

### **Purchasing Division**

### **ADDENDUM NO. 2**

DATE: February 9, 2018

FROM: City of Grand Junction Purchasing Division

TO: All Offerors

RE: Las Colonias Business Park Phase I and Phase IA IFB-4476-18-DH

Offerors responding to the above referenced solicitation are hereby instructed that the requirements have been clarified, modified, superseded and supplemented as to this date as hereinafter described.

Please make note of the following clarifications:

- 1. Pre-Bid Agenda and Attendance list attached.
- 2. Water Valve Box Valve boxes shall weigh a minimum of 90 lbs.
- 3. **Construction Timeline -** 56 calendar days have been added to the project.
- 4. Water Quality Outlet Structure See attached detail.
- 5. **Geotechnical Report** See attached.
- 6. **HP Storm Pipe** Approved equal to Reinforced Concrete Pipe.

### Q&A

- 7. **Discrepancy in Curb Height** The bid schedule shall apply (14" Curb Height). If the Contractor chooses so, spill gutter may be placed in lieu of 6' x 14" curb.
- 8. **Steel Casing Fill Material** Annular space within steel casing shall remain open. The installation of the carrier pipe shall include approved skids, bell restraints and end caps. The end caps may be concrete or approved industry standard boot. Refer to GU 07 for detail.
- 9. Are the triple box culverts intended to be cast in place, pre-cast or either? May be either.
- 10. If cast in place, is it correct we are to use M-601-3 for sizing, thickness and reinforcing of culvert lid, base and walls? If correct: Correct
  - a. Confirm we are to use S-8, R-6 w/ <2' of fill since the table on above standard does not go any smaller. Correct, use S-8, R-6.
  - b. The drawing indicates less than 2' of fill over culvert. Should only the rebar called out in note 5 be epoxy coated or should all rebar be epoxy coated? For cast in place construction rebar shall be epoxy coated in accordance with CDOT M&S Standards, M-601-

- 3 Sheet 2 of 2 (Note 4). Pre-cast construction of box culverts shall be exempt of epoxy coated rebar per M&S Standards.
- c. Detail for head wall (Sheet 20) dimensions base of culvert as 8", if we are to use the table per "a" above, the base is called out as 10" thick. Please clarify. Headwall shall be constructed per dimensions set forth in M-601-3. Yes, 10" base.
- 11. The notes on headwall detail (Sheet 20) refer us to M-601-10 for design. This standard is for pipe headwalls, shouldn't this refer us to M-601-3 which details headwalls for box culverts? Correct, refer to M-601-3.
- 12. Please confirm all reinforcing (retaining wall) shall be epoxy coated per the bid schedule.

  The retaining wall shall require epoxy coated reinforcement throughout.
- 13. The details refer us to M-601-20 for a 4' ht. wall. The bid schedule (Item 54) states "wall design height" should we be using 6' high wall in lieu of 4'? Correct, utilize 6' for design purposes.

\*Revisions to Plan Set(s) and the bid schedule along with geotechnical clarification and the release of existing contour maps shall be included in Addendum No. 3.

The original solicitation for the project noted above is amended as noted.

All other conditions of subject remain the same.

Respectfully,

Duane Hoff Jr., Senior Buyer City of Grand Junction, Colorado



### **Pre-Bid Meeting Agenda**

Date: February 8, 2018

Project: Las Colonias Business Park Phase I and IA Project

Location: City Hall Auditorium

Conducted by: Jerod Timothy, Project Manager

### 1. Introduction, attendance list.

2. **<u>Pre-Bid Meeting</u>** – Attendance at this pre-bid meeting is mandatory for Contractor's submitting bids to become the general contractor.

### 3. Project documents

- a. City of Grand Junction Standard Contract Documents, July, 2010 Edition
- b. Project Bid Documents
- c. Project Plan Set
- d. CDOT Standard Specifications for Road and Bridge Construction, 2017 Edition.

Plans and Bid Documents are available for review or download on the City's Public Works Engineering web page.

### 4. Bid submittal procedures

- a. Contractor's Bid Form
- b. Price Bid Schedule
- c. Attendance at bid opening is optional
- d. Accepting Electronic Responses Only submitted through the Rocky Mountain E-Purchasing System (RMEPS).

### 5. <u>Insurance and bonding requirements</u>

- a. 5% bid bond
- b. Performance and payment bonds (100%)
- c. Insurance in General Conditions



### 6. Addenda

Addendum No. 2 will be posted prior to the end of the Friday, February 9, 2018 and shall include the following:

- Pre-Bid meeting agenda and attendance list along with all notes and questions that are addressed during meeting.
  - Revised Plan Sets Phase I and IA to include sheet numbers, revised joint trench detail (Street and Property Side), removal of 6" irrigation conduit and location of the 6" C-900 recirculation line.
  - Approved Water Valve Box (90 lb. Minimum)
  - Revised Construction timeline (additional 56 calendar days).
  - SP 8 shall be revised as follows:
    - Joint Trench (Street Side) Delete 6" Sched. 80 Landscape Irr.
       Conduit and 6" C-900 Raw Water Irr. Conduit
    - Joint Trench (Property Side) Add 6" C-900 Raw Water Irr.
       Conduit and 6" C-900 Pond Recirculation Conduit
  - o Revised Bid Schedule to include the following:
    - Material quantities for pond bottom.
    - Adjusted quantities to 6" C-900 and 6" Sched. 40 Conduit.
    - Removal of the geotechnical testing line item.
  - Water Quality Outlet Structure Detail
  - Geotechnical Report
  - HP Storm Pipe approved equal for RCP.

It's the bidder's responsibility to make sure they have acknowledged all addendums issued for this project. The bidder can find addendums on the City of Grand Junction Engineering website.

### 7. Project specific issues

- a. **Hours of Operations:** The hours of operations for this Project are as follows: Monday Friday, 7:00 a.m. to 5:00 p.m.
- b. Project Start Date: The project is scheduled begin on Monday, March 26, 2018



- c. **Time of Completion:** The scheduled time of completion for the project has been extended to 152 Calendar days (August 24, 2018) from the starting date specified on the Notice to Proceed.
- d. **Uranium Mill Tailings:** Radioactive mill tailings are not anticipated to be encountered on this Project but in accordance with deed restrictions and the history with the site the Contractor shall adhere to the Uranium Mill Tailings Management Plan supplied in Appendix B.
- e. **Dewatering:** Ground water is expected to be encountered during excavation for deep utilities. When necessary to dewater the Contractor will be required to excavate a settlement pond adjacent to the trench to discharge to. The intent is to capture the water and allow to percolate. Within 30 days of construction of the pond(s) it shall be backfilled to comply with an exemption from the Authority of Solid Waste, Section 9, Temporary Discharge to Impoundment. The cost of said work shall be considered incidental to pipeline installation and will not be measure or paid for separately.

### f. Work by Others:

- i) Xcel Energy and Charter will be providing and placing conduit and installing utilities in Joint Trench (Property Side). The trench is to be excavated by the Contractor per plans and specifications. Along with said work the Contractor will also be responsible for providing and installing conduit in the trench for Century Link. Coordination with Xcel, Charter and Century Link will be required by the Contractor. The Contractor will be responsible for bedding, haunching and backfill of the trench. See Special Provisions 8 (SP 8) for more information.
- ii) The City Traffic Department will supply and install street/stop signs and double yellow striping.
- g. Building Pad Sites Embankment shall be placed in designated pad sites in the following order.
  - i) Phase I A, B, C.
  - ii) Phase IA Refer to sheets 43 46 in Plan Set.



- h. Incidental Items: Any item of work not specifically identified or paid for directly, but which is necessary for the satisfactory completion of any paid items of work, will be considered incidental to those items, and will be included in the cost of those items.
- i. Certified Flatwork Finisher and Technician: Hand finishing concrete will be permitted only when performed under the direct supervision of a craftsman holding the following certificate: ACI Concrete Flatwork Finisher and Technician (ACICFFT) or other Flatwork Finisher certification program approved by the Project Engineer/Manager.

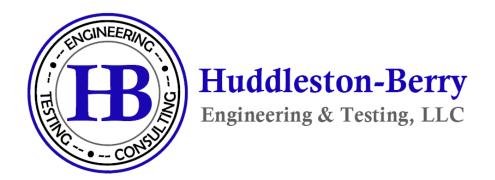
The Contractor shall submit a current certificate at or before the preconstruction meeting.

### 8. Las Colonias Amphitheater:

Access to the east entrance of the Amphitheater main parking lot shall remain open during all events. This will require close coordination between the Contractor and Parks and Recreation. Find a list of scheduled events at www.gjcity.org/residents/parks-recreation/las-colonias-park-amphitheater/upcoming-events-list.

9. **Site Visit** - Suggested to all prospective bidders to visit the locations to see what obstacles they may encounter.

10. Qu	estions and answers
	See Addendum No. 2 for questions and answers.



### GEOTECHNICAL AND GEOLOGIC HAZARDS INVESTIGATION LAS COLONIAS BUSINESS PARK GRAND JUNCTION, COLORADO PROJECT#00208-0077

CITY OF GRAND JUNCTION 333 WEST AVENUE, BUILDING E GRAND JUNCTION, COLORADO 81501

**JANUARY 26, 2018** 

Huddleston-Berry Engineering and Testing, LLC 640 White Avenue,
Grand Junction, Colorado 81501

### TABLE OF CONTENTS

1.0	INTRODUCTION	1
1.1 1.2	ScopeSite Location and Description	
1.3	Proposed Construction	2
2.0	GEOLOGIC SETTING	2
2.1 2.2 2.3	SoilsGeologyGroundwater	2
3.0	FIELD INVESTIGATION	2
3.1	Subsurface Investigation	2
4.0	LABORATORY TESTING	3
5.0	GEOLOGIC INTERPRETATION	3
5.1	Geologic Hazards	
5.2	Geologic Constraints	
5.3	Water Resources	
5.4	Mineral Resources	4
6.0	CONCLUSIONS	4
7.0	RECOMMENDATIONS	4
7.1	Foundations	4
7.2	Seismic Design Criteria	
7.3	Corrosion of Concrete	6
7.4	Non-Structural Floor Slabs and Exterior Flatwork	
7.5	Drainage	
7.6 7.7	Lateral Earth Pressures	
7.7	Excavations	
8.0	GENERAL	8
FIGU	RES Figure 1 – Site Location Map Figure 2 – Site Plan	
APPE	NDICES Appendix A – UDSA NRCS Soil Survey Data	

Appendix B – Typed Boring Logs Appendix C – Laboratory Testing Results



### 1.0 INTRODUCTION

As part of continued development in Western Colorado, the City of Grand Junction proposes to create the Las Colonias Business Park in Grand Junction. As part of the design development process, Huddleston-Berry Engineering and Testing, LLC (HBET) was retained by the City of Grand Junction to conduct a geologic hazards and geotechnical investigation at the site.

### 1.1 Scope

As discussed above, a geologic hazards and geotechnical investigation was conducted for the Las Colonias Business Park in Grand Junction, Colorado. The scope of the investigation included the following components:

- Conducting a subsurface investigation to evaluate the subsurface conditions at the site.
- Collecting soil samples and conducting laboratory testing to determine the engineering properties of the soils at the site.
- Providing preliminary recommendations for foundation types and subgrade preparation.
- Providing preliminary recommendations for bearing capacity.
- Providing recommendations for lateral earth pressure.
- Providing recommendations for drainage, grading, and general earthwork.
- Providing recommendations for pavements.
- Evaluating potential geologic hazards at the site.

The investigation and report were completed by a Colorado registered professional engineer in accordance with generally accepted geotechnical and geological engineering practices. This report has been prepared for the exclusive use of the City of Grand Junction.

### 1.2 Site Location and Description

The site is located east of the Las Colonias Amphitheater in Grand Junction, Colorado. The project location is shown on Figure 1 – Site Location Map.

At the time of the investigation, the site was generally open with a slight slope down to the south. A concrete path ran through the site. Vegetation consisted primarily of scattered weeds. Numerous piles of fill were present across the site. The site was bordered to the north by the Riverside Parkway and existing commercial properties, to the south by the Colorado River, to the west by the Riverside Parkway and the existing Las Colonias Amphitheater, and to the east by existing commercial property.



### 1.3 Proposed Construction

The proposed construction is anticipated to include grading several building pad sites, paved parking lots, and paved site roadways. A generalized site plan is included as Figure 2.

### 2.0 GEOLOGIC SETTING

### 2.1 Soils

Soils data was obtained from the USDA Natural Resource Conservation Service Web Soil Survey. The data indicates that the site is underlain by Massadona silty clay loam, 0 to 2 percent slopes. Soil survey data is included in Appendix A.

Structure construction in the Massadona soils is described as being somewhat limited due to shrink-swell. Road construction in the site soils is indicated to be very limited due to frost action, low strength, and/or shrink-swell. Excavation in the site soils is described as being somewhat limited due to dust, clay content, and/or unstable excavation walls. The site soils are indicated to have a high potential for frost action, high risk of corrosion of steel, and high risk of corrosion of concrete.

### 2.2 Geology

According to the *Geologic Map of the Grand Junction Quadrangle, Mesa County, Colorado* (2002), the site is underlain by alluvium, colluvium, and artificial fill.

### 2.3 Groundwater

Groundwater was encountered in the subsurface at depths of between 5.0 and 10.5 feet below the existing ground surface at the time of the investigation.

### 3.0 FIELD INVESTIGATION

### 3.1 Subsurface Investigation

The subsurface investigation was conducted on January 15<sup>th</sup> and 16<sup>th</sup> and consisted of nineteen borings. The borings were drilled to depths of between 8.0 and 16.0 feet. Boring locations are shown on Figure 2 – Site Plan. Typed boring logs are included in Appendix B. Samples of the native soils were collected during Standard Penetration Testing (SPT) and using bulk sampling methods at the locations shown on the logs.



As shown on the logs, the subsurface conditions were variable. The test pits in the southwestern and eastern portions of the site generally encountered sandy lean clay or lean clay with sand soils to depths of between 4.5 and 13.0 feet. The clay was underlain by dense to very dense sandy gravel and cobbles to the bottoms of most of the borings. However, in boring PL-6, shale bedrock was encountered at a depth of 15.0 feet. Groundwater was encountered in these borings at depths of between 5.0 and 9.0 feet at the time of the investigation.

The borings conducted in the northeastern portion of the site generally encountered fill materials and/or native sand and clay soils to depths of between 4.0 and 10.5 feet. Below the fill/sand/clay, medium dense to very dense sandy gravel and cobbles extended to the bottoms of the borings. Groundwater was encountered in these borings at depths of between 6.0 and 10.5 feet.

### 4.0 LABORATORY TESTING

Selected native soil samples collected from the borings were tested in the Huddleston-Berry Engineering and Testing LLC geotechnical laboratory for natural moisture content, grain size analysis, Atterberg limits, maximum dry density and optimum moisture (Proctor), California Bearing Ratio (CBR), and water soluble sulfates content. The laboratory testing results are included in Appendix C.

The laboratory testing results indicate that the native clay soils are moderately plastic. In addition, the CBR results indicate that the native clay soils are slightly expansive with up to approximately 1.6% expansion measured in the laboratory.

The native sand soils were indicated to be non-plastic. In general, based upon our experience with similar soils in the vicinity of the subject site, the native sand soils are anticipated to be slightly collapsible. Water soluble sulfates were detected in the site soils in a concentration of 0.2%.

### 5.0 GEOLOGIC INTERPRETATION

### 5.1 Geologic Hazards

The most significant geologic hazard identified on the site is the potential impacts to the site of flooding of the Colorado River. However, moisture sensitive soils were also encountered at the site. In addition, shallow groundwater was encountered in portions of the site.

### 5.2 Geologic Constraints

In general, the primary geologic constraint to construction at the site is the presence of moisture sensitive soils. However, shallow groundwater and associated soft soil conditions may also impact the construction.



### 5.3 Water Resources

No water supply wells were observed on the property. As discussed previously, the site lies adjacent to the Colorado River. In general, with proper design and construction, the development of the property is not anticipated to adversely impact surface water or groundwater.

### 5.4 Mineral Resources

Potential mineral resources in western Colorado generally include gravel, uranium ore, and commercial rock products such as flagstone. As discussed previously, gravels were encountered in the subsurface at the site. However, based upon the location of the site and surrounding land use, HBET does not believe that the gravels at the site represent an economically recoverable resource.

### 6.0 CONCLUSIONS

Based upon the available data sources, field investigation, and nature of the proposed construction, HBET does not believe that there are any geologic conditions which should preclude construction at this site. However, foundations, pavements, and earthwork may have to consider the impacts of moisture sensitive soils, potential flooding of the Colorado River, and/or shallow groundwater.

### 7.0 RECOMMENDATIONS

### 7.1 Foundations

As discussed previously, moisture sensitive soils were encountered at the site. However, based upon the nature of the proposed construction, shallow foundations such as spread footings and monolithic structural slabs are likely to be appropriate for lightly loaded commercial structures at the site. However, to provide a uniform subgrade and limit the potential for excessive differential movements, foundations should be constructed above 18 to 36-inches of structural fill depending upon the results of site-specific geotechnical investigations. Where heavily loaded structures are anticipated, deep foundations such as helical piles are appropriate. The foundation alternatives are discussed in the following sections.

### Shallow Foundations

As discussed previously, the native clay soils were shown to be moderately plastic and slightly expansive. Therefore, the native clay soils are not suitable for reuse as structural fill. Imported structural fill should consist of a granular, non-expansive, non-free draining material such as crusher fines or CDOT Class 6 base course. Unless it can be demonstrated that they are not free-draining, pit-run materials should not be used as structural fill.



Prior to placement of structural fill, it is recommended that the bottoms of the foundation excavations be scarified to a depth of 9 to 12-inches, moisture conditioned, and compacted to a minimum of 95% of the standard Proctor maximum dry density, within  $\pm$  2% of the optimum moisture content, as determined in accordance with ASTM D698. However, depending upon the depth of excavation and time of year during construction, shallow groundwater and associated soft soil conditions may exist. It may be necessary to utilize geotextile and/or geogrid in conjunction with up to approximately 30-inches of granular fill to stabilize the subgrade.

Structural fill should extend laterally beyond the edges of the foundation a distance equal to the thickness of structural fill. Structural fill should be moisture conditioned, placed in maximum 8-inch loose lifts, and compacted to a minimum of 95% of the standard Proctor maximum dry density for fine grained soils and 90% of the modified Proctor maximum dry density for coarse grained soils, within  $\pm$  2% of the optimum moisture content as determined in accordance with ASTM D698 and D1557, respectively.

For the foundation building pads prepared as recommended with structural fill consisting of imported granular materials, a maximum allowable bearing capacity of 1,500 to 2,500 psf may be used depending upon the results of site-specific geotechnical investigations. In addition, a modulus of subgrade reaction of 250 pci may be used for structural fill consisting of crusher fines or base course. The bottoms of exterior foundations should extend a minimum of 24-inches below grade for frost protection.

### Helical Piles

Helical piles consist of circular or square steel shafts with load carrying helices attached to them. Some of these types of piers are proprietary. In general, the precise type, size, and quantity of piles should be established by the contractor in conjunction with the structural engineer. However, HBET provides the following preliminary design comments.

In general, helical piles should be designed to penetrate the shallow soils and bear into the dense gravel and cobble soils. It is anticipated that the helical piles will reach refusal within 3 to 10 feet of the top of the gravel and cobble soils. Therefore, pile lengths of up to approximately 23 feet may be possible. However, a minimum pile length of 10 feet is recommended.

In general, for helical piles installed to refusal, the allowable structural capacity is used. Based upon our experience with other projects utilizing helical piles, allowable axial capacities of between approximately 20 and 40 tons are anticipated for helical piles, depending upon the shaft diameter. However, higher capacities are possible, if necessary. The actual allowable capacity should be determined based upon the results of load testing conducted on the individual project sites. To eliminate reductions in capacity from group effects, the piles should be spaced a distance equal to three times the diameter of the largest helix



### 7.2 Seismic Design Criteria

In general based upon the results of the subsurface investigation, the site classifies as Site Class D for a stiff soil profile.

### 7.3 Corrosion of Concrete

As indicated previously, water soluble sulfates were encountered in the site soils in a concentration of 0.2%. This concentration represents a severe degree of potential sulfate attack on concrete. The International Building Code (IBC) specifies Type V cement for this concentration of sulfates. However, Type V cement can be difficult to obtain in Western Colorado. Where Type V cement is unavailable, Type I-II sulfate resistant cement is recommended.

### 7.4 Non-Structural Floor Slabs and Exterior Flatwork

As mentioned above, expansive materials are present in the subsurface at the site. *In general, slabs-on-grade cannot develop sufficient bearing pressures to resist swelling pressures. Therefore, some movement of slabs-on-grade should be expected.* The only way to eliminate the potential for excessive differential movements would be to utilize structural slabs supported by deep foundations. However, structural slabs supported by deep foundations are likely cost prohibitive. In general, the risk of excessive differential movements can be reduced by constructing non-structural floor slabs above 18 to 24-inches of structural fill depending upon the results of site-specific geotechnical investigations. Exterior flatwork should be constructed above a minimum of 12-inches of structural fill.

Floating slabs-on-grade should not be tied in or connected to the foundations in any manner. If a non-structural floating floor slab is used, interior non-bearing partitions should include a slip-joint or framing void which permits a minimum of 2-inches of vertical movement.

### 7.5 Drainage

In order to improve the long-term performance of the foundations and slabs-on-grade, grading around the structures should be designed to carry precipitation and runoff away from the structures. It is recommended that the finished ground surface drop at least twelve inches within the first ten feet away from the structures. However, where impermeable surfaces (i.e. sidewalks, pavements, etc.) are adjacent to the structures, the grade can be reduced to approximately 2.5-inches (ADA grade) within the first ten feet away from the structures. Downspouts should empty beyond the backfill zone. It is recommended that landscaping within five feet of the structures include primarily desert plants with low water requirements. In addition, it is recommended that automatic irrigation within ten feet of foundations, including drip lines, be minimized.



### 7.6 Lateral Earth Pressures

Stemwalls and/or any retaining walls should be designed to resist lateral earth pressures. For backfill consisting of the native soils or imported granular, non-free draining, non-expansive material, we recommend that the walls be designed for an active equivalent fluid unit weight of 55 pcf in areas where no surcharge loads are present. An at-rest equivalent fluid unit weight of 75 pcf may be used. Lateral earth pressures should be increased as necessary to reflect any surcharge loading behind the walls.

### 7.7 Excavations

Excavations in the soils at the site may stand for short periods of time but should not be considered to be stable. The native soils generally classify as Type C soil with regard to OSHA's *Construction Standards for Excavations*. For Type C soils, the maximum allowable slope in temporary cuts is 1.5H:1V.

### 7.8 Pavements

The proposed construction is anticipated to include new parking lots and internal site roadways. As discussed previously, the pavement subgrade materials at the site range from clay soils to fill materials. The design California Bearing Ratio (CBR) of a composite sample of the site soils was determined in the laboratory to be less than 2.0. Therefore, the minimum recommended Resilient Modulus of 3,000 psi was used for the design.

Based upon the subgrade conditions and anticipated traffic loading, pavement section alternatives were developed in accordance with the *Guideline for the Design and Use of Asphalt Pavements for Colorado Roadways* by the Colorado Asphalt Pavement Association and CDOT *Pavement Design Manual*. The following pavement section alternatives are recommended:

### **Automobile Parking Areas (Limited Truck Traffic)**

ESAL's = 100,000, Structural Number = 3.10

		PAVEM	ENT SECTION (	Inches)	
ALTERNATIVE	Hot-Mix Asphalt Pavement	CDOT Class 6 Base Course	CDOT Class 3 Subbase Course	Concrete Pavement	TOTAL
A	3.0	13.0			16.0
В	4.0	10.0			14.0
С	3.0	6.0	10.0		19.0
Rigid Pavement		6.0		6.0	12.0

### **Mixed Use Areas (Higher Truck Traffic)**

ESAL's = 350,000; Structural Number = 3.50

		PAVEM	ENT SECTION (	Inches)	
ALTERNATIVE	Hot-Mix Asphalt Pavement	CDOT Class 6 Base Course	CDOT Class 3 Subbase Course	Concrete	TOTAL
A	4.0	14.0			18.0
В	5.0	11.0			16.0
С	4.0	6.0	11.0		21.0
Concrete Pavement		6.0		8.0	14.0



### **Internal Roadways**

ESAL's = 500,000; Structural Number = 3.91

		PAVEM	ENT SECTION (	Inches)	
ALTERNATIVE	Hot-Mix Asphalt Pavement	CDOT Class 6 Base Course	CDOT Class 3 Subbase Course	Concrete	TOTAL
A	4.0	16.0			20.0
В	5.0	13.0			18.0
С	4.0	6.0	14.0		24.0
Concrete Pavement	•	6.0		8.0	14.0

Prior to new pavement placement, areas to be paved should be stripped of all topsoil, fill, or other unsuitable materials. It is recommended that the subgrade soils be scarified to a depth of 12-inches; moisture conditioned, and recompacted to a minimum of 95% of the standard Proctor maximum dry density, within  $\pm 2\%$  of optimum moisture content as determined by AASHTO T-99. However, as discussed previously, soft soils may be encountered associated with shallow groundwater. It may be necessary to utilize geotextile and/or geogrid in conjunction with up to approximately 30-inches of granular fill to stabilize the subgrade.

Aggregate base course and subbase course should be placed in maximum 9-inch loose lifts, moisture conditioned, and compacted to a minimum of 95% and 93% of the maximum dry density, respectively, at -2% to +3% of optimum moisture content as determined by AASHTO T-180. In addition to density testing, base course should be proofrolled to verify subgrade stability.

It is recommended that Hot-Mix Asphaltic (HMA) pavement conform to CDOT grading SX or S specifications and consist of an approved 75 gyration Superpave method mix design. HMA pavement should be compacted to between 92% and 96% of the maximum theoretical density. An end point stress of 50 psi should be used. It is recommended that rigid pavements consist of CDOT Class P concrete or alternative approved by the Engineer. In addition, pavements should conform to local specifications.

The long-term performance of the pavements is dependent on positive drainage away from the pavements. Ditches, culverts, and inlet structures in the vicinity of paved areas must be maintained to prevent ponding of water on the pavement

### 8.0 GENERAL

The recommendations included above are based upon the results of the subsurface investigation and on our local experience. These conclusions and recommendations are valid only for the proposed construction.



As discussed previously, the subsurface conditions encountered in the borings were variable. However, the precise nature and extent of subsurface variability may not become evident until construction. The recommendations contained herein are designed to reduce the risk and magnitude of differential movements and it is extremely critical that <u>ALL</u> of the recommendations herein be applied to the design and construction. However, HBET cannot predict long-term changes in subsurface moisture conditions and/or the precise magnitude or extent of any volume change in the native soils. <u>Where significant increases in subsurface moisture occur due to poor grading, improper stormwater management, utility line failure, excess irrigation, or other cause, during or after construction, significant movements are possible.</u>

In addition, the success of the structure foundations, slabs, etc. is critically dependent upon proper construction. Therefore, HBET should be retained to provide materials testing, special inspections, and engineering oversight during <u>ALL</u> phases of the construction to ensure conformance with the recommendations herein.

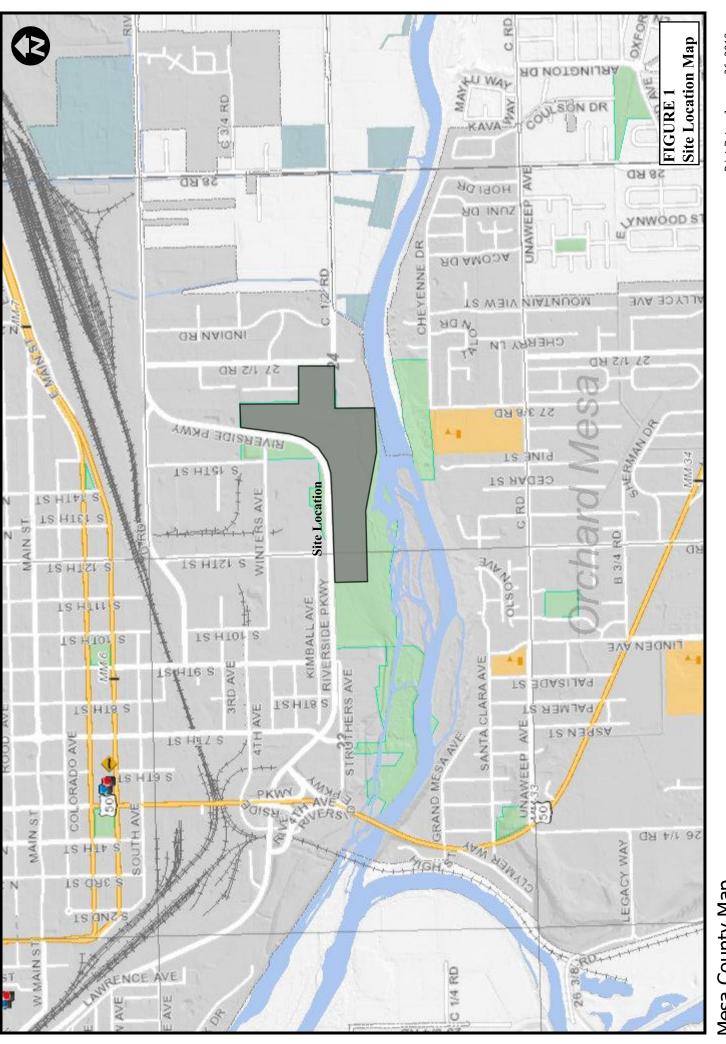
Huddleston-Berry Engineering and Testing, LLC is pleased to be of service to your project. Please contact us if you have any questions or comments regarding the contents of this report.

Respectfully Submitted:

**Huddleston-Berry Engineering and Testing, LLC** 



Michael A. Berry, P.E. Vice President of Engineering



# Mesa County Map



0.15



FIGURE 2 Site Plan





### MAP LEGEND

### Special Line Features Streams and Canals Interstate Highways Very Stony Spot US Routes Stony Spot Spoil Area Wet Spot Other Rails Water Features **Fransportation** W 8 ŧ Soil Map Unit Polygons Area of Interest (AOI) Soil Map Unit Points Soil Map Unit Lines Closed Depression Special Point Features Gravelly Spot Borrow Pit Clay Spot **Gravel Pit** Area of Interest (AOI) Blowout Soils

Major Roads Local Roads

Background

Aerial Photography

Marsh or swamp

Lava Flow

Landfill

Mine or Quarry

Miscellaneous Water

Perennial Water

Rock Outcrop

## MAP INFORMATION

The soil surveys that comprise your AOI were mapped at 1:24,000.

Warning: Soil Map may not be valid at this scale.

contrasting soils that could have been shown at a more detailed Enlargement of maps beyond the scale of mapping can cause misunderstanding of the detail of mapping and accuracy of soil line placement. The maps do not show the small areas of

Please rely on the bar scale on each map sheet for map measurements. Source of Map: Natural Resources Conservation Service Web Soil Survey URL:

Coordinate System: Web Mercator (EPSG:3857)

Maps from the Web Soil Survey are based on the Web Mercator distance and area. A projection that preserves area, such as the projection, which preserves direction and shape but distorts Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required. This product is generated from the USDA-NRCS certified data as of the version date(s) listed below.

Soil Survey Area: Mesa County Area, Colorado

Survey Area Data: Version 8, Oct 12, 2017

Soil map units are labeled (as space allows) for map scales 1:50,000 or larger. Date(s) aerial images were photographed: Dec 31, 2009—Mar

The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident.

Severely Eroded Spot

Slide or Slip

Sinkhole

Sodic Spot

Sandy Spot

Saline Spot

### **Map Unit Legend**

Map Unit Symbol	Map Unit Name	Acres in AOI	Percent of AOI
Ва	Massadona silty clay loam, 0 to 2 percent slopes — DRAFT	41.0	100.0%
Totals for Area of Interest		41.0	100.0%

### **Map Unit Description**

The map units delineated on the detailed soil maps in a soil survey represent the soils or miscellaneous areas in the survey area. The map unit descriptions in this report, along with the maps, can be used to determine the composition and properties of a unit.

A map unit delineation on a soil map represents an area dominated by one or more major kinds of soil or miscellaneous areas. A map unit is identified and named according to the taxonomic classification of the dominant soils. Within a taxonomic class there are precisely defined limits for the properties of the soils. On the landscape, however, the soils are natural phenomena, and they have the characteristic variability of all natural phenomena. Thus, the range of some observed properties may extend beyond the limits defined for a taxonomic class. Areas of soils of a single taxonomic class rarely, if ever, can be mapped without including areas of other taxonomic classes. Consequently, every map unit is made up of the soils or miscellaneous areas for which it is named and some minor components that belong to taxonomic classes other than those of the major soils.

Most minor soils have properties similar to those of the dominant soil or soils in the map unit, and thus they do not affect use and management. These are called noncontrasting, or similar, components. They may or may not be mentioned in a particular map unit description. Other minor components, however, have properties and behavioral characteristics divergent enough to affect use or to require different management. These are called contrasting, or dissimilar, components. They generally are in small areas and could not be mapped separately because of the scale used. Some small areas of strongly contrasting soils or miscellaneous areas are identified by a special symbol on the maps. If included in the database for a given area, the contrasting minor components are identified in the map unit descriptions along with some characteristics of each. A few areas of minor components may not have been observed, and consequently they are not mentioned in the descriptions, especially where the pattern was so complex that it was impractical to make enough observations to identify all the soils and miscellaneous areas on the landscape.

The presence of minor components in a map unit in no way diminishes the usefulness or accuracy of the data. The objective of mapping is not to delineate pure taxonomic classes but rather to separate the landscape into landforms or landform segments that have similar use and management requirements. The delineation of such segments on the map provides sufficient information for the development of resource plans. If intensive use of small areas is planned, however, onsite investigation is needed to define and locate the soils and miscellaneous areas.

An identifying symbol precedes the map unit name in the map unit descriptions. Each description includes general facts about the unit and gives important soil properties and qualities.

Soils that have profiles that are almost alike make up a *soil series*. All the soils of a series have major horizons that are similar in composition, thickness, and arrangement. Soils of a given series can differ in texture of the surface layer, slope, stoniness, salinity, degree of erosion, and other characteristics that affect their use. On the basis of such differences, a soil series is divided into *soil phases*. Most of the areas shown on the detailed soil maps are phases of soil series. The name of a soil phase commonly indicates a feature that affects use or management. For example, Alpha silt loam, 0 to 2 percent slopes, is a phase of the Alpha series.

Some map units are made up of two or more major soils or miscellaneous areas. These map units are complexes, associations, or undifferentiated groups.

A *complex* consists of two or more soils or miscellaneous areas in such an intricate pattern or in such small areas that they cannot be shown separately on the maps. The pattern and proportion of the soils or miscellaneous areas are somewhat similar in all areas. Alpha-Beta complex, 0 to 6 percent slopes, is an example.

An association is made up of two or more geographically associated soils or miscellaneous areas that are shown as one unit on the maps. Because of present or anticipated uses of the map units in the survey area, it was not considered practical or necessary to map the soils or miscellaneous areas separately. The pattern and relative proportion of the soils or miscellaneous areas are somewhat similar. Alpha-Beta association, 0 to 2 percent slopes, is an example.

An *undifferentiated group* is made up of two or more soils or miscellaneous areas that could be mapped individually but are mapped as one unit because similar interpretations can be made for use and management. The pattern and proportion of the soils or miscellaneous areas in a mapped area are not uniform. An area can be made up of only one of the major soils or miscellaneous areas, or it can be made up of all of them. Alpha and Beta soils, 0 to 2 percent slopes, is an example.

Some surveys include *miscellaneous areas*. Such areas have little or no soil material and support little or no vegetation. Rock outcrop is an example.

Additional information about the map units described in this report is available in other soil reports, which give properties of the soils and the limitations, capabilities, and potentials for many uses. Also, the narratives that accompany the soil reports define some of the properties included in the map unit descriptions.

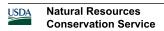
### Report—Map Unit Description

### Mesa County Area, Colorado

Ba—Massadona silty clay loam, 0 to 2 percent slopes — DRAFT

**Map Unit Setting** 

National map unit symbol: k06n



Elevation: 4,500 to 4,900 feet

Mean annual precipitation: 7 to 10 inches

Mean annual air temperature: 50 to 54 degrees F

Frost-free period: 150 to 190 days

Farmland classification: Not prime farmland

### **Map Unit Composition**

Massadona and similar soils: 70 percent

Minor components: 30 percent

Estimates are based on observations, descriptions, and transects of

the mapunit.

### **Description of Massadona**

### Setting

Landform: Fan remnants
Down-slope shape: Concave
Across-slope shape: Linear

Parent material: Alluvium derived from clayey shale

### **Typical profile**

A - 0 to 2 inches: silty clay loam Bw - 2 to 12 inches: silty clay Bky - 12 to 24 inches: silty clay

BCky1 - 24 to 48 inches: stratified silty clay loam to fine sandy

loam

BCky2 - 48 to 60 inches: stratified silty clay loam to fine sandy

loam

### **Properties and qualities**

Slope: 0 to 2 percent

Depth to restrictive feature: More than 80 inches

Natural drainage class: Well drained

Runoff class: High

Capacity of the most limiting layer to transmit water (Ksat): Moderately low to moderately high (0.06 to 0.20 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None Frequency of ponding: None

Calcium carbonate, maximum in profile: 15 percent

Gypsum, maximum in profile: 2 percent

Salinity, maximum in profile: Moderately saline to strongly saline

(10.0 to 32.0 mmhos/cm)

Available water storage in profile: High (about 10.0 inches)

### Interpretive groups

Land capability classification (irrigated): 3s Land capability classification (nonirrigated): 7s

Hydrologic Soil Group: C Hydric soil rating: No



### **Minor Components**

### **Degater**

Percent of map unit: 15 percent Landform: Fan remnants Down-slope shape: Concave Across-slope shape: Linear Hydric soil rating: No

### **Pariette**

Percent of map unit: 15 percent Landform: Fan remnants Down-slope shape: Concave Across-slope shape: Linear Hydric soil rating: No

### **Data Source Information**

Soil Survey Area: Mesa County Area, Colorado Survey Area Data: Version 8, Oct 12, 2017

### **Dwellings and Small Commercial Buildings**

Soil properties influence the development of building sites, including the selection of the site, the design of the structure, construction, performance after construction, and maintenance. This table shows the degree and kind of soil limitations that affect dwellings and small commercial buildings.

The ratings in the table are both verbal and numerical. Rating class terms indicate the extent to which the soils are limited by all of the soil features that affect building site development. *Not limited* indicates that the soil has features that are very favorable for the specified use. Good performance and very low maintenance can be expected. *Somewhat limited* indicates that the soil has features that are moderately favorable for the specified use. The limitations can be overcome or minimized by special planning, design, or installation. Fair performance and moderate maintenance can be expected. *Very limited* indicates that the soil has one or more features that are unfavorable for the specified use. The limitations generally cannot be overcome without major soil reclamation, special design, or expensive installation procedures. Poor performance and high maintenance can be expected.

Numerical ratings in the table indicate the severity of individual limitations. The ratings are shown as decimal fractions ranging from 0.01 to 1.00. They indicate gradations between the point at which a soil feature has the greatest negative impact on the use (1.00) and the point at which the soil feature is not a limitation (0.00).

Dwellings are single-family houses of three stories or less. For dwellings without basements, the foundation is assumed to consist of spread footings of reinforced concrete built on undisturbed soil at a depth of 2 feet or at the depth of maximum frost penetration, whichever is deeper. For dwellings with basements, the foundation is assumed to consist of spread footings of reinforced concrete built on undisturbed soil at a depth of about 7 feet. The ratings for dwellings are based on the soil properties that affect the capacity of the soil to support a load without movement and on the properties that affect excavation and construction costs. The properties that affect the load-supporting capacity include depth to a water table, ponding, flooding, subsidence, linear extensibility (shrink-swell potential), and compressibility. Compressibility is inferred from the Unified classification. The properties that affect the ease and amount of excavation include depth to a water table, ponding, flooding, slope, depth to bedrock or a cemented pan, hardness of bedrock or a cemented pan, and the amount and size of rock fragments.

Small commercial buildings are structures that are less than three stories high and do not have basements. The foundation is assumed to consist of spread footings of reinforced concrete built on undisturbed soil at a depth of 2 feet or at the depth of maximum frost penetration, whichever is deeper. The ratings are based on the soil properties that affect the capacity of the soil to support a load without movement and on the properties that affect excavation and construction costs. The properties that affect the load-supporting capacity include depth to a water table, ponding, flooding, subsidence, linear extensibility (shrink-swell potential), and compressibility (which is inferred from the Unified classification). The properties that affect the ease and amount of excavation include flooding, depth to a water table, ponding, slope, depth to bedrock or a cemented pan, hardness of bedrock or a cemented pan, and the amount and size of rock fragments.

Information in this table is intended for land use planning, for evaluating land use alternatives, and for planning site investigations prior to design and construction. The information, however, has limitations. For example, estimates and other data generally apply only to that part of the soil between the surface and a depth of 5 to 7 feet. Because of the map scale, small areas of different soils may be included within the mapped areas of a specific soil.

The information is not site specific and does not eliminate the need for onsite investigation of the soils or for testing and analysis by personnel experienced in the design and construction of engineering works.

Government ordinances and regulations that restrict certain land uses or impose specific design criteria were not considered in preparing the information in this table. Local ordinances and regulations should be considered in planning, in site selection, and in design.

### Report—Dwellings and Small Commercial Buildings

[Onsite investigation may be needed to validate the interpretations in this table and to confirm the identity of the soil on a given site. The numbers in the value columns range from 0.01 to 1.00. The larger the value, the greater the potential limitation. The table shows only the top five limitations for any given soil. The soil may have additional limitations]

	Dwell	ings and Small Comme	ercial Bu	ildings–Mesa County A	Area, Col	orado	
Map symbol and soil name	Pct. of map	Dwellings witho basements	ut	Dwellings with base	ments	Small commercial bu	ildings
	unit	Rating class and limiting features	Value	Rating class and limiting features	Value	Rating class and limiting features	Value
Ba—Massadona silty clay loam, 0 to 2 percent slopes — DRAFT							
Massadona	70	Somewhat limited		Somewhat limited		Somewhat limited	
		Shrink-swell	0.99	Shrink-swell	0.96	Shrink-swell	0.99

### **Data Source Information**

Soil Survey Area: Mesa County Area, Colorado Survey Area Data: Version 8, Oct 12, 2017

### Roads and Streets, Shallow Excavations, and Lawns and Landscaping

Soil properties influence the development of building sites, including the selection of the site, the design of the structure, construction, performance after construction, and maintenance. This table shows the degree and kind of soil limitations that affect local roads and streets, shallow excavations, and lawns and landscaping.

The ratings in the table are both verbal and numerical. Rating class terms indicate the extent to which the soils are limited by all of the soil features that affect building site development. *Not limited* indicates that the soil has features that are very favorable for the specified use. Good performance and very low maintenance can be expected. *Somewhat limited* indicates that the soil has features that are moderately favorable for the specified use. The limitations can be overcome or minimized by special planning, design, or installation. Fair performance and moderate maintenance can be expected. *Very limited* indicates that the soil has one or more features that are unfavorable for the specified use. The limitations generally cannot be overcome without major soil reclamation, special design, or expensive installation procedures. Poor performance and high maintenance can be expected.

Numerical ratings in the table indicate the severity of individual limitations. The ratings are shown as decimal fractions ranging from 0.01 to 1.00. They indicate gradations between the point at which a soil feature has the greatest negative impact on the use (1.00) and the point at which the soil feature is not a limitation (0.00).

Local roads and streets have an all-weather surface and carry automobile and light truck traffic all year. They have a subgrade of cut or fill soil material; a base of gravel, crushed rock, or soil material stabilized by lime or cement; and a surface of flexible material (asphalt), rigid material (concrete), or gravel with a binder. The ratings are based on the soil properties that affect the ease of excavation and grading and the traffic-supporting capacity. The properties that affect the ease of excavation and grading are depth to bedrock or a cemented pan, hardness of bedrock or a cemented pan, depth to a water table, ponding, flooding, the amount of large stones, and slope. The properties that affect the traffic-supporting capacity are soil strength (as inferred from the AASHTO group index number), subsidence, linear extensibility (shrink-swell potential), the potential for frost action, depth to a water table, and ponding.

Shallow excavations are trenches or holes dug to a maximum depth of 5 or 6 feet for graves, utility lines, open ditches, or other purposes. The ratings are based on the soil properties that influence the ease of digging and the resistance to sloughing. Depth to bedrock or a cemented pan, hardness of bedrock or a cemented pan, the amount of large stones, and dense layers influence the ease of digging, filling, and compacting. Depth to the seasonal high water table, flooding, and ponding may restrict the period when excavations can be made. Slope influences the ease of using machinery. Soil texture, depth to the water table, and linear extensibility (shrink-swell potential) influence the resistance to sloughing.

Lawns and landscaping require soils on which turf and ornamental trees and shrubs can be established and maintained. Irrigation is not considered in the ratings. The ratings are based on the soil properties that affect plant growth and trafficability after vegetation is established. The properties that affect plant growth are reaction; depth to a water table; ponding; depth to bedrock or a cemented pan; the available water capacity in the upper 40 inches; the content of salts, sodium, or calcium carbonate; and sulfidic materials. The properties that affect trafficability are flooding, depth to a water table, ponding, slope, stoniness, and the amount of sand, clay, or organic matter in the surface layer.

Information in this table is intended for land use planning, for evaluating land use alternatives, and for planning site investigations prior to design and construction. The information, however, has limitations. For example, estimates and other data generally apply only to that part of the soil between the surface and a depth of 5 to 7 feet. Because of the map scale, small areas of different soils may be included within the mapped areas of a specific soil.

The information is not site specific and does not eliminate the need for onsite investigation of the soils or for testing and analysis by personnel experienced in the design and construction of engineering works.

Government ordinances and regulations that restrict certain land uses or impose specific design criteria were not considered in preparing the information in this table. Local ordinances and regulations should be considered in planning, in site selection, and in design.

### Report—Roads and Streets, Shallow Excavations, and Lawns and Landscaping

[Onsite investigation may be needed to validate the interpretations in this table and to confirm the identity of the soil on a given site. The numbers in the value columns range from 0.01 to 1.00. The larger the value, the greater the potential limitation. The table shows only the top five limitations for any given soil. The soil may have additional limitations]

Roads and	Streets,	Shallow Excavations,	and Law	ns and Landscaping–N	lesa Cou	unty Area, Colorado	
Map symbol and soil	Pct. of	Lawns and landsca	aping	Local roads and st	reets	Shallow excavation	ons
name	map unit	Rating class and limiting features	Value	Rating class and limiting features	Value	Rating class and limiting features	Value
Ba—Massadona silty clay loam, 0 to 2 percent slopes — DRAFT							
Massadona	70	Somewhat limited		Very limited		Somewhat limited	
		Dusty	0.50	Frost action	1.00	Dusty	0.50
				Low strength	1.00	Too clayey	0.02
				Shrink-swell	0.99	Unstable excavation walls	0.01

### **Data Source Information**

Soil Survey Area: Mesa County Area, Colorado Survey Area Data: Version 8, Oct 12, 2017

### Soil Features

This table gives estimates of various soil features. The estimates are used in land use planning that involves engineering considerations.

A *restrictive layer* is a nearly continuous layer that has one or more physical, chemical, or thermal properties that significantly impede the movement of water and air through the soil or that restrict roots or otherwise provide an unfavorable root environment. Examples are bedrock, cemented layers, dense layers, and frozen layers. The table indicates the hardness and thickness of the restrictive layer, both of which significantly affect the ease of excavation. *Depth to top* is the vertical distance from the soil surface to the upper boundary of the restrictive layer.

Subsidence is the settlement of organic soils or of saturated mineral soils of very low density. Subsidence generally results from either desiccation and shrinkage, or oxidation of organic material, or both, following drainage. Subsidence takes place gradually, usually over a period of several years. The table shows the expected initial subsidence, which usually is a result of drainage, and total subsidence, which results from a combination of factors.

Potential for frost action is the likelihood of upward or lateral expansion of the soil caused by the formation of segregated ice lenses (frost heave) and the subsequent collapse of the soil and loss of strength on thawing. Frost action occurs when moisture moves into the freezing zone of the soil. Temperature, texture, density, saturated hydraulic conductivity (Ksat), content of organic matter, and depth to the water table are the most important factors considered in evaluating the potential for frost action. It is assumed that the soil is not insulated by vegetation or snow and is not artificially drained. Silty and highly structured, clayey soils that have a high water table in winter are the most susceptible to frost action. Well drained, very gravelly, or very sandy soils are the least susceptible. Frost heave and low soil strength during thawing cause damage to pavements and other rigid structures.

Risk of corrosion pertains to potential soil-induced electrochemical or chemical action that corrodes or weakens uncoated steel or concrete. The rate of corrosion of uncoated steel is related to such factors as soil moisture, particle-size distribution, acidity, and electrical conductivity of the soil. The rate of corrosion of concrete is based mainly on the sulfate and sodium content, texture, moisture content, and acidity of the soil. Special site examination and design may be needed if the combination of factors results in a severe hazard of corrosion. The steel or concrete in installations that intersect soil boundaries or soil layers is more susceptible to corrosion than the steel or concrete in installations that are entirely within one kind of soil or within one soil layer.

For uncoated steel, the risk of corrosion, expressed as *low*, *moderate*, or *high*, is based on soil drainage class, total acidity, electrical resistivity near field capacity, and electrical conductivity of the saturation extract.

For concrete, the risk of corrosion also is expressed as *low*, *moderate*, or *high*. It is based on soil texture, acidity, and amount of sulfates in the saturation extract.

# Report—Soil Features

			Soil Fe	Soil Features-Mesa County Area, Colorado	y Area, Co	lorado			
Map symbol and		Re	Restrictive Layer		Subsi	Subsidence	Potential for frost	Risk of c	Risk of corrosion
201112	Kind	Depth to top	Thickness	Hardness	Initial	Total	action	Uncoated steel	Concrete
		Low-RV- High	Range		Low- High	Low- High			
		III	ln		и	ln			
Ba—Massadona silty clay loam, 0 to 2 percent slopes — DRAFT									
Massadona		1	1		0	1	High	High	High

# Data Source Information

Soil Survey Area: Mesa County Area, Colorado Survey Area Data: Version 8, Oct 12, 2017

# 640 White Avenue, Unit B PAGE 1 OF 1 Grand Junction, CO 81501 970-255-8005 970-255-6818 PROJECT NAME Las Colonias Business Park **CLIENT** City of Grand Junction PROJECT NUMBER 00208-0077 **PROJECT LOCATION** Grand Junction, CO **DATE STARTED** 1/15/18 **COMPLETED** 1/16/18 GROUND ELEVATION HOLE SIZE 4-Inches DRILLING CONTRACTOR S. McKracken **GROUND WATER LEVELS:** $\sqrt{2}$ AT TIME OF DRILLING 8.0 ft DRILLING METHOD Simco 2000 Truck Rig **TAT END OF DRILLING** 8.0 ft LOGGED BY CM \_\_\_\_\_ CHECKED BY MAB NOTES AFTER DRILLING \_---**ATTERBERG** FINES CONTENT (%) DRY UNIT WT. (pcf) SAMPLE TYPE NUMBER MOISTURE CONTENT (%) POCKET PEN. (tsf) LIMITS RECOVERY (RQD) BLOW COUNTS (N VALUE) GRAPHIC LOG DEPTH (ft) PLASTICITY INDEX PLASTIC LIMIT LIQUID MATERIAL DESCRIPTION Sandy Lean CLAY with Gravel (cl), brown, moist, very stiff SS 16-12-6 33 (18)5.0 Sandy GRAVEI and COBBLES (gw), brown, moist to wet, very GEOTECH BH COLUMNS 00208-0077 LAS COLONIAS.GPJ GINT US LAB.GDT 1/26/18 SS 50 32-36 SS 75 19-37 Bottom of hole at 11.0 feet.

**BORING NUMBER P-1** 

# 640 White Avenue, Unit B PAGE 1 OF 1 Grand Junction, CO 81501 970-255-8005 970-255-6818 PROJECT NAME Las Colonias Business Park **CLIENT** City of Grand Junction PROJECT LOCATION Grand Junction, CO PROJECT NUMBER 00208-0077 **DATE STARTED** 1/15/18 **COMPLETED** 1/16/18 GROUND ELEVATION HOLE SIZE 4-Inches DRILLING CONTRACTOR S. McKracken **GROUND WATER LEVELS:** $\sqrt{2}$ AT TIME OF DRILLING <u>6.5 ft</u> DRILLING METHOD Simco 2000 Truck Rig **TAT END OF DRILLING** 6.5 ft LOGGED BY CM CHECKED BY MAB NOTES Auger Refusal at 7.5-Ft AFTER DRILLING \_---**ATTERBERG** FINES CONTENT (%) DRY UNIT WT. (pcf) SAMPLE TYPE NUMBER MOISTURE CONTENT (%) POCKET PEN. (tsf) LIMITS BLOW COUNTS (N VALUE) GRAPHIC LOG RECOVERY (RQD) PLASTICITY INDEX PLASTIC LIMIT LIQUID MATERIAL DESCRIPTION Sandy Lean CLAY with Gravel (cl), brown, moist, very stiff SS 8-8-7 (15)5.0 GEOTECH BH COLUMNS 00208-0077 LAS COLONIAS.GPJ GINT US LAB.GDT 1/26/18 Sandy GRAVEL and COBBLES (gw), brown, moist to wet, very SS 23-29-156 39/0" Bottom of hole at 9.0 feet.

**BORING NUMBER P-2** 

## **BORING NUMBER P-3** 640 White Avenue, Unit B PAGE 1 OF 1 Grand Junction, CO 81501 970-255-8005 970-255-6818 PROJECT NAME Las Colonias Business Park **CLIENT** City of Grand Junction PROJECT NUMBER 00208-0077 **PROJECT LOCATION** Grand Junction, CO **DATE STARTED** 1/15/18 **COMPLETED** 1/16/18 GROUND ELEVATION HOLE SIZE 4-Inches DRILLING CONTRACTOR S. McKracken **GROUND WATER LEVELS:** DRILLING METHOD Simco 2000 Truck Rig $\sqrt{2}$ AT TIME OF DRILLING <u>5.0 ft</u> **TAT END OF DRILLING** 5.0 ft LOGGED BY CM CHECKED BY MAB NOTES AFTER DRILLING \_---**ATTERBERG** FINES CONTENT (%) DRY UNIT WT. (pcf) SAMPLE TYPE NUMBER MOISTURE CONTENT (%) POCKET PEN. (tsf) LIMITS RECOVERY (RQD) GRAPHIC LOG BLOW COUNTS (N VALUE) PLASTICITY INDEX PLASTIC LIMIT LIQUID MATERIAL DESCRIPTION Sandy Lean CLAY with Gravel (cl), brown, moist to wet, very stiff to medium stiff 2.5 SS 21-6-11 78 (17)5.0 SS 2-3-4 89 (7) Sandy GRAVEL and COBBLES (gw), brown, wet, dense SS 16-21-28 72 (49)Bottom of hole at 11.5 feet.

Huddleston-Berry Engineering & Testing, LLC

# Huddleston-Berry Engineering & Testing, LLC **BORING NUMBER P-4** 640 White Avenue, Unit B PAGE 1 OF 1 Grand Junction, CO 81501 970-255-8005 970-255-6818 PROJECT NAME Las Colonias Business Park **CLIENT** City of Grand Junction PROJECT NUMBER 00208-0077 PROJECT LOCATION Grand Junction, CO **DATE STARTED** 1/15/18 **COMPLETED** 1/16/18 GROUND ELEVATION HOLE SIZE 4-Inches DRILLING CONTRACTOR S. McKracken **GROUND WATER LEVELS:** DRILLING METHOD Simco 2000 Truck Rig $\sqrt{2}$ AT TIME OF DRILLING 8.0 ft **TAT END OF DRILLING** 8.0 ft LOGGED BY CM CHECKED BY MAB NOTES AFTER DRILLING \_---**ATTERBERG** FINES CONTENT (%) DRY UNIT WT. (pcf) MOISTURE CONTENT (%) POCKET PEN. (tsf) LIMITS SAMPLE TYPE NUMBER RECOVERY (RQD) GRAPHIC LOG BLOW COUNTS (N VALUE) PLASTICITY INDEX PLASTIC LIMIT LIQUID MATERIAL DESCRIPTION Sandy Lean CLAY with Gravel (cl), brown, moist, medium stiff 3-5-3 SS 72 (8) 5.0 GEOTECH BH COLUMNS 00208-0077 LAS COLONIAS.GPJ GINT US LAB.GDT 1/26/18 Sandy GRAVEL and COBBLES (gw), brown, moist to wet, very SS 4-26-25 56 (51)<u>10.0</u> Bottom of hole at 10.0 feet.

# **BORING NUMBER P-5** 640 White Avenue, Unit B PAGE 1 OF 1 Grand Junction, CO 81501 970-255-8005 970-255-6818 PROJECT NAME Las Colonias Business Park **CLIENT** City of Grand Junction PROJECT NUMBER 00208-0077 **PROJECT LOCATION** Grand Junction, CO **DATE STARTED** 1/15/18 **COMPLETED** 1/16/18 GROUND ELEVATION HOLE SIZE 4-Inches DRILLING CONTRACTOR S. McKracken **GROUND WATER LEVELS:** $\sqrt{2}$ AT TIME OF DRILLING <u>6.0 ft</u> DRILLING METHOD Simco 2000 Truck Rig **TAT END OF DRILLING** 6.0 ft LOGGED BY CM \_\_\_\_\_ CHECKED BY MAB NOTES AFTER DRILLING \_---**ATTERBERG** FINES CONTENT (%) SAMPLE TYPE NUMBER DRY UNIT WT. (pcf) MOISTURE CONTENT (%) POCKET PEN. (tsf) LIMITS BLOW COUNTS (N VALUE) GRAPHIC LOG RECOVERY (RQD) DEPTH (ft) PLASTICITY INDEX PLASTIC LIMIT LIQUID MATERIAL DESCRIPTION Sandy GRAVEL and COBBLES (FILL), brown, moist, very dense Sandy GRAVEL and COBBLES (gw), brown, moist to wet, very GEOTECH BH COLUMNS 00208-0077 LAS COLONIAS.GPJ GINT US LAB.GDT 1/26/18 5-27-23 SS 56 (50)SS 16-29-50/2" Bottom of hole at 11.2 feet.

# **BORING NUMBER P-6** 640 White Avenue, Unit B PAGE 1 OF 1 Grand Junction, CO 81501 970-255-8005 970-255-6818 PROJECT NAME Las Colonias Business Park CLIENT City of Grand Junction PROJECT NUMBER 00208-0077 **PROJECT LOCATION** Grand Junction, CO DATE STARTED \_1/15/18 \_\_\_\_\_ COMPLETED \_1/16/18 \_\_\_\_\_ GROUND ELEVATION \_\_\_\_\_ HOLE SIZE \_4-Inches DRILLING CONTRACTOR S. McKracken **GROUND WATER LEVELS:** DRILLING METHOD Simco 2000 Truck Rig $\sqrt{2}$ AT TIME OF DRILLING $\sqrt{7.0 \text{ ft}}$ **T** AT END OF DRILLING 7.0 ft LOGGED BY CM CHECKED BY MAB NOTES AFTER DRILLING \_---**ATTERBERG** FINES CONTENT (%) DRY UNIT WT. (pcf) SAMPLE TYPE NUMBER MOISTURE CONTENT (%) POCKET PEN. (tsf) LIMITS RECOVERY (RQD) BLOW COUNTS (N VALUE) GRAPHIC LOG DEPTH (ft) PLASTICITY INDEX PLASTIC LIMIT LIQUID MATERIAL DESCRIPTION Silty SAND (sm), br, moist, medium dense 2.5 SS 8-9-9 78 (18)Sandy GRAVEL and COBBLES (gw), brown, moist to wet, medium dense to dense SS 8-12-8 67 (20)10.0 Bottom of hole at 10.0 feet.

Huddleston-Berry Engineering & Testing, LLC

# **BORING NUMBER P-7** 640 White Avenue, Unit B PAGE 1 OF 1 Grand Junction, CO 81501 970-255-8005 970-255-6818 PROJECT NAME Las Colonias Business Park **CLIENT** City of Grand Junction PROJECT NUMBER 00208-0077 PROJECT LOCATION Grand Junction, CO **DATE STARTED** <u>1/15/18</u> **COMPLETED** <u>1/16/18</u> GROUND ELEVATION HOLE SIZE 4-Inches DRILLING CONTRACTOR S. McKracken **GROUND WATER LEVELS:** DRILLING METHOD Simco 2000 Truck Rig $\sqrt{2}$ AT TIME OF DRILLING 10.5 ft **TAT END OF DRILLING** 10.5 ft LOGGED BY CM CHECKED BY MAB NOTES AFTER DRILLING \_---**ATTERBERG** FINES CONTENT (%) DRY UNIT WT. (pcf) POCKET PEN. (tsf) MOISTURE CONTENT (%) LIMITS SAMPLE TYPE NUMBER GRAPHIC LOG RECOVERY (RQD) BLOW COUNTS (N VALUE) PLASTICITY INDEX PLASTIC LIMIT LIQUID MATERIAL DESCRIPTION Sandy Lean CLAY with Gravel and trace Cobbles (FILL), brown, moist, hard SS 15-13-27 (40)Lean CLAY with Sand (cl), brown, moist to wet, very stiff SS 6-8-15 100 (23)10.0 SS Sandy GRAVEL and COBBLES (gw), brown, wet, very dense 7-14-50/5" Bottom of hole at 12.0 feet.

Huddleston-Berry Engineering & Testing, LLC

## **BORING NUMBER P-8** 640 White Avenue, Unit B PAGE 1 OF 1 Grand Junction, CO 81501 970-255-8005 970-255-6818 PROJECT NAME Las Colonias Business Park **CLIENT** City of Grand Junction PROJECT NUMBER 00208-0077 **PROJECT LOCATION** Grand Junction, CO **DATE STARTED** 1/15/18 **COMPLETED** 1/16/18 GROUND ELEVATION HOLE SIZE 4-Inches DRILLING CONTRACTOR S. McKracken **GROUND WATER LEVELS:** DRILLING METHOD Simco 2000 Truck Rig $\sqrt{2}$ AT TIME OF DRILLING <u>5.5 ft</u> **TAT END OF DRILLING** 5.5 ft LOGGED BY CM CHECKED BY MAB NOTES AFTER DRILLING \_---**ATTERBERG** FINES CONTENT (%) DRY UNIT WT. (pcf) SAMPLE TYPE NUMBER MOISTURE CONTENT (%) POCKET PEN. (tsf) LIMITS RECOVERY (RQD) BLOW COUNTS (N VALUE) GRAPHIC LOG PLASTICITY INDEX PLASTIC LIMIT LIQUID MATERIAL DESCRIPTION Lean CLAY with Sand (CL), brown, moist, stiff \*\*\* Lab Classified SS1 SS 6-4-5 89 18 43 22 73 21 (9)Sandy GRAVEL and COBBLES (gw), brown, moist to wet, dense GEOTECH BH COLUMNS 00208-0077 LAS COLONIAS.GPJ GINT US LAB.GDT 1/26/18 SS 20-19-14 (33)Bottom of hole at 11.5 feet.

## **BORING NUMBER P-9** 640 White Avenue, Unit B PAGE 1 OF 1 Grand Junction, CO 81501 970-255-8005 970-255-6818 PROJECT NAME Las Colonias Business Park **CLIENT** City of Grand Junction PROJECT NUMBER 00208-0077 PROJECT LOCATION Grand Junction, CO **DATE STARTED** 1/15/18 **COMPLETED** 1/16/18 GROUND ELEVATION HOLE SIZE 4-Inches DRILLING CONTRACTOR S. McKracken **GROUND WATER LEVELS:** DRILLING METHOD Simco 2000 Truck Rig $\sqrt{2}$ AT TIME OF DRILLING <u>8.0 ft</u> **TAT END OF DRILLING** 8.0 ft LOGGED BY CM CHECKED BY MAB NOTES AFTER DRILLING \_---**ATTERBERG** FINES CONTENT (%) DRY UNIT WT. (pcf) SAMPLE TYPE NUMBER MOISTURE CONTENT (%) POCKET PEN. (tsf) LIMITS RECOVERY (RQD) BLOW COUNTS (N VALUE) GRAPHIC LOG PLASTICITY INDEX PLASTIC LIMIT LIQUID MATERIAL DESCRIPTION Lean CLAY with Sand and trace Gravel and Cobbles (cl), brown, moist to wet, stiff to hard SS 5-5-6 61 (11)5.0 7.5 SS 4-39-14 (53)Sandy GRAVEL and COBBLES (gw), brown, wet, dense SS 13-17-21 83 (38)Bottom of hole at 11.5 feet.

Huddleston-Berry Engineering & Testing, LLC

# Huddleston-Berry Engineering & Testing, LLC **BORING NUMBER P-10** 640 White Avenue, Unit B PAGE 1 OF 1 Grand Junction, CO 81501 970-255-8005 970-255-6818 PROJECT NAME Las Colonias Business Park **CLIENT** City of Grand Junction PROJECT NUMBER 00208-0077 PROJECT LOCATION Grand Junction, CO GROUND ELEVATION HOLE SIZE 4-Inches DRILLING CONTRACTOR S. McKracken **GROUND WATER LEVELS:** DRILLING METHOD Simco 2000 Truck Rig $\sqrt{2}$ AT TIME OF DRILLING 6.0 ft **TAT END OF DRILLING** 6.0 ft LOGGED BY CM CHECKED BY MAB NOTES Auger Refusal at 7-Ft AFTER DRILLING \_---**ATTERBERG** FINES CONTENT (%) DRY UNIT WT. (pcf) SAMPLE TYPE NUMBER MOISTURE CONTENT (%) POCKET PEN. (tsf) LIMITS RECOVERY (RQD) GRAPHIC LOG BLOW COUNTS (N VALUE) PLASTICITY INDEX PLASTIC LIMIT LIQUID MATERIAL DESCRIPTION Sandy Lean CLAY with Gravel (cl), brown, moist, very stiff \*\*\* Lab Cassified SS1 2.5 7-8-17 SS 83 40 22 55 (25)Sandy GRAVEL and COBBLES (gw), brown, moist to wet, very GEOTECH BH COLUMNS 00208-0077 LAS COLONIAS.GPJ GINT US LAB.GDT 1/26/18 SS 58 37-32 2

Bottom of hole at 8.0 feet.

#### **BORING NUMBER PL-1** 640 White Avenue, Unit B PAGE 1 OF 1 Grand Junction, CO 81501 970-255-8005 970-255-6818 PROJECT NAME Las Colonias Business Park **CLIENT** City of Grand Junction PROJECT NUMBER 00208-0077 PROJECT LOCATION Grand Junction, CO GROUND ELEVATION HOLE SIZE 4-Inches DRILLING CONTRACTOR S. McKracken **GROUND WATER LEVELS:** DRILLING METHOD Simco 2000 Truck Rig $\sqrt{2}$ AT TIME OF DRILLING 9.0 ft **TAT END OF DRILLING** 9.0 ft LOGGED BY CM CHECKED BY MAB NOTES AFTER DRILLING \_---**ATTERBERG** FINES CONTENT (%) DRY UNIT WT. (pcf) MOISTURE CONTENT (%) POCKET PEN. (tsf) LIMITS SAMPLE TYPE NUMBER GRAPHIC LOG BLOW COUNTS (N VALUE) RECOVERY (RQD) DEPTH (ft) PLASTICITY INDEX PLASTIC LIMIT LIQUID MATERIAL DESCRIPTION Granular Base Course Sandy GRAVEL (FILL), brown, moist, medium dense Sandy Lean CLAY (CL), brown, moist, very stiff \*\*\* Lab Classified SS1 2.5 SS 11-10-9 78 12 38 19 19 61 (19)5.0 Sandy GRAVEL and COBBLES (gw), brown, moist to wet, very SS 67 21-35 SS 83 12-47 Bottom of hole at 11.0 feet.

Huddleston-Berry Engineering & Testing, LLC

# **BORING NUMBER PL-2** 640 White Avenue, Unit B PAGE 1 OF 1 Grand Junction, CO 81501 970-255-8005 970-255-6818 PROJECT NAME Las Colonias Business Park **CLIENT** City of Grand Junction PROJECT NUMBER 00208-0077 PROJECT LOCATION Grand Junction, CO **DATE STARTED** <u>1/15/18</u> **COMPLETED** <u>1/16/18</u> GROUND ELEVATION HOLE SIZE 4-Inches DRILLING CONTRACTOR S. McKracken **GROUND WATER LEVELS:** $\sqrt{2}$ AT TIME OF DRILLING $\sqrt{7.0 \text{ ft}}$ DRILLING METHOD Simco 2000 Truck Rig **TAT END OF DRILLING** 7.0 ft LOGGED BY CM CHECKED BY MAB NOTES AFTER DRILLING \_---**ATTERBERG** FINES CONTENT (%) DRY UNIT WT. (pcf) SAMPLE TYPE NUMBER POCKET PEN. (tsf) MOISTURE CONTENT (%) LIMITS GRAPHIC LOG RECOVERY (RQD) BLOW COUNTS (N VALUE) PLASTICITY INDEX PLASTIC LIMIT LIQUID MATERIAL DESCRIPTION Sandy Lean CLAY (cl), brown, moist, very stiff Sandy GRAVEL (gw), brown, moist, medium dense SS 6-6-11 72 (17)Sandy Lean CLAY (cl), brown, moist to wet, very stiff 5.0 Sandy GRAVEL and COBBLES (gw), brown, wet, very dense SS 83 21-35 SS Bottom of hole at 10.5 feet.

Huddleston-Berry Engineering & Testing, LLC

GEOTECH BH COLUMNS 00208-0077 LAS COLONIAS.GPJ GINT US LAB.GDT 1/26/18

# BORING NUMBER PL-3 PAGE 1 OF 1

CLIEN	<b>IT</b> <u>Ci</u>	ty of Grand Junction	PROJECT NAME Las Colonias Business Park										
PROJ	ECT N	UMBER _00208-0077	PROJEC	T LOCAT	ION _	Grand June	ction, C	0					
DATE	STAR	TED _1/15/18	GROUNE	ELEVAT	TION _			HOLE	SIZE	4-Inc	hes		
DRILL	ING C	CONTRACTOR S. McKracken	GROUNE	WATER	LEVE	LS:							
DRILL	ING N	IETHOD Simco 2000 Truck Rig	AT	TIME OF	DRIL	LING dry							
LOGG	ED B	Y _CM CHECKED BY _MAB	AT	END OF	DRILL	.ING dry							
NOTE	<b>S</b> _Au	ger Refusal at 7-Ft	AF	TER DRII	LING								
				ш	%		j	Τ.	(9)		ERBE		ΝΤ
DEPTH (ft)	GRAPHIC LOG	MATERIAL DESCRIPTION		SAMPLE TYPE NUMBER	RECOVERY 9 (RQD)	BLOW COUNTS (N VALUE)	POCKET PEN. (tsf)	DRY UNIT WT. (pcf)	MOISTURE CONTENT (%)			PLASTICITY INDEX	FINES CONTENT (%)
0.0	ŋ			SAM	REC	ΟS	POC	DRY	CON	CIC	PLA	PLAS INI	FINES
  2.5		Sandy Lean CLAY with Gravel (CL), brown, moist, very stif											
  <u>5.0</u>		Sandy GRAVEL and COBBLES (gw), brown, moist, very de	ense	SS 1	83	6-8-9 (17)			15	37	19	18	54
 7.5		Bottom of hole at 8.0 feet.		SS 2	83	37-42							

# **BORING NUMBER PL-4** 640 White Avenue, Unit B PAGE 1 OF 1 Grand Junction, CO 81501 970-255-8005 970-255-6818 PROJECT NAME Las Colonias Business Park **CLIENT** City of Grand Junction PROJECT NUMBER 00208-0077 PROJECT LOCATION Grand Junction, CO **DATE STARTED** <u>1/15/18</u> **COMPLETED** <u>1/16/18</u> **HOLE SIZE** 4-Inches GROUND ELEVATION DRILLING CONTRACTOR S. McKracken **GROUND WATER LEVELS:** DRILLING METHOD Simco 2000 Truck Rig AT TIME OF DRILLING dry LOGGED BY CM CHECKED BY MAB AT END OF DRILLING dry NOTES Auger Refusal at 7.5-Ft AFTER DRILLING \_---**ATTERBERG** FINES CONTENT (%) SAMPLE TYPE NUMBER DRY UNIT WT. (pcf) POCKET PEN. (tsf) MOISTURE CONTENT (%) LIMITS RECOVERY (RQD) BLOW COUNTS (N VALUE) GRAPHIC LOG PLASTICITY INDEX PLASTIC LIMIT LIQUID MATERIAL DESCRIPTION Sandy Lean CLAY with Gravel (cl), brown, moist, very stiff 2.5 SS 9-8-10 33 (18)5.0 GEOTECH BH COLUMNS 00208-0077 LAS COLONIAS.GPJ GINT US LAB.GDT 1/26/18 Sandy GRAVEL and COBBLES (gw), brown, moist, very dense SS 58 21-50 2 Bottom of hole at 8.0 feet.

# BORING NUMBER PL-5 PAGE 1 OF 1

CLIEN	LIENT City of Grand Junction			PROJECT NAME Las Colonias Business Park										
PROJ	ECT N	UMBER <u>00208-0077</u>	,	PROJEC	T LOCAT	ION _	Grand June	ction, (	co					
DATE	STAR	TED <u>1/15/18</u>	COMPLETED _1/16/18	GROUNI	D ELEVA	TION _			HOLE	SIZE	<u>4-Inc</u>	ches		
DRIL	ING C	ONTRACTOR S. Mc	Kracken											
DRILI	ING M	ETHOD Simco 2000	Truck Rig	∑ AT	TIME OF	DRIL	LING <u>8.0</u>	ft						
LOGO	SED BY	CM	CHECKED BY MAB	<b>▼</b> AT	END OF	DRILL	.ING <u>8.0 f</u>	t						
NOTE	S Au	ger Refusal at 9-Ft		AF	TER DRI	LLING								
					111						AT	TERBE		누
O DEPTH (ft)	GRAPHIC LOG		MATERIAL DESCRIPTION		SAMPLE TYPE NUMBER	RECOVERY % (RQD)	BLOW COUNTS (N VALUE)	POCKET PEN. (tsf)	DRY UNIT WT. (pcf)	MOISTURE CONTENT (%)	LIQUID	PLASTIC MI LIMIT ALI	PLASTICITY INDEX	FINES CONTENT (%)
		Sandy GRAVEL a	and COBBLES (FILL), brown, moist,	very dense										
5.0	(XXX)	Silty SAND (SM) I *** Lab Classified	orown, moist, medium dense SS1		SS 1	67	9-7-8 (15)			17	NP	NP	NP	50
PJ GINI US LAB.GDI 17														
8-0077 LAS COLONIAS.GI		Sandy GRAVEL a dense	and COBBLES (gw), brown, moist to	wet, very	SS 2	53	14-17- 50/3"							
GEOTECH BH COLUMNS 00208-0077 LAS COLONIAS GINT US LAB GDT  1 2 7 7			Bottom of hole at 9.0 feet.											
GEOTE														

GEOTECH BH COLUMNS 00208-0077 LAS COLONIAS.GPJ GINT US LAB.GDT 1/26/18

# **BORING NUMBER PL-6**

PAGE 1 OF 1

CLIEN	NT Cit	y of Grand Junction P	PROJECT NAME Las Colonias Business Park										
PROJ	ECT N	UMBER <u>00208-0077</u> P	ROJEC	T LOCAT	ION _	Grand June	ction, C	0					
DATE	STAR	TED <u>1/15/18</u> COMPLETED <u>1/16/18</u> G	ROUND	ELEVAT	ION _			HOLE	SIZE	4-Inc	hes		
DRILL	ING C	ONTRACTOR S. McKracken G	ROUND	WATER	LEVE	LS:							
DRILL	ING M	ETHOD Simco 2000 Truck Rig	oxtime Z at	TIME OF	DRILI	L <b>ING</b> 9.0 f	ft						
LOGO	SED BY	CM CHECKED BY MAB	<b>▼</b> AT	END OF	DRILL	.ING <u>9.0 ft</u>	i .						
NOTE	:s		AF	TER DRII	LING								
				J.	%			Ŀ		ATT	ERBE	RG	Þ
DEPTH (ft)	GRAPHIC LOG	MATERIAL DESCRIPTION		SAMPLE TYP NUMBER	RECOVERY 9 (RQD)	BLOW COUNTS (N VALUE)	POCKET PEN. (tsf)	DRY UNIT WT (pcf)	MOISTURE CONTENT (%)	LIQUID	PLASTIC WI	PLASTICITY   INDEX	FINES CONTENT (%)
0	/////	Lean CLAY with Sand (cl), brown, moist to wet, stiff to media	um										ш
		stiff	,	SS 1	33	3-4-5 (9)							
  		<u>7</u>	,	SS 2	61	2-2-2 (4)							
		Sandy GRAVEL and COBBLES (gw), brown, wet, dense  SHALE, black, medium hard, highly weathered		SS 3	89	3-5-18 (23) 16-49							
		Bottom of hole at 16.0 feet.											

## **BORING NUMBER PL-7** 640 White Avenue, Unit B PAGE 1 OF 1 Grand Junction, CO 81501 970-255-8005 970-255-6818 PROJECT NAME Las Colonias Business Park **CLIENT** City of Grand Junction PROJECT NUMBER 00208-0077 PROJECT LOCATION Grand Junction, CO **DATE STARTED** 1/15/18 **COMPLETED** 1/16/18 GROUND ELEVATION HOLE SIZE 4-Inches DRILLING CONTRACTOR S. McKracken **GROUND WATER LEVELS:** DRILLING METHOD Simco 2000 Truck Rig $\sqrt{2}$ AT TIME OF DRILLING <u>8.0 ft</u> **TAT END OF DRILLING** 8.0 ft LOGGED BY CM CHECKED BY MAB NOTES AFTER DRILLING \_---**ATTERBERG** FINES CONTENT (%) DRY UNIT WT. (pcf) SAMPLE TYPE NUMBER MOISTURE CONTENT (%) POCKET PEN. (tsf) LIMITS GRAPHIC LOG RECOVERY (RQD) BLOW COUNTS (N VALUE) DEPTH (ft) PLASTICITY PLASTIC LIMIT LIQUID MATERIAL DESCRIPTION Lean CLAY with Sand (cl), brown, moist, stiff SS 5-5-5 61 (10)Sandy Gravel (gw), brown, moist, dense Lean CLAY with Sand (cl), brown, moist, stiff Sandy GRAVEL and COBBLES (gw), brown, moist to wet, dense SS 5-7-21 2 (28)SS 3-15-26 61 (41) Bottom of hole at 11.5 feet.

Huddleston-Berry Engineering & Testing, LLC

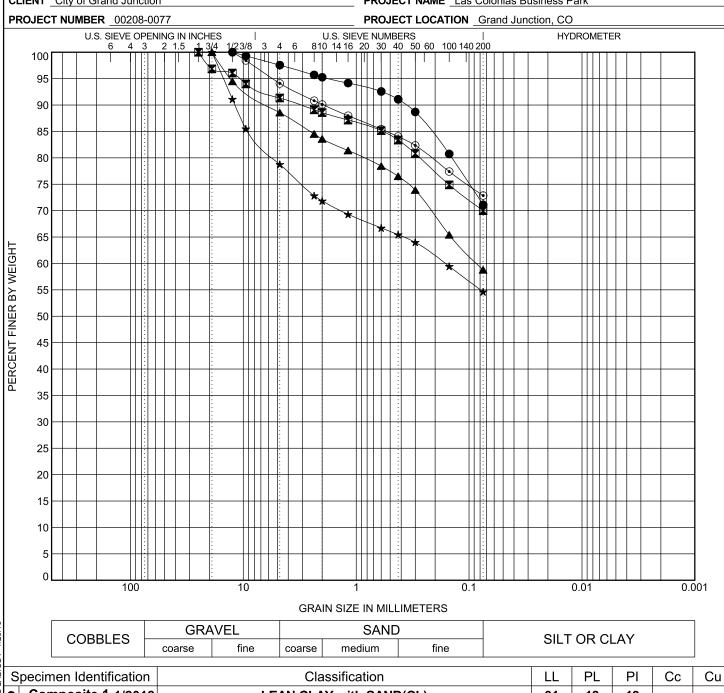
# **BORING NUMBER Deep-1** 640 White Avenue, Unit B PAGE 1 OF 1 Grand Junction, CO 81501 970-255-8005 970-255-6818 PROJECT NAME Las Colonias Business Park **CLIENT** City of Grand Junction PROJECT NUMBER 00208-0077 PROJECT LOCATION Grand Junction, CO **DATE STARTED** 1/15/18 **COMPLETED** 1/16/18 GROUND ELEVATION HOLE SIZE 4-Inches DRILLING CONTRACTOR S. McKracken **GROUND WATER LEVELS:** $\sqrt{2}$ AT TIME OF DRILLING $\sqrt{7.0 \text{ ft}}$ DRILLING METHOD Simco 2000 Truck Rig **TAT END OF DRILLING** 7.0 ft LOGGED BY CM CHECKED BY MAB NOTES Auger Refusal at 9-Ft AFTER DRILLING \_---**ATTERBERG** FINES CONTENT (%) DRY UNIT WT. (pcf) SAMPLE TYPE NUMBER POCKET PEN. (tsf) MOISTURE CONTENT (%) LIMITS GRAPHIC LOG RECOVERY (RQD) BLOW COUNTS (N VALUE) PLASTICITY PLASTIC LIMIT LIQUID MATERIAL DESCRIPTION Sandy GRAVEL and COBBLES (FILL), brown, moist, dense 2.5 Sandy Lean CLAY with Gravel (cl), brown, moist to wet, very stiff 6-10-13 SS 0 (23)5.0 GEOTECH BH COLUMNS 00208-0077 LAS COLONIAS.GPJ GINT US LAB.GDT 1/26/18 Sandy GRAVEL and COBBLES (gw), brown, wet, very dense SS 42 37-36 Bottom of hole at 9.0 feet.

#### **BORING NUMBER Deep-2** 640 White Avenue, Unit B PAGE 1 OF 1 Grand Junction, CO 81501 970-255-8005 970-255-6818 PROJECT NAME Las Colonias Business Park **CLIENT** City of Grand Junction PROJECT NUMBER 00208-0077 PROJECT LOCATION Grand Junction, CO **DATE STARTED** 1/15/18 **COMPLETED** 1/16/18 GROUND ELEVATION HOLE SIZE 4-Inches DRILLING CONTRACTOR S. McKracken **GROUND WATER LEVELS:** DRILLING METHOD Simco 2000 Truck Rig $\sqrt{2}$ AT TIME OF DRILLING <u>8.0 ft</u> **TAT END OF DRILLING** 8.0 ft LOGGED BY CM CHECKED BY MAB NOTES Auger Refusal at 10-Ft AFTER DRILLING \_---**ATTERBERG** FINES CONTENT (%) DRY UNIT WT. (pcf) SAMPLE TYPE NUMBER POCKET PEN. (tsf) MOISTURE CONTENT (%) LIMITS RECOVERY (RQD) GRAPHIC LOG BLOW COUNTS (N VALUE) PLASTICITY INDEX PLASTIC LIMIT LIQUID MATERIAL DESCRIPTION Sandy Lean CLAY (CL), brown, moist, very stiff \*\*\* Lab Classified SS1 SS 7-7-8 67 21 59 14 41 20 (15)5.0 GEOTECH BH COLUMNS 00208-0077 LAS COLONIAS.GPJ GINT US LAB.GDT 1/26/18 Sandy GRAVEL and COBBLES (gw), brown, moist to wet, dense to very dense SS 10-11-27 50 2 (38)SS Bottom of hole at 10.5 feet.

#### **GRAIN SIZE DISTRIBUTION**

**CLIENT** City of Grand Junction

PROJECT NAME Las Colonias Business Park

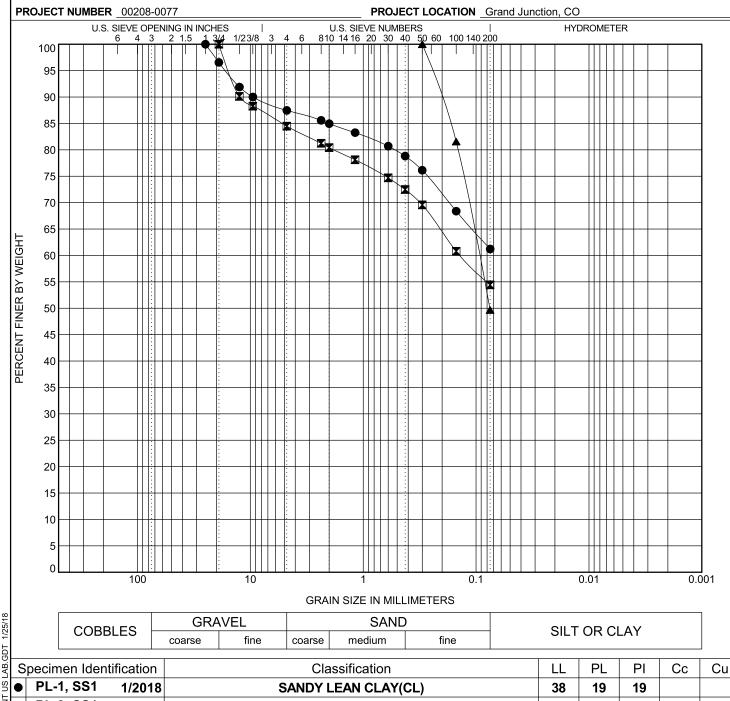


9				coarse	IIIIE	coarse	mediam	""	e					J
LAB.C	Sp	ecimen Identif	ication			Cla	ssification			LL	PL	PI	Сс	Cu
SN		Composite 1	1/2018		L	EAN CLA	Y with SANI	D(CL)		31	18	13		
GINT		Composite 2	1/2018		L	EAN CLA	Y with SANI	D(CL)		37	17	20		
GP.	<b>A</b>	Deep-2, SS1	1/2018	1		SANDY L	EAN CLAY(	CL)		41	20	21		
NIAS	*	P-10, SS1	1/2018	}	SAND	LEAN C	LAY with GF	RAVEL(C	CL)	40	18	22		
COLONIAS.	<u> </u>	P-8, SS1	1/2018	1	L	EAN CLA	Y with SANI	D(CL)		43	21	22		
LAS	Sp	ecimen Identif	ication	D100	D6	0	D30	D10	%Gravel	%Sand		%Silt	%(	Clay
7200	•	Composite 1	1/2018	12.5					2.4	26.5		7	71.1	
00208-0077		Composite 2	1/2018	25					8.7	21.3		7	70.0	
ы ы	<b>A</b>	Deep-2, SS1	1/2018	19	0.0	85			11.4	29.8			58.8	
N SIZE	*	P-10, SS1	1/2018	19	0.1	63			21.2	24.1		;	54.6	
GRAIN	•	P-8, SS1	1/2018	12.5					5.9	21.2			72.9	

#### **GRAIN SIZE DISTRIBUTION**

**CLIENT** City of Grand Junction

PROJECT NAME Las Colonias Business Park



					.A I (OL)		30	19	19	<b>I</b>
PL-3, SS1	1/2018		SANDY LEA	N CLAY wit	h GRAVEL(	CL)	37	19	18	
PL-5, SS1	1/2018		S	ILTY SAND(	SM)		NP	NP	NP	
			T	Г	Г	1				
pecimen Ident	tification	D100	D60	D30	D10	%Gravel	%Sand		%Silt	%Clay
PL-1, SS1	1/2018	25				12.5	26.2		6	1.2
PL-3, SS1	1/2018	19	0.138			15.5	30.1		5	4.4
PL-5, SS1	1/2018	0.3	0.094			0.0	50.3		4	9.7
	PL-5, SS1  Decimen Ident PL-1, SS1 PL-3, SS1	PL-5, SS1 1/2018  Decimen Identification PL-1, SS1 1/2018 PL-3, SS1 1/2018	PL-5, SS1 1/2018  Decimen Identification D100 PL-1, SS1 1/2018 25 PL-3, SS1 1/2018 19	PL-5, SS1 1/2018 S  Decimen Identification D100 D60 PL-1, SS1 1/2018 25 PL-3, SS1 1/2018 19 0.138	PL-5, SS1 1/2018 SILTY SAND(  Decimen Identification D100 D60 D30  PL-1, SS1 1/2018 25  PL-3, SS1 1/2018 19 0.138	PL-5, SS1 1/2018 SILTY SAND(SM)  Decimen Identification D100 D60 D30 D10  PL-1, SS1 1/2018 25  PL-3, SS1 1/2018 19 0.138	PL-5, SS1 1/2018 SILTY SAND(SM)  Decimen Identification D100 D60 D30 D10 %Gravel PL-1, SS1 1/2018 25 12.5 PL-3, SS1 1/2018 19 0.138 15.5	PL-5, SS1 1/2018 SILTY SAND(SM) NP  Decimen Identification D100 D60 D30 D10 %Gravel %Sand PL-1, SS1 1/2018 25 12.5 26.2 PL-3, SS1 1/2018 19 0.138 15.5 30.1	PL-5, SS1 1/2018 SILTY SAND(SM) NP NP  Decimen Identification D100 D60 D30 D10 %Gravel %Sand PL-1, SS1 1/2018 25 12.5 26.2 PL-3, SS1 1/2018 19 0.138 15.5 30.1	PL-5, SS1         1/2018         SILTY SAND(SM)         NP         NP         NP           Decimen Identification         D100         D60         D30         D10         %Gravel         %Sand         %Silt           PL-1, SS1         1/2018         25         12.5         26.2         6           PL-3, SS1         1/2018         19         0.138         15.5         30.1         5

#### ATTERBERG LIMITS' RESULTS

970-255-6818 **CLIENT** City of Grand Junction PROJECT NAME Las Colonias Business Park PROJECT NUMBER 00208-0077 PROJECT LOCATION Grand Junction, CO (CL)(CH) 50 A S T 40 Ċ 30  $\odot$ N D E X 20 10 CL-ML (ML)(MH)20 40 60 80 100 LIQUID LIMIT PI #200 Classification LL PL Specimen Identification Composite #1 1/2018 31 18 13 71 | LEAN CLAY with SAND(CL) **▼** Composite #2 1/2018 37 17 20 70 LEAN CLAY with SAND(CL) ▲ Deep 2, SS1 1/2018 41 20 21 59 SANDY LEAN CLAY(CL) ★ P-10, SS1 18 22 1/2018 40 55 SANDY LEAN CLAY with GRAVEL(CL) ⊙ P-8, SS1 1/2018 43 21 22 73 | LEAN CLAY with SAND(CL) 
 ▶
 PL-1, SS1
 1/2018 38 19 19 61 SANDY LEAN CLAY(CL) O PL-3, SS1 1/2018 37 19 18 54 SANDY LEAN CLAY with GRAVEL(CL) △ PL-5, SS1 1/2018 NP NP NP 50 | SILTY SAND(SM) GINT US LAB.GDT 00208-0077 LAS COLONIAS.GPJ ATTERBERG LIMITS

#### Huddleston-Berry Engineering & Testing, LLC MOISTURE-DENSITY RELATIONSHIP 640 White Avenue, Unit B Grand Junction, CO 81501 970-255-8005 970-255-6818 CLIENT City of Grand Junction PROJECT NAME Las Colonias Business Park PROJECT NUMBER 00208-0077 PROJECT LOCATION Grand Junction, CO 1/15/2018 Sample Date: 18-0044 Sample No.: Composite #1 Source of Material: 145 LEAN CLAY with SAND(CL) Description of Material: **ASTM D698B** Test Method: 140 **TEST RESULTS** 135 114.0 PCF Maximum Dry Density 15.0 % **Optimum Water Content** 130 **GRADATION RESULTS (% PASSING)** <u>#200</u> <u>#4</u> <u>3/4"</u> 98 100 71 125 DRY DENSITY, pcf ATTERBERG LIMITS 120 LL 31 115 Curves of 100% Saturation for Specific Gravity Equal to: 2.80 110 2.70 COMPACTION 00208-0077 LAS COLONIAS.GPJ GINT US LAB.GDT 1/25/18 2.60 105 100 95 90 10 15 20 25 <del>3</del>0 WATER CONTENT, %

#### Huddleston-Berry Engineering & Testing, LLC MOISTURE-DENSITY RELATIONSHIP 640 White Avenue, Unit B Grand Junction, CO 81501 970-255-8005 970-255-6818 CLIENT City of Grand Junction PROJECT NAME Las Colonias Business Park PROJECT NUMBER 00208-0077 PROJECT LOCATION Grand Junction, CO 1/15/2018 Sample Date: 18-0045 Sample No.: Composite #2 Source of Material: 145 LEAN CLAY with SAND(CL) Description of Material: **ASTM D698A** Test Method: 140 **TEST RESULTS** 135 115.0 PCF Maximum Dry Density 15.0 % **Optimum Water Content** 130 **GRADATION RESULTS (% PASSING)** <u>#200</u> <u>#4</u> <u>3/4"</u> 80 100 100 125 DRY DENSITY, pcf ATTERBERG LIMITS 120 LL 37 115 Curves of 100% Saturation for Specific Gravity Equal to: 2.80 110 2.70 COMPACTION 00208-0077 LAS COLONIAS.GPJ GINT US LAB.GDT 1/25/18 2.60 105 100 95 90 10 15 20 25 <del>3</del>0 WATER CONTENT, %



# CALIFORNIA BEARING RATIO ASTM D1883

Project No.: 00208-0077 **Authorized By:** Client Date: 01/15/18 01/15/18 **Project Name:** Las Colonias Business Park Sampled By: CMDate: City of Grand Junction **Submitted By:** 01/16/18 **Client Name:** CM Date: 01/25/18 Sample Number: 18-044 Location: Composite #1 Reviewed By: MAB Date:

### Compaction Method ASTM D698, Method B

**Maximum Dry Density (pcf):** 

114.0

**Opt. Moisture Content (%):** 

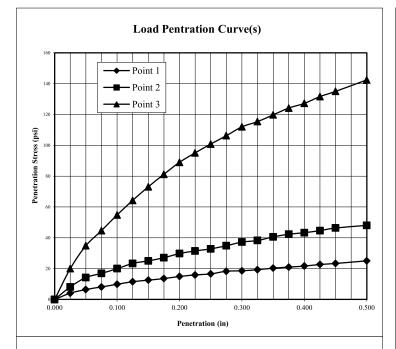
15.0

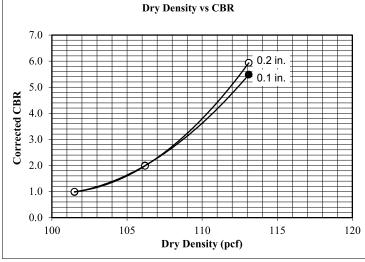
**Sample Condition:** 

Soaked

Remarks:

Method B		Sample Data					
	_	Point 1	Point 2	Point 3			
Blow	s per Compacted Lift:	15	25	56			
St	urcharge Weight (lbs):	10.0	10.0	10.0			
Dry Density Before Soak (pcf):		101.5	106.2	113.1			
Dry De	nsity After Soak (pcf):	99.9	104.6	112.2			
e +	Bottom Pre-Test	15.0	15.1	14.6			
oistur onten (%)	Top Pre-Test	15.3	14.7	14.4			
Moisture Content (%)	Top 1" After Test	27.3	23.8	20.4			
7	Average After Soak:	21.4	19.1	17.0			
Pero	cent Swell After Soak:	1.6	1.5	0.8			





			Pene	etration	Data			
	Point 1			Point 2			Point 3	
Dist.	Load	Stress	Dist.	Load	Stress	Dist.	Load	Stress
(in)	(lbs)	(psi)	(in)	(lbs)	(psi)	(in)	(lbs)	(psi)
0.000	0	0	0.000	0	0	0.000	0	0
0.025	12	4	0.025	24	8	0.025	59	20
0.050	19	6	0.050	42	14	0.050	103	35
0.075	24	8	0.075	50	17	0.075	132	45
0.100	29	10	0.100	59	20	0.100	162	55
0.125	34	12	0.125	69	23	0.125	190	64
0.150	37	13	0.150	74	25	0.150	216	73
0.175	40	14	0.175	80	27	0.175	240	81
0.200	44	15	0.200	88	30	0.200	263	89
0.225	47	16	0.225	93	31	0.225	281	95
0.250	49	17	0.250	97	33	0.250	298	101
0.275	54	18	0.275	103	35	0.275	314	106
0.300	55	19	0.300	110	37	0.300	331	112
0.325	57	19	0.325	113	38	0.325	341	115
0.350	60	20	0.350	120	41	0.350	354	120
0.375	62	21	0.375	125	42	0.375	367	124
0.400	64	22	0.400	128	43	0.400	376	127
0.425	67	23	0.425	132	45	0.425	389	132
0.450	69	23	0.450	137	46	0.450	399	135
0.500	74	25	0.500	142	48	0.500	421	142

Corrected CBR @ 0.1"								
1.0	2.0	5.5						
Corrected CBR @ 0.2"								
1.0	2.0	5.9						

Penetration Distance Correction (in)								
0.000	0.000	0.000						

Figure:

