Table of Contents

File 1987-0026 Project Name: NE corner of Wellington & Bookcliff - Final Plat & Development Plan A few items are denoted with an asterisk (*), which means they are to be scanned for permanent record on the in some instances, not all entries designated to be scanned by the department are present in the file. There are also documents specific to certain files, not found on the standard list. For this reason, a checklist has been provided. Remaining items, (not selected for scanning), will be marked present on the checklist. This index can serve as a quick e n n e guide for the contents of each file. Files denoted with (**) are to be located using the ISYS Query System. Planning Clearance will need to be typed in full, as well as other entries such as Ordinances, Resolutions, Board of Appeals, and etc. X X Table of Contents X X **Review Sheet Summary** X Application form X Review Sheets Receipts for fees paid for anything *Submittal checklist *General project report Reduced copy of final plans or drawings Reduction of assessor's map Evidence of title, deeds, easements *Mailing list to adjacent property owners Public notice cards Record of certified mail Legal description Appraisal of raw land Reduction of any maps – final copy *Final reports for drainage and soils (geotechnical reports) Other bound or non-bound reports Traffic studies X X *Petitioner's response to comments *Staff Reports *Planning Commission staff report and exhibits *City Council staff report and exhibits *Summary sheet of final conditions *Letters and correspondence dated after the date of final approval (pertaining to change in conditions or expiration date) **DOCUMENTS SPECIFIC TO THIS DEVELOPMENT FILE:** X X Action Sheet X Review Sheet Summary Certificate of Occupancy - 10/31/88 Notice of Public Hearing - 7/7/87 Development Summary - 7/8/87 Devleopment Application - 5/20/87 Certification of Plat – 1/15/86 Record of Final Plat & Plan Recording - 8/14/87 Public Notice Posting – 6/26/87 Planning Commission Minutes - ** - 7/7/87 Affidavit of Correction - 12/23/86 Request for Treasurer's Certificate of Taxes Due - 5/20/87 Warranty Deed Subsurface Soils Investigation - 12/27/78 South and West Elevation Map Site Plan Replat of Part of Lot 1 and all of Lot 2 **Utility Composite**

FS: NARRATV/DRS

May 27, 1987

NARRATIVE

FINAL PLAT AND DEVELOPMENT PLAN

TO: City of Grand Junction Planning Department

FROM: Dillon-Hunt P.C. 804 Grand Avenue

Grand Junction, Colorado 81501

SUBJECT: Final plat, development plan, vacation and revision of easement boundaries to allow proposed construction at the NE corner of Wellington Avenue and Little Bookcliff Drive.

METHOD: The following items are listed according to subject and order as indicated on the City of Grand Junction submittal legend.

GENERAL REQUIREMENTS:

Item A: Application Form: 12 copies enclosed. See Exhibit "A". A filled-out pre-application form is also included in the submittal. See Exhibit "FF".

Item B: Project Narrative:

- 1. The purpose of this submittal is to re-subdivide an existing PB partial of land in reaction to need for additional parking for an existing office building and to provide a larger building site for a proposed eye care facility, plus eliminate and restructure on-site utility easements.
- 2. Vacated Easements: Through discussions with the Land Owners, Public Service, City Planning and the Owners' Representatives, a conclusion was reached that one utility easement could be abandoned to provide a site large enough for the eye clinic and also reduce the width of an easement parallel to Little Bookcliff Drive and still provide all required utility routes for this project and the one remaining site in this partial of land.
- 3. Project Scope: The proposed building is primarily an eye care clinic with accessory use spaces for outpatient surgery and an optical shop. The building will be a

single-story structure founded on concrete footings with wood framing throughout. Exterior materials are to be masonry veneer walls, clay tile roof, metal trim, glass glazing and miscellaneous painted metal. Gross square footage is 11,000 S.F.

- 4. Traffic Analysis: Maximum traffic to and from the site will be approximately 40 cars per hour. Staff and patient parking have been divided to reduce possible conflict. On-site patient traffic flow is one-way (enter on south and exit on west) with a patient/handicap pick-up area at the front door. This occupancy use will impact the existing local street system minimally compared to other possible uses.
- 5. Signage: A single 4' x 8' free-standing sign will be placed in the landscaped area at the south property. One lighted sign on the building will be used. This sign is to be raised letters lighted with a ground spot.
- 6. Lighting Schedule: Wall-pack lighting will be used around the perimeter of the building for security and safety. The patient parking lot will have two free-standing light poles.
- 7. Project Schedule: Complete bid documents by July 1, 1987, start construction August 1, 1987, and complete construction February 1, 1988.

Item C: Summary Form: Does not apply.

Item D: Appraisal of Application For Open Space: Does not apply.

Item E: Evidence of Title: See Exhibit "E".

Item F: Draft of Covenants/Restrictions: None in effect.

Item G: Legal Description: See enclosed Exhibit "G".

Item H: Names and Addresses of Adjacent Property: See enclosed Exhibit "H".

Item I: Flood Plan Analysis: Does not apply.

Item J & L: Geology Report/Soils Report, Subsurface Soils
Investigation: See Exhibit "N" - Lincoln DeVore Job No.
25215.

Item K: Gamma Radiation Report: No formal report is planned at this time. Reports shall be obtained prior to any actual construction.

Item M: Improvements Agreement: Does not apply.

Item N: Improvements Guarantee: Does not apply.

Item 0: Development Schedule: See Item B - Project
Narrative, No. 7.

Item P: See enclosed Exhibit "P", which indicates boundary, easements and acreage for the combination of lots.

Item Q: Site Plan: (24" x 32" site plan and 24" x 32"
elevation plan) See Exhibits "Q" and "Z".

Item R: Adjacent Land Use and Zoning: Current City of Grand Junction zoning information indicates the subject site to be surrounded by PB, B-1, RMF-64, RSF-8. Also see Site Plan.

Item S: Drainage/Grading Plan: See Exhibit "Q".

Item T: Utilities Composite: See Exhibit "T".

Item U: Landscaping/Screening/Buffering: See Site Plan, Exhibit "Q".

Item V: Parking: See Site Plan, Exhibit "Q".

Item W: Roadway Plan/Profile: Does not apply.

Item X: Traffic Circulation Patterns: See Narrative and Exhibit "Q".

Item Y: Traffic Analysis: See Narrative.

Item Z: Structural Information: See Exhibit "Q" (Site Plan) and Exhibit "Z" (Exterior Elevations). Lighting, signage and building systems addressed in narrative Item B.

Item AA: Location and Vicinity Map: See Exhibit "AA".

Item BB: Assessor's Map with Subject Property Outlined in Red: See Exhibit "BB".

Item CC: Reduction of Assessor's Map: See Exhibit "AA".

Item DD: Reduction of Plan: See Exhibit "DD".

Item EE: Reduction of Plat: See Exhibit "EE".

Item FF: Action Sheet: See Exhibit "FF".

Item GG: County Treasurer Tax Certification: See Exhibit "GG".

2945-111-25-005
F & S Investments
P.O. Box 3025
Grand Junction, Colo. 81502

2945-111-00-946 City of Grand Junction 250 N. 5th Street Grand Junction, Colo. 81501

Jim Patty Rolland Engineering 844 Grand Ave. Grand Junction, CO 81501

2945-111-25-009 Corbett/Fine Investments 1120 Wellington Ave, Suite 105 Grand Junction, Colo. 81501 2945-111-00-010
Don H. Hutchison
2709 Midway
Grand Junction, Colo. 81501

2945-111-25-008

David P. Noffsinger
1120 Wellington Ave, Suite 104
Grand Junction, Colo. 81501

2945-111-00-009
Ronald E. Ryan
1101 Patterson Road
Grand Junction, Colo. 81501

2945-111-25-007 Carl A. Lepisto P.O. Box 3025 Grand Junction, Colo. 81502

2945-111-20-005 Health Services, Inc. P.O. Box 40 Glenwood Springs, CO 81602

2945-111-25-006
Gregg K. Omura
P.O. Box 3025
Grand Junction, Colo. 81502

2945-111-02-951
Bishop of Pueblo
1001 N. Grand Avenue
Pueblo. Colorado 81003

2945-111-25-003
Western Colorado Surgery
Center Association
P.O. Box 2919
Grand Junction, Colo. 81502

2945-111-16-005
Wellington V
2754 Compass Drive
P.O. Box 2026
Grand Junction, CO 81502

2945-111-21-002 Stella M. Shanks 2606 Kelly Drive Grand Junction, Colo. 81506

2945-111-27-006 Village Fair P.O. Box 518 Grand Junction, Colo. 81502

2945-111-21-001
Glenn Ross Kempers
1001 Wellington Avenue
Grand Junction, Colo. 81501

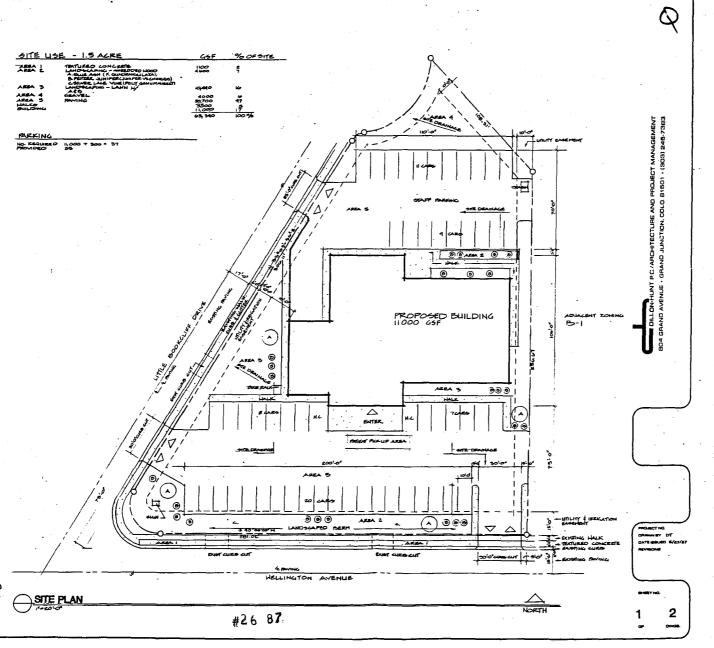
SSM Investments 735 Bookcliff Ave. Grand Junction, CO 81501

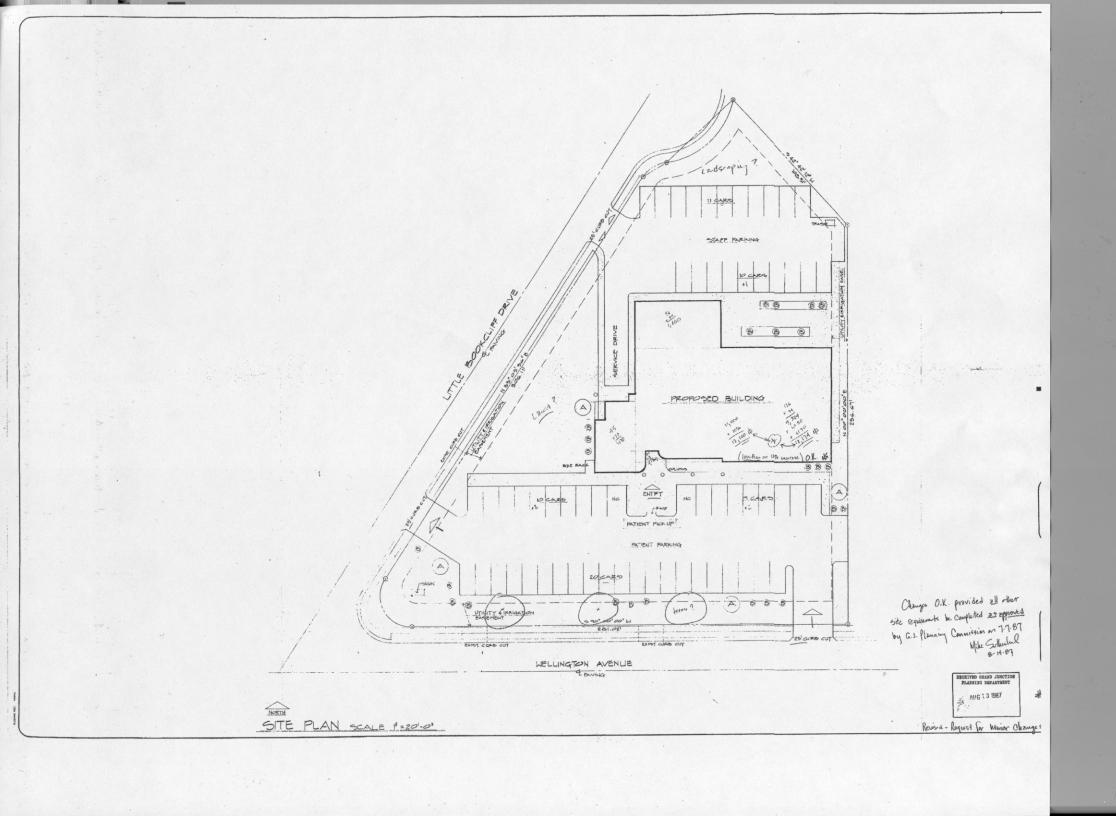
2945-111-00-973
Colorado West Senior
Citizens, Inc.
1000 West Temple St.
Los Angeles, Calif. 90074

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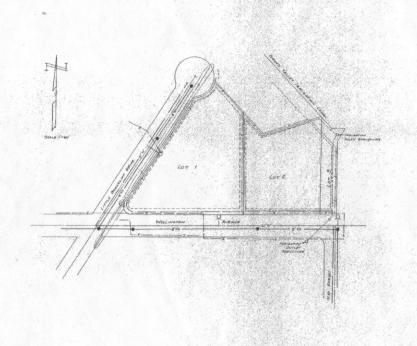
Duncan & Campbell Investments 790 Wellington Ave. Grand Junction, CO 81501

2945-111-16-974 Bethepda Care Center 1955 N. Union Blvd. Colorado Springe, CO 80909





REPLAT OF PART OF LOT I, ALL OF LOT 2 LITTLE BOOKCLIFF SUBDIVISION CITY OF GRAND JUNCTION REPLAT OF PART OF LOT I, ALL OF LOT 2 LITTLE BOOKCLIFF SUBDIVISION CITY OF GRAND JUNCTION Original
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City of Grand Junction

Public Service Company of Colorade

Mountain Ball

The above signatures are for approval of the Ukility Composite.

LEGEND

SANITARY SEWER - EXISTING POMERIC WATER - EXISTING C FIRE HVDRANT - EXISTING 30" DRAIN LINE - EXISTING

ELECTRIC -----I MRIGATION TOLEPHONE

Jun 05 1987



REPLAT OF PART OF LOT 2. LITTLE BOOKQLIFF SUBDIVISION CITY OF GRAND JUNCTION

ROLLAND ENGINEERING 844 Grand Avenue UTILITY COMPOSITE

es AUE



Lincoln DeVore

1000 West Fillmore St. Colorado Springs, Colorado 80907 (303) 632-3593 Home Office

December 27, 1978

C. E. Maquire 760 Horizon Drive Grand Junction, CO 81501

Re:

SUBSURFACE SOILS INVESTIGATION

CAPITOL HILL SUBDIVISION

GRAND JUNCTION, COLORADO

Gentlemen:

Transmitted herewith is the report concerning a subsurface soils investigation for the proposed Capitol Hill Subdivision to be located in Grand Junction, Colorado.

Respectfully submitted,

LINCOLN-DeVORE

George D. Morris, P.E.

GDM/cm

LD Job No. 25215

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ABSTRACT:

The contents of this report are a subsurface soils investigation and foundation recommendation for the proposed Capitol Hill Subdivision which is located in the northern portion of the city of Grand Junction, Colorado. The Laboratory has not at this time seen a set of construction drawings for the structures proposed for this development.

After consideration of the investigation and testing program described herein, it is our recommendation that shallow foundation systems, consisting of continuous foundations beneath bearing walls and isolated spread footings beneath columns and other points of concentrated load, be used to carry the weight of the proposed structures. Foundation systems located a minimum of 3 feet below the present ground surface may be proportioned on the basis of a maximum allowable bearing capacity of 1600 psf as an overall site average. A minimum deadload pressure of 500 psf should be maintained at all times, also as an oversite average. It was noted that the maximum bearing value varies from 800 psf to 1800 psf while the minimum pressure varied from zero to 900 psf. Precise values should not be taken for design until the specific building site is inspected.

It is recommended that the proposed structures be well balanced and heavily reinforced.

Contact stresses beneath exterior load bearing walls should be balanced to within ± 500 psf around the entire structure.

Isolated interior column footings should be designed for contact pressures of about 200 psf greater than the average of those selected for the exterior walls. The criteria for this building balance will depend upon the nature of the structure. Single-story, slab on grade structures may be balanced on the basis of dead load only. Multi-story structures or structures with basements should be balanced on the basis of dead load plus approximately one-half the live load.

All stem walls for continuous foundations should be designed as grade beams capable of spanning at least 12 feet. Heavy structures, if any, may require special raft foundations to properly spread the load. As an alternate, driven piles could be used as a foundation.

The upper soils on this site can be expected to experience significant loss of strength upon saturation. For this reason, adequate drainage must be provided at all times. Water should never be allowed to pond above the foundation materials. Landscape irrigation in the vicinity of the structures should be kept to an absolute minimum.

Floor slabs should be free to act independently of structural members of the building.

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These slabs should contain deep construction or contraction joints to facilitate even breakage. This will keep to a minimum any unsightly cracking which could be caused by differential movement.

More detailed recommendations can be found within the body of this report. All recommendations are subject to the limitations set forth herein.

GENERAL:

The purpose of this investigation was to determine the general suitability of the site for construction of a series of light weight apartment structures. Characteristics of the individual soils found in the test borings were examined for use in designing foundations for these structures.

The proposed construction site is located in the northern portion of the city of Grand Junction, Colorado. The site is a short distance to the southwest of the intersection of 27 Road and Patterson Road. This location is in the NE 1/4 of Section 11, Township 1 South, Range 1 West of the Ute Principal Meridian. This location is shown on the enclosed Site Location Map.

The topography in the vicinity of the site is relatively flat, being located on an alluvial

plain of the Colorado River. The site has a slight gradient to the southwest towards the river. The unlined Grand Valley Canal is located along the northerly boundary of the site. The exact direction of surface runoff on the site will be variable due to the influence of streets and buildings in this vicinity. In general, however, surface runoff will travel to the south and west, eventually entering the Colorado River. Surface and subsurface drainage can be characterized as fair to poor.

alluvial in nature, having been deposited on the site by the action of the Colorado River in the past. The soil profile was found to consist of a layer of alluvial silt and clay approximately 60 feet in thickness overlying an alluvial terrace consisting mainly of gravel and cobble sized particles. The silt and clay layer tends to be somewhat dry and desiccated near the ground surface, but with increasing depth, becomes wetter and softer. The desiccated, upper silts and clays can be expected to form the primary foundation material for shallow foundations placed on this site. It should be pointed out, however, that these upper, drier silts and clays can be expected to experience a considerable loss of strength with increasing moisture, and that the density of the upper materials varies considerably over the site. For this reason,

it is important that proper drainage be maintained over the site. All of the alluvial materials on this site have been deposited on dense, formational material of the Mancos Shale formation. The Mancos Shale can be considered as bedrock beneath this site.

The Mancos Shale can broadly be described as a thinly bedded, drab, light to dark grey marine shale with thinly interbedded, fine-grained sandstone and limestone. Some layers of the Shale contain a high proportion of bentonite and, therefore, are highly expansive. The majority of the Shale, however, has only a moderate expansion potential. No formational material was encountered in any of the test borings placed on this site. The Shale exists beneath this site at depths sufficient to insure that formational material will not affect construction or performance of the proposed foundation systems.

BORINGS, LABORATORY TESTS & RESULTS:

on this site, as is indicated on the enclosed Test Boring

Location Diagram. These test borings were placed in such a

manner as to obtain a reasonably good profile of the subsurface

soils beneath the site. Test Borings 1 and 6 were drilled

to 45 and 60 foot depths in an attempt to find the depth to

shale or to the underlying gravel terrace materials. None was found to a depth of 60 feet. Some variations in the soil profile were noted from point to point, but in general, the soil profile was sufficiently uniform that no further test borings were deemed necessary. All test borings were advanced with a power driven, continuous auger drill. Samples were taken with the California sampler, thin walled tubes, and by bulk methods.

The subsurface profile encountered during our field exploration program can broadly be described as a two-layer system. The upper layer of this system, which was encountered very near the ground surface generally consists of a dry, medium density clay and silt crust. This will be the supporting soil for most of the foundations on the site. The second layer of the soil profile consists of the same types of silts and clays, but in a much higher moisture condition. This material, which was deposited by the action of the Colorado River in the past, was generally low density, of a light brown to tan color and was noted to be stratified with numerous sand layers and occasional scattered gravel. Below this silt and clay layer, at a depth of over 60 feet below the ground surface, a layer of dense alluvial gravel and cobbles, should be found, which represent an old terrace of the Colorado River. Under this, the Mancos

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Shale forms the bedrock.

The samples obtained during our field exploration program have been grouped into four soil types. These materials are representative of the basic clays and of the silts and silty sand lenses within the soil profile. The clay of Soil Type No. 3 will be the primary foundation soil, but some foundations will rest on the silts and silty sands. More precise engineering characteristics of the soil types are given on the enclosed Summary Sheets. The following discussion will be general in nature.

soil Type No. 1 classified as a silt (ML) of fine grain size. Generally, this material is of low plasticity, of low permeability and was encountered in a low density condition. It will have a minor tendency to expand upon the addition of moisture, with expansion pressures on the order of 500 psf being measured on drier samples. In the high moisture condition in which is was generally encountered, these silts will have a great tendency to consolidate upon application of load. Soil Type No. 1 will have a distinct tendency to experience loss of strength upon saturation. For this reason, proper drainage is considered very important on this site. Additionally, proper balancing and reinforcing of foundation components is considered important, since this will help the structure

maintain its integrity if localized strength loss occurs in relatively small isolated areas of the foundation soils. Foundations which rest at least 2 feet below the present ground surface may be proportioned on the basis of a maximum allowable bearing capacity of 800 psf. A minimum dead load pressure of 500 psf should be maintained at all times. Soil Type No. 1 was found to contain sulfates in detrimental quantities.

Soil Type No. 2 is a very fine grained silty sand found primarily in borings 6 and 8.

This material is of low plasticity, is permeable and generally of low to medium density. This material has no tendency to expand upon the addition of moisture and only a minor tendency to true consolidation. This soil is generally found in relatively thin layers, however, and the foundations will be affected by the basic clays and silts. Within the upper 10 feet of the soil profile, the maximum allowable bearing value of this material can be taken as 1600 psf with no minimum load required if the sand extends at least 3 feet below foundation level. This soil type contains mildly detrimental quantities of sulfates.

Soil Type No. 3 is a lean clay and is the predominant soil type under the site. This soil is plastic, of low permeability and of quite variable

level. This soil type contains only minor amounts of sulfates.

most of the test borings between 9 1/2 and 16 feet below ground surface at the time drilled. At this depth, free water could interfere with basement foundations. Due to the presence of this water and to low density at greater depth, basements cannot be recommended over most of the site.

This water table is probably subject to seasonal fluctuation and it is also possible that seepage may be encountered from the unlined Grand Valley Canal which lies north of this site.

CONCLUSIONS & RECOMMENDATIONS:

Since the magnitude and nature of the foundation loads for the proposed structures are not precisely known to the Laboratory at this time, the recommendations contained herein must be quite general in nature.

Any special loads or unusual design conditions should be reported to the Laboratory so that changes in recommendations may be made, if necessary. We understand that the structures on the site will be two-story multi-family structures, some single-family residences and perhaps a commercial type "professional building". Basements are not planned. Based upon our analysis of the soil conditions and project characteristics previously outlined, the following recommendations are made.

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It is recommended that shallow

foundation systems, consisting of continuous foundations beneath load bearing walls and isolated spread footings beneath columns and other points of concentrated load, be used to carry the weight of the proposed structures. Foundations which extend less than 6 feet below the present ground surface may be proportioned on the basis of a maximum allowable bearing capacity of 1800 psf over most of the site. A minimum dead load pressure of 900 psf should be maintained at all times above the 6 foot level. It should be noted that the term "spread footings" can be applied to the wall on grade foundation type for lightweight structures.

In order to minimize the possibility for differential movement, it is recommended that the foundation system be well balanced. Structures such as these are usually more heavily loaded on some walls and columns than on others. The amount of variation in this load can be quite high. Balancing can be achieved by placing larger footings beneath heavier loads and smaller footings beneath lighter loads in such a manner that the stress on the soil is approximately the same at all points. The criteria for balancing will depend somewhat upon the nature of the structure. Single-story, slab on grade structures may be balanced on the basis of dead load only. Multi-story

on the basis of dead load plus approximately one-half the live load. Using whichever criteria is applicable, the contact stresses beneath exterior foundation walls should be balanced to within ± 300 psf at all points. Isolated interior column footings should be designed for unit stresses of about 200 psf greater than the average selected for the exterior walls.

Stem walls for continuous foundations should be designed as grade beams capable of spanning at least 12 feet. The horizontal reinforcement required for this design should be placed continuously around the building with no gaps or breaks in the reinforcing steel, unless they are specially designed. Stem walls should be reinforced at both top and bottom with the majority of the reinforcing being located at the bottom of the beam. Where stem walls will retain soil in excess of 4 feet in height, vertical reinforcing may be necessary and should be designed. To design such vertical reinforcing, the equivalent fluid pressure of the soil may be taken as about 45 pcf in the active state. Due to the moisture content of the soil below a depth of 6 feet and the lower density found at this level, full basements will be difficult to design and construct. Full basements are therefore not recommended on the site.

Where floor slabs are to be used, they may be placed directly on grade or over a compacted gravel blanket of 4 to 6 inches in thickness. If the gravel bed is chosen, however, it must be provided with a free drainage outlet to the surface and must not be allowed to act as a water trap beneath the floor slab. A vapor barrier is recommended beneath all floor slabs placed on this site. Floor slabs should be constructed in such a manner that they act independently of columns and bearing walls. Additionally, concrete floor slabs should be placed in sections no greater than 25 feet on a side. Deep construction or contraction joints should be placed at these lines to facilitate even breakage. This will help reduce unsightly cracking which could be caused by differential movement. Adequate drainage must be provided in the foundation area, both during and after construction, to prevent the ponding of water. The ground surface around the building should be graded such that surface water will be carried quickly away from the structure. Minimum gradient within 10 feet of the structure will depend upon surface landscaping. Bare or paved areas should have a minimum gradient of 2%, while landscaped areas should have a minimum gradient of 7%. Roof drains, if used, should be Original Do NOT Remove #26 87 From Office -13carried across all backfilled areas and discharged well away from the structure. The amount of landscape irrigation in the immediate vicinity of the structures should be kept to an absolute minimum. Since the foundation soils can be expected to experience a loss of strength upon saturation, drainage recommendations are considered very important.

structure and in utility trenches leading to the structure should be compacted to at least 90% of the maximum Proctor dry density, ASTM D-698. The native soils on the site may be used for this purpose. Material should be placed in lifts not to exceed 6 inches compacted thickness and at a moisture content approximately equal to the Proctor optimum moisture content ± 2%. Backfill should be compacted to the required density by mechanical means. No water flooding techniques of any type should be used in the placement of fill on this site. Since proper placement of backfill will aid in the rapidity of runoff and help prevent surface water from reaching the foundation area, backfill recommendations are considered important. If proper drainage cannot be provided by grading, peripheral drains are recommended.

Any topsoil or debris should be removed from the construction area prior to the beginning of construction of foundations. In addition, should any

pockets of debris, organic material, or unusually loose material be encountered during excavation for footings, this material should be removed and replaced with backfill compacted to 95% of the maximum Proctor dry density, ASTM D-698.

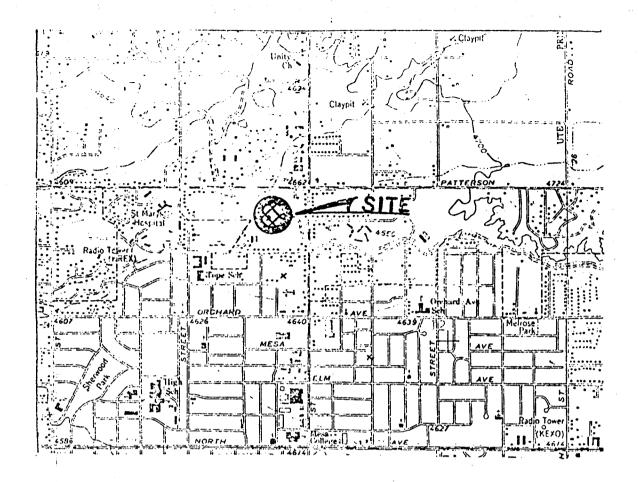
should be inspected prior to the construction of forms or placement of concrete to establish that proper design bearing material has been reached and that no debris, soft spots, or other unsuitable materials are located in the foundation area.

The silt and clay soils on this site were found to contain sulfates in detrimental quantities. For this reason, a sulfate-resistant cement such as Type II Modified Cement is recommended for use in all concrete which will be in contact with the foundation soils. Under no circumstances should calcium chloride ever be added to a Type II Cement. In the event that Type II Cement is difficult to obtain, a Type I Cement may be used, providing the concrete is separated from the soils by water-resistant membranes.

Heavy structures which cannot be designed for the relatively light allowable bearing values will require special foundations. A raft type structural slab foundation or a driven pile and grade beam foundation could be used. The choice of foundation should be made depending on the type of building and load configuration.

Special foundations of this type will not be described here, but recommendations for these foundation types can be made in a short time if it becomes necessary to use them.

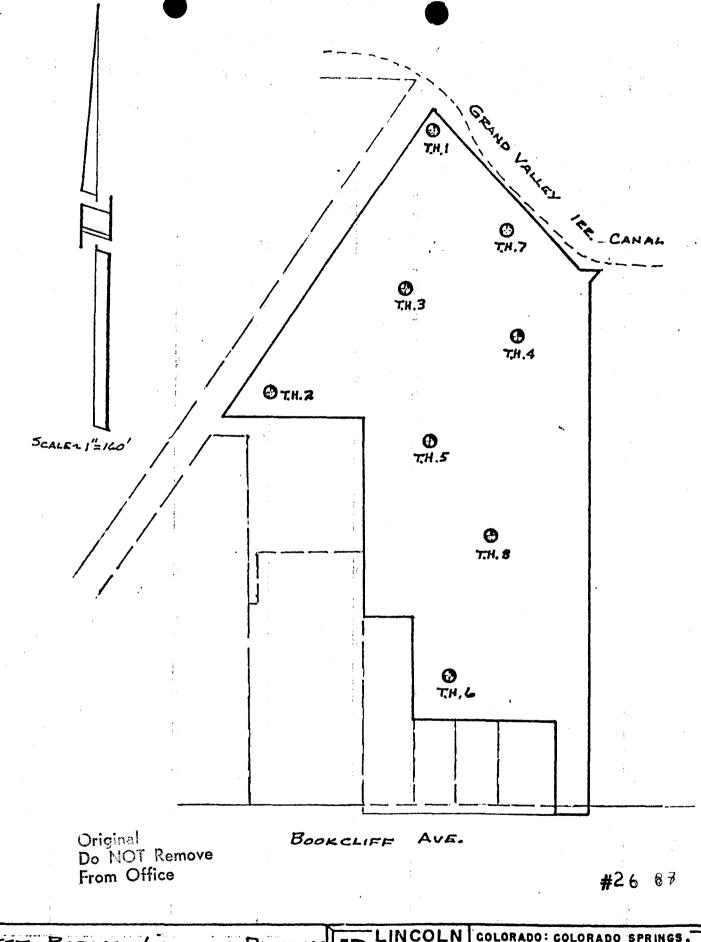
It is believed that all pertinent points concerning the subsurface soils on this site have been covered in this report. If soil types and conditions other than those described herein are noted during construction on the site, these should be reported to the Laboratory so that changes in recommendations may be made, if necessary. If questions arise or further information is required, please feel free to contact the Laboratory.



SCALE 1"=2000'

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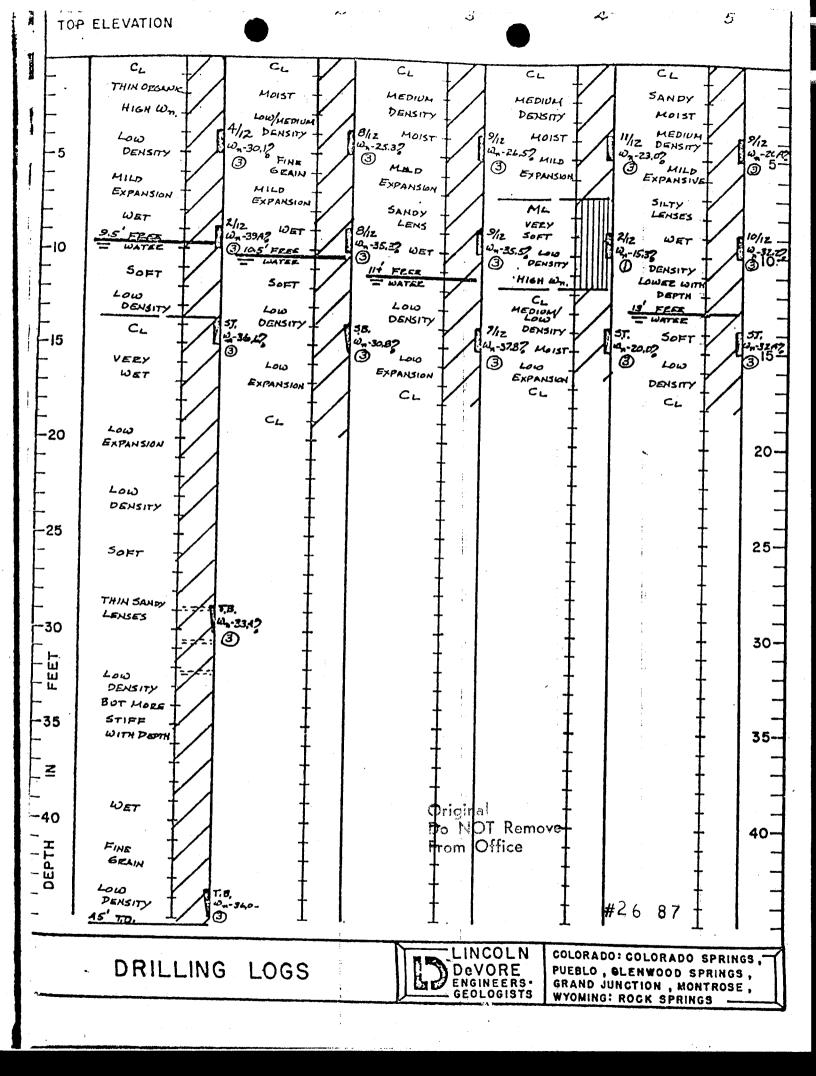


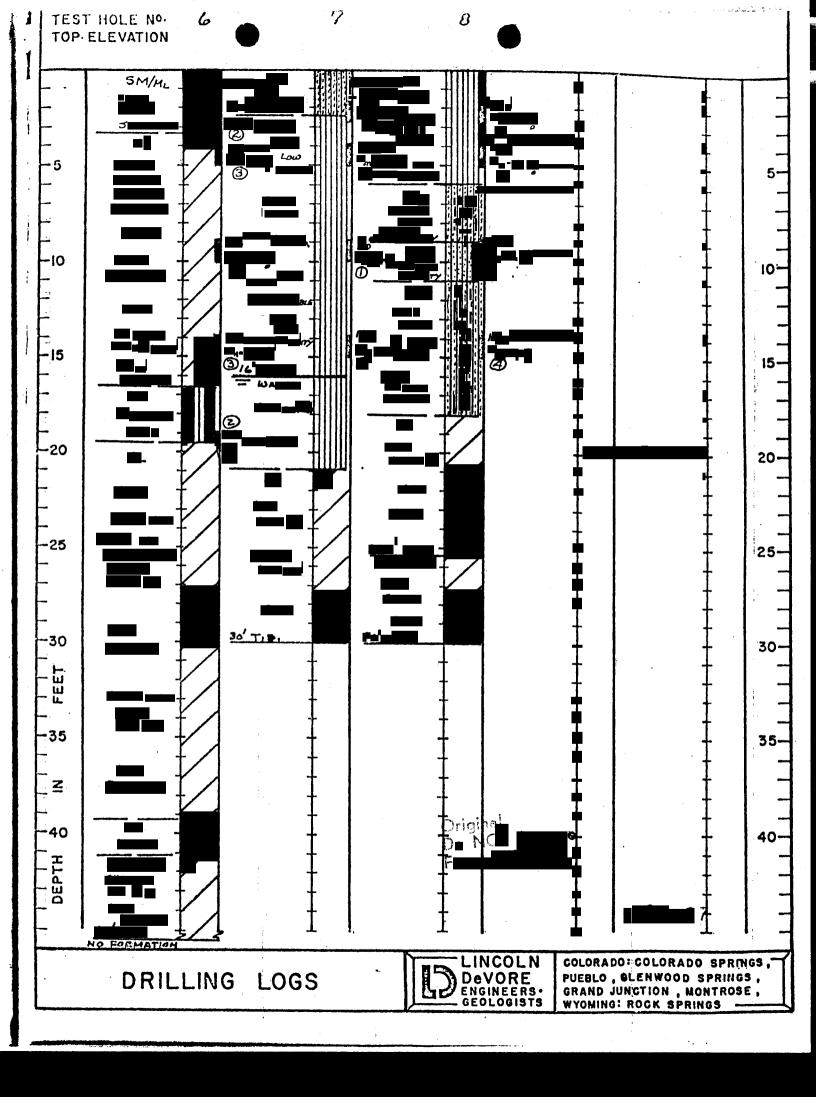
TEST BORING LOCATION DIAGRAM
CAPITOL HILL SUBDIV. GRAND JONITION



Devore ENGINEERS COLORADO: COLORADO SPRINGS, PUEBLO, GLENWOOD SPRINGS, GRAND JUNCTION, MONTROSE, WYOMING: ROCK SPRINGS

| SOILS | DESC <u>uscs</u> | RIPTIONS: DESCRIPTION | ROCK SYMBOL | DESCRIPTIONS: | SYMB! | OLS & NOTES: |
|--------------|---------------------|---|---------------------------------------|---------------------------------------|--------------------|---|
| SYMBOL | 0262 | | | DIMENTARY HOCKS CONGLOMERATE | 21111105 | Protein 1141 |
| 22 | | Topsoil -Man-made Fill | Ø. 65 | SANDSTONE | £ | 9/12 Standard penetration drive Numbers indicate 9 blows to drive |
| 0000 | | -Man made ini | | SAMDSTONE | | the spoon 12" into ground. |
| 00000 | GW | Well-graded Gravel | | SILTSTONE | Z | ST 2-1/2" Shelby thin wall sample |
| 0000 | GP | Poorly-graded Gravel | | SHALE | 1 | |
| 9 9 9 | GM | Silty Gravel | XXX | CLAYSTONE | | W _o Natural Moisture Content |
| 000 | GC | Clayey Gravel | | COAL | F | W _X Weathered Material |
| | SW | Well-graded Sand | 盅 | LIMESTONE | Vwater | Free water table |
| | SP | Poorly-graded Sand | 岩 | DOLOMITE | | Yo Natural dry density |
| | SM | Silty Sand | | MARLSTONE | | T.B. — Disturbed Bulk Sample |
| | sc | Clayey Sand | | GYPSUM | | ② Soil type related to samples |
| ШЩ | ML | Low-plasticity Silt | | Other Sedimentory Rocks | | in report |
| | CL | Low-plasticity Clay | 1777 | GRANITIC ROCKS | 15' W _X | Top of formation |
| | OL | Low-plasticity Organic Silt and Clay | +++++++++ | DIORITIC ROCKS | | Test Boring Location |
| | МН | High-plasticity Silt | 11 / 11 | GABBRO | | ▼ Test Pit Location |
| لوقو | СН | High-plasticity Clay | | RHYOLITE | | Seismic or Resistivity Station. |
| Z=Z -Z- | ОН | High-plasticity Organic Clay | # # # # # # # # # # # # # # # # # # # | ANDESITE | - | Lineation indicates approx. length a orientation of spread |
| HALL LLLL | Pt | Peat | | BASALT | | (S = Seismic , R=Resistivity) |
| | GW/GM | Well-graded Gravel, Silty | 444 | TUFF & ASH FLOWS | by dr | dard Penetration Drives are made riving a standard 1.4" split spoon |
| 0000 | GW/GC | Well-graded Gravel, Clayey | 000 | BRECCIA & Other Volcanics | 140 [| pler into the ground by dropping a D. weight 30". ASTM test D-1586. |
| 00000 | GP/GM | Poorly-graded Gravel, Silty | -2 54 1962 V W | Other Igneous Rocks | Sam | ples may be bulk , standard split on (both disturbed) or 2-½°1.D. |
| 0000 | GP/GC | Poorly-graded Gravel, Clayey | | GNEISS | thin | wall ("undisturbed") Shelby tube ples. See log for type. |
| | GM/GC | Silty Gravel, Clayey | | SCHIST | The I | boring logs show subsurface conditions address and locations shown, and it is |
| | GC/GM | Clayey Gravel, Silty | | PHYLLITE | not w | varranted that they are representative bsurface conditions at other locations |
| | SW/SM | Well – graded Sand, Silty | | SLATE | ondit | imes. |
| | sw/sc | Well-graded Sand, Clayey | 1/2 | METAQUARTZITE | Origin | al |
| | SP/SM | Poorly-graded Sand, Silty | 000 | MARBLE | DO VI | OT Remove |
| | SP/SC | Poorly-graded Sand, Clayey | 11/1 | HORNFELS | - mass 2 , 3 | ≺™ce |
| | SM/SC | | 25 26 36 3 26 26 3 26 26 | SERPENTINE | 1 1 | #26 87 |
| | -SC/SM | Clayey Sand, Silty | 1553 | Other Metamorphic Rocks | | |
| | CL/ML | Silty Clay | DEVORE TESTING LABORATORY | Glenwood Springs, Montrose, Gunnison, | EXPLAN AND | IATION OF BOREHOLE LOGS LOCATION DIAGRAMS |

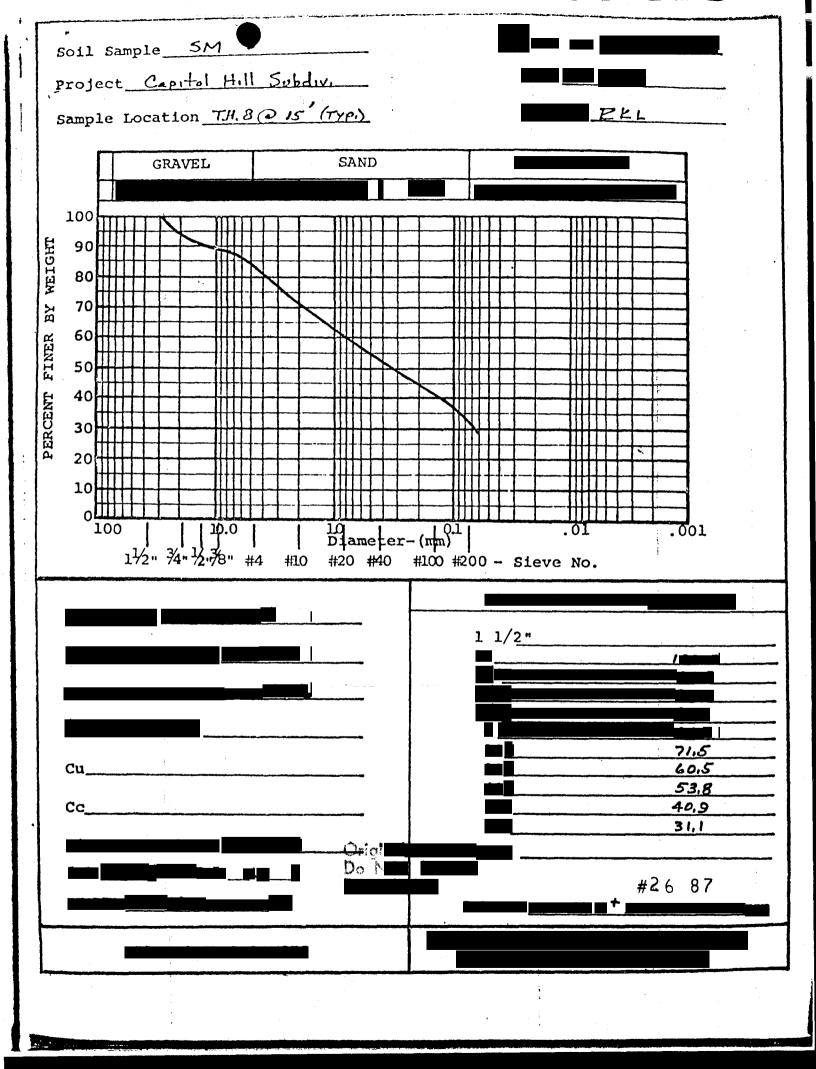




| Test No. 25215 Somple ML Subdiv. Date 12/3/28 Test No. 25215 Date 12/3/28 Test by KL Test by Test by | SUMMARY | YSHIET |
|---|---|-------------------------------------|
| Date 12/3/28 Date 12/3/28 Test by KL | Soil Sample ML | Test 140. 25215 |
| Natural Water Content (w) 22.2 % Specific Gravity (Gs) 2.22 In Place Density (Fo) 109.7 pcf | | Date 12/3/28 |
| Natural Water Content (w) 22.2 % Specific Gravity (Gs) 2.22 In Place Density (Fo) 109.7 pcf | Boring No. 7 Depth 5' (Tye) | Toolby |
| Specific Gravity (Gs) | Sample No. | lesi by |
| Sieve No. % Passing Plastic Limit P.L. 17.3 % 1/2" | Natural Water Content (w) <u>22.2</u> % Specific Gravity (Gs) <u>2.72</u> | In Place Density (50) 109,7 pcf |
| Liquid Limit L. L. 20.2 % Plasticity Index P.1. 2.9 % Shrunkage Limit 12.8 % Flow Index 1/2" | SIEVE ANALYSIS: | |
| 1 2 1 2 2 3 5 5 5 5 5 5 5 5 5 | Sieve No. % Passing | Plastic Limit P.L. 17.3 % |
| 1 | | Liquid Limit L. L. 20.2 % |
| 1/2" | 11/2" | Flasticity Index P.1. 2.9 % |
| 10 | 3/4" | Shrinkage Limit 17:8 % |
| 10 | 1/2" /00,0 | Shrinkage Ratio |
| 20 | 499.4 | Volumetric Change % |
| 20 | 1092.2 | Lineal Shrinkage % |
| MOISTURE DENSITY: ASTM METHOD Optimum Moisture Content - we% Moximum Dr., Density -7d pcf California Bearing Ratio (av)% Swell Days | 20 | |
| Optimum Moisture Content - we | 40 <u>92.4</u> | |
| Optimum Moisture Content - wo | 10085.2 20072.4 | MOISTURE DENSITY: ASTM METHOD |
| Moximum Dr, Density -7dpcf California Bearing Ratio (av)% Swell:lab% Swell against 615 psf Wo gain_9.4 % HYDROMETER ANALYSIS: Grain size (mm) | | Ontinum Maisture Content |
| California Bearing Ratio (av) 9% Swell: 1 Days 1.8 % Swell: 215 psf Wo gain 9.4 % BEARING: 1.0200 35.1 Housel Penetrometer (av) 800 psf Unconfined Compression (qu) psf Plate Bearing: psf Inches Settlement Consolidation 4.8 % under 2000 psf PERMEABILITY: K (at 20°C) Void Ratio Sulfates 1000+ ppm. | | Maximum Dr. Density -7d |
| HYDROMETER ANALYSIS: Grain size (mm) % BEARING: Housel Penetrometer (av) | - | California Bearing Ratio (av) % |
| HYDROMETER ANALYSIS: Grain size (mm) % BEARING: Housel Penetrometer (av) | · | Swell: 1 Days 1.8 % |
| Grain size (mm) % .0200 35.1 .0050 20:3 Unconfined Compression (qu) psf Plate Bearing: psf Inches Settlement Consolidation 4.8% under 2000 psf PERMEABILITY: K (at 20°C) Void Ratio Sulfates 1006+ ppm. | INCOROLUCTED ANIALYCIC | Swell against 615 psf Wo gain 9,4 % |
| #26 87 | HYDROMETER ANALYSIS: | |
| Unconfined Compression (qu) psf Plate Bearing: psf Inches Settlement Consolidation 4.8% under 2000 psf PERMEABILITY: K (at 20°C) Void Ratio Sulfates 1006+ ppm. | Grain size (mm) % | BEARING: |
| Unconfined Compression (qu) psf Plate Bearing: psf Inches Settlement Consolidation 4.8% under 2000 psf PERMEABILITY: K (at 20°C) Void Ratio Sulfates 1006+ ppm. | .0200 35.1 | Housel Panetrometer (av) 800 auf |
| Plate Bearing: | | |
| Inches Settlement Consolidation 4.8% under zooo psf PERMEABILITY: K (at 20°C) Void Ratio Sulfates 1006+ ppm. Original Do NOT Remove #26 87 | | |
| Consolidation 4.8% under 2000 psf PERMEABILITY: K (at 20°C) Void Ratio Sulfates 1006+ ppm. Original Do NOT Remove #26 87 | | Inches Settlement |
| K (at 20°C) | | Consolidation 4.8% under 2000 psf |
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| Sulfates 1000+ ppm. Original Do NOT Remove #26 87 | | |
| Original Do NOT Remove #26 87 | · · | YOIG NGIIO |
| Do NOT Kemove #29 8/ | | Sulfates 1006+ ppm. |
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| SOIL ANALYSIS LINCOLN-DEVORE TESTING LABORATORY | SOU ANALYSIS | LINCOLN-DeVORE TESTING LABORATORY |
| COLORADO SPRINGS, COLORADO | 0014 / 11/1010 | COLORADO SPRINGS, COLORADO |

| SUMMAI | RY SHI ET |
|--|--|
| Soil Sample 5M (very silty) Location Capital Hill Subdiv. Boring No. 6 Depth 2 (TYP) Sample No. 3 | Date: 12/13/78 |
| Natural Water Content (w) 18,55 % Specific Gravity (Gs) 2,62 | In Place Density (To) 111.1 pcf |
| SIEVE ANALYSIS: Sieve No. % Passing 1 1/2" 1" 3/4" 1/2" 4 10 | Plastic Limit P.L |
| Original Do NOT Remo From Office | PERMEABILITY: K (at 20°C) Void Ratio Sulfates 1000+ ppm. *26 87 |
| SOIL ANALYSIS | LINCOLN-DeVORE TESTING LABORATORY COLORADO SPRINGS, COLORADO |

| SUMMARY | TELLA |
|---|---|
| Soil Sample CL | Test 1 to. 25215 |
| Location Capital Hill Subdiv. Boring No. 3 Depth 10' | Date: 12/12/78 |
| Boring No. 3 Depth 10' | Table Phi |
| Sample No. 3 (TYP) | Test by- RKL |
| Natural Water Content (w) 35.5 % Specific Gravity (Gs) 2.70 | · In Place Density (To) 110,1 pcf |
| SIEVE ANALYSIS: | |
| Sieve No. % Passing | Plastic Limit P.L. 16,9 % |
| 1 1/2" | Liquid Limit L. L. 24.1 % Plasticity Index P.1. 7.2 % |
|]n | Shinkage Limit 15.9 % |
| 3/411 | Flow Index% Shrinkage Ratio% |
| 1/2" | Shrinkage Ratio% |
| 10 <u>100.0</u> | Volumetric Change% |
| 2098;3 | Lineal Shrinkage% |
| 4097,2 | |
| 100 | MOISTURE DENSITY: ASTM METHOD |
| | Optimum Moisture Content - we% |
| | Maximum Dr. Density -7d pcf |
| | California Bearing Ratio (av) % Swell: Days 2.7 % |
| | Swell: 1 Days 2.7 % |
| HYDROMETER ANALYSIS: | Swell against_960 psf Wo gain_11.3_% |
| | 17 12 |
| Grain size (mm) % | BEARING: |
| | Housel Penetrometer (av) 1800 psf |
| .0050 32.9 | Unconfined Compression (qu)psf |
| | Plate Bearing:psf |
| | Inches Settlement |
| ************************************** | Competition of Chines 2200 has |
| | |
| | PERMEABILITY: |
| | K (at 20°C) |
| | Sulfates 1500+ ppm. |
| Original | |
| Do NOT Rem From Office | #26 87 |
| | LINCOLN-DeVORE TESTING LABORATORY |
| SOIL ANALYSIS | COLORADO SPRINGS, COLORADO |



REVEW SHEET SUCMARY

| ACTIVITY - | | Little Bookcliff Sub. |
|------------|--|--|
| | | |
| | Lots 1 6 2 Little Bookeliff Subdivision, Northeast corner of Little Bookeliff Dr. and Wellington Ave. contains 2.73 acres. Patitioner: SSM Investments. Roger C. Shenkel TITIONER ADDRESS 735 Bookelliff Ave. (GINEER Jim Patty, Rolland Engineering VIE REC. AGENCY COMMENTS A-87 Police Dept. I see no problems. 3-87 City Engineer All of the drainage from this site is designed to flow into Little Bookeliff Dr. and Wellington Ave. through the drivway cuts. The water will then collect at an existing inlet on the northeast corner of the intersection. This inlet discharges into the Buthorne Drain pipe through a 10 Inch connector pipe. The inlet and pipe were designed for the street drainage from Little Bookeliff Ave. and Wellington Ave. Any additional runoff directed to this inlet may cause substantial ponding in Wellington Ave. In order to determine if the inlet is adequate or not, I will need drainage calculations showing anticipated runoff from the proposed development during 2 year and 10 year rain fall events. Our policy has been to size all pipes and drainage inlets to pass the two year historic runoff and to provide on site detention volume for all excess runoff up to the 10 year storm under fully developed conditions. In this drainage basin it is especially critical that the runoff rate be limited to the historic rate because the lowe sections of the Buthorne Drain pipe are under sized and ofter surcharged during rainfall events. If the existing inlet at the intersection of Little Bookeliff and Wellington is to be used to outlet runoff from this development an engineering analysis will be required to determine the extent and affect of ponding in Wellington is to be used to outlet runoff from this development an engineering analysis will be required to determine the extent and affect of ponding in Wellington is to be used to outlet runoff from this development an engineering analysis will be required to determine the extent and affect of ponding is excessive, creating a hazard to motorists, then on site | |
| | | ontains 2./3 acres. retitioner: SSM investments. |
| F | Roger C. Shenkel | |
| | | |
| PETITIONER | ADDRESS 735 Books | liff Aye. |
| ENGINEER | lim Patty, Rolland Eng | ineering |
| DATE REC. | AGENCY | COMMENTS |
| 6-04-87 | Police Dept. | I see no problems. |
| 6-09-87 | City Engineer | Little Bookcliff Dr. and Wellington Ave. through the driveway cuts. The water will then collect at an existing inlet on the northeast corner of the intersection. This inlet discharges into the Buthorne Drain pipe through a 10 inch connector pipe. The inlet and pipe were designed for the street drainage from Little Bookcliff Ave. and Wellington Ave. Any additional runoff directed to this inlet may cause substantial ponding in Wellington Ave. In order to determine if the inlet is adequate or not, I will need drainage calculations showing anticipated runoff from the proposed |
| | | pass the two year historic runoff and to provide on site detention volume for all excess runoff up to the 10 year |
| | | runoff rate be limited to the historic rate because the lowe sections of the Buthorne Drain pipe are under sized and |
| | | and Wellington is to be used to outlet runoff from this development an engineering analysis will be required to determine the extent and affect of ponding in Wellington Age during 2 and 10 year storms. If such ponding is excessive, creating a hazard to motorists, then on site detention will be required. Depending upon the historic runoff rate from the proposed development, a separate connection to the Buthorne Drain pipe may be required. All storm runoff rate and connections to the Buthorne Drain pipe must be reviewed |
| | | |
| 6-09-87 | Public Works | |
| 6-10-87 | Mt. Bell | No objections. |
| 6-15-87 | GJ Drainage | documents was made on the 9th of June. The site is in the |
| | | The existing storm sewer (drain tile) is not correctly shown on the utility composite. There is a manhole in the sidewalk on the east side of Little Bookcliff Drive. The manhole is 8 feet from the point of Lot 1 and 36 feet from |

GH Just

REV.EW SHEET SUMMARY

| FILE NO. 26- | 87 TITLE HEADING | Little Booke | liff Cont ¹ d | | DUE DATE_ | 6-16-87 | | |
|--|------------------|--------------|--------------------------|---------------------------------------|-----------|------------|--|--|
| ACTIVITY - PETITIONER - LOCATION - PHASE - ACRES | | | | | | | | |
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| | | | | | | <i>-</i> 1 | | |
| , | | | | | | | | |
| | | | | | | | | |
| PETITIONER ADD | RESS | | | | | | | |
| ENGINEER | | <u>.</u> | | | | | | |
| | | | | | | | | |

DATE REC.

AGENCY

COMMENTS

Grand Junction Drainage

the PC Lot 1 on the Little Bookcliff Drive, Wellington Avenue intersection. The drain tile centerline appears to be in the right of way of Little Bookcliff Drive as compared to observed property pins with yellow caps stamped 9960.

After field review and document check, the full width of easement C may not be necessary. Vacation of the easement C should only preced dedication of a new easement, as with the replat... However, please require drainage be included in the easement designation for that 10 foot easement adjacent to Little Bookcliff Drive in Lot 1. Such action will reinforce the easement previously granted, but described from a lot corner in La Villa Grande Subdivision.

The Grand Junction Drainage District and the City of Grand Junction recently completed a major reconstruction/upgrade on the Buthorn Drain downstream of the project site. The upsizing was completed realizing the adopted policy of storm water management of the city, supported by the drainage district. That policy of detention of the volume over the two year histoic runoff up to the ten year developed runoff is reasonable. The site plan, prepared by Dillon-Hunt shows that 71% of the Lot will be impervious, thus capable of adding significant volume of runoff. It is suggested that the petitioners engineer calculate the historic and anticipated runoff amounts, design a plan for detention and be required to do so before approval of the project. Either parking area of the gravel area (4) might be used for detention.

Any tie-in(s) to the Buthorn Drain will have to have approval of both the City of Grand Junction (because the drain is in public road right of way) and the Drainage District, the agency responsible for operation and maintenance of the Buthorn Drain below the Grand Valley Irrigation Company Canal. Drainage District policy is to require manholes at each point where storm water or irrigation waste water is dumped into the system. Cost of such manholes and installation will be the responsibility of the developer.

New construction is subject to the District Capitol Improvement Fee. -0- (sic)

REVIEW SHEET SUMMARY

| FILE NO. | 26-87 TITLE HEAD! | NG Little Bookcliff Cont'd | DUE DATE 6-16-87 |
|------------|----------------------|--|---|
| ACTIVITY - | PETITIONER - LOCATIO | ON - PHASE - ACRES | |
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| DETITIONED | ADDDECC | | |
| PETITIONER | AUDRESS | | |
| ENGINEER | | | • |
| DATE REC. | AGENCY | COMMENTS | |
| -15-87 | Bldg. Dept. | *State of Colorado licensed archi structure. | itect required to design |
| | | *City licensed general contractor *Would recommend early submittal review. | r required. of preliminary drawings for |
| | | *Foundation designed per soils po time of permit application. | ermit will be required at |
| -16-87 | Public Service | Electric: Need to retain 15 foo vacation page - also the south 1 be retained as utility easement. Gas: See electric comments. | 5 feet of proposed Lot 3 to |
| -18-87 | Planning Dept. | This is a review of three develo 1. Vacation of existing ea 2. Replacement with new ea lot configuration. 3. Final development plan building. | sements. sements along with revising |
| | | We have no problems regarding th locations, only that concerns of be addressed. | |
| | | clinic space (in square | for total retail sales areas covered under offices or |
| WRITTE | 4 | | ut at the southeast corner |
| RESPONSE N | 4ecessary | Will irrigation water b | e used for the landscaping o |
| July 6, | 1987 | system will be used for | |
| | | parking areas. Please bearing trees in the la ern edge of the lot. Y Tree Program offered b | ees should be provided near consider providing more shadendscaped area along the soutlou might check into the Strewy the Grand Junction Parks uses trees will be provided a |

6-26-87

Fire Dept.

LATE

This office has no objections to this Replat as long as fire protection in maintained and if and when building is done it be in accordance with fire codes at that time.

5. Will there be continuous concrete curbing around all

6. Is there a particular reason why "Area 4" at the north end will be gravelled rather than landscaped?7. Outside lighting must be directional to limit glare

Any signage will require a separate sign permit by a

no charge to the property owner.

of the panking areas?

and unwanted illumination.

licensed sign contractor.

FS:SUMRESP/DRS:144

REVIEW SHEET SUMMARY RESPONSE

FILE NO: 26-87

TITLE HEADING: Final Plat & Plan, Lots 1 & 2

Little Bookcliff Subdivision

ACTIVITY: Final Plat & Development Plan, Replat Lots 1 & 2

Little Bookcliff Subdivision, Northeast Corner of Little Bookcliff Drive and Wellington Avenue

PETITIONER: SSM Investments

AGENCY RESPONSE:

POLICE DEPARTMENT: No comment.

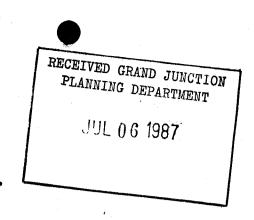
CITY ENGINEERING: 1. Runoff calculations have been completed and delivered to the City Engineer. Resolution of site runoff water will be according to City requirements once final determinations are made.

2. Unused curb-cuts will be closed and replaced with curb/walk according to City specifications.

PUBLIC WORKS: Corrections to legal description have been made and copies will be delivered to the City Planning Department.

MOUNTAIN BELL: No comment.

- GRAND JUNCTION DRAINAGE: 1. Storm sewer location has been changed and copies will be delivered to the City Planning Department.
 - 2. The 10' easement adjacent to Little Bookcliff Drive will be labeled "drainage".
 - 3. See City Engineer response regarding site runoff.
- BUILDING DEPARTMENT: 1. Colorado Architectural License B-629 will be attached to the construction documents.
 - 2. City licensed Contractor will be employed to construct the project.
 - 3. Preliminary drawings and code check will be submitted at preliminary design.



- 4. A Structural Engineer will be employed to design the footings according to the soil type encountered.
- PUBLIC SERVICE COMPANY: Easement requirements will be honored and indicated on corrected drawings and will be delivered to the City Planning Department.
- PLANNING DEPARTMENT: 1. Retail space will account for approximately 1,000 GSF for use as an optical shop.
 - 2. Fire hydrant/curb-cut interference (if any) will be resolved with the City Engineers and Fire Department.
 - 3. Landscape irrigation will be by automatic system. Water source is not known at this time.
 - 4. Additional trees will be proposed on the south provided they do not pose a traffic hazard.
 - 5. Concrete curbing will be used to contain parking surfacing.
 - 6. Area 4 is gravel to reduce maintenance and provide future parking.
 - 7. Design of outside lighting will take into consideration limitations on glare.
 - 8. Signage will be accomplished by a licensed Sign Contractor.
- FIRE DEPARTMENT: The proposed building will be constructed to meet the current adopted UBC and sections of the Life Safety Code.

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\$ 225 fee Payable to City of Gr. Lot upon Submittal

development summary



| P * 1 | | | | | | |
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| FILA | | 26_87 | Nama | Wallington Final | Ilata | 7/8/87 |
| 1110 | ₩- | 26-87 | . INAIIIC | Wellington Final | Date. | |

PROJECT LOCATION: Northeast corner of Wellington and Little Bookcliff Ave.

PROJECT DESCRIPTION:

- 1) Vacation of easements created under original plat
- 2) Replat depicting revised lot lines and new easements
- Final Development Plan for Lot 1 of replatted subdivision for construction of an optical/medical facility

| REVIEW SUM | MA | RY | (Major Concerns) | | |
|--|-----|-----|------------------------|-----------|-------|
| POLICIES COMPLIANCE | YES | ₩ 0 | TECHNICAL REQUIREMENTS | SATISFIED | NOT # |
| Complies with adopted policies | х | | Streets/Rights Of Way | х | |
| Complies with adopted criteria | Х | | Water/Sewer | Х | |
| Meets guidelines of Comprehensive Plan | х | | Irrigation/Drainage | x | |
| | | | Landscaping/Screening | Х | |
| , | | | Other: | | |

^{*} See explanation below

One concern was about the new lot 3 being a small unbuildable lot. The lot is being created to be sold to the adjacent owners for use as additional parking. It was the feeling of the Planning Commission and staff that once the sale was complete, an Adjustment to Boundary Lines be filed to absorb the small parcel into the larger property.

STATUS & RECOMMENDATIONS:

All technical requirements have been met and review comments addressed and accepted.

Planning Commission Action

Planning Commission gave final approval of the Final Plat and Plan subject to staff comments, along with a condition for approval of the Final Plat that Lot 3 be absorbed into the neighbor's property or back into Lot 2 of this replat within one year. Planning Commission recommended approval of the easement vacations.