

# Table of Contents

File 1992-0027

Name: High Fashion Fabrics - Rezone & Final Plan

**P** **S** A few items are denoted with an asterisk (\*), which means they are to be scanned for permanent record on the ISYS  
**r** **c** retrieval system. In some instances, items are found on the list but are not present in the scanned electronic development  
**e** **a** file because they are already scanned elsewhere on the system. These scanned documents are denoted with (\*\*) and will  
**s** **n** be found on the ISYS query system in their designated categories.  
**e** **n** Documents specific to certain files, not found in the standard checklist materials, are listed at the bottom of the page.  
**n** **e** Remaining items, (not selected for scanning), will be listed and marked present. This index can serve as a quick guide for  
**t** **d** the contents of each file.

X	X	<b>Table of Contents</b>
		<b>*Review Sheet Summary</b>
X	X	<b>*Application form</b>
X		Review Sheets
X		Receipts for fees paid for anything
		<b>*Submittal checklist</b>
		<b>*General project report</b>
		Reduced copy of final plans or drawings
X	X	Reduction of assessor's map.
		Evidence of title, deeds, easements
X	X	<b>*Mailing list to adjacent property owners</b>
		Public notice cards
		Record of certified mail
X		Legal description
		Appraisal of raw land
		Reduction of any maps – final copy
		<b>*Final reports for drainage and soils (geotechnical reports)</b>
		Other bound or non-bound reports
		Traffic studies
X	X	<b>*Review Comments</b>
		<b>*Petitioner's response to comments</b>
		<b>*Staff Reports</b>
		<b>*Planning Commission staff report and exhibits</b>
		<b>*City Council staff report and exhibits</b>
		<b>*Summary sheet of final conditions</b>

### DOCUMENT DESCRIPTION:

X	X	Action Sheet - 8/19/92 - Final Plat-Approved, Zoning - Approved	X		Dept. Revenue Recap Sheet - 8/17/92
X	X	Development Plan	X	X	Ordinance No. 2592 - **
X	X	Correspondence	X		Improvements List / Detail - 11/4/92
X		Quit Claim Deed not conveyed to City - 9/1/291	X	X	Hydrologic Analysis - 11/11/92
X	X	Supplemental Traffic Analysis - 5/14/92	X		Public Notice Posting - 6/1/92
X	X	Special Conditional Use Submittal	X	X	List of Subcontractors - 11/12/92
X	X	Hi-Fashion Fabrics Preliminary Estimate of Costs - 5/22/92	X	X	City Council Minutes - 4/7/92 - **
X	X	Drainage Report	X	X	South Elevation - Meander Drive Street Section
X		Legal Ad - 6/30/92, 7/8/92, 8/12/92	X	X	Landscape Plan
X		Notes to file	X	X	Sewer and Water Plan
X		Utility Coordinating Committee Approval - 7/8/92	X	X	Grading Plan
X		Land Appraisal Report - 7/20/92	X	X	Site Development Plan
X	X	Planning Commission Minutes - 8/4/92	X	X	Agreement for detention/retention facilities - missing last page
X		City Council Agenda - 8/5/92	X	X	Development Improvements Agreement - **





Carroll L. Ely  
600 Meander Drive  
Grand Jct. CO 81505

Perry Christensen  
2945 Fruitridge Dr.  
Grand Jct. CO. 81505

John M. Harris  
602 Meander Dr.  
Grand Jct. CO 81505

Larry Kempton  
607 26 Road  
Grand Jct. CO 81505

Mildred Vandover  
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Pat Gormley  
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2595 Fruitridge Dr.  
Grand Junction, CO 81505



**THOMAS A. LOGUE**

LAND DEVELOPMENT CONSULTANT

May 1, 1992

City of Grand Junction  
City Council  
Planning Commissions  
250 North 5th. Street  
Grand Junction, CO 81501

Dear Members:

Accompanying is a Zone Change Request and Development Plan for a new retail business location for Hi-Fashion Fabrics. The requested change in zoning is from RSF-4 to PB "Planned Business". The subject site is located on approximately 2.1 acres northwest of Patterson Road and Meander Dive, 660 feet west of North 1st. Street.

The enclosed information is intended to provide sufficient data to assess the merits of the requested change in zoning and development plans.

Given the opportunity, the proposal demonstrates that a quality business coupled with a development plan that is sensitive to the existing neighborhood, can be desirable for redeveloping an area such as that which exists west of 1st. Street along Patterson Road.

To proceed further with the development of the Hi-Fashion Fabrics facility requires a great deal of investment and risk to the petitioner. The owners of Hi-Fashion Fabrics, who have operated their business since 1965, believe they will be introducing an expanded existing business which will prove to profitable and desirable to the City of Grand Junction. They request that you, the City Council and Planning Commission give the petition and the owners of Hi-Fashion Fabrics your best consideration, and trust you will make a knowledgeable and wise decision in this matter.

The petitioner will be present at the scheduled public hearings to discuss the project and answer any questions which may arise.

Respectfully,

Thomas A. Logue

#27 92

## SITE ANALYSIS

### Introduction

The purpose of this section is to identify the physical and technical characteristics of the property selected for the Hi-Fashion Fabrics facility.

This section evaluates potential site development assets and constraints.

### Location

The subject site is located northwest of Patterson Road and Meander Drive, 660 feet west of North 1st. Street in Grand Junction, Colorado. The site is located in part of the SE 1/4 SE 1/4 of Section 3, Township 1 South, Range 1 West of the Ute Meridan.

### Existing Land Use

The site is somewhat rectangular in shape and is approximately 325 feet long north and south and 270 feet east and west. Most of the site is currently being used as grazing land. The northerly end of the property is barren. As shown on the accompanying maps, the topography ranges from flat to a gentle rolling landscape. Total difference in elevation is 16 feet. No permanent structures are found on the property.

The subject property is zoned RSF-4 (residential, 4 dwelling units per acre) by the City of Grand Junction.

### Surrounding Land Use

Surrounding land uses are considered to be low intensity. Most of the land in the surrounding vicinity is vacant and used as grazing land. "Estate type" housing uses can be found to the north of the property. The closest residential structure to the property boundary is estimated to be about 250 feet north of the site.

Even though much of the surrounding property is vacant and being utilized for grazing all of the land is zoned for other uses by either the City or Mesa County. The Grand Junction City Limits form the north boundary of the subject property.

Surrounding land use zones in the area include County zoned land designated as R-1-A, a residential zone requiring at least two acres per building site. This land is located north of the property. City zoned properties include:

East	PB, Planned Business
West	RSF - 4
South	PR, Planned Residential (max. 10 du/ac.)

Utility Service

**WATER SERVICE** - Domestic Water Service is available from the Ute Water Conservancy District. An eight inch water main is located within the Patterson Road right-of-way. This main is sufficient in size to provide adequate water for fire protection.

**SANITARY SEWER** - The *Horizon Drive Sewer Interceptor* main is located in Patterson Road along the south boundary of the property. This line currently is operating within its' design capacity.

**ELECTRIC, GAS & COMMUNICATION** - Underground communication and natural gas mains adjoin the property within the existing road right-of-ways. Overhead electrical service is also located adjacent to the subject property within the adjoining roadways.

**IRRIGATION WATER** - An existing underground irrigation water pipe line is located along the properties northerly boundary and along the east side of Meander Drive. It appears that this pipe line carries "return" water flow from the Grand Valley Irrigation Companies' system to the *Ranchmans Ditch*.

Access

Primary access to the site is Patterson Road which is fully improved four lane roadway. Traffic counts for 1988 were made by the City and are shown on the following page.





Site Drainage

The subject site is not adversely affected by any off-site drainage influence. Storm water is carried on the surface to Patterson Road and ultimately discharged into an existing box culvert located along the south side of Patterson Road.

Soils and Geologic Conditions

No major man-made or geologic hazards are not to exist on the subject property. The Soil Conservation Service has classified soils on the property to be Fc, Fruita and Ravola Loams. This class of soils does not have severe limitations when slopes are less than 7%

## PROPOSED LAND USE

The accompanying development plans indicates the proposed development of a retail fabric store to be located on a 2.1 acre tract of land northwest of Patterson Road and Meander Drive in the City of Grand Junction.

The primary focal point of the development will be the construction of a new 11,250 square foot building. Building materials will be masonry and steel.

In addition to the building, 73 paved parking spaces will be provided for the customers and employees of the facility.

Hours of operation will be between 9:30 A.M. and 5:30 P.M., Monday thru Saturday.

This new facility will replace the petitioners existing operation located at the corner of 1st. Street and Orchard Avenue a short distance south of the subject property.

At this time Hi-Fashion Fabrics employees seven full time people. Upon the expansion of their business it is conceivable that they will expand the number of employees by at least two.

In addition to a wall mounted sign on the building, a single "monument" type sign will be located near the primary entrance. The sign will identify the facility name and address. All signs will meet the current City sign code requirements.

Access - The primary access drive will be from Patterson Road, 106 feet west of the centerline of Meander Drive. A secondary access is also proposed from Meander Drive 290 feet north of Patterson Road. Both access drives will be constructed in accordance with the City of Grand Junction's driveway standards.

According to the Colorado State Highway Department's, *Trip Generator*, approximately 61 average weekday trips will be generated once the facility opens.

Since the City requires the improvement or escrow payment of adjoining half street improvements, the proposal calls for the construction of full width improvements to Meander Drive for approximately one-half of the site's street frontage. Further, the proposal call for participation from the City in the expense of the improvement exceeding normal escrow payments. The petitioner is willing to absorb the cost of engineering the and project management.

Utility Service - Electric, gas and communication service will be extended from existing facilities which adjoin the site.

Domestic water service will be extended to the building from an existing 8 inch diameter main located in Patterson Road which is owned and operated by the Ute Water Conservancy District. Estimated water requirements are expected to be 500 gal./day. The existing water main will also be utilized for fire protection. A new fire hydrant will be installed near the access drive on Patterson Road.

The proposal calls for the utilization of the Horizon Drive Interceptor Sewer of sewage disposal. The proposed building will be connected to an existing 4 inch sewer service.

The petitioner has one share of Grand Valley Water Company irrigation water. This water will be utilized for irrigation of the landscaped open areas. A pumping facility will be located near an existing irrigation structure along the north boundary of the property.

Grading and Drainage - Grading of the site will be conducted in a manner to provide positive drainage away from the building. Two drainage discharge points are proposed, both of about equal area. Drainage flows in excess of the total historic flow will be detained on-site in a detention basin near the corner of Patterson Road and Meander Drive. All of the drainage water discharged from the site will ultimately be received by the Ranchmans Ditch located along the south side of Patterson Road in a box culvert.

Buffering and Screening - The proposal utilizes the existing site topography as its primary method of buffering and screening. The proposed building and parking areas are located as close as practical to Patterson Road.

Review of the proposed site plan indicates about 1.0 acres or one-half of the total site will be left as landscaped open space. Two types of landscaped areas are proposed. A formal landscaped area consisting of "street trees" and turf grass ground cover along the adjoining roadways. Natural grasses and existing vegetative ground cover is proposed for the area located north of the building and parking area. Additionally, a picnic area and gravel walking path are also proposed for this area. Existing irrigation water will be utilized to maintain all of the landscaped areas.

Development Schedule - It is anticipated that site development will begin immediately upon the City's acceptance of the proposal. With completion of the project within a 12 to 18 month period.

## REZONE CRITERIA

The City of Grand Junction has established seven criteria for evaluation of zone change requests. A response to each follows:

A. Since the underlying zone was established during the annexation process by the City without the benefit of a specific use for the property an error in the existing zone could be considered to have occurred.

B. Substantial changes in the character of the surrounding area have occurred. Specific changes include:

1. The construction of Patterson Road to arterial standards.
2. The establishment of a non-residential zone along the east boundary of the subject site.
3. The construction of Mesa Mall.

C. It is widely accepted fact that any community that does not have some new development activity will wither and die economically. It is important for any community to encourage development of new and existing business endeavors which maintains its economic stability.

D. Other than economic impacts to the City of Grand Junction, the proposed site in its present state does not present major adverse impact on the adjoining areas. However, once development of the Hi-Fashion Fabrics facility is completed, some impact of the adjoining properties would most likely be realized. Impacts to the adjoining non-residential zones would be positive, while impact to the adjoining residential zones could be considered negative.

Utilizing the "Planned Unit Development" (PUD) zone concept, any such negative impacts can be minimized. The PUD zone allows for specific site plan reviews of the proposed development plans by the general public and various governmental agencies.

Preparation of the Site Development Plan meets several goals in development of the site:

1. Protect the adjoining residential uses from any adverse impacts.
2. Maintain visibility of the use from Patterson Road.
3. Maintain ease of accessibility for customers and delivery of goods.
4. Achieve a desirable surrounding for the employees and projects a positive image to the consumer.

In order to meet the goals established above the following key design elements were incorporated within the Site Development Plan:

1. 54% of the total site is landscaped open space.
2. Adequate parking for employees and customers.
3. Utilization of the topography of the site for buffering from adjoining residential uses.
4. Hours of operation are 9:30 A.M. to 5:30 P.M.
5. Low intensity security lighting will be used.
6. The proposed building is located as far away as possible from residential uses.

E. Because the requested land use zone is non-residential in nature, the requirement upon local government services is considered to be minimal. Revenues generated by the proposed use should more than off-set costs incurred by the City in providing services. Revenues generated will be from the following:

1. Property Taxes
2. Sales Taxes
3. Special Use and Tap Fees

F. The City of Grand Junction has adopted numerous land use policies. Of the adopted policies, the *Patterson (F) Road Corridor Guideline* is the most applicable to the request. According to the guideline, "Light business and mixed use development is appropriate along the north (side) of Patterson Road from 25 1/2 Road to 1st. Street ...". The request for a Planned Business Zone meets the recommendations within this policy.

G. All public utilities required for the development of the subject property exists within the adjoining roadways and have the available capacity to serve the proposed use.

## SUMMARY AND CONCLUSIONS

The proposal calls for the development of a new retail business located on 2.1 acres northwest of Patterson Road and Meander Drive, 660 feet west of 1st. Street. Site development plans include to construction of a 11,250 square foot retail fabric store.

The site of the proposed use adjoins an existing non-residential zoned property.

Approximately 50% of the total site area is designated as open space to creating a buffer between the proposed use and the existing residential uses in the vicinity of the request. Additionally, the proposed building is located as far as possible from existing residential uses.

Access to the subject site is gained from a fully improved principle arterial. Given the current traffic volumes, the design capacity, and projected traffic increases from the proposed use, no adverse affects occur.

All of the necessary utility services required for development of the type have available capacity. Adequate water supplies for fire protection exist, as well as, central sewage disposal.

Fiscal Impacts, once the site is fully developed are positive. Adverse impacts to public facilities are almost non-existent.

The proposal meets or exceeds the criteria set forth in the City's Patterson Road Policy Statement.

The site meets the requirements of the operators to be within 3 minutes of their existing facility.

HI-FASHION FABRICS  
SUPPLEMENTAL TRAFFIC ANALYSIS

May 14, 1992

This analysis is supplemental to the project narrative for Hi-Fashion Fabrics on file with the Community Development Department, the reader of this analysis is encouraged to read the narrative in order to gain a full understanding of the proposal.

According to the Colorado Department of Highways' Memorandum dated November 10, 1981, *Estimating Trip Generation*, approximately 70 vehicle trips per weekday would be generated once the Hi-Fashion Fabrics facility is complete. The highway departments generator does not include a specific category for fabric stores. The category of "General Light Industrial was use for this analysis.

For the purposes of this study a "trip" is a single (one direction) vehicle movement with its destination inside the study site. In other words a total of 140 movements could be expected on a daily basis.

Utilizing the cash receipts from the petitioners existing operation, it was determined that the facility peak operating hours is between 11:30 A.M. and 2:30 P.M. daylight savings time. Further, their peak sales season is in the months of October and November. The formentioned project narrative indicates that the facility will be open Monday thru Saturday between the hours of 9:30 A.M. and 5:30 P.M.

Therefore, peak traffic can be expected to occur around the noon hour. It is estimated that this peak would represent 50% of the daily total traffic, or, 70 movements at the peak hour.

The ITE *Trip Generation Report* does not include a specific category for fabric stores. However, it does include a category for Furniture Stores which is considered to be equivalent to the Hi-Fashion Fabric operation in terms of intensity of the use. The ITE report indicates that the traffic direction (in and out) would be equal.

Two access drives are proposed for the new facility. It is impossible to accurately determine what the future habits of the motorist would be in terms of the extent each driveway would be utilized, for the purpose of this study it is felt that at least 75% of all generated traffic would utilize the Patterson Road driveway.





**CITY ATTORNEY 05/15/92**

**John Shaver 244-1506**

1. The applicant needs to clarify its proposal relative to improvement of Meander Drive. The statement that the proposal calls "for participation from the City in the expense of the improvement exceeding normal escrow payments" makes no sense.
2. The applicant must demonstrate compliance with all Zoning & Development Code requirements relative to rezone.

**CITY UTILITIES ENGINEER 05/15/92**

**Bill Cheney 244-1590**

Water - The City reserves the right to supply this development with water at a later date. The development is within the City limits and is therefore required to connect to City water when available. A 2" tap appears to be larger than required for a development of this nature.

Sewer - A grade of 2% should be maintained on the sewer service if possible. A 4" sewer service will provide adequate service to the building unless other uses are being contemplated.

**US WEST 05/08/92**

**Leon Peach 244-4964**

No comments at this time.

**PUBLIC SERVICE 05/08/92**

**Dale Clawson 244-2695**

Request the south five (5) feet of lot be dedicated as utility easement.

**PARKS & RECREATION 05/08/92**

**Don Hobbs 244-1542**

Need appraisal for determination of open space fee requirement.

Note: If the irrigation water comes from up on Meander Drive there may not be sufficient water available for this site due to a small "ditch" pipe. We water Foresight Village Park from this line and when all users are on-line there is not enough water capability.

Page 3 of 5, File #27-92

**GRAND VALLEY IRRIG. CO. 05/11/92**

**Phil Bertrand 242-2762**

Please note the following comments:

The Grand Valley has a piped irrigation line on the north side of proposed property and south and near the pavement of Meander Drive. We are exercising an exclusive right-of-use ownership and title that needs to be stated on the plat (GVIC exclusive right-of-way).

With the change of use of the property, the property owner is totally liable for any waters or return water that may cause damage or injury to GVIC system.

**POLICE DEPARTMENT 05/14/92**

**Marty Currie 244-3563**

From a police perspective there are no problems anticipated.

**GRAND JUNCTION DRAINAGE DISTRICT (GJDD) 05/12/92**

**John L Ballagh 242-4343**

There are some technical inaccuracies on the sheets submitted for review. On sheet 3 of 5 the GJDD Gormley Tile on the east side of Meander is incorrectly identified as an "existing irrigation water pipeline." On sheet 2 of 5 the material called out in that Gormley Tile is not 12" CMP but 12" NRCP. The STD City inlet elevations for grates and inverts seem to be incorrect. Where are the surface runoff calculations which support the inlets, pipe sizes and slopes and the detention sizing? What of the higher ground north of the immediate parcel. What surface runoff originates off site and flows across this parcel. Any tie in to the GJDD manhole on the east of Meander and north of Patterson will be in accordance with GJDD specs. The area is known to have a high water table, the Gormley Tile is on three sides of the parcel east of Meander Drive. There are two tile lines to the south across F Road. The beehive drain is just to the west.

**CITY DEVELOPMENT ENGINEER 05/19/92**

**Gerald Williams 244-1577**

Rejected as incomplete - see attached. (See attachment "A")

**MESA COUNTY SURVEYING**

**06/16/92**

**Fred A. Weber**

**244-1822**

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The following issues need to be clarified prior to recording the plat:

1. The bearing and distance need to be shown on the line common to Lot 1 & Lot 2.
2. The true point of beginning needs to be shown.
3. The distance of 1309.91' from the SE 1/16 to the SW corner of SE 1/4, SE 1/4 appears graphically to represent the distance from the S 1/16 to the P.O.B. Please clarify if this distance is 846.41'.
4. The 7.5' easement referenced as Book 701, Page 360 calculates as 8.18' at the SW corner of Clifford D. Harwin's property. Should Harwin's east and west lines parallel the Aliquot Line or as shown?
5. The SW corner of SE 1/4, SE 1/4 should be monumented, noted on the plat and a monument record filed.
6. The side referenced as 7.65' in length appears to be more appropriately 7.50' in length. Please check.
7. Minor differences seem to exist in the curve data.
8. All dimensions are required by County regulations to be shown to the nearest 1/100th of a foot, both in the dedication and the graphic portion of the plat.

**COMMUNITY DEVELOPMENT DEPARTMENT**

**05/19/92**

**Karl G. Metzner**

**244-1439**

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The proposed use and zone is in conformance with the adopted Patterson Road Corridor Guidelines. Landscape plan must specify proposed species and planting sizes. How will irrigation be provided to the various landscaped areas? Landscape in front of building should have non-turf ground cover and shrubs to reduce maintenance and water requirements.

A number of technical deficiencies have been identified by other review agencies. These must be resolved 48 hours prior to hearing or staff may recommend tabling or denial of this project.



**THOMAS A. LOGUE**

LAND DEVELOPMENT CONSULTANT

May 20, 1992

Karl Metzner  
Community Development Dept.  
City of Grand Junction  
250 N. 5th. Street  
Grand Junction, CO 81501

RE: Hi-Fashion Fabrics

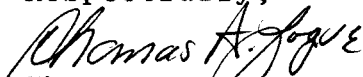
Dear Mr. Metzner:

In response to your initial review of our application for a change in zone and site development plan approval, the following is offered for your consideration:

1. It is the petitioners proposal to obtain a "revocable permit" for the proposed site improvements which are located within the Patterson Road right-of-way. These improvements consist of parking, driveway, sign, and landscaping. Due to the nature of the development schedule, a Right-of-Way Vacation Application will be processed sometime after acceptance of the application.
2. Accompanying is a Supplemental Traffic Analysis.
3. Additional drainage data will be transmitted to the City Engineering Department under separate cover.
4. Accompanying is a revised Landscaping Plan which indicates specie and size of planting, and a description of what is proposed for the natural grass areas.
5. Due to the time and expense coupled with the potential for modifications to the building location which may be requested by other review agencies, it is the petitioners desired to provide a sub-surface soils investigation and appraisal upon the citys final acceptance of the application.

We are confident that this provides you with the additional information you have requested.

Respectfully,

  
Thomas A. Logue

xc: Jeff Vogel

**SPECIAL & CONDITIONAL USE SUBMITTAL**  
(MOST APPLICABLE CHECKLIST FOR TYPE OF PROJECT)

HI - FASHION FABRICS

1

5/1/92

Project Name

Submittal No.

Submittal Date

**ENGINEERING CHECKLIST**

The following checklist is an abbreviated form based primarily on Section 4-7 of the Development Code, which should be referred to for additional information. Items marked "Not Req'd" are not necessary for the initial submittal, but may be required as a result of agency review.

CODE ITEM	DESCRIPTION	Received		Not Rec'd	Not Req'd
		Complete	Incomp		
4-7-1 &	Existing Features	✓			
5-6-13	Proposed Improvements	✓			
4-7-2 A	Elevation or Perspective Drawings				YRW
B	Development Schedule and Phasing	✓			
C	Agreements, Provisions, and Covenants				YRW
E-i	Grading and Drainage Plan & Report		✓	✓	
E-ii	Utility Composite: Sewer, Water, Gas, Electric TV, Telephone, Storm Drain, Irrigation, Ditches	✓			
E-iii	Landscape Plan		✓		
E-iv	Irrigation Plan			✓	
E-v	Level I Environmental Site Assessment				YRW
E-vi	Level II Environmental Site Assessment (if recommended by Level I ESA)				YRW
E-vii	CDOT Access Permit				YRW
E-viii	Section 404 Permit				YRW
E-ix	Restoration or Reclamation Plans				YRW
E-x	Traffic Impact Study				YRW
E-xi	Best Management Practices Plan				YRW
E-xii	Water Supply, Water Usage, and Sewage Generation Estimates			✓	
E-xiii	Improvements Agreement and Guarantee			✓	
E-xiv	Power of Attorney for Annexation and I.D.				YRW
E-xv					
E-xvi					

**EVALUATION OF SUBMITTAL**

Submittal is:  accepted  conditionally accepted  rejected as incomplete  
(Submitted as final, is more appropriate as Prelim)

E-i Basin boundaries are not shown, no drainage report or calculations of hydrology, hydraulics, detention, etc. provided.

E-iii Landscape items not identified

E-xiii For street, SW, C & G

Plans (and report when submitted) must be sealed and signed by a registered engineer who has "responsible charge" per state law.

HI-FASHION FABRICS PRELIMINARY ESTIMATE MAY 22, 1992

ROADWAY IMPROVEMENTS

ITEM	UNIT	QUAN.	UNIT PRICE	TOTAL	
1	Excavation and Embankment	CY	1670	\$5.00	\$8,350.00
2	Sub-Grade Preperation	SY	2400	\$1.00	\$2,400.00
3	Class 6 ABC	CY	550	\$16.50	\$9,075.00
4	3" Grading C HBP	TON	280	\$26.00	\$7,280.00
5	18" RCP	LF	30	\$20.00	\$600.00
6	6 ft. Curbwalk	LF	600	\$15.00	\$9,000.00
7	Remove Existing Pavement	SY	1200	\$1.50	\$1,800.00
8	Relocate Irrigation Pipe	LS			\$5,000.00
9	12" RCP Storm Sewer	LF	66	\$20.00	\$1,320.00
10	Standard Inlet	EA	2	\$3,000.00	\$6,000.00
11					\$0.00
12					\$0.00
13					\$0.00
14					\$0.00
15	Traffic Control Signs	EA	2	\$125.00	\$250.00
16	Raise Manholes and Valves	EA	7	\$200.00	\$1,400.00
18	Engineering	LS			\$25,000.00
19	Construction Management	LS			\$15,000.00
TOTAL ROADWAY IMPROVEMENTS					\$92,475.00

SANITARY SEWER

ITEM	UNIT	QUAN.	UNIT PRICE	TOTAL	
1	8" Sanitary Sewer Main	LF	690	\$10.00	\$6,900.00
2	4" Sanitary Sewer Main	LF	0	\$5.50	\$0.00
3	Standard Manhole	EA	5	\$750.00	\$3,750.00
4	Shallow Manhole	EA	0	\$48.00	\$0.00
5	Service Connections	EA	0	\$8.00	\$0.00
6	Trench Compaction	LF	690	\$4.00	\$2,760.00
7	Pipe Bedding Material	CY	200	\$10.00	\$2,000.00
8	Pavement Replacement	LF	30	80	\$2,400.00
9					\$0.00
10					\$0.00
11					\$0.00
12					\$0.00
13					\$0.00
14					\$0.00
15					\$0.00
16					\$0.00
18	Engineering	LS			\$5,000.00
19	Construction Management	LS			\$3,500.00
TOTAL SANITARY SEWER IMPROVEMENTS					\$26,310.00

DOMESTIC WATER

ITEM	UNIT	QUAN.	UNIT PRICE	TOTAL	
1	8" PVC Water Main	LF	700	\$12.00	\$8,400.00
2	6" PVC Water Main	LF			
3	3" PVC Water Main	LF		\$5.50	\$0.00
4	8" Gate Valve w/Box	EA	2	\$525.00	\$1,050.00
5	6" Gate Valve w/Box	EA		\$500.00	
6	3" Gate Valve w/Box	EA		\$300.00	\$0.00
7	Join Exist. Water Main	EA	1	\$2,500.00	\$2,500.00

HI-FASHION FABRICS PRELIMINARY ESTIMATE MAY 22, 1992

8	Service Connection	EA	0	\$300.00	\$0.00
9	Trench Compaction	LF	700	\$4.00	\$2,800.00
10	Fire Hydrant Assembly	EA	0	\$170.00	\$0.00
11	Asphalt Replacement	LF	30	\$80.00	\$2,400.00
12					\$0.00
13					\$0.00
14					\$0.00
15					\$0.00
16					\$0.00
18	Engineering	LS			\$5,000.00
19	Construction Management	LS			\$3,500.00
					\$25,650.00

SUMMARY

ITEM

1	ROADWAY IMPROVEMENTS				\$92,475.00
2	SANITARY SEWER IMPROVEMEN				\$26,310.00
3	DOMESTIC WATER IMPROVEMEN				\$25,650.00
4	sub-total				\$144,435.00
5	CONTINGENCY				\$14,443.50
6	TOTAL				\$158,878.50

700 LF STREET FRONTAGE = \$132/LF (st only)

\$227/LF (everything)



May 22, 1992

Mr. Jeffery Vogel  
Hi Fashion Fabrics  
1938 N. 1st Street  
Grand Junction, CO 81501

Grand Junction Community Development Department  
Planning • Zoning • Code Enforcement  
250 North Fifth Street  
Grand Junction, Colorado 81501-2668  
(303) 244-1430 FAX (303) 244-1599

Dear Mr. Vogel:

With regard to your submittal for a zone change and planned Business development at Patterson Road and Meader Drive, we are sorry to inform you that we cannot process your application because it does not meet the minimum requirements of the Grand Junction Zoning and Development Code.

Section 7-5 B entitled "Submittal Requirements" lists:

"1. All materials required by the Preliminary Plan Section of the Subdivision Regulations (see Section 6-7)..."

"6-7-2 B. The preliminary plan shall include:

9. Grading, Drainage, Storm Runoff and Flooding

- a. The existing and proposed contours at two foot intervals for ground slopes within the tract between level slopes...
- b. Existing drainage features...
- c. Proposed drainage system...
- d. Hydrology..

(see attached)

Until these plans and documents are submitted we cannot process your application.

Your application, therefore, will not be heard at the June 2, 1992 City Planning Commission hearing. The submittal will not be considered complete until the required documents are reviewed and approved by City staff.

Sincerely,

Bennett Boeschstein  
Community Development Director

xc. Karl Metzner  
Dan Wilson  
John Shaver



HI-FASHION FABRICS  
DRAINAGE REPORT  
PATRICK M. O'CONNOR, P.E.  
JUNE, 1992

Prior to studying the contents of this report, it is advised to read the *Project Narrative For Hi-Fashion Fabrics*. This narrative statement includes all aspects of the current site conditions and the proposed land use.

The Hi-Fashion Fabrics site, in its current state, is mostly covered with pasture grass. Some barren ground is evident along the face of a small hill near the north property line. The contour of the historic drainage basin directs stormwater runoff to the southwest corner of the property. The runoff is overland flow.

The 2.10 Hi-Fashion Fabrics site is located within a total 7.7 acre drainage basin which is indicated on the accompanying Figure I. For the purpose of this study, it is assumed that stormwater runoff east of the subject property would be intercepted by Meander Drive, due to its present grade.

The proposed site grading plan divides the existing drainage basin into two separate basins. Consisting of 2.5 acres to the east and 5.2 acres to the west.

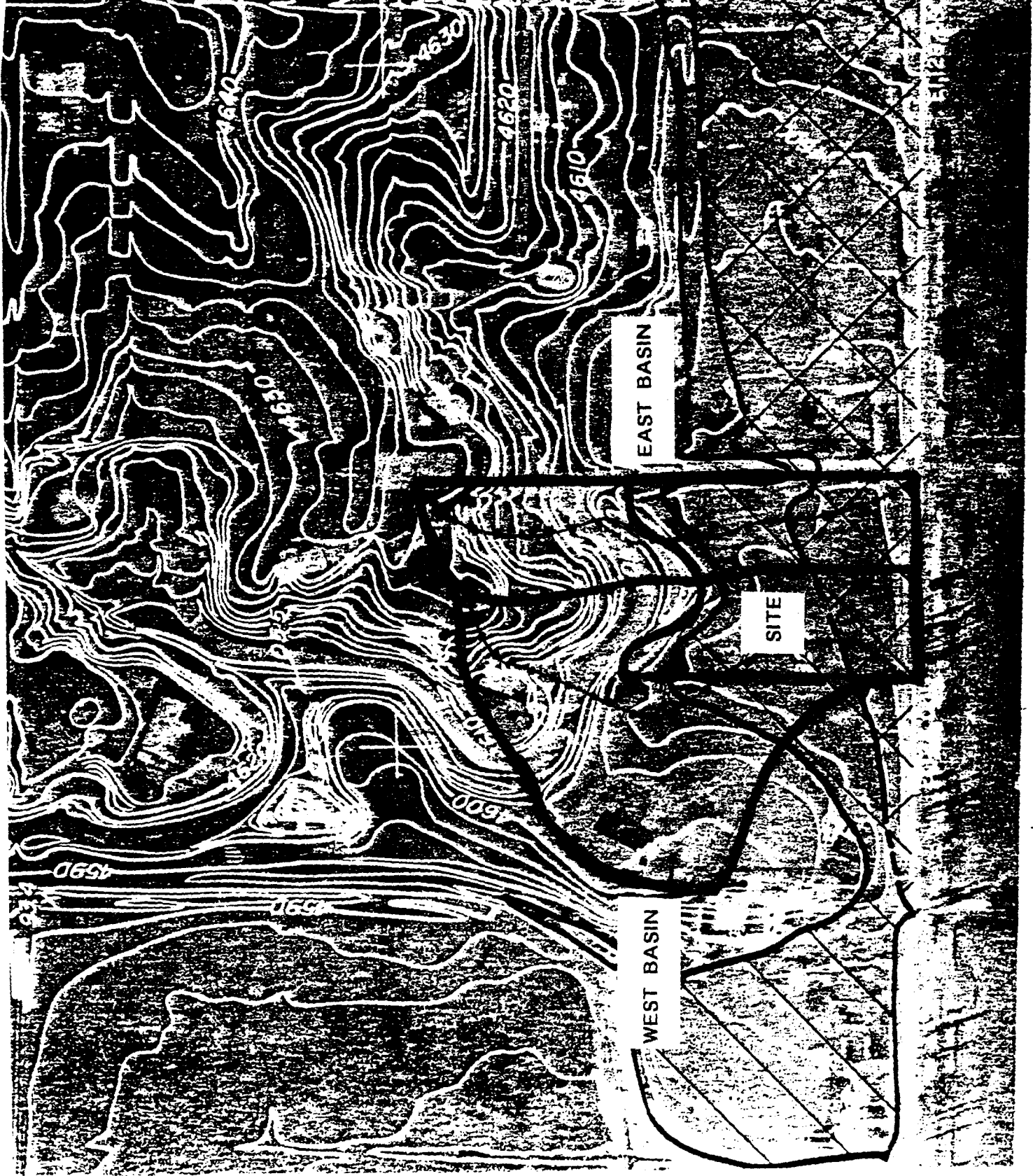
Utilizing the *Rational Method*, it is estimated that a 10 year frequency storm for the historic drainage basin would generate 5.8 cfs of storm water which is discharge on the ground surface near the southwest corner of the subject site. The proposed grading plan for the new west basin would generate approximately 4.3 cfs of storm water at the historic discharge point. The new east basin would generate 2.2 cfs of stormwater which would be discharged at the southeast corner of the site.

In order to control developed stormwater flows, a storm water detention is proposed near the southeast corner of the subject site for the new east basin. Based on the accompanying calculations it is estimated that stormwater storage requirements for a 10 year frequency storm would be 6456 cubic feet. The grading plan for the proposed stormwater detention basin has a capacity of 8572 cubic feet. In order to control "nuisance water" created by the irrigation of open areas, snow melt, and minor rain fall, an inlet is planned in the detention basin. The grate for the inlet is sized to maintain a maximum discharge flow rate less than 1.0 cfs.



MATCH SHEET

SCALE 1:25,000



WEST BASIN

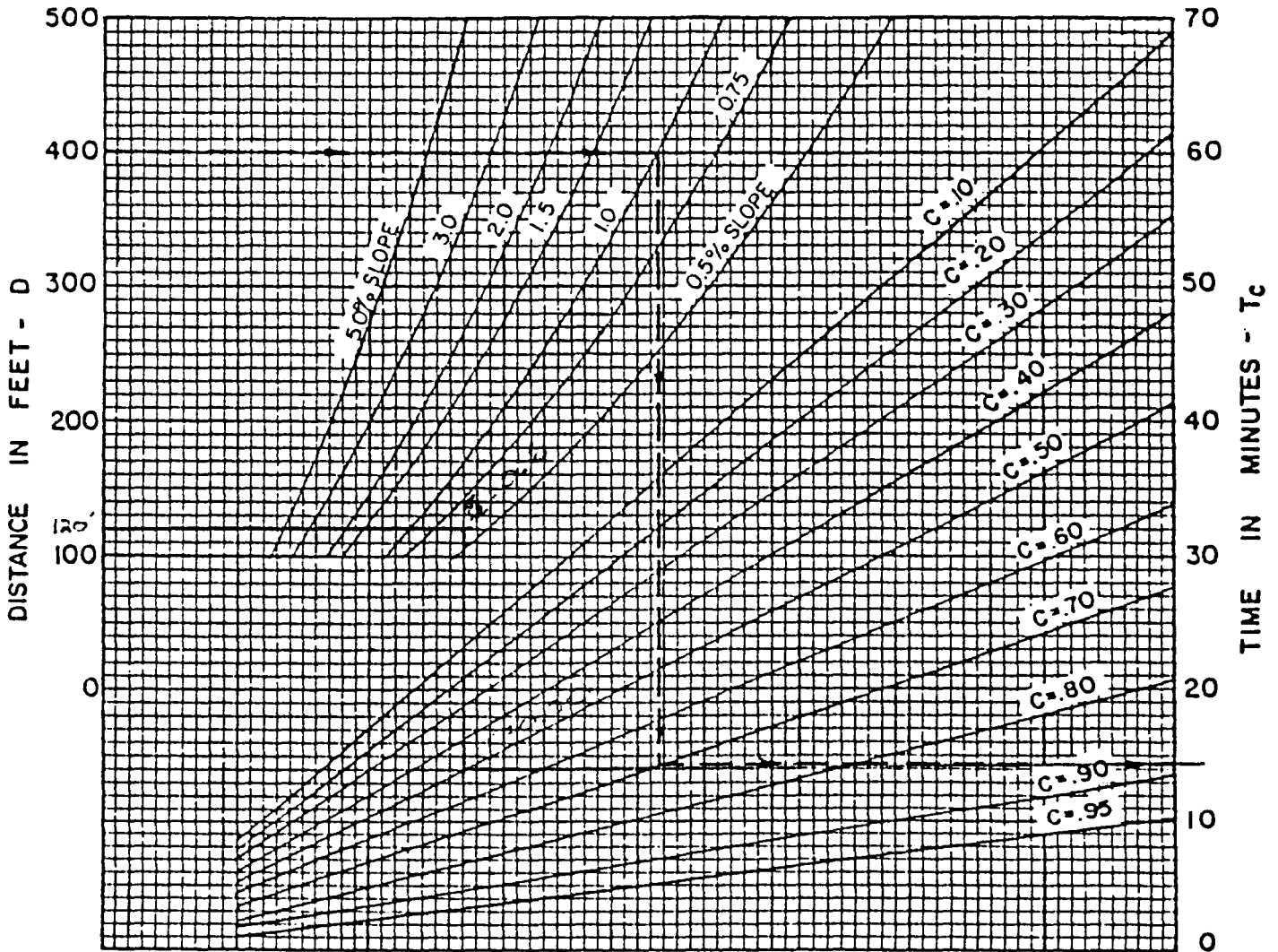
SITE

EAST BASIN

RUNOFF COEFFICIENTS FOR RATIONAL METHOD

LAND USE OR SURFACE CHARACTERISTICS	PERCENT IMPERVIOUS	C, Runoff Coefficients			
		FREQUENCY			
		2	5	10	100
<b>Business:</b>					
Commercial Areas	95	.87	.87	.88	.89
Neighborhood Areas	70	.60	.65	.70	.80
<b>Residential:</b>					
Single-Family	40	.40	.45	.50	.60
Multi-Unit (detached)	50	.45	.50	.60	.70
Multi-Unit (attached)	70	.60	.65	.70	.80
½ Acre Lot or Larger	30	.30	.35	.40	.60
Apartments	70	.65	.70	.70	.80
<b>Industrial:</b>					
Light Areas	80	.71	.72	.76	.82
Heavy Areas	90	.80	.80	.85	.90
<b>Parks, Cemeteries</b>	7	.10	.10	.35	.60
<b>Playgrounds:</b>	13	.15	.25	.35	.60
<b>Schools:</b>	50	.45	.50	.60	.70
<b>Railroad Yard Areas:</b>	40	.40	.45	.50	.60
<b>Undeveloped Areas:</b>					
Historic Flow Analysis-	2	(See "Lawns")			
Greenbelts, <u>Agricultural</u>					
Offsite Flow Analysis	45	.43	.47	.55	.65
(when land use not defined)					
<b>Streets:</b>					
Paved	100	.87	.88	.90	.93
Gravel	13	.15	.25	.35	.65
<b>Drive and Walks:</b>	96	.87	.87	.88	.89
<b>Roofs:</b>	90	.80	.85	.90	.90
<b>Lawns, Sandy Soil:</b>	0	.00	.01	.05	.20
<b>Lawns, Clayey Soil:</b>	0	.05	.10	.20	.40

TIME OF CONCENTRATION  $\approx T_c$   
FOR OVERLAND FLOW



BASED ON EQUATION

$$T_c \approx \frac{1.8(1.1-C)\sqrt{D}}{\sqrt[3]{S}}$$

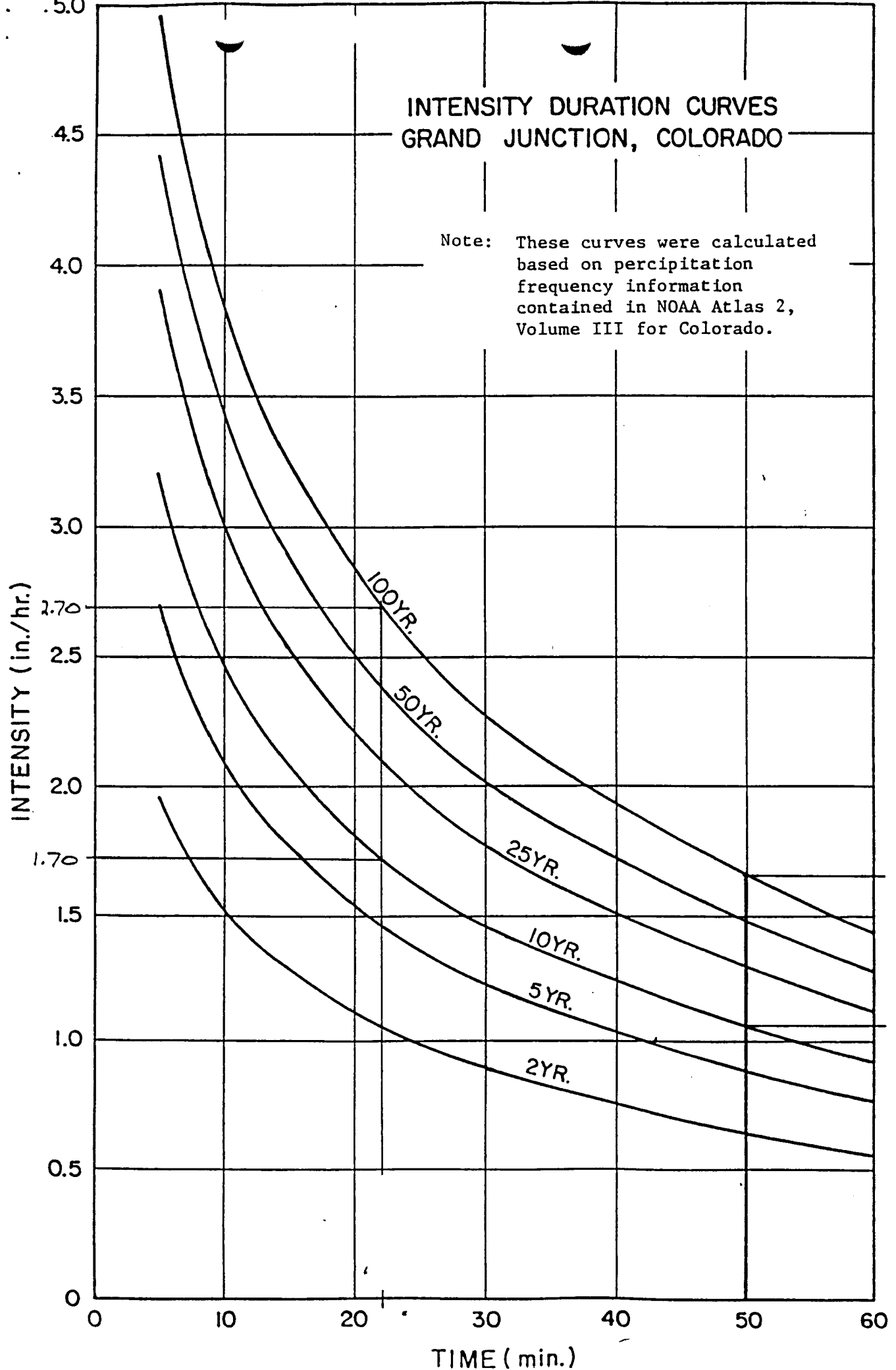
- C = Coefficient of runoff
- D = Distance of flow in feet
- S = Slope in %

EXAMPLE

- D = 400'
- S = 1%
- C = 0.70
- $T_c$  = 15 Minutes

# INTENSITY DURATION CURVES GRAND JUNCTION, COLORADO

Note: These curves were calculated based on percipitation frequency information contained in NOAA Atlas 2, Volume III for Colorado.



DEVELOPED:

EAST BASIN:

2.5 AC. TOTAL (0.5 AC @ C=0.90 + 2.0 AC @ C=0.50)

COMPOSITE C =  $\frac{(0.9 \times 0.5) + (0.5 \times 2.0)}{2.5} = 0.58$

$t_c$ : 400 L.F. OVERLAND @ S=5.0% C=0.4

300 L.F. OVERLAND @ S=1.5% C=0.6

$t_c = 14.8 + 13.6 = 28$  MINUTES

$I_{10} = 1.5$  IN./HR.

$Q_{10} = 0.58 (1.5) (2.5) = 2.2$  CFS

FLOW/STORAGE ANALYSIS

<u>TIME</u> <u>(MINUTES)</u>	<u>RAINFALL</u> <u>INTENSITY (IN/HR)</u>	<u>Q</u> <u>(CFS)</u>	<u>Q<sub>AVG.</sub></u> <u>(CFS)</u>	<u>RELEASE</u> <u>Q<sub>0</sub></u>	<u>STORED</u> <u>Q</u>	<u>TIME</u> <u>(MIN.)</u>	<u>STORED</u> <u>VOLUME (FT<sup>3</sup>)</u>
0	-	0					
28 ( $t_c$ )	1.5	2.2	1.1	0	1.1	28	1848
50	1.1	1.6	1.9	0	1.9	22	2508
75 ( $2.67t_c$ )	0.8 (EST.)	1.2	1.4	0	1.4	25	2100
							<u>6456 FT<sup>3</sup></u>

HISTORIC: (7.7 AC. @ C = 0.50)

$t_c$ : OVERLAND FLOW 500 L.F. @ S = 6.0%

350 L.F. @ S = 1.71%

$$t_c = 1.8(1.1 - C)(D)^{1/2} / (S)^{1/3}$$

$$t_c = 13.3 + 16.9 = 30 \text{ MINUTES}$$

$$I_{10} = 1.5 \text{ IN./HR.}$$

$$Q_{10} = CIA = 0.5(1.5)(7.7) = 5.8 \text{ CFS}$$

DEVELOPED: (TWO BASINS)

WEST BASIN:

5.2 AC. TOTAL (0.6 AC. @ C = 0.90 + 4.6 @ C = 0.50)

$$\text{COMPOSITE } C = \frac{(0.9 \times 0.6) + (0.5 \times 4.6)}{5.2} = 0.55$$

$t_c$ : 300 L.F. OVERLAND @ S = 8.7% C = 0.4

500 L.F. OVERLAND @ S = 1.6% C = 0.6

$$t_c = 10.7 + 17.2 = 28 \text{ MINUTES}$$

$$I_{10} = 1.5 \text{ IN./HR.}$$

$$Q_{10} = 0.55(1.5)(5.2) = 4.3 \text{ CFS}$$

To: KarlM  
Cc: ClaudiaH, MarkR, GeraldW  
From: Don Newton  
Subject: Hi Fashion Fabrics  
Date: 7/07/92 Time: 4:41p

I have the following additional comments regarding the revised plans for this development:

1. The proposed street improvements on Meander Drive do not meet the Developmet Code requirements for half street improvments along the entire frontage of the subdivision. However, at this location the proposed plan to widen Meander Drive full width along the frontage of the proposed development may be of more functional benefit than half street improvements along the entire property frontage.

If the street improvements are approved as proposed, this approval should not preclude the requirement for half street improvements along the remaining property frontage at such time that the remaining property is developed.

2. The site plan, grading & drainage plan and street improvement plans lack sufficient detail for final plan approval. I would recommend that these plans either be considered as "preliminary" or that the final plan approval be tabled until such time that complete plans are submitted.

3. I remain opposed to the proposed curb cut on patterson Road. This access is not needed with Meander Drive adjacent to the property. Two curb cuts to the parking lot would be allowed from Meander Drive. Access to arterial streets like Patterson Road should be minimized



**REVIEW COMMENTS**  
**HI-FASHION FABRICS**  
**7-8-92**

by: **Gerald Williams**

1. Improvements Agreement
  - a. The improvements agreement submitted was on the old form. A new form should be picked up from Community Development and submitted.
  - b. The street grading quantity is listed as cubic yards which should probably read square yards.
  - c. A more appropriate cost for this type of street paving work would be \$40 per ton instead of \$28 per ton.
  - d. A more appropriate figure for the curb, gutter and sidewalk is \$25 per linear foot instead of \$15 per linear foot.
  - e. A more appropriate figure for water mains (including valves) would be \$16 a linear foot instead of \$12 a linear foot.
  - f. There should be an amount for traffic control.
2. We previously requested documentation of the detention volume available, and also indicated that average end-area methods were inappropriate and provided the conic method for use. The drainage report provides volume calculations which do not use the conic method nor do they appropriately use average end-area methods; i.e., between contour 4 and contour 5, one would use the average area times the depth between, not the depth between times the higher area as was done in the calculations provided. Using the conic equation, as was required, and which would be more appropriate, would yield a total volume of 3,928 cubic feet. This is less than the calculated 4,521 cubic feet required. However, inasmuch as the volume required was based on no release during the storm, it is highly probable that such volume would not be necessary. Therefore, we will not request a resubmittal of calculations, but please keep in mind that such submittals will not be acceptable in the future.
3. On the grading plan, the elevation 6 contour was slightly modified to make it appear that 1 percent slope is provided on the parking lot when in reality much of the site does not have a minimum 1 percent slope. This must be revised to make sure that there is at least 1 percent slope on asphalt.
4. Grades, slopes and contours on the parking lot do not match each other. These should be reworked.

REVIEW COMMENTS  
HI-FASHION FABRICS

July 8, 1992

page 2

5. Grade changes on the pavement should be shown and located adequately for construction staking.
6. Grading detail was requested for the entrance off of Meander Drive. These must be provided on the plans.
7. On the drain trough detail, much definition and grading is lacking. There is a sidewalk behind the building which connects to public sidewalk. The cross-section shows that the private sidewalk dips down and goes underneath the other sidewalk. It would appear that part of the private sidewalk would and should remain at the elevation of the back of the public sidewalk. However, grading and slope information is lacking on the detail.
8. The public sidewalk cut shown would be approximately 1 foot away from the private sidewalk. The proposed fire hydrant is at least 3 foot away. It would appear that the sidewalk cut should be shown to extend further to the east to allow for the installation of the fire hydrant, and the additional sidewalk amount should also be included in the improvement agreement.
9. The grate elevation shown in Section A-A is at 3.23 feet, and on the grading plan it is shown at 3.25 feet. These should be consistent.
10. There is a note on the street section that the base should be per the soils engineer's recommendations. We had indicated before that these were final plans, and information from the soils engineer should be on the plans. Note that 6 inches is a minimum.
11. Also regarding the street section, we requested previously that two core samples be taken to determine if the existing pavement section and base material, plus the inch and a half overlay, is adequate to meet current city standards.
12. On the detail of the 4 foot walk and curb, it shows a 5 foot drainage and slope easement. This has been changed to 15 feet on the plans and grading plan. Also please change the easement to be a drainage, utility, and slope easement.
13. In conjunction with what was just stated, the 15 foot easement shown on the plat should read drainage, utility and slope easement.

REVIEW COMMENTS  
HI-FASHION FABRICS

July 8, 1992

page 3

14. As previously mentioned, a maintenance agreement for the detention facility will be required. We will submit City approved forms as soon as they are ready.

If you have any questions regarding the above comments, please feel free to call or stop by to discuss them.



**THOMAS A. LOGUE**

LAND DEVELOPMENT CONSULTANT

July 15, 1992

Mr. Gerald Williams  
City Development Engineer  
City of Grand Junction  
250 North 5th. Street  
Grand Junction, CO 81501

RE: Hi-Fashion Fabrics

Dear Mr. Williams:

In response to your comments dated July 8, 1992 and recommendations made by Don Newton, the following is provided for your consideration:

1. Revised Sheets 1, 2, and 5 are attached for your use.
2. A new Improvements Agreement is attached utilizing the new form. Unit prices have been modified as you have suggested.
3. New calculations for the detention basin are attached. The driveway relocation requested by Don Newton, resulted in some change to the basin's volume. The "conic" method was utilized.
4. All grades, slopes, and contours have been double checked to insure a minimum of 1.0% slope on all paved surfaces.
5. Additional detail information for the Drain Trough near the southwest corner of the site have been added to Sheet 5.
6. The the length of the sidewalk replacement along Patterson Road has been increased.
7. Other incidental comments have been incorporated within the attached drawings.
8. Two outstanding items remain un-answered at this time, includes core samples and pavement design recommendations, and the maintenance agreement for the detention facility. Field samples have been taken and the test results and recommendations should be available late next week. The petitioner will respond to the maintenance agreement as soon as possible after receipt.

Respectfully,

  
Thomas A. Logue  
xc: Jeff Vogel

# IMPROVEMENTS LIST/DETAIL

DATE: July 15, 1992

NAME OF DEVELOPMENT: Hi-Fashion Fabrics

LOCATION: N.W. Meander Drive & Patterson Road

PRINTED NAME OF PERSON PREPARING: Thomas A. Leque

	UNITS	TOTAL QTY.	UNIT PRICE	TOTAL AMOUNT
<b>I. SANITARY SEWER (Existing)</b>				
1. Clearing and grubbing				
2. Cut and remove asphalt				
3. PVC sanitary sewer main (incl. trenching, bedding & backfill)				
4. Sewer Services (incl. trenching, bedding, & backfill)				
5. Sanitary sewer manhole(s)				
6. Connection to existing manhole(s)				
7. Aggregate Base Course				
8. Pavement replacement				
9. Driveway restoration				
10. Utility adjustments				
<b>II. DOMESTIC WATER</b>				
1. Clearing and grubbing				
2. Cut and remove asphalt				
3. Water Main (incl. excavation, bedding, backfill, valves and appurtenances)	<u>LF</u>	<u>180</u>	<u>16.00</u>	<u>2880.00</u>
4. Water services (incl. excavation, bedding, backfill, valves, and appurtenances)	<u>LF</u>	<u>30</u>	<u>5.00</u>	<u>150.00</u>
5. Connect to existing water line	<u>LS</u>	<u>-</u>	<u>1500.00</u>	<u>1500.00</u>
6. Aggregate Base Course				
7. Pavement Replacement				
8. Utility adjustments				
<b>III. STREETS</b>				
1. Clearing and grubbing	<u>None</u>			
2. Earthwork, including excavation and embankment construction	<u>CY</u>	<u>725</u>	<u>3.00</u>	<u>2175.00</u>
3. Utility relocations	<u>None</u>			
4. Aggregate sub-base course (square yard)	<u>CY</u>	<u>150</u>	<u>16.00</u>	<u>2400.00</u>
5. Aggregate base course (square yard)	<u>Above</u>			
6. Sub-grade stabilization	<u>SY</u>	<u>660</u>	<u>2.00</u>	<u>1320.00</u>
7. Asphalt <del>or concrete</del> pavement (square yard)	<u>Ton</u>	<u>40</u>	<u>350.00</u>	<u>14,000.00</u>
8. Curb, gutter & sidewalk (linear feet)	<u>LF</u>	<u>614</u>	<u>25.00</u>	<u>15,350.00</u>
9. Driveway sections (square yard)	<u>Inc. Above</u>			
10. Crossspans & fillets	<u>None</u>			
11. Retaining walls/structures	<u>None</u>			
12. Storm drainage system	<u>EA</u>	<u>2</u>	<u>1200.00</u>	<u>2400.00</u>
12" PVC Storm Sewer	<u>LF</u>	<u>66</u>	<u>20.00</u>	<u>1386.00</u>

13. Signs and other traffic control devices	<u>EA</u>	<u>1</u>	<u>150.00</u>	<u>150.00</u>
14. Construction staking	<u>LS</u>	<u>-</u>	<u>-</u>	<u>750.00</u>
15. Dust control	<u>None</u>			
16. Street lights (each)	<u>Existing</u>			

**IV. LANDSCAPING**

1. Design/Architecture	<u>LS</u>	<u>-</u>	<u>-</u>	<u>500.00</u>
2. Earthwork (includes top soil, fine grading, & berming)	<u>SY</u>	<u>12,750</u>	<u>0.50</u>	<u>6375.00</u>
3. Hardscape features (includes <i>Pathway</i> walls, fencing, and paving)	<u>LP</u>	<u>320</u>	<u>5.00</u>	<u>1600.00</u>
4. Plant material and planting	<u>LS</u>	<u>-</u>	<u>-</u>	<u>5000.00</u>
5. Irrigation system	<u>LS</u>	<u>-</u>	<u>-</u>	<u>2000.00</u>
6. Other features (incl. statues, water displays, park equipment, and outdoor furniture)	<u>LS</u>			<u>250.00</u>
7. Curbing	<u>none</u>			
8. Retaing walls and structures	<u>none</u>			
9. One year maintenance agreement	<u>LS</u>			<u>500.00</u>

**V. MISCELLANEOUS**

1. Design/Engineering	<u>L.S.</u>			<u>3500.00</u>
2. Surveying	<u>L.S.</u>			<u>2500.00</u>
3. Developer's inspection costs	<u>L.S.</u>			<u>3000.00</u>
4. Quality control testing	<u>L.S.</u>			<u>2000.00</u>
5. Construction traffic control	<u>L.S.</u>			<u>750.00</u>
6. Rights-of-way/Easements	<u>none</u>			
7. City inspection fees	<u>L.S.</u>			<u>1000.00</u>
8. Permit fees	<u>none</u>			<u>100.00</u>
9. Recording costs	<u>L.S.</u>			
10. Bonds	<u>none</u>			
11. Newsletters	<u>none</u>			
12. General Construction Supervision	<u>Inc. Above</u>			
13. Other _____				
14. Other _____				

**TOTAL ESTIMATED COST OF IMPROVEMENTS: \$ 73,536.00**

\_\_\_\_\_  
SIGNATURE OF DEVELOPER

(If corporation, to be signed by President and attested  
to by Secretary together with the corporate seals.)

\_\_\_\_\_  
DATE

I have reviewed the estimated costs and time schedule shown above and, based on the plan layouts submitted to date and the current costs of construction, I take no exception to the above.

\_\_\_\_\_  
CITY ENGINEER

\_\_\_\_\_  
DATE

\_\_\_\_\_  
COMMUNITY DEVELOPMENT

\_\_\_\_\_  
DATE

HI-FASHION DRAINAGE DETENTION VOLUMES CONNOR 7/21/92 1/1

AREA @ INLET = 2 FT<sup>2</sup> ELEV. = 03.23

ΔELEV. = 0.77'

AREA @ CONTOUR (04) = 1240 FT<sup>2</sup>

ELEV. 04.00 (GEOMETRIC BREAK @ PARKING LOT)

ΔELEV. = 1.0'

AREA @ CONTOUR (05) = 11,880 FT<sup>2</sup>

ELEV. 05.00

CONIC EQUATION (FROM CITY OF G.J.):

{ A<sub>1</sub> + A<sub>2</sub> + (A<sub>1</sub>A<sub>2</sub>)<sup>0.5</sup> } H/3 = VOLUME (V)

V<sub>1</sub> (BETWEEN GRATE AND 04), V<sub>2</sub> = (BETWEEN 04 + 05)

V<sub>1</sub> = { 2 + 1240 + (2 x 1240)<sup>0.5</sup> } 0.77/3 = 332 FT<sup>3</sup>

V<sub>2</sub> = { 1240 + 11,880 + (1240 x 11,880)<sup>0.5</sup> } 1/3 = 5653 FT<sup>3</sup>

TOTAL VOLUME = 5984 FT<sup>3</sup>

VOLUME REQUIRED = 4500 FT<sup>3</sup>

∴ O.K. ✓

42 SHEETS 5 SQUARE  
42 SHEETS 5 SQUARE  
42 SHEETS 5 SQUARE  
NATIONAL

## RESPONSE TO REVIEW COMMENTS

---

Project: Hi-Fashion Fabrics

File No: 27-92

Activity: Rezone RSF-4 to PB and Final

Location: NW Patterson Road and Meander Drive

---

### CITY FIRE DEPARTMENT

Two emergency fire door exits will be provided along the west building wall. A sidewalk has been added to the site plan adjacent to the west building wall. Detailed building plans will be submitted to the department for review during the building permit process. The west building wall will be constructed in accordance with the *Uniform Building Code* which requires a one hour fire wall for the building occupancy load of B-2.

### CITY PROPERTY AGENT

The following items have been added to the final plat:

1. The True Point of Beginning has been identified.
2. The second to the last course has been added to the legal description within the dedication.
3. The Meander Drive right-of-way dedicated area has been drawn and described within the limits of the subdivision boundary.
4. Data has been added to the lot line between Lots 1 and 2.

### CITY ATTORNEY

See response to City Development Engineer

### CITY UTILITIES ENGINEER

The water plan have been modified to include a 3/4 inch water tap.

Sewer grades have been changed to maintain a minimum of 2% slope for a 4 inch service line.

### US WEST

A response to comments not required.

### PUBLIC SERVICE

A 5 foot utility easement has been added to the final plat along the south side of each lot.

### PARKS AND RECREATION

An appraisal will be prepared by a certified appraiser and presented to the City staff once the Zone Change Request has



been granted. 5% of the appraised raw land value will be paid to the City prior to obtaining a building permit.

A central pressurized irrigation system is proposed to water the landscaped areas. The system will be fully automated. Watering can be accomplished during off peak usage hours.

GRAND VALLEY IRRIG. CO.

The final plat has been changed to reflect an exclusive right-of-way for the irrigation company.

POLICE DEPARTMENT

A response to comments not required.

GRAND JUNCTION DRAINAGE DISTRICT

The following has been incorporated within the development plan sheets:

1. The *Gormley Tile* has been identified.
2. Inlet elevation for grates and inverts have been changed.
3. Existing tile lines adjoining the subject property have been identified.

A copy of the drainage report which addresses both on site and off site drainage flows historic and developed has been transmitted to the district.

Connection of the proposed storm sewer to the district's manhole will be done in accordance with their specifications has been added to the plan sheets.

CITY DEVELOPMENT ENGINEER

A drainage report has been transmitted to the department.

The following is the petitioners justifications for not re-locating Meander Drive in accordance with the request by the City Engineering Department:

1. Surrounding land owners which utilize Meander Drive prefer that the alignment remain as it now exists.

2. Relocation of Meander Drive will create conflicts with the existing underground irrigation delivery system.

3. There are ten parcels of land in addition to the subject property which utilize Meander Drive for access. Upon review of these parcels it is suggested that the maximum future average daily vehicle trips would be in the range of 130 since Meander Drive is a "dead end" street.

4. The *Patterson Road Corridor Guidelines* say, "Meandering pedestrian walks can be considered as an alternative to standard City sidewalk requirements." This has been incorporated within the Landscape Plan.

5. Meander Drive adjacent to the subject properties north boundary is owned and maintained by Mesa County, not the City of Grand Junction.

6. Properties along Meander Drive do not have central sewage collection lines available. Additionally, existing domestic water mains are not sufficient in size to accommodate fire protection. It is felt by the petitioner that utility upgrades within Meander Drive are most likely to occur in the near future. Therefore, it would be undesirable to complete a major street relocation without the installation of upgraded utility service. As the accompanying Preliminary Cost Estimate indicates, the cost for these extensions would be \$51,960. It should be pointed out that the petitioners property would not benefit from these utility up-grades since existing services are available in Patterson Road.

7. The accompanying Preliminary Construction Cost Estimate indicates a total improvement cost, including necessary underground utility improvements is \$181,753. This total exceeds the current property value by 40%. The roadway improvement only, and lost land value for right-of-way, represent 89% of the property value.

The application has been modified to accommodate the City Engineering Department's request to widen the existing intersection at Meander and Patterson Road. This will allow a left turn lane on Meander.

#### COMMUNITY DEVELOPMENT DEPARTMENT

A new landscape plan has been prepared which specify proposed species and planting sizes. The landscaping plan has been modified to include a planting area adjacent to the south side of the building for shrubbery in lue of turf ground cover.

HI-FASHION FABRICS PRELIMINARY ESTIMATE MAY 22, 1992

ROADWAY IMPROVEMENTS

ITEM	UNIT	QUAN.	UNIT PRICE	TOTAL
1 Excavation and Embankment	CY	1670	\$5.00	\$8,350.00
2 Sub-Grade Preperation	SY	2400	\$1.00	\$2,400.00
3 Class 6 ABC	CY	550	\$16.50	\$9,075.00
4 3" Grading C HBP	TON	280	\$26.00	\$7,280.00
5 18" RCP	LF	30	\$20.00	\$600.00
6 6 ft. Curbwalk	LF	600	\$15.00	\$9,000.00
7 Remove Existing Pavement	SY	1200	\$1.50	\$1,800.00
8 Relocate Irrigation Pipe	LS			\$5,000.00
9 12" RCP Storm Sewer	LF	66	\$20.00	\$1,320.00
10 Standard Inlet	EA	2	\$3,000.00	\$6,000.00
11				\$0.00
12				\$0.00
13				\$0.00
14				\$0.00
15 Traffic Control Signs	EA	2	\$125.00	\$250.00
16 Raise Manholes and Valves	EA	7	\$200.00	\$1,400.00
18 Engineering	LS			\$25,000.00
19 Construction Management	LS			\$15,000.00
TOTAL ROADWAY IMPROVEMENTS				\$92,475.00

SANITARY SEWER

ITEM	UNIT	QUAN.	UNIT PRICE	TOTAL
1 8" Sanitary Sewer Main	LF	690	\$10.00	\$6,900.00
2 4" Sanitary Sewer Main	LF	0	\$5.50	\$0.00
3 Standard Manhole	EA	5	\$750.00	\$3,750.00
4 Shallow Manhole	EA	0	\$48.00	\$0.00
5 Service Connections	EA	0	\$8.00	\$0.00
6 Trench Compaction	LF	690	\$4.00	\$2,760.00
7 Pipe Bedding Material	CY	200	\$10.00	\$2,000.00
8 Pavement Replacement	LF	30	80	\$2,400.00
9				\$0.00
10				\$0.00
11				\$0.00
12				\$0.00
13				\$0.00
14				\$0.00
15				\$0.00
16				\$0.00
18 Engineering	LS			\$5,000.00
19 Construction Management	LS			\$3,500.00
TOTAL SANITARY SEWER IMPROVEMENTS				\$26,310.00

DOMESTIC WATER

ITEM	UNIT	QUAN.	UNIT PRICE	TOTAL
1 8" PVC Water Main	LF	700	\$12.00	\$8,400.00
2 6" PVC Water Main	LF			
3 3" PVC Water Main	LF		\$5.50	\$0.00
4 8" Gate Valve w/Box	EA	2	\$525.00	\$1,050.00
5 6" Gate Valve w/Box	EA		\$500.00	
6 3" Gate Valve w/Box	EA		\$300.00	\$0.00
7 Join Exist. Water Main	EA	1	\$2,500.00	\$2,500.00

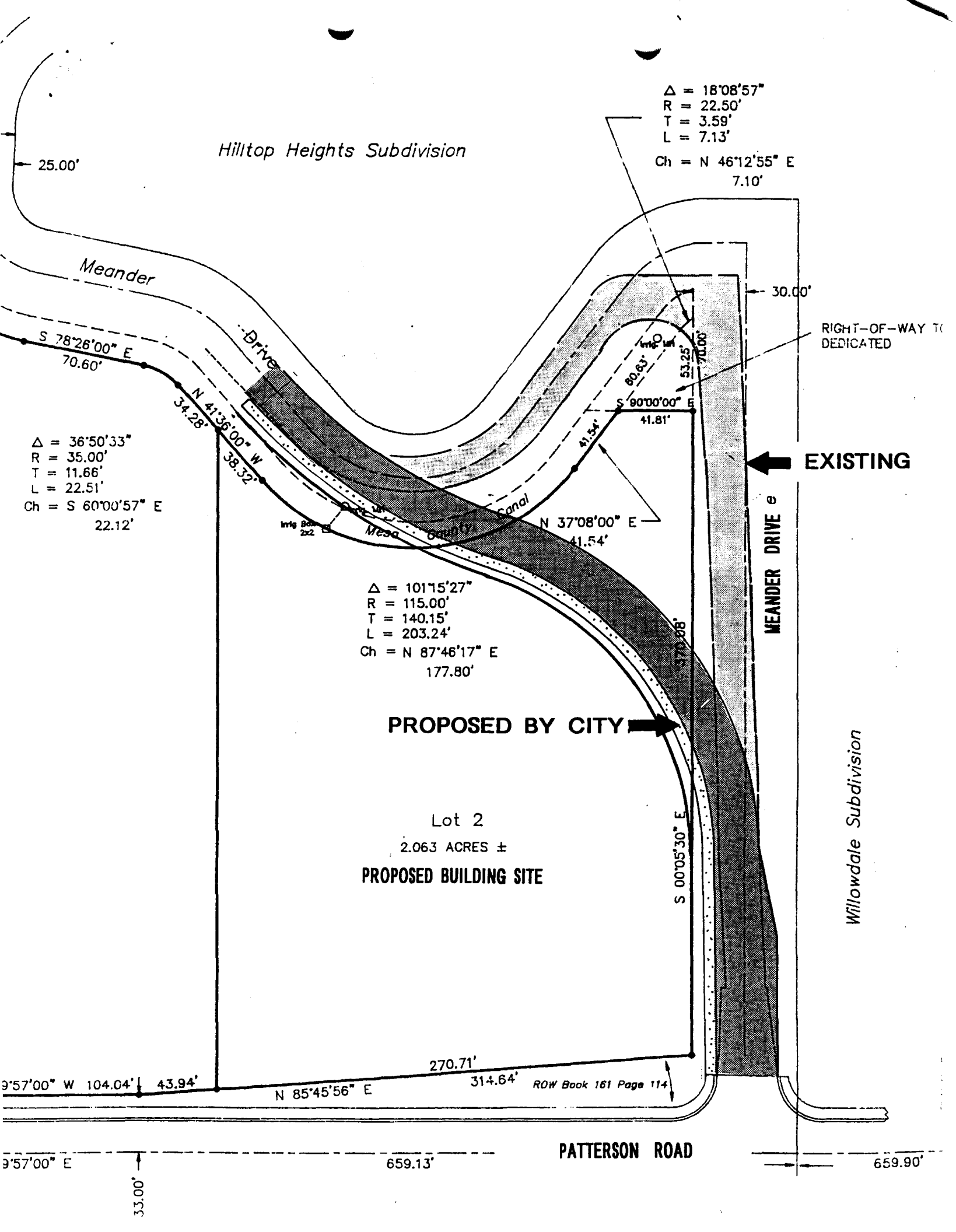
HI-FASHION FABRICS PRELIMINARY ESTIMATE MAY 22, 1992

8	Service Connection	EA	0	\$300.00	\$0.00
9	Trench Compaction	LF	700	\$4.00	\$2,800.00
10	Fire Hydrant Assembly	EA	0	\$170.00	\$0.00
11	Asphalt Replacement	LF	30	\$80.00	\$2,400.00
12					\$0.00
13					\$0.00
14					\$0.00
15					\$0.00
16					\$0.00
18	Engineering	LS			\$5,000.00
19	Construction Management	LS			\$3,500.00
					\$25,650.00

SUMMARY

ITEM

1	ROADWAY IMPROVEMENTS				\$92,475.00
2	SANITARY SEWER IMPROVEMENTS				\$26,310.00
3	DOMESTIC WATER IMPROVEMENTS				\$25,650.00
4	sub-total				\$144,435.00
5	CONTINGENCY				\$14,443.50
6	subtotal				\$158,878.50
7	ROW (15,250 SF @ \$1.50/SF)				\$22,875.00
8	GRAND TOTAL				\$181,753.50



Hilltop Heights Subdivision

$\Delta = 18^{\circ}08'57''$   
 $R = 22.50'$   
 $T = 3.59'$   
 $L = 7.13'$   
 Ch = N  $46^{\circ}12'55''$  E  
 7.10'

25.00'

Meander

Drive

S  $78^{\circ}26'00''$  E  
70.60'

N  $41^{\circ}36'00''$  W  
34.28'

38.32'

$\Delta = 36^{\circ}50'33''$   
 $R = 35.00'$   
 $T = 11.66'$   
 $L = 22.51'$   
 Ch = S  $60^{\circ}00'57''$  E  
 22.12'

Irrig Box 222

Mesa

Canal

N  $37^{\circ}08'00''$  E  
41.54'

S  $90^{\circ}00'00''$  E  
41.81'

41.54'

30.00'

RIGHT-OF-WAY TO DEDICATED

EXISTING

MEANDER DRIVE

$\Delta = 101^{\circ}15'27''$   
 $R = 115.00'$   
 $T = 140.15'$   
 $L = 203.24'$   
 Ch = N  $87^{\circ}46'17''$  E  
 177.80'

PROPOSED BY CITY

Lot 2

2.063 ACRES  $\pm$

PROPOSED BUILDING SITE

S  $00^{\circ}05'30''$  E  
170.28'

Willowdale Subdivision

S  $9^{\circ}57'00''$  W 104.04' 43.94'

N  $85^{\circ}45'56''$  E

270.71'

314.64'

ROW Book 161 Page 114

PATTERSON ROAD

S  $9^{\circ}57'00''$  E

659.13'

659.90'

33.00'



Lincoln DeVore, Inc.  
Geotechnical Consultants  
1441 Motor St.  
Grand Junction, CO 81505

TEL: (303) 242-8968  
FAX: (303) 242-1561

July 29, 1992

Mr. Thomas A. Logue  
537 Fruitwood Drive  
Grand Junction, CO 81504

Re: Suggested Pavement Sections  
Hi-Fashion Fabrics  
Patterson Road & Meander Lane  
Grand Junction, Colorado

Dear Mr. Logue;

Samples of the surficial native soils at this property that may be required to support pavements have been evaluated using the Hveem-Carmany method to determine their support characteristics. The results of the laboratory testing are as follows:

	R =	20
Expansion @ 300 psi =		0
Displacement @ 300 psi =		2.38

The soil profile consists of low density, very moist to saturated soils which will control the road section design and construction. The analysis assumed the placement of a Geotextile Separation Fabric (Mirafi 140, Polyfelt TS or an approved, equivalent Needle Punched Spun Geotextile Fabric) at the bottom of the road section for the areas which are soft, wet and unstable. These soft, wet and unstable areas may be found across the majority of the site and will prevent proper reworking and compaction of the native subgrade soils.

It is our recommendation that any areas of heavy truck traffic, such as loading and unloading areas, be constructed using a Rigid Concrete Pavement.

Traffic volumes of 170 single unit cars and pickup trucks per day and 34 heavy vehicles for Meander Lane, were provided to Lincoln DeVore. Based on the above traffic volumes and the tested R value of the subgrade soils, pavement recommendations have been provided. Recommendations are provided for Meander Lane Improvements, for the commercial main drive areas (heavy load areas) and parking areas assuming a 20-year design life. The pavement sections are summarized below.

Mr. Thomas A. Logue  
Hi-Fashion Fabrics  
July 29, 1992 Page 2

The owner of the structure should be aware that the traffic volume and the loads on pavement will be considerably higher during the construction phase than during the design life of the pavement structure. Therefore, some repair may be required after construction of the pavement is complete. An alternative would be to design a heavier pavement section at this time, utilizing the expected construction volume. It has been our experience that pavement failures during construction are minimal, and that it is more economical to repair localized failures due to construction traffic rather than construct a heavier pavement section.

**Automobile Parking Areas:  
20-Year Design Life**

3 inches of asphaltic concrete pavement  
on 9 inches of aggregate base course  
on 8 inches of recompacted subgrade soils

**Full Depth Asphalt  
20 Year Design Life**

5.5 inches of asphaltic concrete pavement  
on 8 inches of recompacted subgrade soils

**Main Drive Areas and Meander Lane:**

**20-Year Design Life**

3 inches of asphaltic concrete pavement  
on 10 inches of aggregate base course  
on 8 inches of recompacted subgrade soils

**Full Depth Asphalt  
20-Year Design Life**

6 inches of asphaltic concrete pavement  
on 8 inches of recompacted subgrade soils

We recommend that the asphaltic concrete pavement have a minimum  $R_t$  value of 95, and meet the State of Colorado requirements for a Grade C mix. In addition, the asphaltic concrete pavement should be compacted to a minimum of 95% of its maximum Hveem density. The aggregate base course should meet the requirements of State of Colorado Class 5 material, and

Mr. Thomas A. Logue  
Hi-Fashion Fabrics  
July 29, 1992 Page 3

have a minimum R value of 78. We recommend that The base course be compacted to a minimum of 95% of its maximum Modified Proctor dry density (ASTM D-1557), at a moisture content within + or -2% of optimum moisture. The native subgrade shall be scarified and recompacted to a minimum of 90% of their maximum Modified Proctor day density (ASTM D-1557) at a moisture content within + or -2% of optimum moisture.

All pavement should be protected from moisture migrating beneath the pavement structure. If surface drainage is allowed to pond behind curbs, islands or other areas of the site and allowed to seep beneath pavement, premature deterioration or possibly pavement failure could result.

#### **Rigid Concrete Pavement - 20-Year Design Life**

##### **Non-Dowelled**

7.5 inches of rigid concrete pavement  
on 4 inches of aggregate base course  
on 8 inches of recompacted subgrade soils

##### **Dowelled**

6 inches of rigid concrete pavement  
on 4 inches of aggregate base course  
on 8 inches of recompacted subgrade soils

We recommend that the rigid concrete pavement have a minimum flexural strength ( $F_t$ ) of 550 psi at 28 days. This strength requirement can be met using Class P or AX or A or B Concrete as defined in Section 600 of the Standard Specifications for Road and Bridge Construction, Colorado DOT. It is recommended that field control of the concrete mix be made utilizing compressive strength criteria. Flexural Strength should be only be used for the design process. Control joints should be placed at a minimum distance of 12 feet in all directions. If it is desired to increase the spacing of control joints, then 66-66 welded wire fabric should be placed in the mid-point of the slab. If the welded wire fabric is used, the control joint spacing can be increased to 40 feet. Construction joints designed so that positive joint transfer is maintained by the use of dowels is recommended.

The concrete should be placed at the lowest slump practical for the method of placement. In all cir-



Mr. Thomas A. Logue  
Hi-Fashion Fabrics  
July 29, 1992 Page 4

cumstances, the maximum slump should be limited to 4 inches. Proper consolidation of the plastic concrete is important. The placed concrete must be properly protected and cured.

Control joints should be placed at a minimum distance of 12 feet along the slab/road lane length or to match curb and gutter jointing and 15 feet in width. If it is desired to increase the spacing of control joints, then 66-66 welded wire fabric should be placed in the mid-point of the slab. If the welded wire fabric is used, the control joint spacing can be increased to a maximum of 40 feet.

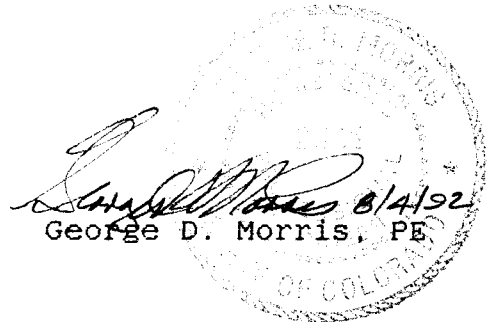
It is believed that all pertinent points have been addressed. If any further questions arise regarding this project or if we can be of any further assistance, please do not hesitate to contact this office at any time.

Respectfully Submitted,

LINCOLN DeVORE, Inc.

  
by: Edward M. Morris EIT  
Engineer/Western Slope Manager

Reviewed By: George D. Morris, PE



LD Job No.: 76604-J

TEST BORING

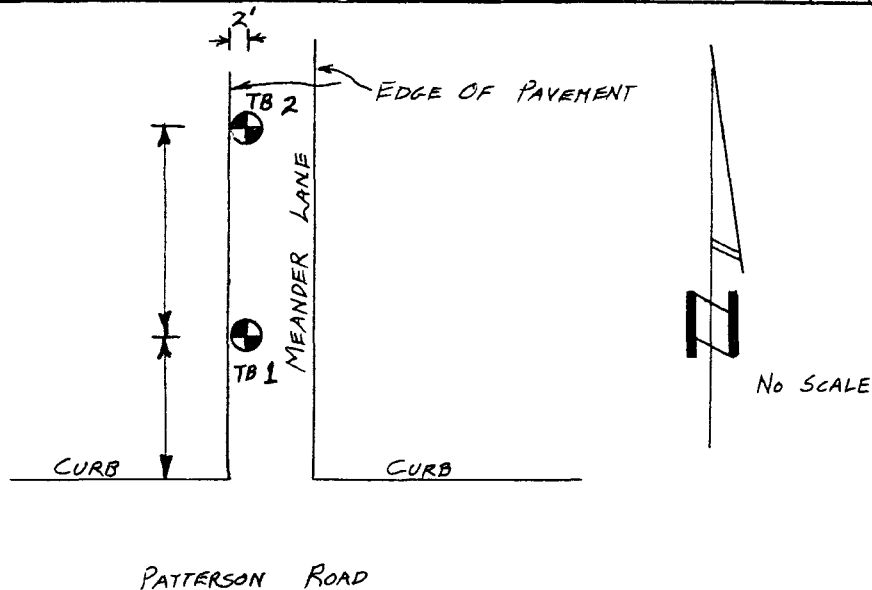
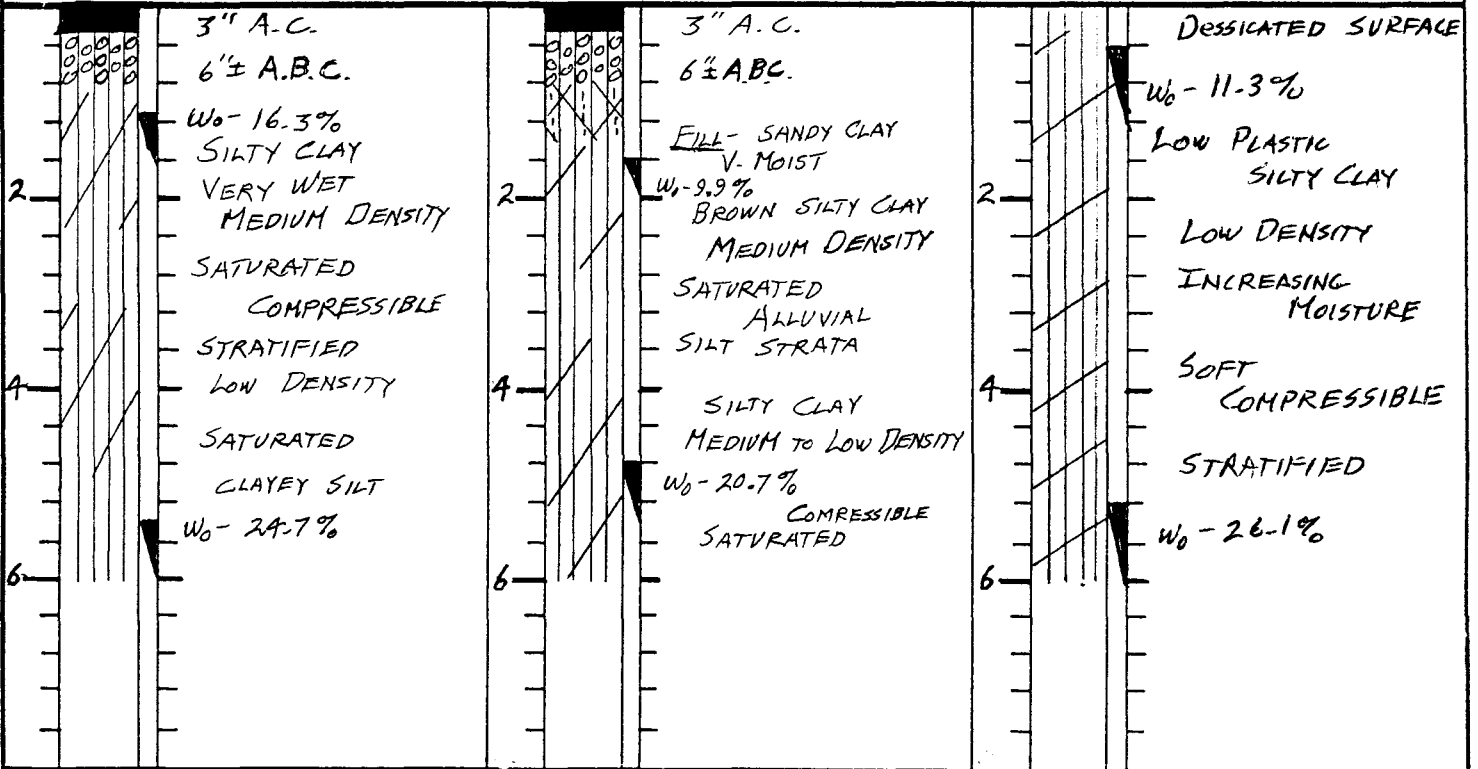
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5

ELEVATION \_\_\_\_\_

PARKING LOT



LOG OF SUBSURFACE EXPLORATION

ROAD SECTION (EXISTING) - MEANDER LANE

Hi-FASHION FABRICS

DATE

7-30-92

JOB NO.

76604-J

DRAWN

EHM



Lincoln DeVore, Inc.  
Geotechnical Consultants



Lincoln DeVore, Inc.  
Geotechnical Consultants  
1441 Motor St.  
Grand Junction, CO 81505

TEL: (303) 242-8968  
FAX: (303) 242-1561

August 10, 1992

Hi Fashion Fabrics  
1938 N 1st Street  
Grand Junction, CO 81501

Re: Subsurface Soils Exploration  
Hi Fashion Fabrics  
Patterson and Meander Lane  
Grand Junction, Colorado

Dear Clients:

As requested, Lincoln-DeVore personnel have recently completed a geotechnical exploratory program at the above referenced site. Two shallow test borings were placed within the building pad to determine as closely as possible the soil types which exist beneath the proposed structure. Our conclusions and recommendations for this site are presented below.

Soil Classification: The soils on this site consist of a series of silty clay and sandy clay soils which are a product of mud flow/debris flow features which originate on the south-facing slopes of the Bookcliffs. These mud flow/debris flow features are a small part of a very extensive mud flow/debris flow complex along the base of the Bookcliffs and extending to the Colorado River. Utilizing recent events and standard evaluation techniques, this tract is not considered to be within with an active debris flow hazard area. The surface soils are an erosional product of the upper Mancos Shale and the Mount Garfield Formations which are exposed on the slopes of the Bookcliffs. The soils contained within these mud flow/debris flow features normally exhibit a metastable condition which can range from very slight to severe. Metastable soil is subject to internal collapse and is very sensitive to changes in the soil moisture content. Based on the field and laboratory testing of the soils on this site, the severity of the metastable soils can be described as low.

This Soil Type was classified as a silty clay and low-plastic clay (CL/ML) under the Unified Classification System. This material is of low plasticity, of low to moderate permeability, and was encountered in a low density, wet condition. It undergoes mild expansion with the entry of small amounts of moisture, but will undergo long-term consolidation upon the addition of larger amounts of moisture. This soil will settle after being loaded. The maximum allowable bearing capacity for this soil was

found to be 700 psf, with 150 psf minimum dead load pressure required. The finer grained portion of this soil type contain sulfates in detrimental quantities.

Man-made Fill: An extensive layer of very soft native soils was encountered on this site. These soils are of extremely low density and are not judged suitable for support of the proposed shallow foundation system. Owing to the depths to which this low density soil was encountered and the relatively shallow excavation depths anticipated, it is recommended that an overexcavation/replacement scheme be used on this site.

The existing low density soils should be removed to a minimum depth of two feet below the proposed bottom footing elevation. Once it is felt that adequate soil removal has been achieved, it is recommended that the excavation be closely examined by a representative of Lincoln-DeVore to ensure that an adequate overexcavation depth has indeed occurred and that the exposed soils are suitable to support the proposed structural man-made fill.

Once this examination has been completed, it is recommended that a coarse-grained, non-expansive, non-free draining man-made structural fill be imported to the site. This imported fill should be placed in the overexcavated portion of this site in lifts not to exceed 6 inches after compaction. A minimum of 90% of the soils maximum Modified Proctor dry density (ASTM D-1557) must be maintained during the soil placement. These soils should be placed at a moisture content conducive to the required compaction (usually Proctor optimum moisture content  $\pm$  2%). The granular material must be brought to the required density by mechanical means. No soaking, jetting or puddling techniques of any type should be used in placement of fill on this site. To ensure adequate lateral support, we must recommend that the zone of overexcavation extend at least 2 feet around the perimeter of the proposed footing. To confirm the quality of the compacted fill product, it is recommended that surface density tests be taken at maximum 2 foot vertical intervals.

The placement of a geotextile fabric for separation between the native soils and the structural fill is recommended to aid the fill placement and to improve the stability of the completed fill.

When The structural fill is completed, an allowable bearing capacity of 1700 psf maximum may be assumed for proportioning the footings.

Soil Moisture Conditions: A free water table came to equilibrium during drilling at 12 feet below the present ground surface. This is probably very close to the true phreatic surface rather than a perched water table. In our opinion the subsurface water

conditions shown are a permanent feature on this site. The depth to free water would be subject to fluctuation on this site depending upon external environmental effects.

Because of capillary rise, the soil zone within a few feet above the free water level identified in the borings will be quite wet. Pumping and rutting may occur during the excavation process, particularly if the bottom of the foundations are near the capillary fringe. Pumping is a temporary, quick condition caused by vibration of excavating equipment on the site. If pumping occurs, it can often be stopped by removal of the equipment and greater care exercised in the excavation process. In other cases, geotextile fabric layers can be designed or cobble sized material can be introduced into the bottom of the excavation and worked into the soft soils. Such a geotextile or cobble raft is designed to stabilize the bottom of the excavation and to provide a firm base for equipment.

Data presented in this report concerning ground water levels are representative of those levels at the time of our field exploration. Groundwater levels are subject to change seasonally or by changed environmental conditions. Quantitative information concerning rates of flow into excavations or pumping capacities necessary to dewater excavations is not included and is beyond the scope of this report. If this information is desired, permeability and field pumping tests will be required.

Foundation Type Recommended: Assuming that some amount of differential movement can be tolerated, then a conventional shallow foundation system, underlain by structural fill, placed in accordance with the recommendations contained within this report may be utilized. The foundation would consist of continuous spread footings beneath all bearing walls and isolated spread footings beneath all columns and other points of concentrated load. Such a shallow foundation system, resting on the properly constructed structural fill may be designed on the basis of an allowable bearing capacity of 1700 psf maximum. Recommendations pertaining to balancing, reinforcing, drainage, and inspection are considered extremely important and must be followed. Contact stresses beneath all continuous walls should be balanced to within + or - 200 psf at all points. Isolated interior column footings should be designed for contact stresses of about 150 psf less than the average used to balance the continuous walls. The criteria for balancing will depend somewhat on the nature of the structure. Single-story, slab-on-grade structures may be balanced on the basis of dead load only. Multi story structures may be balanced on the basis of dead load plus one half live load, for up to three stories.

If the design of the upper structure is such that loads can be balanced reasonably well, or as in the case of a steel-frame structure some degree of movement can be tolerated, a floating structural slab or raft type of foundation could be used on this site. Such a slab would require heavy reinforcing to resist differential bending. It is possible to design such a slab either as a solid or ribbed slab, but in either case, a rimwall must be used for confinement. Any such slab must be specifically designed for the anticipated loading. Such a foundation system will settle to some degree as the softer, underlying soils consolidate, but differential movement is held to a minimum. Because of the potential of the heavily loaded portions of the slab settling more than the non-loaded interior portions, some minor cracking and heave are possible unless the slabs are specifically designed with the movement in mind. For design purposes, the modulus of subgrade reaction for this soil may be taken as 75 pci for the native soils and 150 pci for slabs which are underlain by a granular, properly compacted structural fill, a minimum of two feet in thickness.

Reinforcing: Stem walls for a shallow foundation system should be designed as grade beams capable of spanning at least twelve feet. These "grade beams" should be horizontally reinforced both near the top and near the bottom. The horizontal reinforcement required should be placed continuously around the structure with no gaps or breaks. A foundation system designed in this manner should provide a rather rigid system and, therefore, be better able to tolerate differential movements associated with the compressible soils found on this site.

The stem wall recommendations given above apply principally to conventional masonry construction. If a rigid frame (or steel frame) building is used, the foundation configuration would probably take the form of isolated bearing pads located directly beneath the exterior wall columns with a concrete grade beam spanning from pad to pad and supporting the exterior wall. In this case, we recommend that the exterior grade beams be designed to span at least half the distance between pad to pad with a load transfer at this point. Horizontal reinforcing in the grade beams is recommended to be continuous around the building exterior with no gaps or breaks unless they are properly designed.

It is extremely important, due to the nature of data obtained by the random sampling of a nonhomogeneous material such as soil, that a shallow foundation system be used only if all recommendations are strictly followed. All the listed recommendations regarding fill compaction, site grading, drainage and subsurface water control are exceedingly important. **CAUTION :** Failure to follow these recommendations will void part or all of the recommendations contained in this report.

Floor Slabs: Floor slabs on grade, if not a part of the structural foundation system, should be positively separated from all structural portions of this building and allowed to float freely. Frequent scoring (control joints) of the slabs should be provided to allow for possible shrinkage cracking of the slab. These control joints should be placed to provide maximum slab areas of approximately 200 to 360 square feet. Any man-made fill placed below floor slabs on grade should be compacted to a minimum of 90% of its maximum Modified Proctor dry density, ASTM D-1557. These soils should be placed at a moisture content conducive to the required compaction (usually Proctor optimum moisture content +2%).

Drainage and Grading: Surface grading should be completed in such a manner that all runoff moisture is removed from the vicinity of the structure as quickly as possible. It is recommended that a minimum surface gradient of 8% be maintained away from the structure for the first 10 feet. Roof downspouts and sill cocks should be carried across all backfill areas and allowed to discharge well away from the building. All lawn sprinkling heads should be placed at least 10 feet away from the foundation. Future owners of this structure should be advised to fill in any settled yard areas to eliminate ponding of water near the structure and to provide adequate slope for proper drainage away from the structure and off the site at all times.

The existing drainage on the site must either be maintained carefully or improved. We recommend that water be drained away from structures as rapidly as possible and not be allowed to stand or pond near the building. We recommend that water removed from one building not be directed onto the backfill areas of adjacent buildings. We recommend that a hydrologist or drainage engineer experienced in this area be retained to complete a drainage plan for this site.

If adequate surface drainage cannot be maintained, or if subsurface seepage is encountered during excavation for foundation construction, a full perimeter drain is recommended for this building. It is recommended that this drain consist of a perforated drain pipe and a gravel collector, the whole being fully wrapped in a geotextile filter fabric. We recommend that this drain be constructed with a gravity outlet. If sufficient grade does not exist on the site for a gravity outlet, then a sealed sump and pump is recommended. Under no circumstances should a dry well be used on this site.

Backfill: To reduce settlement and aid in keeping water from reaching beneath this building, all backfill around this building should be mechanically compacted to 80% of its maximum Modified


Proctor dry density ASTM D-1557. The only exception to this would be the components of the perimeter foundation drain, if any. All backfill should be composed of the native soils and should not be placed by soaking, jetting or puddling. All backfill placed in utility trenches around this structure or below foundation walls should be mechanically compacted to a minimum of 90% of its maximum Modified Proctor dry density ASTM D-1557. These soils should be placed at a moisture content conducive to the required compaction (usually Proctor optimum content  $\pm 2\%$ ).

Cement Type: Type II, Type I-II or Type II-V cement is recommended for all concrete which is in contact with the soils on this site. Calcium chloride should not be added to a Type II, Type I-II or Type II-V cement under any circumstances.

Remarks: The bottoms of all exterior foundations should be located a minimum of 24 inches below finished grade for frost protection.

Respectfully submitted,

LINCOLN-DEVORE, INC.

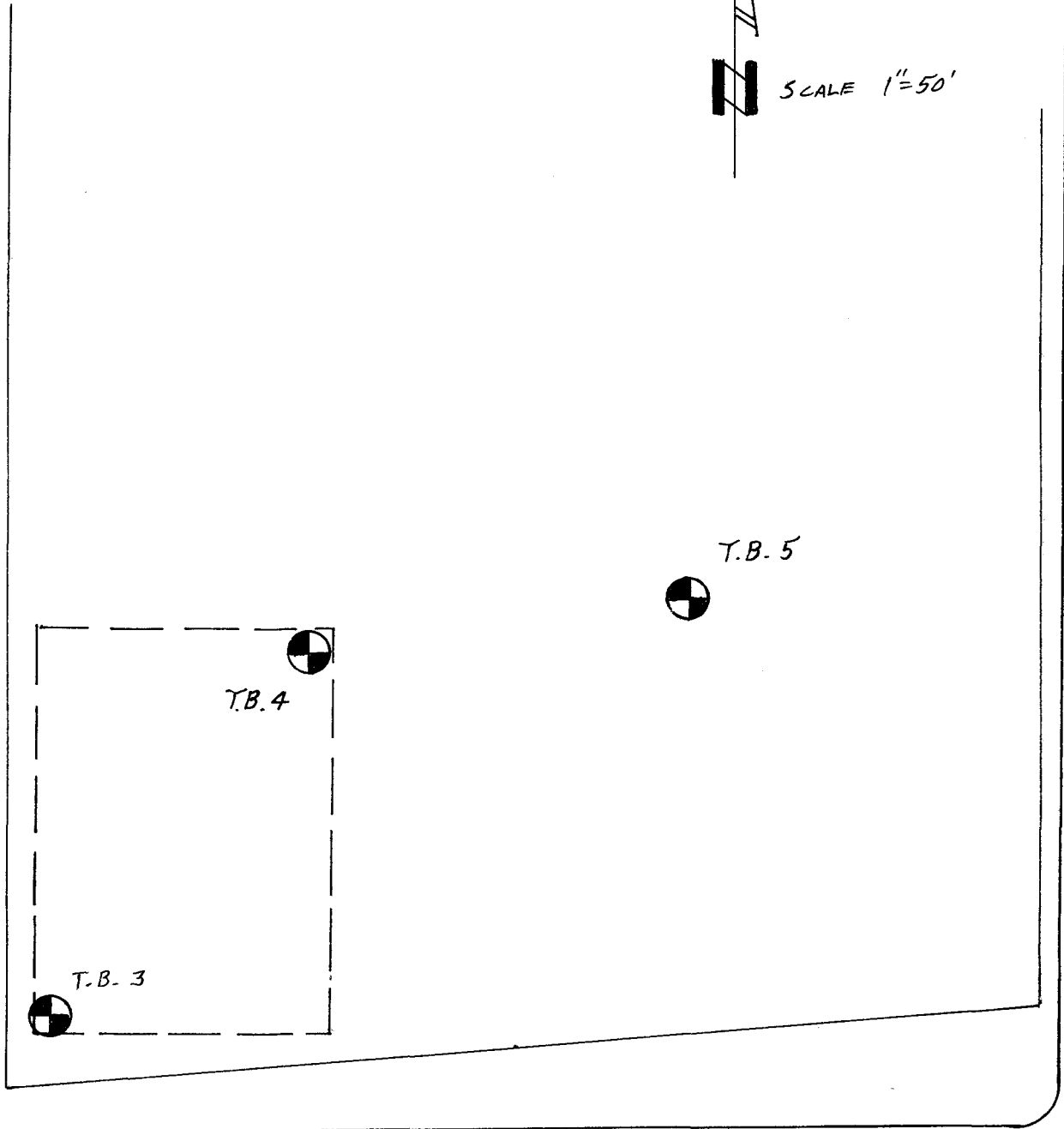
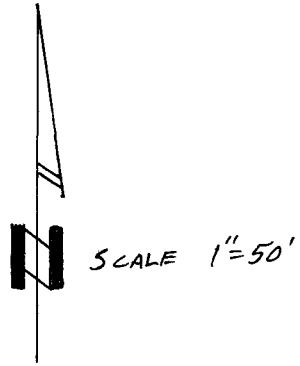
  
By: Edward M. Morris EIT  
Western Slope Manager

Reviewed by:

  
George D. Morris PE

LD Job # 76604-J





PATTERSON ROAD



TEST BORING LOCATION

HI FASHION FABRICS - 6d. Jct.

DATE 7-30-93

JOB NO. 76604-J

DRAWN EMM

TEST BORING

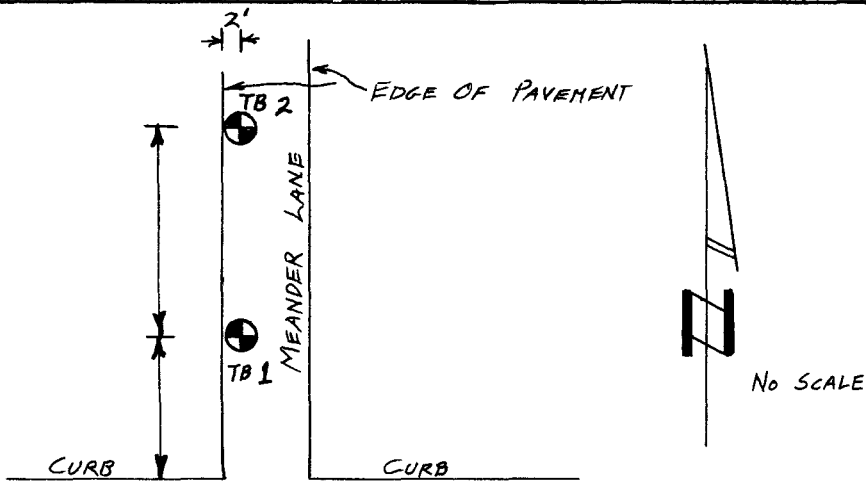
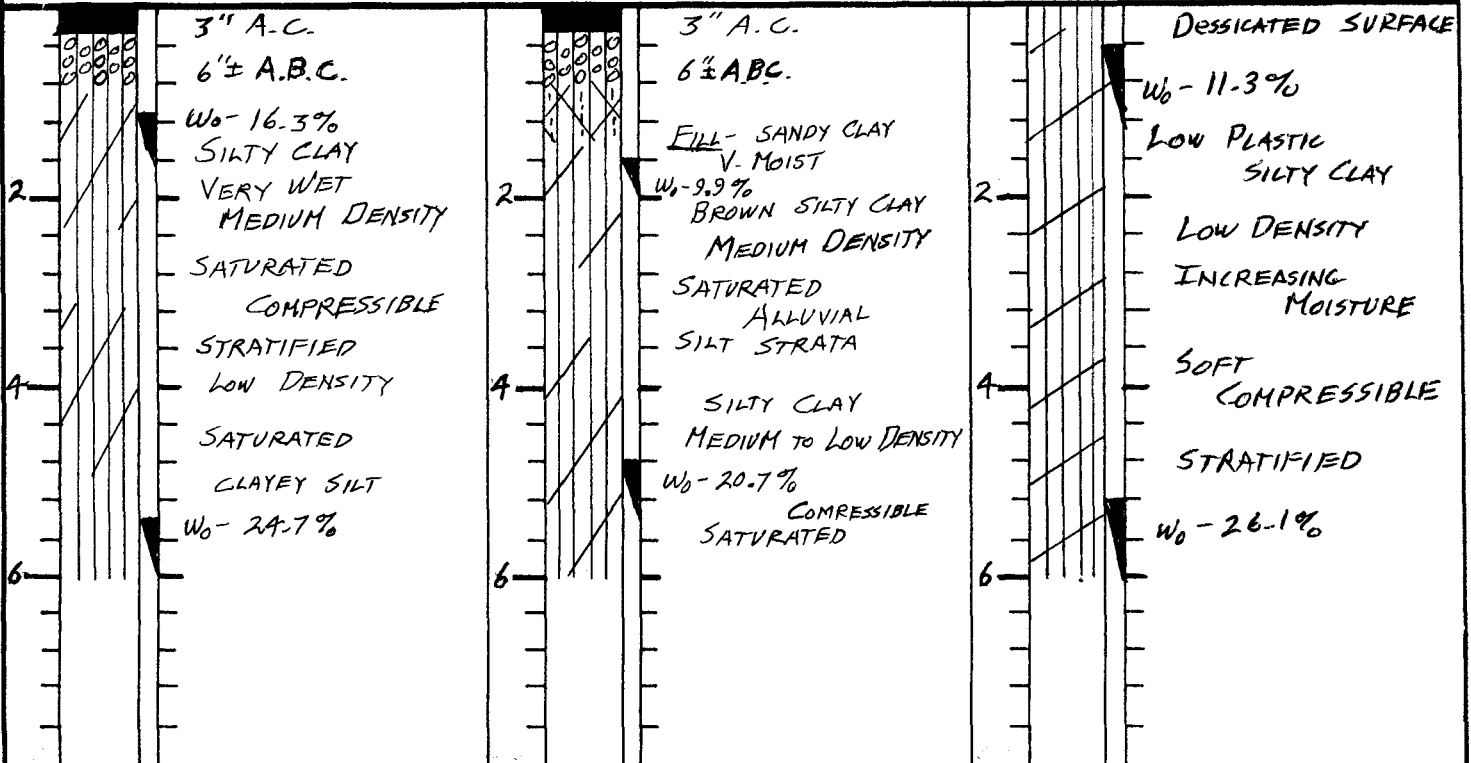
No. 1

2

5

ELEVATION \_\_\_\_\_

PARKING LOT



LOG OF SUBSURFACE EXPLORATION

ROAD SECTION (EXISTING) - MEANDER LANE

Hi-FASHION FABRICS

DATE

7-30-92

JOB NO.

78604-J

DRAWN

EHM



Lincoln DeVore, Inc.  
Geotechnical Consultants

		BORING NO. 3		PENETRATION RESISTANCE	IN-SITU DENSITY (PCF)	MOISTURE CONTENT (%)
DEPTH (FT)	SAMPLE	ELEVATION:				
	SYMBOL	DESCRIPTION				
		THIN DESSICATED SURFACE				
		LOW PLASTIC SILTY CLAYS AND CLAYEY SILTS - SOME SANDS		S.T.	106.4	25.9%
5		NEAR SATURATED - VERY HIGH SULFATE				
		LOW DENSITY - SOME CLAYEY STRATA				
		LIGHT BROWN COMPRESSIBLE SILTY CLAY & CLAYEY SILT		ST	103.2	26.2%
10		THIN SAND STRATA				
		FREE WATER DURING DRILLING		ST	112.5	26.6%
15		14' SOFT HOLE SQUEEZING SHUT				
		INCREASING SAND STRATA				
		SATURATED		ST	97.8	29.5
20		SAME AS ABOVE				
		LOW PLASTIC SILTY CLAY				
		SOFT SATURATED		BULK		23.4%
30		T.D. @ 30'				
		HIGH SULFATES				
		ALL SOILS ARE DEBRIS FLOW				

**LOG OF SUBSURFACE EXPLORATION**



Lincoln DeVore, Inc.  
Geotechnical Consultants

PATTERSON & MEANDER, GRAND JUNCTION, CO

HI FASHION FABRICS


DATE  
7-30-92

JOB NO.  
76604

DRAWN  
EMM

DEPTH (FT)	SYMBOL	SAMPLE	BORING NO. 4		PENETRATION RESISTANCE	IN-SITU DENSITY (PCF)	MOISTURE CONTENT (%)
			ELEVATION:	DESCRIPTION			
				THIN DESSICATED SURFACE			
5				SILTY CLAYS Low DENSITY Low PLASTIC SOFT TO VERY SOFT S.T. VERY HIGH SULFATE NEARLY SATURATED		92.2	29.5%
10				Low DENSITY SOME VERY SILTY STRATA SOFT COMPRESSIBLE	S.T.	99.6	27.6%
				12' FREE WATER DURING DRILLING			
15				THIN SAND STRATA - Low DENSITY CLAYS VERY STRATIFIED VERY SANDY	S.T.	110.4	27.4
20				SILTY CLAYS		107.1	25.7
25				INCREASED DENSITY - SHALE CHIPS SOME SANDSTONE FRAGMENTS AND GRAVELS			
30				SOFTER SILTY CLAYS - AS ABOVE	BULK		27.5%

**LOG OF SUBSURFACE EXPLORATION**

 Lincoln DeVore, Inc. Geotechnical Consultants	PATTERSON & MEANDER, GRAND JUNCTION, CO.	
	HI FASHION FABRICS	DATE 7-30-92
	JOB NO. 76604	DRAWN EMM

SUMMARY SHEET

Soil Sample LOW PLASTIC CLAY-SILTY (CL-ML)

Test No. 76604

Location HI FASHION FABRIC - PATTERSON ST.

Date 7-30-92

Boring No. 4 Depth 8'

Sample No. I

Test by J.S.

Natural Water Content (w) 27.4 %  
Specific Gravity (Gs) 2.63

In Place Density ( $\gamma_o$ ) 99.6 pcf

SIEVE ANALYSIS:

Sieve No.	% Passing
1 1/2"	
1"	
3/4"	
1/2"	
4	100
10	99.9
20	98.8
40	99.4
100	90.5
200	78.2

HYDROMETER ANALYSIS:

Grain size (mm)	%
.02	47.6
.005	29.9

Plastic Limit P.L. 15.9 %  
Liquid Limit L.L. 22.1 %  
Plasticity Index P.I. 7.2 %  
Shrinkage Limit \_\_\_\_\_ %  
Flow Index \_\_\_\_\_  
Shrinkage Ratio \_\_\_\_\_ %  
Volumetric Change \_\_\_\_\_ %  
Lineal Shrinkage \_\_\_\_\_ %

MOISTURE DENSITY: ASTM METHOD

Optimum Moisture Content -  $w_o$  \_\_\_\_\_ %  
Maximum Dry Density -  $\gamma_d$  \_\_\_\_\_ pcf  
California Bearing Ratio (av) \_\_\_\_\_ %  
Swell: \_\_\_\_\_ Days \_\_\_\_\_ %  
Swell against \_\_\_\_\_ psf  $W_o$  gain \_\_\_\_\_ %

BEARING:

Housel Penetrometer (av) \_\_\_\_\_ psf  
Unconfined Compression (qu) \_\_\_\_\_ psf  
Plate Bearing: \_\_\_\_\_ psf  
Inches Settlement \_\_\_\_\_  
Consolidation % under psf

PERMEABILITY:

K (at 20°C) \_\_\_\_\_  
Void Ratio \_\_\_\_\_

Sulfates 2000+ ppm.

SOIL ANALYSIS

LINCOLN-DeVORE TESTING LABORATORY  
COLORADO SPRINGS, COLORADO

SOIL SAMPLE \_\_\_\_\_

Test No. 76604-J

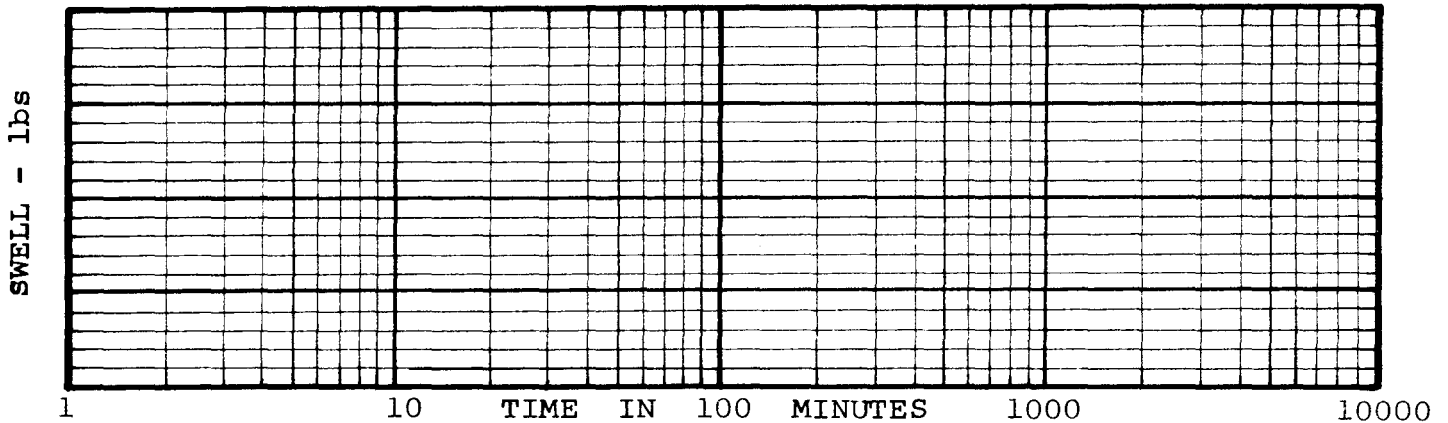
Project HI FASHION FABRICS - PATTERSON ROAD

Date 7-30-92

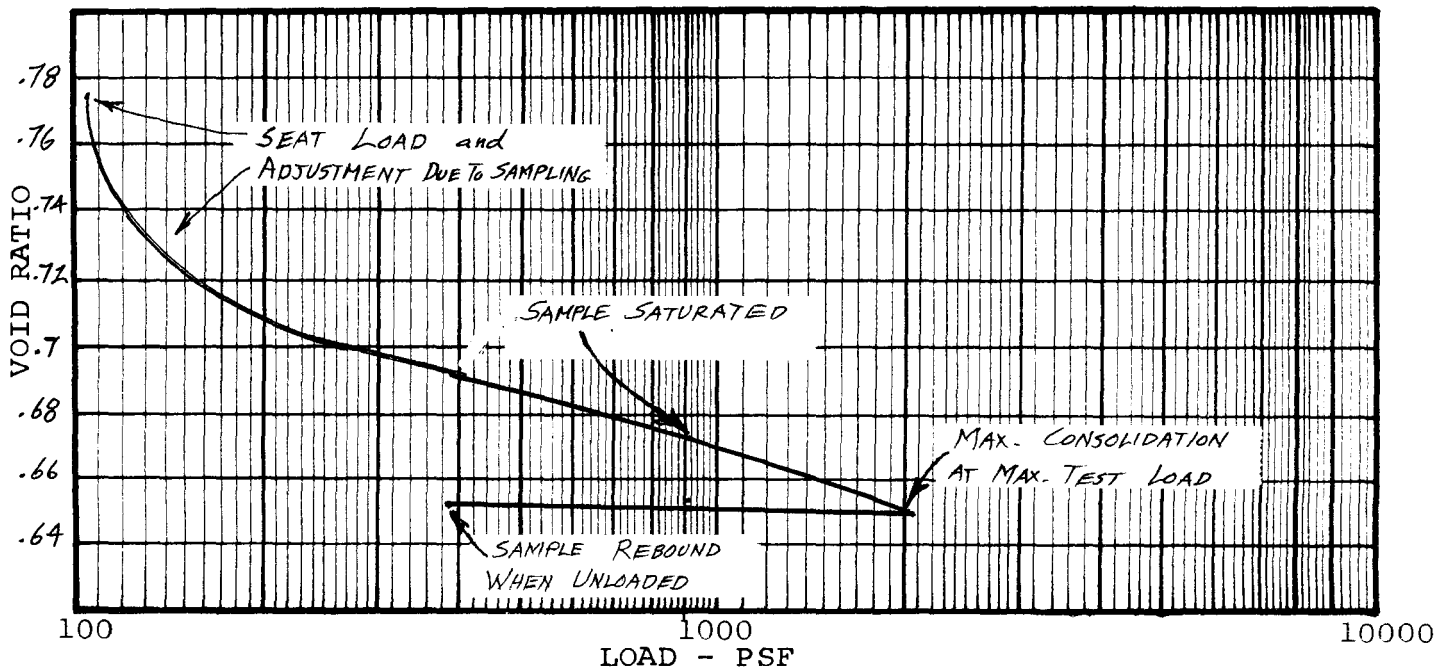
Sample Location T.H. # 4 @ 3'

Test by JS

SWELL



CONSOLIDATION



Sample Conditions	Initial	Maximum Load	Expanded
Dry Density	92.2 #/ft <sup>3</sup>	99.1 #/ft <sup>3</sup>	98.9 #/ft <sup>3</sup>
% Moisture	29.5%	24.8%	24.9%
% Saturation	99.9%	100%	100%
Void Ratio	.774	.649	.653

Specific Gravity 2.62  
 Maximum Load used 2059 lb.  
 Apparatus DENSOIL 4

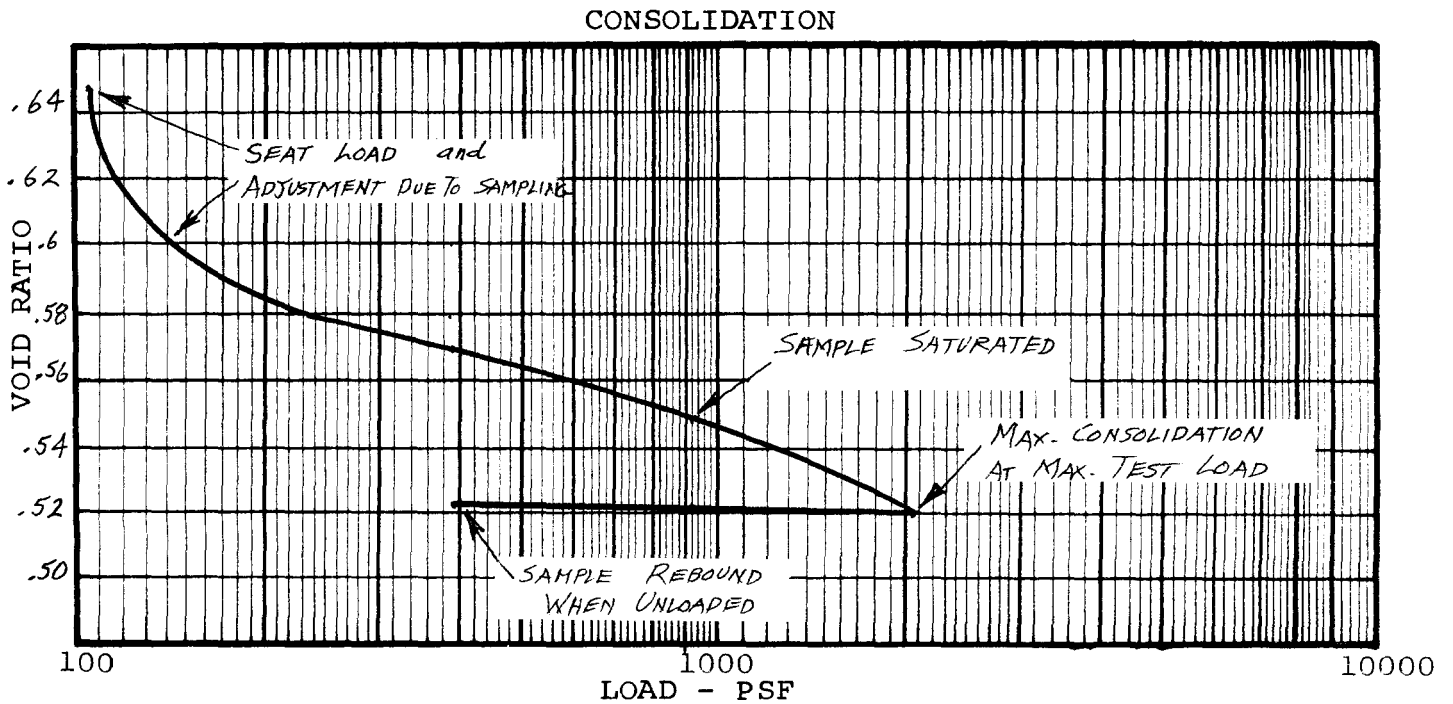
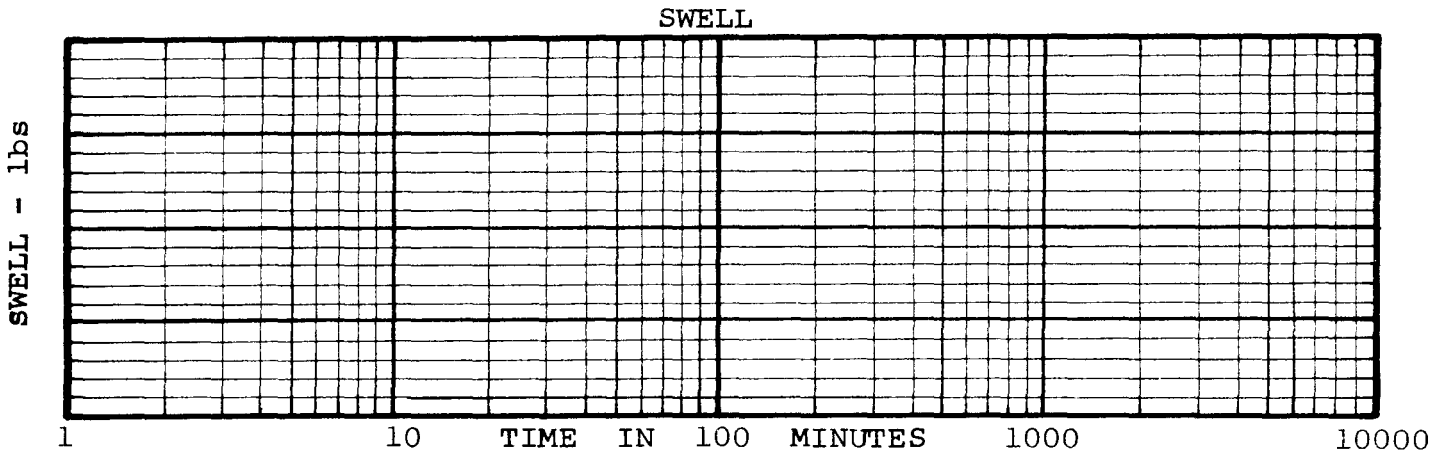
Ring Number 143-1  
 Volume 2.5" Ring .002841 cu. ft.

LOAD - CONSOLIDATION

LINCOLN-DeVORE, INC.  
 COLORADO SPRINGS, COLORADO

SOIL SAMPLE \_\_\_\_\_  
 Project HI FASHION FABRICS PATTERSON ROAD  
 Sample Location T.H. # 4 @ 8'

Test No. 76604-J  
 Date 7-30-92  
 Test by JS



Sample Conditions	Initial	Maximum Load	Expanded
Dry Density	99.6 #/ft <sup>3</sup>	108.0 #/ft <sup>3</sup>	107.8 #/ft <sup>3</sup>
% Moisture	27.4%	19.8%	19.9%
% Saturation	100%	100%	100%
Void Ratio	.648	.520	.522

Specific Gravity 2.63  
 Maximum Load used 2042 lb.      Ring Number 144-39  
 Apparatus DENSOIL 2      Volume 2.5" Ring -002841 cu. ft.

LOAD - CONSOLIDATION

LINCOLN-DEVORE, INC.  
 COLORADO SPRINGS, COLORADO







City of Grand Junction, Colorado  
250 North Fifth Street  
81501-2668  
FAX: (303) 244-1599

September 1, 1992

Mr. Jeff Vogel  
1938 N. 1st Street  
Grand Junction, CO 81501

Re: Hi-Fashion Fabrics

Dear Jeff:

The plans for Hi-Fashion Fabrics have been approved for construction. We now request that the following information be submitted for site work (not buildings) as soon as possible:

- (i) Construction schedule;
- (ii) List of contractors to be used;
- (iii) Testing laboratory that will provide materials and other testing; and
- (iv) Name of developer's designated inspector.

In addition to the above, Walt Hoyt at 244-1577 or 244-6232 (mobile) should be called for inspection for the various stages of construction as outlined on the attached form which will be used to keep track of construction inspection and approvals.

If you have any questions regarding the above, please call.

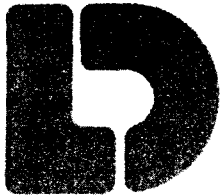
Sincerely,

A handwritten signature in cursive script that reads "Gerald R. Williams".

Gerald R. Williams, P.E.  
Development Engineer

Attachment

xc: Don Newton, City Engineer  
Karl Metzner, Planner ✓  
File



Lincoln DeVore, Inc.  
Geotechnical Consultants  
1000 West Fillmore St.  
Colorado Springs, CO 80907

Planning Dept.'s Copy (2)

TEL: (719) 632-3593  
FAX: (719) 632-2648

November 11, 1992

Hi Fashion Fabrics  
1938 North 1st Street  
Grand Junction, CO 81501

Attn: Mr. Jeff Vogel

Re: Hydrologic Analysis, High Fashion Fabrics, Patterson  
and Meander Lane, Grand Junction, Colorado

Dear Mr. Vogel:

As requested, Lincoln DeVore has investigated runoff conditions at the proposed High Fashion Fabrics site at the intersection of Patterson and Meander Lanes in Grand Junction, Colorado. This analysis was completed in November, 1992, and consisted of analyzing the historic 2-year and 100-year runoff at the site outlet, together with the developed 2- and 100-year runoff at the site outfall. The proposed internal drainage and parking area storage was computed to determine the holding capacity and means to allow developed runoff from the site which will not exceed historic rates.

Scope and Sources:

The purpose of the analysis was to size proposed outlets from the site which restrict outflow runoff to the equivalent historic rates. The analysis was based on the "Interim Outline of Grading and Drainage Criteria" obtained from the City Engineering Office of Grand Junction, Colorado. We understand that the copy obtained is not yet in its final form, but the basic outline of procedure appears to be complete. The results obtained following the Grand Junction criteria were checked using methods outlined in CUHP, Vols. 1 and 2. Information concerning soil drainage characteristics was taken from Soil Conservation Service and U. S. Geological Survey publications, and was corroborated by information from geotechnical work performed in the area by Lincoln DeVore.

Coefficients for the Rational Method, n values and Intensity, Duration, Frequency Values used herein were taken from Appendices attached to the Interim Grading and Drainage Criteria, Grand Junction, Colorado. We understand that the Criteria requires design of outlets for the 2-year runoff and the 100-year runoff so that the equivalent "historic" flow is not exceeded through

this range. The project site and contributing basin areas are small. Therefore, the modified Rational Formula method was used for these calculations.

Site Description:

The site is located in the northwesterly portion of Grand Junction, at the northwest corner of the intersection of Patterson (F Road) and Meander Lane. The project site consists of a mild, low gradient slope toward Patterson. This area was fed by a small basin to the north which lies on the south slope of a low northeast-southwest trending hill. The slopes in this area are steeper than those found on the project site. Most runoff from the higher area consisted of overland sheetflow with some runoff carried in shallow swales. Predevelopment topography forced runoff into sheetflow and shallow swales, so that concentration time was relatively slow.

Development of the area has changed runoff directions somewhat. The attached basin map divides the area into four subbasins. Subbasin A flows generally south, to an outfall a short distance west of the project site, and included a strip of land in the western portion of the project site. The majority of the project site (Subbasin C) received runoff from Subbasin B on the slope north of the project site. Construction of Meander Lane cut off the upper portion of Subbasin A, adding this runoff to runoff from Subbasin B along Meander lane. In effect, this runoff and the runoff from Subbasin B has been cut off from feeding the project site, and carries runoff along Meander Lane to its intersection with Patterson. In addition, drainage changes on the project site have reclaimed most of the runoff from the site which originally added to Subbasin A. For all practical purposes, developed runoff from the project site consists only of the precipitation falling directly on the site.

At the time of our observations of the site, some runoff was noted to have escaped from Meander Lane and entered the project site. Without any available method of measurement, the amount of this escape could not be determined. In our opinion, Meander Lane should be improved to contain all runoff from Subbasins A2 and B. The Mesa County Canal, running along the northerly property line of the project site, has been converted to a piped system and has been covered. For this reason, the lateral cannot be utilized to accept runoff water at this site.

Soil Conditions:

The soils on the site are described by the U.S.G.S. as residually weathered clays derived from the Mancos Shale, occasionally covered with Piedmont deposits consisting of clayey sands and gravels. The Soil Conservation Service describe the soils as being variations of Fruita and Ravola Loams and Gravelly Loams. Their classification shows these site soils in Subbasins A2, B and C (project site) as being in Hydrologic Group B. Coefficients for use in both the "historic" analysis and in the developed analysis were taken from the Grand Junction Criteria based on the S.C.S hydrologic classification of "B". Development on site will cover most of the site with roof areas, paved areas and landscaped areas. Coefficients for each of these conditions were taken from the Grand Junction Criteria.

Historic Runoff:

The time of concentration for each of the subbasins was calculated based on overland flow not to exceed 300 feet, added to swale flow times to the outfall point at Patterson. Examination of the subbasins indicated that most runoff was either sheetflow (overland) or concentrated in shallow, relatively wide swales on the hillside, expanding in width and reducing in depth at the lower project site gradients. Therefore, the time of concentration for "historic" flow was relatively long to the point of outfall. The historic peak flow found by the modified Rational Formula varied from 0.235 cfs for the 2-year runoff to 1.66 cfs for the 100-year runoff.

Developed Runoff:

The time of concentration for the project site runoff in the developed condition is relatively short, since much of the area will be paved or roofed. Conversely, the gradient overall has been reduced. In this manner, the time of concentration is not reduced as much as if the original gradients had not been lowered. The coefficients for the formula were increased to fit the paved and landscaped conditions. The developed peak flows found by the modified Rational Formula varied from 1.69 cfs for the 2-year runoff to 5.59 cfs for the 100-year runoff.

The geometry of the project site was maintained as designed. This plan was given to Lincoln DeVore for our use in developing the proper sizes for runoff systems. Other than some minor changes in grade, the plan was used as given to us. In this manner, the desired site layout could be preserved with few changes.

As designed, the parking area is to be constructed as a basin, graded to a subsurface pipe outfall system leading to the City drainage system at Meander and Patterson. The pipe system is to be constructed as a 6-inch PVC outlet pipe end, covered with a restricting plate orifice as required. The runoff will collect in the parking area and be carried by surface grades to a drop inlet covered with a City Standard "street strength" grated cover, then entering the system. The volumetric capacity of the parking lot was computed at ascending elevations of 0.2 feet, from the grate at elevation 2.55 to the high point elevation of 4.0.

Computations show that this system will restrict runoff to "historic" levels for the 2-year to 10-year runoff. It was further determined that this system will not satisfactorily extend to the 50-year and 100-year runoff. Therefore, a higher level outfall was found to be required. The topography of the site is such that an upper level pipe system cannot be easily designed. In our opinion, a small concrete weir set at a parking lot elevation of 0.5 feet below the highest elevation of the parking lot will add to the ongoing runoff taken by the pipe system, to allow discharge of the 100-year runoff without exceeding the "historic" 100-year runoff.

The required size of the plate orifice to cover the pipe system outfall was found to be a round orifice with a diameter of 2.36 inches. This will provide "historic" discharge at the 2-year runoff level (or less) until water level in the parking lot reaches the critical elevation of 3.42. Above this level, a weir with a bottom level 1-1/2 foot in length with side slopes of 5:1 (horizontal to vertical) will provide additional outfall to the level of the 100-year "historic" runoff if the bottom of the weir opening is set at elevation 3.50.

#### Conclusions:

The geometry of the site restricts the use of a double pipe system or a riser system to a large degree, although such a system is possible. In our opinion, the system described in the report above will maintain the "historic" runoff from the site for storms ranging from very small to a 100-year runoff, and will better fit the geometry of the site.

Also, in our opinion, the developed site as shown on the attached map is capable of storing the runoff for the required range of storms with overflow only at the points designated and sized.


Patterson and Meander Lane  
November 11, 1992  
Page -5-


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This opportunity to be of professional service is sincerely appreciated. If you have any questions or require additional information, please feel free to contact the undersigned engineer at your convenience.

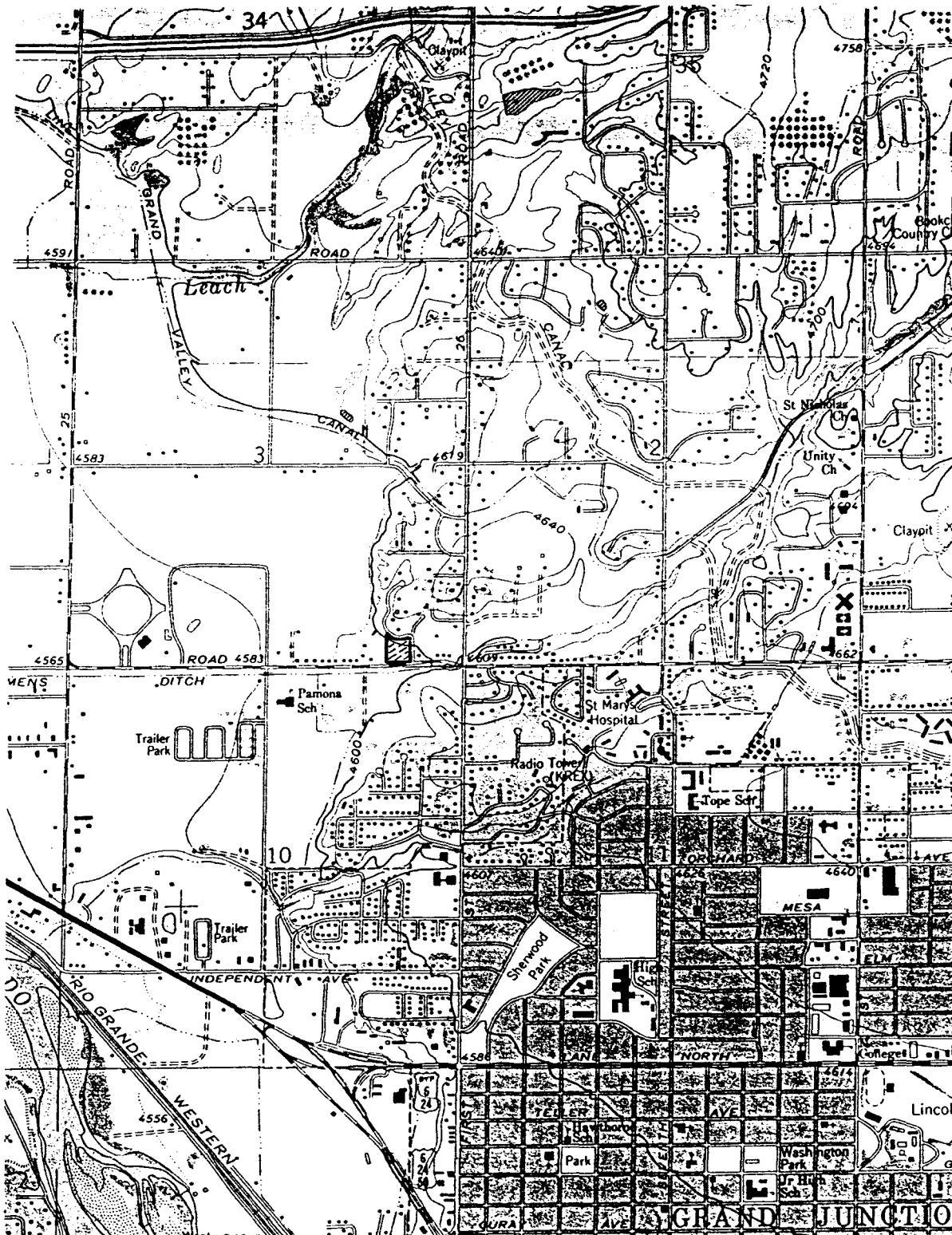
Respectfully submitted,

LINCOLN DeVORE, INC.

  
By: George D. Morris, P.E.

  
Reviewed by: Edward M. Morris

GDM/lab  
LD Job No. 76604-J  
Enclosures  
cc: Lincoln DeVore, Grand Junction



SCALE ~  
1" = 2000'



Lincoln DeVore, Inc.  
Geotechnical Consultants

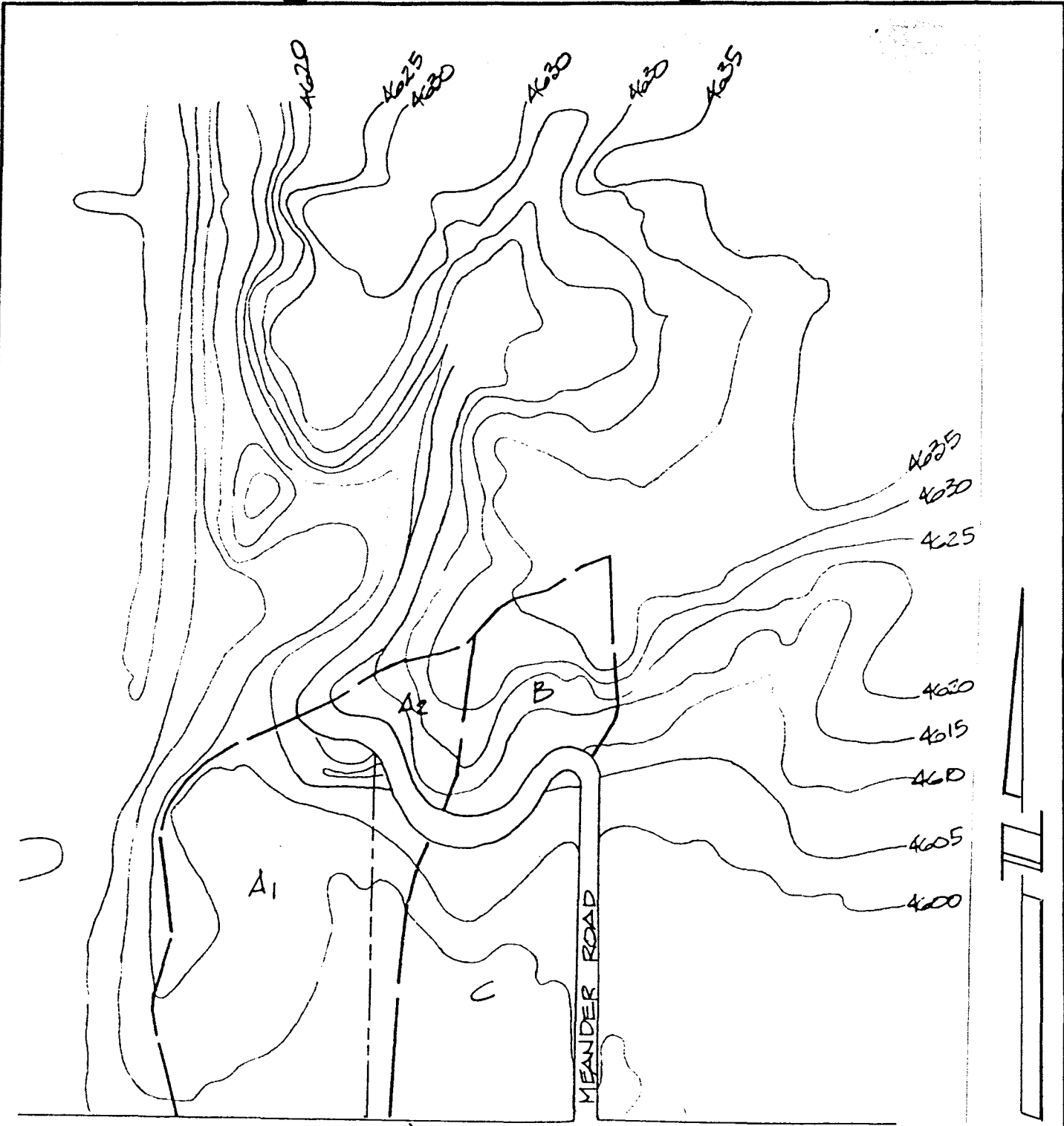
Patterson and Meander Lane, Grand Junction

Hi Fashion Fabrics

DATE 11/11/92

JOB NO.  
76604-J

DRAWN  
GDM



F ROAD (PATTERSON)

AREA BASIN MAP

1" = 200'



Lincoln DeVore, Inc.  
Geotechnical Consultants

Patterson and Meander Lane, Grand Junction

Hi Fashion Fabrics

DATE 11/11/92

JOB NO.  
76604-J

DRAWN  
KD/GDM



## APPENDIX A

### **Basic Data:**

#### Soil Types in Site Area by SCS Classification:

- Fa - Fruita and Ravola Gravelly Loams, 2-5%. Alluvial fans and some gravel terrace.  
Derived from Kmc, Hydro Class B
- Fc - Fruita and Ravola Loams, 2-5%. Derived from Kmc. Hydro Class B
- Ra - Ravola Clay Loam, 0-2%. Alluvium and Kmc. Hydro Class B

#### West of Site:

- Ba - Billings Silty Clay, 0-2%, Derived from Kmc. Hydro Class C

#### Soil Types by U.S.G.S. Classification:

- Qp - Pediment deposits, clayey silts, sands and gravels, slope wash Kmc. Hydro Class B to C.
- Qr - Weathered shale, silty and clayey residual deposit on Kmc. Hydro Class C.

None of these soils are listed as hydric.

### **Runoff Notes:** (see map for subbasin locations)

Subbasin A1 and A2 historically drained to F Road (Patterson) immediately west of the project site.

Subbasin B historically drained to F Road across Subbasin C (project site).

Construction of Meander changed this by cutting off drainage from A2, combining it with Subbasin B and conducting drainage to F Road at Meander (east of the project site).

In effect, Meander isolates the project site from incoming flow unless the curb or side ditch on Meander cannot carry this runoff. Observation indicates some water crosses onto the project site from Meander at the present time. This water should be carried by Meander to F Road.

Historic flow, therefore, is the combination of Subbasins B and C (the project site). For all practical purposes, Subbasin C consists of the entire project site.

The Developed Flow, however, consists only of Subbasin C, the project site. Subbasins A2 and B are intercepted by Meander and carried to F Road. The west line of the (historic) C Basin is changed by a collector to bring the entire Basin into a single site--minor change at west property line.

Grand Junction rules limit Std. Tc form to 300'. Tc will then equal the sum of overland and swale flow velocities. Areas are quite small, so qp will be small.

**Historic Flow:**

Basin C: A = 2.10 ac., total L = 470', total H = 23', Av. S = 0.0657, 2-yr. storm, C = 0.1

2-year: Overland L = 160' S = 9/160 = 0.0563  
Swale L = 310' S = 4/310 = 0.0129

Swale in C - assume rounded, b = 10', d = 0.25'

$$\text{then: } V = \frac{1.486}{0.1} \times 0.35106 \times 0.1664 = 0.868 \text{ fps}$$

$$\begin{aligned} T_{c_2} = \text{overland} &= 1.87 (1.1-0.1) 160^{.5} \times 5.63^{-.33} = 13.4 \text{ min.} \\ \text{swale} &= 310/0.868 = 357/60 = \underline{6.0 \text{ min.}} \end{aligned}$$

$$T_{c_2} \text{ at outfall} = 19.4 \text{ min.}$$

$$Q_2 = 0.1 \times 1.12 \times 2.10 = 0.235 \text{ cfs}$$

100-year:

Swale in C - b = 10', d = 0.30' rounded bottom

$$\text{then: } V = \frac{1.486}{0.1} \times 0.45846 \times 0.1664 = 1.13 \text{ fps}$$

$$\begin{aligned} T_{c_2} = \text{overland} &= 1.87 (1.1-0.25) 160^{.5} \times 5.63^{-.33} = 11.4 \text{ min.} \\ \text{swale} &= 310/1.13 = 274/60 = \underline{4.6 \text{ min.}} \end{aligned}$$

$$T_{c_{100}} \text{ at outfall} = 16.0 \text{ min.}$$

$$Q_{100} = 0.25 \times 3.17 \times 2.10 = 1.66 \text{ cfs}$$

**Developed Flow:**

Roof Area	= 11,250 ft. <sup>2</sup> , C2 = 0.90 C100 = 0.95 )	
Concrete	= 1,880 ft. <sup>2</sup> , C2 = 0.90 C100 = 0.95 )	Total = 0.88 ac.
A/C	= 25,340 ft. <sup>2</sup> , C2 = 0.90 C100 = 0.95 )	
Landscaped	= 15,024 ft. <sup>2</sup> , C2 = 0.15 C100 = 0.30	0.35 ac.
Rough Landscape	= 37,897 ft. <sup>2</sup> , C2 = 0.45 C100 = 0.60	0.87 ac.

Then:

$$\text{Composite C2} = (0.90 \times 0.88 + 0.35 \times 0.15 + 0.87 \times 0.45) / 2.10 = 0.589, \text{ use } 0.59$$

$$\text{Composite C100} = (0.95 \times 0.88 + 0.30 \times 0.35 + 0.60 \times 0.87) / 2.10 = 0.697, \text{ use } 0.70$$

Subbasin C

slight difference in swale flow due to grade lowering and widening

Then:

2-year flow:

$$\begin{aligned} T_{c_2} = \text{overland} &= 1.87 (1.1-0.59) 160^{.5} \times 5.63^{-.33} = 6.82 \text{ min.} \\ \text{"swale"} &= 310/0.882 = 351/60 = \underline{5.85 \text{ min.}} \end{aligned}$$

$$T_{c_2} \text{ at outfall} = 12.67 \text{ min.}, \text{ use } 13 \text{ min.}$$

$$Q_{p_2} = 0.59 \times 1.36 \times 2.10 = 1.69 \text{ cfs}$$

100-year flow:

$$\begin{aligned} T_{c_{100}} \text{ overland} &= 1.87 (1.1-0.70) 160^{.5} \times 5.63^{-.33} = 5.35 \text{ min.} \\ \text{"swale"} &= 310/1.19 = 261/60 = \underline{4.34 \text{ min.}} \end{aligned}$$

$$T_{c_{100}} \text{ at outfall} = 9.69 \text{ min.}, \text{ use } 10 \text{ min.}$$

$$Q_{p_{100}} = 0.70 \times 3.50 \times 2.10 = 5.59 \text{ cfs}$$

Parking Area Storage: (note: islands are painted, not raised curbs)

Comment	Elev.	Form = $[Ax+Ag+1+(AxAg+1)^.5] h/3$	Cum. Volume
Flow Line, Outlet	00.71	--	--
C orifice & pipe	01.04	--	--
Top manhole grate	02.55	start with volume in C.B. above	5 ft. <sup>3</sup>
	02.60	$.05/3 [3 + 132 + (3 \times 132)^.5]$	8 ft. <sup>3</sup>
	02.80	$.2/3 [132+628 + (132 \times 628)^.5]$	78 ft. <sup>3</sup>
	03.00	$.2/3 [628+1424+ (628 \times 1424)^.5]$	278 ft. <sup>3</sup>
	03.20	$.2/3 [1424+2788+(1424 \times 2788)^.5]$	692 ft. <sup>3</sup>
Anticipate spillway	03.40	$.2/3 [2788+4816+(2788 \times 4816)^.5]$ $d_2$	1443 ft. <sup>3</sup>
	03.60	$.2/3 [4816+7596+(4816 \times 7596)^.5]$	2674 ft. <sup>3</sup>
	03.80	$.2/3 [7596+10544+(7596 \times 10544)^.5]$ $d_{100}$	4480 ft. <sup>3</sup>
Top of parking lot	04.00	$.2/3 [10544+14392+(10544 \times 14392)^.5]$	6964 ft. <sup>3</sup>
	04.20	$.2/3 [14392+16692+(14392 \times 16692)^.5]$	10.070 ft. <sup>3</sup>

Summary:

Basin	Area	2-vr Historic		100-vr Historic		Developed					
		Tc <sub>2</sub>	qp2	Tc <sub>100</sub>	qp100	Tc <sub>2</sub>	qp2	C	Tc <sub>100</sub>	qp100	C
C	2.10 ac.	20 min	.235	16 min	1.66	13 min	1.69	.59	10 min	5.59	0.70
			cfs		cfs		cfs			cfs	

Basin C:

2-year Storm: Q<sub>o</sub> orifice only - .75 x .235 = .176

$$Td_2 = [633.4 \times .59 \times 2.1 / (.176 - .176^2 \times 13 / (81.2 \times .59 \times 2.1))]^{.5} - 15.6 = 51.95$$

$$Id_2 = 40.6 / (51.95 + 15.6) = .601''/\text{hr.}$$

$$Qd_2 = .59 \times 2.1 \times .601 = .745 \text{ cfs}$$

$$K = 20/13 = 1.538$$

$$V = 66 [ .745 \times 51.95 - .176 \times 51.95 - .176 \times 13 + 1.538 \times .176 \times 13 / 2 + .176^2 \times 13 / (2 \times .745) ] = 1934 \text{ ft.}^3$$

100-year Storm: Q<sub>o</sub> - will probably need spillway for this = .65 x 1.66 = 1.079

$$Td_{100} = [2925 \times .70 \times 2.1 / (1.079 - 1.079^2 \times 10 / (234 \times .70 \times 2.1))]^{.5} - 25 = 39.1 \text{ min.}$$

$$Id_{100} = 117 / (39.1 + 25) = 1.825''/\text{hr.}$$

$$Qd_{100} = .70 \times 2.1 \times 1.825 = 2.683 \text{ cfs}$$

$$K = 16/10 = 1.60$$

$$V = 66 [ 2.683 \times 39.1 - 1.079 \times 39.1 - 1.079 \times 10 + 1.6 \times 1.079 \times 10 / 2 + 1.079^2 \times 10 / (2 \times 2.683) ] = 4140 \text{ ft.}^3$$

Orifice Outlet:

C orifice = elev. 01.04, grate elev. = 02.55 . 1.51' head exists in catch basin.

Take H pond = H head above this.

$$Q = CA (2gH)^{.5} \quad \text{Max. Q allowable} - 0.235 \text{ cfs, max. H} = 2.96' \text{ above C of orifice}$$

$$\text{Then: } .235 = .60A (64.4 \times 2.96)^{.5} \text{ or } A = .235 / 8.284 = 0.02837 \text{ ft.}^2 \text{ } d = 2.28''$$

and: 2-year critical elevation in parking lot is 3.60', H = 2.56'

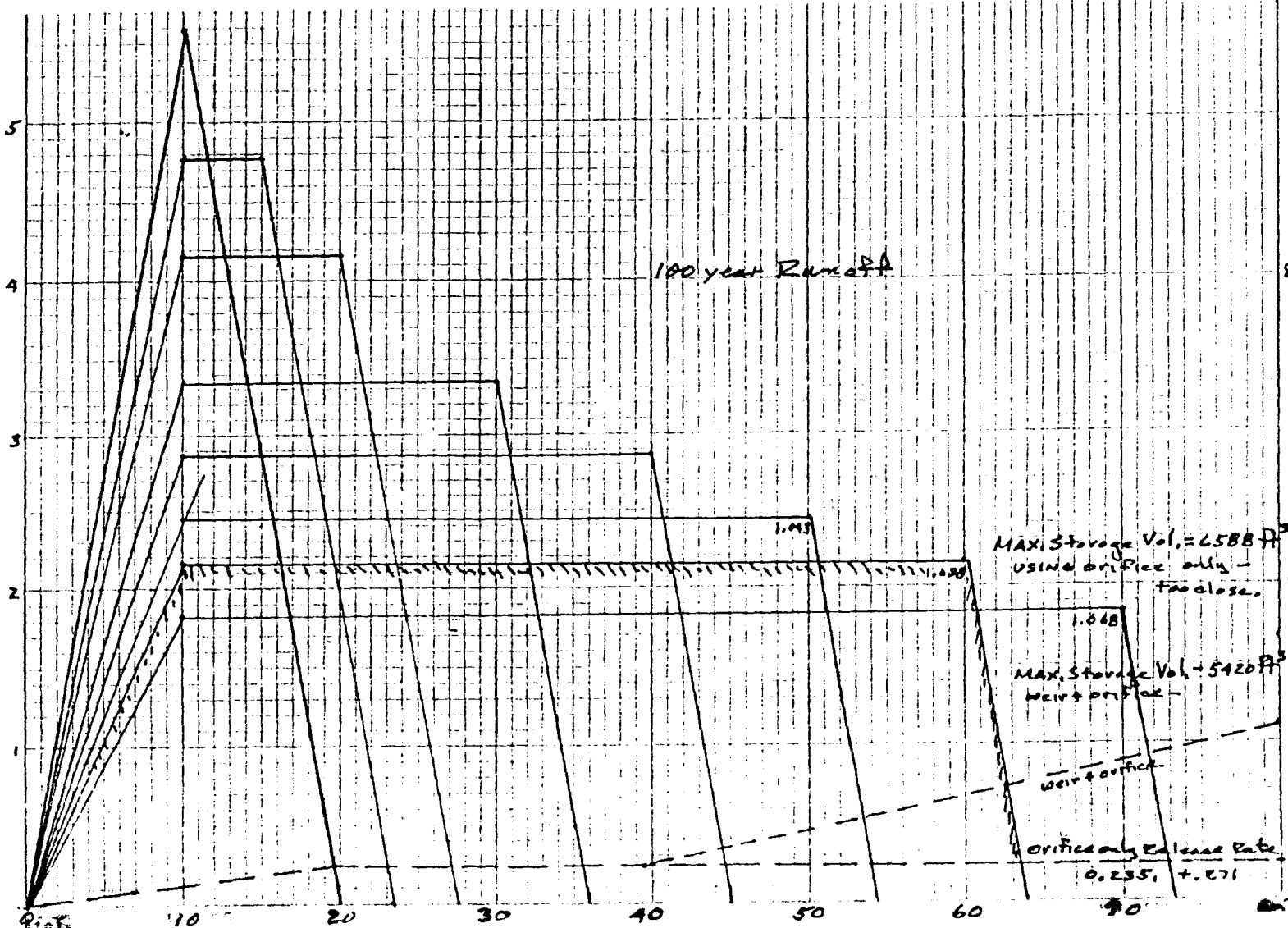
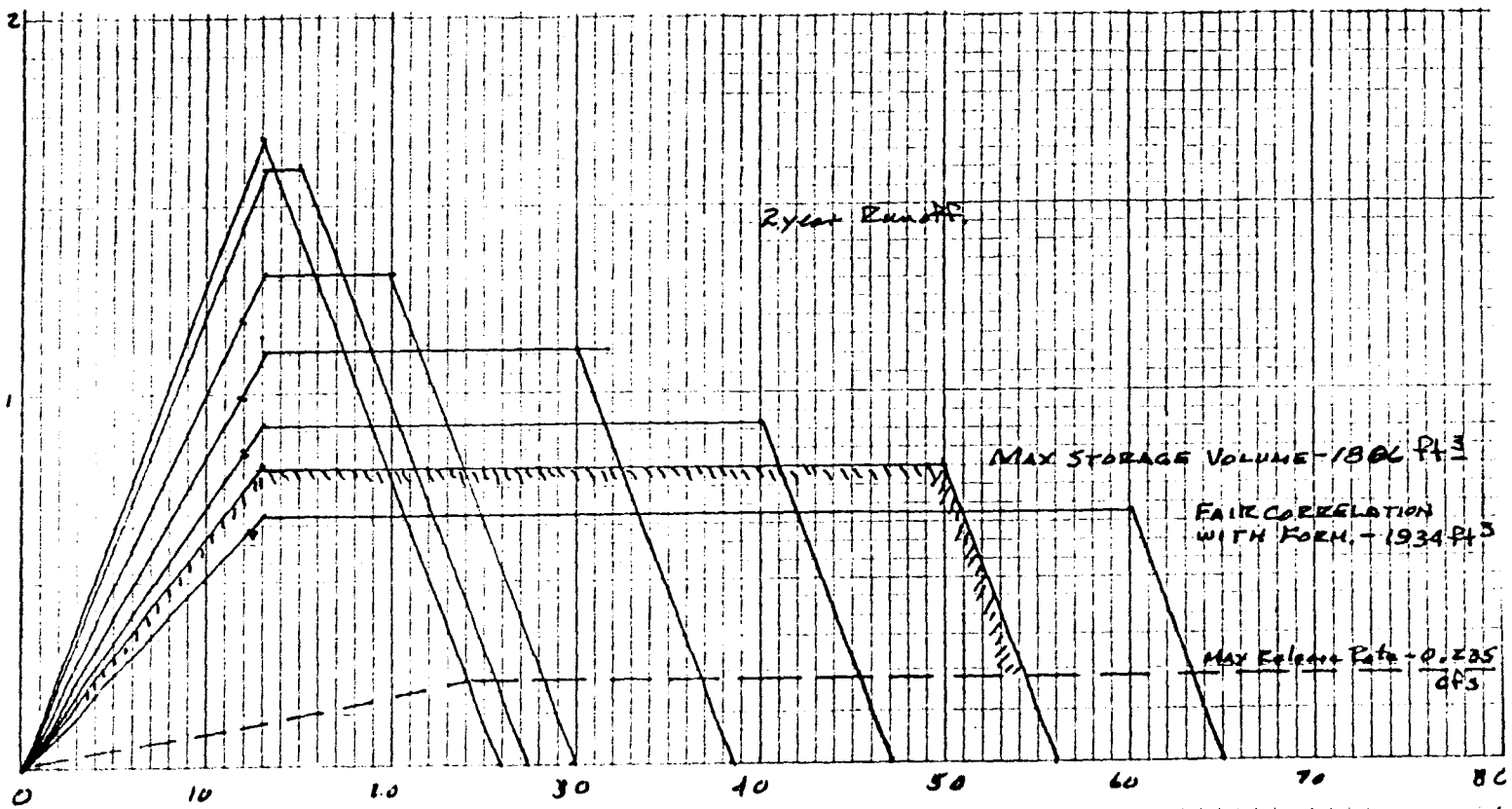
$$A = .235 / 7.7040 = 0.0305 \text{ ft.}^2$$

.0305 ft.<sup>2</sup> d = 2.36'' orifice with diameter of 2.36'' will hold historic flow at the critical elevation.

So: Overflow at various heads.

<u>Water Elevation</u>	<u>q out (cfs)</u>
2.55	.180
2.60	.183
2.80	.195
3.00	.206
3.20	.216
3.40	.226
3.60	.235
3.80	.244
4.00	.253 (top of parking lot berm)
4.20	.261

Check by CUPP / Mod. Rational Procedure:  
Che



Since CUHP Graphical Procedure indicates that parking lot may hold the 100-year flow. check this 100-year condition using  $Q_0 = .75 Q \text{ max.}$

Then:

Basin C - Redo to check graph -  $Q_0 = .75 \times .271 = .2032$

100-year storm -

$$T_{d_{100}} = \{2925 \times .70 \times 2.1 / (0.2032 - .2032^2 \times 10 / (234 \times .70 \times 2.1))\}^{.5} - 25 = 120.9 \text{ min.}$$

$$I_{d_{100}} = 117 / (120.9 + 25) = 0.802 \text{ "/hr.}$$

$$Q_{d_{100}} = .70 \times 2.1 \times 1.802 = 1.179 \text{ cfs}$$

$$K = 16 / 10 = 1.60$$

$$V = 66 [1.179 \times 120.9 - 0.2032 \times 120.9 - 0.2032 \times 10 + 1.6 \times 0.2032 \times 10 / 2 + 0.2032^2 \times 10 / (2 \times 1.179)] = 7786.7 \text{ ft.}^3$$

Won't take it - original thought correct - use upper overflow

Pipe overflow does not fit site well due to cover and dimension restrictions.

Use weir type spillway, 1.5' wide, side slopes 5:1 . C = 3.39 (King)

County requires general weir form  $Q = CLH^{1.5}$

Then: 100-year overflow at various heads:

<u>Elevation H</u>	<u>q out (cfs)</u>	
03.55	0.00	E - weir
03.60	0.05	
03.80	0.64	
04.00	1.54	top of berm
04.20	2.66	

## APPENDIX B

Basic data and notes are the same as shown on Appendix A. These computations indicate the movement of Developed runoff along Meander Lane, with and without loss to Basin C. Some loss is presently occurring, but it has been recommended that the loss be stopped.

### Historic Flow:

Basin B: A = 1.14 ac., Total L = 350', Total H = 23', Av. S = 0.0657, n = 0.2

2-year: Overland L = 150' S = 8/150 = 0.0453

Swale L = 200' S = 15/200 = 0.0750

swale B - b = 5', d = 0.20'

$$\text{then: } V = \frac{1.486}{0.2} \times 0.2888 \times 0.2739 = 0.588 \text{ fps}$$

Swale to F - b = 10', d = 0.25', n = 0.1

$$\text{then: } V = \frac{1.486}{0.1} \times 0.35106 \times 0.1664 = 0.868 \text{ fps}$$

$$T_{C_2} = \text{overland} = 1.87 (1.1-0.1) 150^{.5} \times 4.53^{-.33} = 13.9 \text{ min.}$$

$$\text{Basin B swale} = 200/0.588 = 340/60 = \underline{5.7 \text{ min.}}$$

$$\text{Swale to F Road} = 470/0.868 = 541/60 = \underline{9.0 \text{ min.}}$$

$T_{C_2}$  at outfall = 28.6 min., use 29 min.

$$\text{Outfall B} = Q_{2(B)} = 0.1 \times 1.13 \times 1.14 = 0.129 \text{ cfs}$$

$$\text{Outfall at F} = Q_2 = 0.1 \times 0.90 \times 3.04 = 0.273 \text{ cfs}$$

100-year:  $C_{100} = 0.25$

$$T_{C_{100}} = \text{overland} = 1.87 (1.1-0.25) 150^{.5} \times 4.53^{-.33} = 11.8 \text{ min.}$$

$$\text{Basin B swale} = 200/0.863 = 232/60 = 3.9 \text{ min.}$$

$$\text{Swale to F Road} = 470/1.13 = 416/60 = \underline{6.9 \text{ min.}}$$

$T_{C_{100}}$  at outfall = 22.6 min., use 23 min.

$$\text{Outfall at F} = Q_{100} = 0.25 \times 2.63 \times 3.04 = 2.00 \text{ cfs}$$

### Developed Flow:

Meander Lane added Subbasin A2 to B. Area developing slowly as 1/2-acre + tracts. Unit average lower due to hillside, ditch and soil types.

So: Take  $C_2 = 0.30$  and  $C_{100} = 0.45$

Meander street pavement = 1,000 x 34 = 34,000 ft.<sup>2</sup> = 0.781 ac. at  $C_2 = 0.90$  and  
 $C_{100} = 0.95$ , L = 550'

$$\text{Composite } C_2 = (A2+B) = (0.90 \times 0.781 + 0.30 \times 1.542) / 2.323 = 0.50$$

$$\text{Composite } C_{100} = (A2+B) = (0.95 \times 0.781 + 0.45 \times 1.542) / 2.323 = 0.62$$

Developed Flow: (cont'd)

2-year:

Subbasin A2

$$Tc_2 = \text{overland} = 1.87 (1.1-0.3) 180^{.5} \times 7.78^{-.33} = 10.2 \text{ min.}$$

$$\text{Street to B out} = 450/1.30 = 346/60 = 5.8 \text{ min.}$$

$$\text{Street to F out} = 550/2.29 = 240/60 = \underline{4.0 \text{ min.}}$$

$$Tc_2 \text{ at outfall} = 20.0 \text{ min.}$$

Subbasin B

$$Tc_2 = \text{overland} = 1.87 (1.1-0.3) 150^{.5} \times 4.53^{-.33} = 11.13 \text{ min.}$$

$$\text{Swale in Basin} = 200/0.955 = 234/60 = 3.90 \text{ min.}$$

$$\text{Street to F out} = 550/2.29 = 240/60 = \underline{4.00 \text{ min.}}$$

$$Tc_2 \text{ at outfall} = 19.00 \text{ min.}$$

Peak will be at Tc 19 min. (only 1 min. difference) and: R Coeff. = 1.14

$$Q_2 = 0.50 \times 1.14 \times 2.32 = 1.32 \text{ cfs}$$

100-year:

Subbasin A2

$$Tc_{100} \text{ overland} = 1.87 (1.1-0.45) 150^{.5} \times 7.78^{-.33} = 8.29 \text{ min.}$$

$$\text{Street to B out} = 450/1.32 = 341/60 = 5.68 \text{ min.}$$

$$\text{Street to F out} = 550/2.32 = 237/60 = \underline{3.95 \text{ min.}}$$

$$Tc_{100} \text{ at outfall} = 17.92 \text{ min.} \text{.. use 18 min.}$$

Subbasin B

$$Tc_{100} \text{ overland} = 1.87 (1.1-0.45) 150^{.5} \times 4.53^{-.33} = 9.04 \text{ min.}$$

$$\text{Swale in B} = 200/0.92 = 217/60 = 3.62 \text{ min.}$$

$$\text{Street to F out} = 550/2.33 = 236/60 = \underline{3.93 \text{ min.}}$$

$$Tc_{100} \text{ at outfall} = 16.59 \text{ min.} \text{.. use 17 min.}$$

Peak will be at Tc 17 min. and: R Coeff. = 3.07

$$Q_{100} = 0.62 \times 3.07 \times 2.32 = 4.42 \text{ cfs}$$

Summary:

		Subbasin B Only									
		Historic Flow						Developed (A2+B)			
		2-year		100-year							
Basin	Area	Tc <sub>2</sub>	qp2	Tc <sub>100</sub>	qp100	Tc <sub>2</sub>	qp2	C	Tc <sub>100</sub>	qp100	C
C	3.04 ac.	29 min	.273	23 min	2.00	19 min	1.32	.50	17 min	4.42	0.62
		cfs		cfs		cfs				cfs	

Totals to catch basins on Meander Lane at F Road (Patterson)





P.O. Box 55065, Grand Junction, Colorado 81505 (303) 245-9343 Fax (303) 245-5090

November 12, 1992

List of Subcontractors

RE: Site Development  
Hi Fashion Fabrics  
2586 Patterson Road  
Grand Junction, CO 81501

General Contractor: Kelco  
P.O. Box 55065  
Grand Junction, CO 81505  
Kelly Ford  
245-9343

Skyline Excavation  
2477 Industrial Blvd.  
Grand Junction, CO 81505  
Mike Kelleher  
245-2606

Elam Construction  
1225 S 7th St  
Grand Junction, CO 81501  
Kevin Combs  
242-5370

Crigger Concrete  
595 Agana  
Grand Junction, CO 81504  
Bob Crigger  
434-1074

Lincoln Devore (Testing Laboratory)  
1441 Motor Street  
Grand Junction, CO 81501  
Ed Morris  
242-8968

The developer designated inspectors are:  
Kelly Ford  
Kelco General contractors  
and  
Ed Morris  
Lincoln Devore

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**MEMORANDUM**

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**DATE:** November 23, 1992

**TO:** Karl Metzner

**FROM:** Gerald Williams

**SUBJ:** Hi Fashion Fabrics

We have reviewed the recent resubmittals for Hi Fashion Fabrics prepared by Kelco General Contractors and Lincoln DeVore. Several revisions have been made this past week based upon our review comments. The latest drawings received November 20, 1992 still do not address the following comments:

- 1) The handicap spaces do not meet ADA requirements, although adequate space is provided and additional change required pertains to paint striping;
- 2) The grading plan and drainage report do not yet coincide in terms of grades and detention outlet design;
- 3) Curbing or concrete wheel chocks are not provided on the east side of the parking lot;
- 4) Concrete edge curb or thickened pavement edge is not provided around the perimeter of the paved parking lot which will likely result in pavement raveling and deterioration in the short run; and
- 5) The pavement section of 2 inches of asphalt on 6 inches of base course does not meet the geotechnical recommendations of 3 inch asphalt on 9 inches of base for the site soil conditions, nor does it appear adequate for normal design life based upon other applications within the City.

It is our understanding that Kelco will be submitting 4 new sets of prints today, which will address item (1) above. Item (2) is not yet resolved, but does not impact the building, site grading (except minimally), water and sewer, and storm drain except minimally in the parking lot and overflow drain line. Therefore, it is our intent to conditionally sign the new plans so that construction may begin, but with the understanding that the grading and drainage issues must be resolved.

Jeff Vogel, the owner, has elected not to install concrete wheel chocks, pavement edge treatment, nor an increased pavement section despite the geotechnical engineer's recommendations and City concern that the result of such decision will be a significantly reduced pavement life. Notwithstanding, being informed, we feel to honor the Jeff's decision. We have received a letter dated November 19, 1992 from Jeff regarding the pavement section, and a subsequent telephone conversation between Jeff and I held November 20, 1992 also disclosed Jeff's preference to forego the pavement edge treatment.

While writing this memorandum, we received the 4 sets of plans for conditional approval, and only await a revised drainage report.

xc: Don Newton - City Engineer

Parking Area Storage: (note: islands are painted, not raised curbs)

Comment	Elev.	Form = $[A_1 + A_2 + 1 + (A_1 \times A_2 + 1)^{.5}] h/3$	Cum. Volume
Flow Line, Outlet	00.71 ✓	--	--
C orifice & pipe	<del>01.04</del> 00.96	--	--
Top manhole grate	02.55	start with volume in C.B. above	5 ft. <sup>3</sup>
	02.60	.05/3 $[3 + 132 + (3 \times 132)^{.5}]$	8 ft. <sup>3</sup>
	02.80	.2/3 $[132 + 628 + (132 \times 628)^{.5}]$	78 ft. <sup>3</sup>
	03.00	.2/3 $[628 + 1424 + (628 \times 1424)^{.5}]$	278 ft. <sup>3</sup>
	03.20	.2/3 $[1424 + 2788 + (1424 \times 2788)^{.5}]$	692 ft. <sup>3</sup>
Anticipate spillway	03.40	.2/3 $[2788 + 4816 + (2788 \times 4816)^{.5}]$	1443 ft. <sup>3</sup>
ELEV <sub>2</sub> = 2.18' ✓	03.60	.2/3 $[4816 + 7596 + (4816 \times 7596)^{.5}]$	2674 ft. <sup>3</sup>
ELEV <sub>100</sub> = 2.76' ✓	03.80	.2/3 $[7596 + 10544 + (7596 \times 10544)^{.5}]$	4480 ft. <sup>3</sup>
Top of parking lot	04.00	.2/3 $[10544 + 14392 + (10544 \times 14392)^{.5}]$	6964 ft. <sup>3</sup>
	04.20	.2/3 $[14392 + 16692 + (14392 \times 16692)^{.5}]$	10,070 ft. <sup>3</sup>

$V_2 = 1934 \text{ ft}^3$  (with  $Q_0 = .176$ )  
 $V_{100} = 4140 \text{ ft}^3$  (with  $Q_0 = 1.079$ )

Summary:

Basin	Area	2-yr Historic		100-yr Historic		Developed					
		Tc <sub>2</sub>	qp2	Tc <sub>100</sub>	qp100	Tc <sub>2</sub>	qp2	C	Tc <sub>100</sub>	qp100	C
C	2.10 ac.	20 min	.235	16 min	1.66	13 min	1.69	.59	10 min	5.59	0.70
			cfs		cfs			cfs			cfs

Basin C:

2-year Storm:  $Q_0$  orifice only -  $.75 \times .235 = .176$

*This would apply if the orifice was at and not below the pond bottom. However, using it will result in less than historic inflow (which is acceptable) and greater storage volume req'd. for runoff purposes, I'll use it.*

$Td_2 = [633.4 \times .59 \times 2.1 / (.176 - .176^2 \times 13 / (81.2 \times .59 \times 2.1))]^{.5} - 15.6 = 51.95$   
 $Id_2 = 40.6 / (51.95 + 15.6) = .601''/\text{hr.}$   
 $Qd_2 = .59 \times 2.1 \times .601 = .745 \text{ cfs}$   
 $K = 20 / 13 = 1.538$   
 $V = 66 [ .745 \times 51.95 - .176 \times 51.95 - .176 \times 13 + 1.538 \times .176 \times 13 / 2 + .176^2 \times 13 / (2 \times .745) ] = 1934 \text{ ft}^3$

100-year Storm:  $Q_0$  - will probably need spillway for this =  $.65 \times 1.66 = 1.079$

$Td_{100} = [2925 \times .70 \times 2.1 / (1.079 - 1.079^2 \times 10 / (234 \times .70 \times 2.1))]^{.5} - 25 = 39.1 \text{ min.}$  *Condition of crest @ pond bottom does not exist. Therefore this does not really apply. It is doubtful that it can easily be obtained, but we'll forge ahead with calculations and checks anyway.*  
 $Id_{100} = 117 / (39.1 + 25) = 1.825''/\text{hr.}$   
 $Qd_{100} = .70 \times 2.1 \times 1.825 = 2.683 \text{ cfs}$   
 $K = 16 / 10 = 1.60$   
 $V = 66 [ 2.683 \times 39.1 - 1.079 \times 39.1 - 1.079 \times 10 + 1.6 \times 1.079 \times 10 / 2 + 1.079^2 \times 10 / (2 \times 2.683) ] = 4140 \text{ ft}^3$

Orifice Outlet:

C orifice = elev. ~~01.04~~ <sup>00.96</sup>, grate elev. = 02.55 . <sup>1.59</sup> ~~1.51~~ head exists in catch basin.  
 Take H pond = H head above this.

$Q = CA (2gH)^{.5}$  Max. Q allowable - 0.235 cfs, max. H = 2.96' above C of orifice

SEE ATTACHED

Then:  $.235 = .60A (64.4 \times 2.96)^{.5}$  or  $A = .235 / 8.284 = 0.02837 \text{ ft}^2$   $d = 2.28''$

and: 2-year critical elevation in parking lot is 3.60', H = 2.56'

$A = .235 / 7.7040 = 0.0305 \text{ ft}^2$

.0305 ft.<sup>2</sup>  $d = 2.36''$  orifice with diameter of 2.36'' will hold historic flow at the critical elevation.

Using info on the preceding page...

### 2-YR ANALYSIS

Given:  $Q_{02}$  was selected at 0.176 cfs, which resulted in a req'd  $V_2$  of 1934 ft<sup>3</sup> and  $EL_2$  of 03.48'.

Find: low level outlet orifice size

Soln: Normally, the orifice would be sized to ensure that at  $EL_2$ ,  $Q_{2h}$  at 0.235 cfs is not exceeded, which is the only check that would be required for the 2 yr condition. However, the original use of the "0.75" factor was incorrect inasmuch as the orifice is below the bottom of the pond. Therefore, the orifice will be sized for  $Q_0$ , then verified that  $Q_{2h}$  is not exceeded.

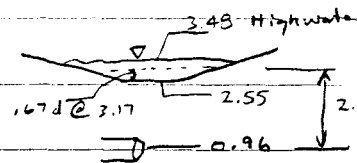
$$Q = CA(2gH)^{.5}, \text{ H used is } H_{avg}, H = 2.21$$
$$.176 = (.6)(A)[2 \times 32.2 \times 2.21]^{.5}$$

$$.0246 = A(ft^2)$$

$$3.54 = A(m^2) = \frac{\pi d^2}{4}$$

$$4.51 = d^2$$

$$2.12" = d \approx 2.125"$$



check for  $Q_{2h}$

$$Q = CA(2gH)^{.5}; \text{ H is max H, } H = 3.48 - 0.96 = 2$$

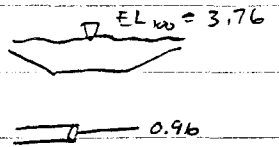
$$Q = (.6)(.0246)[2 \times 32.2 \times 2.52]^{.5} = 0.188 \text{ cfs} < 0.235$$

OK

## 100 YR ANALYSIS

Given: Orifice with area of  $.0246 \text{ ft}^2$  ( $d = 2.125''$ ) @ elev  $0.96$

Find: Orifice capacity at  $H_{100}$ ,  $H_{100} = 3.76 - 0.96 = 2.80'$



Soln:  $Q = CA(2gH)^{1/2}$

$$Q = (.6)(.0246)(2 \times 32.2 \times 2.80)^{1/2} = 0.198 \approx 0.20 \text{ cfs}$$

Given:  $Q_{100h} = 1.66 \text{ cfs}$  - This may not be exceeded

Find: Capacity of add'l outflow req'd/allowed; check design

Soln:  $Q_{100h} - Q_{\text{orifice}} = Q_{\text{add'l outflow}}$

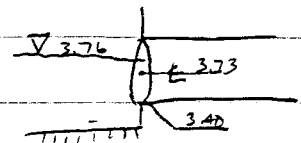
$$1.66 - 0.2 = 1.46$$

The calculated  $V_{100}$  of  $4140 \text{ ft}^3$  is based upon an average outflow of  $1.079 \text{ cfs}$ . Since the low level orifice takes an approximate average of  $0.19 \text{ cfs}$ , the add'l outflow must average  $1.079 - 0.19 = 0.889 \approx 0.9 \text{ cfs}$ . This cannot be accomplished with the current design, not only is  $Q_0$  not  $0.9$ , but  $Q_{\text{max}}$  is not  $0.9$  based upon the  $EL_{100}$  of  $3.76'$ .

The depth of flow is  $3.76 - 3.40 = 0.36'$

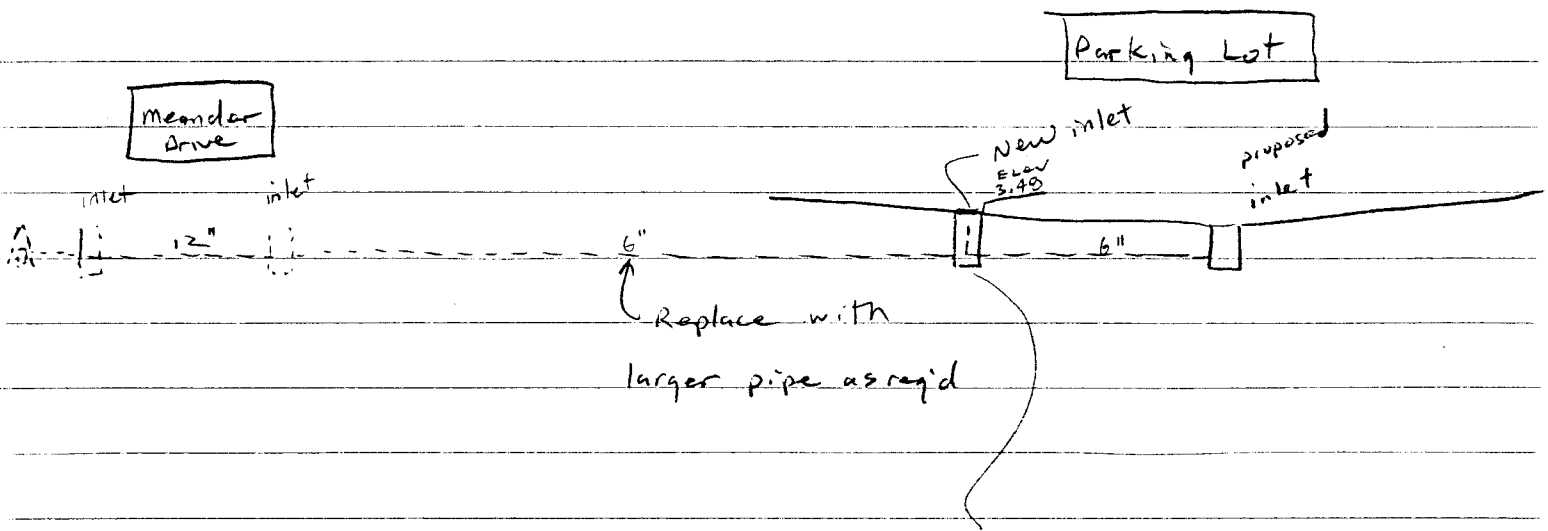
Even a 12" CMP under inlet control can't get  $0.9 \text{ cfs}$  at the maximum ponding.

$V_{100}$  per previous calculation =  $3.76$



CONCLUSION: The designed system does not match the calculations; That is, 1.0789 cfs average cannot be achieved, which is what the volume calcs are based upon. With the current design, the outflow is less, therefore the volume will be more, and the depth of ponding increased. Criteria only allows 1.0' of ponding on parking areas. If the design worked per calculations (which it does not), the 1.0 foot would be exceeded. However, as the current design is, it is probable that the depth would approach 1.75' feet. That is unacceptable.

We suggest looking at the following:



$$Q_0 = 0.9 \text{ cfs} \therefore \text{Avg } h = (3.76 - 3.40)(1.67) = 0.19'$$

$$Q_0 = 0.9 \text{ cfs} = 3pd^{1.5}$$

$3.62' = p \rightarrow$  Grate opening is subject to clogging, and should not be used to meter outflow. Figure 50% clogging, use grate with  $p = 3.62 \times 2 = 7.2$ .

The City std area inlet has a perimeter of 9 L.F.

Then, have orifice opening below the grate that:

1) Has a capacity of 0.9 cfs +/- when the ponded  
w.s. elevation is at  $3.48 + 0.67(3.76 - 3.48) = 3.69$ ; and

2) At w.s. elev at 3.76,  $Q$  does not exceed  
 $1.66 - 0.2 = 1.46$  cfs.



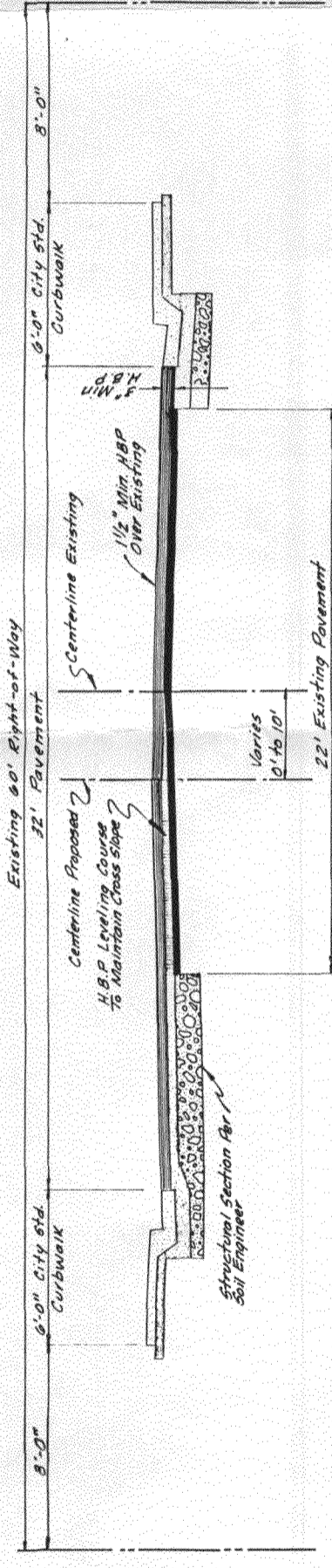
REVISIONS	BY

**TAL**  
 LAND DEVELOPMENT CONSULTANT  
**THOMAS A. LOUHE**

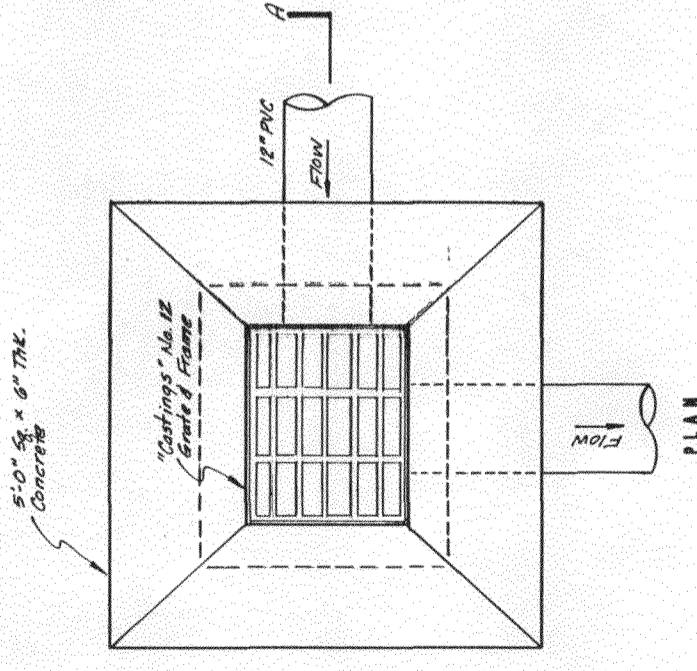
D O P A S H I O N P A R T N E R S  
 1938 N. 1st STREET, GRAND JUNCTION, CO. 81505

DETAIL SHEET

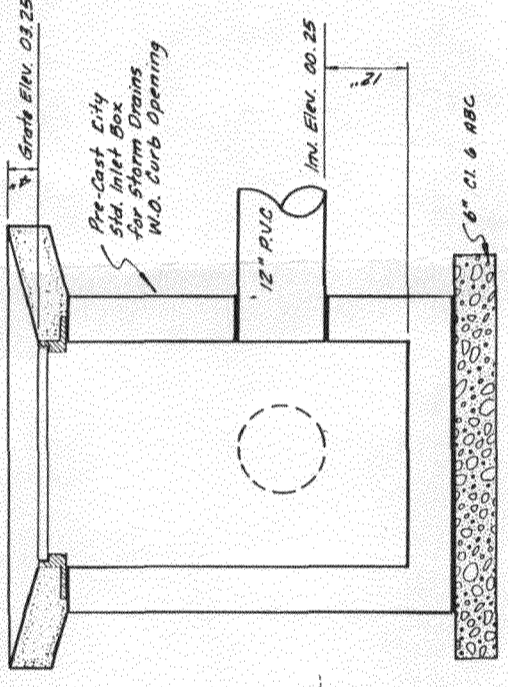
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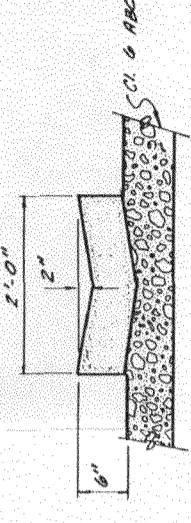
MEANDER DRIVE STREET SECTION



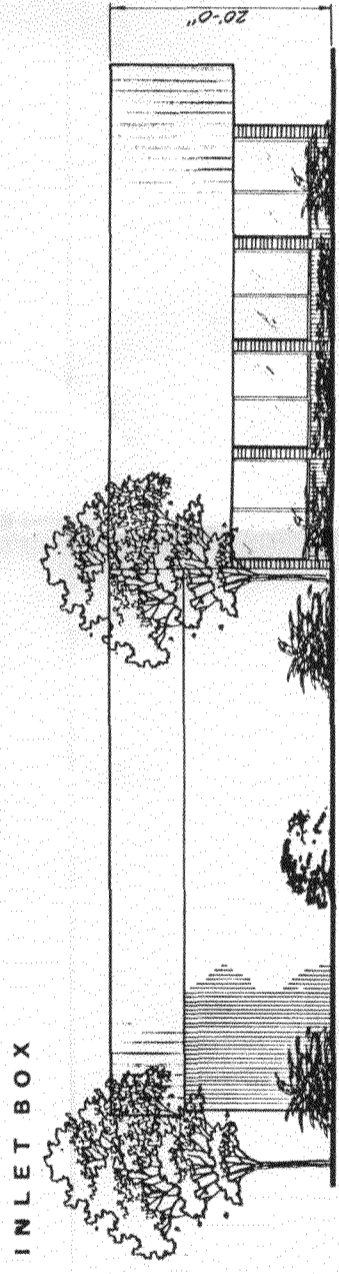
PLAN



SECTION A-A



2 FL. 1/4\"/>



SOUTH ELEVATION

#27 92

















