company. That the c mortgagee not estimated or r	rado, hereby certify ti won described proper- ul to G&R Weet, LLC, surrent taxes have he visesed of record nor	hat we have ty, that we find th a Colorado Limite on paid; That all otherwise termin	and a second	
by law are shown hereon and record: That all assements, i shown hereon.	that there are no off secretions and right	te of way of recon	of Lare	
DATE JUNE 19, 2003	BT- NAME AN Moridian L	DA LAWRENT	<u>E D</u> VENT EXAMINER	
CITY APPROVAL This plat of DAROTA WEST I	SUEDMBION, a substit	vision of the City (	of Grand	
Junction Country of Moses, 5 shin2415 day of	Late of Colorado, was 2005.	Approved	2	
City Mandan	t Gra	Council Hemb	lmen	
CLERK AND RECORDERS OF	RIFICATE			
State of Colorado ) jea County of Mase )				
This plat was accepted for fi	We in the office of the	Clerk and Kecon	ler of	
June 2	DOD, A.D., and was ro	conded at Recept	lon	
NN-124 rm # 20.	00 4 #1.00	Drawer No		
Dyt Clerk and Recorder	Deputy			_
SURVEYOR'S STATEMENT				
of Colorado, do hereby state SUDDIVISION, a subdivision o	that the accompany if a part of the City of	ne plat of DAKOT f Granel Junction,	A WEDT Colorado,	-
a field survey of the same. T plate specified in the City of	his plat conforms to I Grand Junction Devel	the requirements lopment Code and	for subdiMelon the	
and ballet. The state provert is and doesn't the transferment is	only applicable to the per manty or opinion as t	e ourvey data here e ownership, lienh	e Ion, oldere,	
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Color A Statement (2) (2)	63			
or colored	DAKOTA	WEST	SUBD	VISION
	G	& R W	EST LLC	
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I	HOMPSON	LANGE	URD COR	ORATION
6	rand Junet	ion 00 81	508 tloot	lowest.com
5	Survey 10543 GGR	West \plat pro	Job .	No. 0543-001



# **DAKOTA WEST SUBDIVISION PHASE 2** A REPLAT OF LOTS 10 AND 12, BLOCK 1 OF DAKOTA WEST SUBDIVISION CITY OF GRAND JUNCTION, MESA COUNTY, COLORADO



. . . .

inigation assement located on the north boundary of subdivision to be granted by



STATEMENT OF OWNERSHIP AND DEDICA KNOW ALL MEN BY THESE PRESENTS:

That the undersioned, G&E West, LLC, a Colorado Limited Liability Co property in the Country of Mess, State of Colorado, 055195, 2090557, 2054768 and 2122546 of the r

Los 10 Block I, Datata West Bu

Lot 12 Block 1, Dakota Wort Subdivision, sooo

the same as DALOTA WER A58 2. a put

ion for the use of the

her cartify that all lienholders are represented hereon



#### LENHOLDERS RATIFICATION OF PLAT

hereby part then that it is a holder of a a raby join in and con mt to the ny the owners thereof n Book 3371 at Fage (

caused these presents to be signed In the authority of its Board of Directs Michael Unit

(Title) Vice Presider

nieston actives: 01-25-06

State of Colorados Course of Mesa.)

The foregoing Lionholder's Ratifica

by Michael Mast, Vice President\_ of Bank of Colored

Vice President pres 231d any of July Sharm Tibbette

DATE JULY 13. 1003

CITY AFFECTVAL This plat of DAKOTA WEST SUBCIVISION PHASE 2, a subdivision of the City of Grane Junction, County of Mean, State of Colorado, was approve this 24 day of Th 2005

Otato of Colorado ) County of Mees This plat was accepted for films in the office of the Clerk and R Ares County, Colorado, at 15 dock P. M. on this 24th day of July 2000, AD, and was recorded at Ray No. 2136663 In Plat Book 9 at Pag 375 Draws July

Clark and Karns

FP-2003-079 RMF-5 292.00 SIF 500.00 TCP

DECLARATION OF CONFNANTS

The property is subject to the terms of the covenants, conditions, and contained in an instrument recorded in Book 3395 at Fage 9.70

THE CERTIFICATION

an Land The LLC a this he

E TITLE EXAMINER

atarry

GLERK AND RECORDER'S CERTIFICATE

00-19 roo \$ 20.00+ \$1.00

SURVEYOR'S STATEMEN

a dated March 25, 2002 March 20, 2002, and Mr

report by a licensed Enginee

