# **Table of Contents**

File PDR-1996-217

P S Name: \_\_\_\_The Knolls - SE Corner 27 Road /Cortland Avenue\_\_\_

A few items are denoted with an asterisk (\*), which means they are to be scanned for permanent record on the ISYS r с retrieval system. In some instances, items are found on the list but are not present in the scanned electronic development е a file because they are already scanned elsewhere on the system. These scanned documents are denoted with (\*\*) and will n s be found on the ISYS query system in their designated categories. e n Documents specific to certain files, not found in the standard checklist materials, are listed at the bottom of the page. n е d t Remaining items, (not selected for scanning), will be listed and marked present. This index can serve as a quick guide for the contents of each file. al mana a X **Table of Contents** х 1.11 **\*Review Sheet Summary** Roya X \* Application form X Massaala sa X **Review Sheets** X Receipts for fees paid for anything . X X \*Submittal checklist Manager Manager and States \*General project report Reduced copy of final plans or drawings Righted any of stated XX Reduction of assessor's map. Reduction of a con-Evidence of title, deeds, easements Evidence en enter de la serie X X \*Mailing list to adjacent property owners Winning has to adjacent proje Palvas as aco casos Public notice cards Record of certified mail Redend of Contrained States XX Legal description Legal description ξ (L. Appraisal of raw land Apprecial of raw rand 1 Reduction of this maps. Reduction of any maps - final copy 1 1 The man the second a second on the \*Final reports for drainage and soils (geotechnical reports) Other bound on occurbon th Other bound or non-bound reports Traffic studies Franks starts X **X** \*Review Comments READ AND A WARDEN AND 1118.1.1.2. X X \*Petitioner's response to comments x X \*Staff Reports Ni \*Stall Reports \*Planning Commission staff report and exhibits Phatman Contraction and a Mary Council stail a port on-\*City Council staff report and exhibits \*Summary sheet of final conditions INVERTICAL STREET, STREET, STREET, STREET, ST **DOCUMENT DESCRIPTION:** X X Final Decision – Approved with conditions X Grading and Stormwater Management Plan XX X Water, Sewer Plan and Profile Final Drainage Report - 9/96 - and addendum - 10/30/96 X Preliminary Plan X Preliminary Drainage Report - 9/96 X Warranty Deed - Bk 2239 / Pg 154 X Standard Concrete Details Contract Deca x Х Preliminary Subsurface Soils Investigation - 8/17/81 Х Storm Drain Details X Declaration of Covenants - Bk 2403 / Pg 866 x Water Line Details X Х X General Report Sanitary Sewer Details Signed Final Plat Composite Plan – not signed X Treasurer's Certificate of Taxes Due - 9/25/96 X X Х Posting of Public Notice Signs - 102/22/96 Х X Planning Commission Minutes – 11/5/96 - \*\* X X Final Plat – not signed version X X Correspondence Х X File close-out summary X X Utility Committee Approval – 12/11/96 X Notice of Public Hearing Mail-out - sent 10/4/96 x x DIA – Released Bk 3018 / Pg 734 X X Certification of Plat – 1/17/97 X Final Plat- signed and dated - See GIS Historical Maps - \*\* Х Utility Composite



## **DEVELOPMEN** APPLICATION

Community Development Department 250 North 5th Street, Grand Junction, CO 81501 (970) 244-1430

Keceipt	
Date	
Rec'd By	
Rec'd By File No. <u>PDR-96-217</u>	

We, the undersigned, being the owners of property
situated in Mesa County, State of Colorado, as described herein do hereby petition this:

PETITION	PHASE	SIZE	LOCATION	ZONE	LAND USE
Subdivision Plat/Plan	<ul><li>Minor</li><li>Major</li></ul>		REMSED PRELIM	PD-38 From ESF. 4 to PR	SF
🙇 Rezone		2	FILIN6#1		SF-
Planned Development	DODP Prelim Final		172221 MINANY	FOR REMANING BRF.Y PROPOSED	SF
Conditional Use					
Zone of Annex					
Variance					
X Special Use		LOWN	enkity sif res	IDENTIAL & CHURCH IN,	Anzione criment
Vacation					<b>Z ₹ ₹</b> □ Right-of Way □ Easement
Revocable Permit					
🗅 Site Plan Review		·			
🗅 Property Line Adj.					

0.P. Development Co., LLC	0.P. Development Co., LLC	Robert C. Knapple
Property Owner Name	Developer Name	Representative Name
2421 Applewood Circle	2421 Applewood Circle	2421 Applewood Circle
Address	Address	Address
Grand Junction, CO 81506	Grand Junction, CO 81506	Grand Junction, CO 81506
City/State/Zip	City/State/Zip	City/State/Zip
(970)241-2373	(970)241-2373	(970)241-2373
Business Phone No.	Business Phone No.	Business Phone No.

NOTE: Legal property owner is owner of record on date of submittal.

We hereby acknowledge that we have familiarized ourselves with the rules and regulations with respect to the preparation of this submittal, that the foregoing information is true and complete to the best of our knowledge, and that we assume the responsibility to monitor the status of the application and the review comments. We recognize that we or our representative(s) must be present at all required hearings. In the event that the petitioner is not represented, the item will be dropped from the agenda, and an additional fee charged to cover rescheduling expenses before it can again be placed on the agenda.

0-Signature o erson Complet oplication For St. Matthews Foiscora mint Regetor -96 X Kould Signature of Property Owner(s) - attach additional sheets if necessary

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NOTES: * An asterisk in the item description column indicates that a form is supplied by the City.																															

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### **PRE-APPLICATION CONFERENCE**

Date: 8-13-96 Conference Attendance: BILL IN Proposal: REVIEW PIZELW Location: SEC CONTRACT	336KEP, OMO CHASE, JOH MARY RINAL DAT, REZO 9 27'12 120	DENNY BRANAM to MALSON BOB KNAPPLE DNE & SPIEML USE PARMIT
Tax Parcel Number: Review Fee: <u>820 + 10</u> (Fee is due at the time of submittal. M Additional ROW required? <u></u> Adjacent road improvements required Area identified as a need in the Master Parks and Open Space fees required? Recording fees required? <u></u> Half street improvement fees/TCP recorded Revocable Permit required? <u></u> State Highway Access Permit require	(34) <u>5 A CRE</u> 53.9 ADES * Take check payable to the City of Grand. <u>CORTIAND NETODS 30</u> 1? <u>CORTIAND YES</u> 2711 or Plan of Parks and Recreation? <u>-</u> <u>YES</u> <u>* 225/UNIT</u> <u>YES</u> puired? <u>1/2 STIMP. TO COVARY</u> d? <u>ND</u>	<u>'/z ST. 27/z 30'/z ST.</u> <u>Estimated Amount:</u> <u>Estimated Amount:</u> <u>Estimated Amount:</u>
	ge fee required?	
Located in identified floodplain? FIR	M panel #	
	Clear Zone, Critical Zone, Area of Influ	
	oposal require careful thought, preparatio attention as needing special attention or review process.	
O Access/Parking O Drainage O Floodplain/Wetlands Mitigation O Other Related Files:		O Land Use Compatibility O Traffic Generation O Geologic Hazards/Soils
It is recommended that the applicant i	nform the neighboring property owners	and tenants of the proposal prior to the

It is recommended that the applicant inform the neighboring property owners and tenants of the proposal prior to the public hearing and preferably prior to submittal to the City.

### **PRE-APPLICATION CONFERENCE**

WE RECOGNIZE that we, ourselves, or our representative(s) must be present at all hearings relative to this proposal and it is our responsibility to know when and where those hearings are.

In the event that the petitioner is not represented, the proposed item will be dropped from the agenda, and an additional fee shall be charged to cover rescheduling expenses. Such fee must be paid before the proposed item can again be placed on the agenda. Any changes to the approved plan will require a re-review and approval by the Community Development Department prior to those changes being accepted.

WE UNDERSTAND that incomplete submittals will not be accepted and submittals with insufficient information, identified in the review process, which has not been addressed by the applicant, may be withdrawn from the agenda.

WE FURTHER UNDERSTAND that failure to meet any deadlines as identified by the Community Development Department for the review process may result in the project not being scheduled for hearing or being pulled from the agenda.

Signature(s) of Petitioner(s)

Signature(s) of Representative(s)

2945-011-24-003 FRANK A DIEHL BETTY J 4011 APPLEWOOD ST GRAND JUNCTION, CO 81506-8405

2945-011-24-006 KAREN TURNER 3915 APPLEWOOD ST GRAND JUNCTION, CO 81506-8407

2945-011-24-014 TOMMY DALE PETTY GLINDA L 3920 APPLEWOOD ST GRAND JUNCTION, CO 81506-8408

2945-011-32-002 ROBERT R RHYNE PAULA SUE WADKINS 3725 APPLEWOOD ST GRAND JUNCTION, CO 81506-8411

2945-011-32-005 RICHARD W TUMA JEANNETTE S 3720 ELDERBERRY CIR GRAND JUNCTION, CO 81506-8475

2945-011-33-006 DICK OLSEN DORRIS JEAN PO BOX 3565 GRAND JUNCTION, CO 81502-3565

2945-011-33-012 GORDON N MCFERRON MARY C 3520 PONDEROSA WAY GRAND JUNCTION, CO 81506-8458

2945-011-39-002 MURIEL F CRAWFORD TRUSTEE 3943 S PIAZZA PL GRAND JUNCTION, CO 81506-8501

2945-011-45-002 ST MATTHEWS PARISH PO BOX 776 GRAND JUNCTION, CO 81502-0776

2945-012-16-003 ALTON B CRISMAN GAE E 1819 RIDGE DR GRAND JUNCTION, CO 81506-4032 ► 2945-011-24-004 MARY CHRISTINE HEIMBURGER

JOHN W 3935 APPLEWOOD ST GRAND JUNCTION, CO 81506-8407 2945-011-24-007 JEROME F PALMER EVELYN E 3910 APPLEWOOD ST GRAND JUNCTION, CO 81506-8408

2945-011-28-001 MICHAEL O RAMLOW B J & K L RAMLOW 4010 APPLEWOOD ST GRAND JUNCTION, CO 81506-8406

2945-011-32-003 GARY L WUSTER JUDITH A 3735 APPLEWOOD ST GRAND JUNCTION, CO 81506-8411

2945-011-32-006 ROBERT L BENAC ARLENE E & LYNN A WALSH 3710 ELDERBERRY CIR GRAND JUNCTION, CO 81506-8475

2945-011-33-008 JAMES E FRASER GUDRUN H - C/O COLDWELL BANKER 3530 PONDEROSA WAY GRAND JUNCTION, CO 81506-8458 2945-011-33-015 ROBERT D YOUNGQUIST GAIL L 3620 PONDEROSA WAY GRAND JUNCTION, CO 81506-8483

2945-011-40-001 JOSE L GALLEGOS VICTORIA A GALLEGOS 2257 S SEVILLE CIR GRAND JUNCTION, CO 81506-8508

2945-012-16-001 ROBERT W BERSHENYI MARCIA C 1837 RIDGE DR GRAND JUNCTION, CO 81506-4032

2945-012-16-010 KENNETH E GREGORY CAROL L 1820 BELL RIDGE CT GRAND JUNCTION, CO 81506-4011

PDR-96-217

2945-011-24-005 HAROLD E CRUSON JOYCE E CRUSON 3925 APPLEWOOD ST GRAND JUNCTION, CO 81506-8407

2945-011-24-013 DONALD E LOVERN LYNDA L 2421 APPLEWOOD PL GRAND JUNCTION, CO 81506-8480

2945-011-31-034 ROSE MARIE MARFITANO 3750 APPLEWOOD ST GRAND JUNCTION, CO 81506-8412

2945-011-32-004 JACK D ELLIOTT BARBARA G 3730 ELDERBERRY CIR GRAND JUNCTION, CO 81506-8475

2945-011-32-007 LOUIS A MCCOWEN MARION G 3630 ELDERBERRY CIR GRAND JUNCTION, CO 81506-8453

2945-011-33-009 MARK A TWARDOWSKI DEBORAH 3610 PONDEROSA WAY GRAND JUNCTION, CO 81506-8483

2945-011-39-001 WESLEY JAMES PIDCOCK DOLORES K 2256 S SEVILLE CIR GRAND JUNCTION, CO 81506-8507

2945-011-45-001 WILLIAM L DAVIS CATHARINE S 652 27 1/2 RD GRAND JUNCTION, CO 81506-4102

2945-012-16-002 ALLEN L STEVENSON DOROTHY L STEVENSON 1829 RIDGE DR GRAND JUNCTION, CO 81506-4032

2945-012-16-011 MICHAEL J DEBUONO WILMA A 1828 BELL RIDGE CT GRAND JUNCTION, CO 81506-4011 2945-012-16-012 LAWRENCE W BROZOVICH

NADINE S BROZOVICH 1830 BELL RIDGE CT GRAND JUNCTION, CO 81506-4011 2945-012-64-001 GAIL PALMER MARY F BARTON-PALMER 1810 CORTLAND CT GRAND JUNCTION, CO 81506-5249

2945-012-68-002 RUFUS JONES FLORENCE M JONES 3716 CHRISTENSEN CT GRAND JUNCTION, CO 81506-5250

2945-013-10-002 HENRY J FAUSSONE 1755-B CRESTVIEW DR GRAND JUNCTION, CO 81506-5227

2945-011-34-011 LEONARD L SARTZ MARGUERITE E 3805 APPLEWOOD ST GRAND JUNCTION, CO 81506-8409

2945-011-34-005 A PENKO LUCILLE M 3635 PONDEROSA WAY GRAND JUNCTION, CO 81506-8444

2945-011-34-014 JACK C STOUT KATHERINE E 3515 PONDEROSA WAY GRAND JUNCTION, CO 81506-8482

2945-011-34-008 STEVEN J JOHNSON CYNTHIA A 3725 ELDERBERRY CIR GRAND JUNCTION, CO 81506-8485

2945-011-34-016 DANIEL KUDZY GLORIA E 3618 RIDGE DR GRAND JUNCTION, CO 81506-8497

2945-011-36-008 HAROLD L GRAFE MARILYN G 510 TIARA DR GRAND JUNCTION, CO 81503-9747 2945-012-16-016 RICHARD E HOLLINGER WYONA J 1831 BELL RIDGE CT GRAND JUNCTION, CO 81506-4069

2945-012-64-002 RUDY HERRERA LINDA L HERRERA PO BOX 41025 GRAND JUNCTION, CO 81501

2945-012-68-003 R LEON MOORE MARTHA S MOORE 3745 CHRISTENSON CT GRAND JUNCTION, CO 81506-5250

2945-013-10-009 WILLIAM A COOPER MYRNA M 1755 CRESTVIEW DR GRAND JUNCTION, CO 81506-5236

2945-011-34-012 M IRENE DARLINGTON 3815 APPLEWOOD ST GRAND JUNCTION, CO 81506-8409

2945-011-34-017 RODNEY SUNDHEIM SHERI 3615 PONDEROSA WAY GRAND JUNCTION, CO 81506-8444

2945-011-34-006 DONALD J MCFARLAND BETTY I 3705 ELDERBERRY CIR GRAND JUNCTION, CO 81506-8485

2945-011-34-009 ELIJAH DEAN HINES BERNA SUE 3735 ELDERBERRY CIR GRAND JUNCTION, CO 81506-8485

2945-011-34-018 GENE C COLEMAN KARLA A 3626 RIDGE DR GRAND JUNCTION, CO 81506-8497

2945-011-36-002 E WILLIAM TRAINOR PHYLLIS E 2297 SEVILLE CIR GRAND JUNCTION, CO 81506 96-217 2945-012-16-017 ELIZABETH ANN WILLIS TR - ELIZABETH A WILLIS TRUST 1825 BELL RIDGE CT GRAND JUNCTION, CO 81506-4069

2945-012-68-001 KENT W MARSH 192 EDLUN RD GRAND JUNCTION, CO 81503

2945-013-10-001 CAROL A CADEZ TRUST 1755 CRESTVIEW DR APT A GRAND JUNCTION, CO 81506-5236

2945-014-00-038 DARLA M BANKERT 8023 HYGIENE RD LONGMONT, CO 80503-9120

2945-011-34-013 EVERETT L POND DOREEN L POND 3825 APPLEWOOD ST GRAND JUNCTION, CO 81506-8409

2945-011-34-015 ROBERT H BLOM KARALEE P 3526 RIDGE DR GRAND JUNCTION, CO 81506-8478

2945-011-34-007 LYNN E LICKERS ETAL 3715 ELDERBERRY CIR GRAND JUNCTION, CO 81506-8485

2945-011-34-010 CLAUDE E EARLY JUNE E 3745 ELDERBERRY CIR GRAND JUNCTION, CO 81506-8485

2945-011-36-006 COLORADO NATIONAL BANK -TRUSTEE MARY E L JONES TRUST PO BOX 608 GRAND JUNCTION, CO 81502-0608 2945-011-36-007 JAMES M FLYNN CAROLE L 3918 S SEVILLE CIR GRAND JUNCTION, CO 81506-8472 2945-011-36-009 DAVID L DOTY CANDACE D 3934 S SEVILLE CIR GRAND JUNCTION, CO 81506-8472

2945-011-36-004 THOMAS G SARMO ELAINE R 2325 S SEVILLE CIR GRAND JUNCTION, CO 81506-8494

2945-011-37-010 E ROMAINE MAHAFFEY PO BOX 773035 STEAMBOAT SPRINGS, CO 80477-3035

2945-011-37-003 GORDON A HARSHMAN TRUDORA V 2312 S SEVILLE CIR GRAND JUNCTION, CO 81506-8456

2945-011-37-007 DAVID G MICKLE MILDRED L 2325 N SEVILLE CIR GRAND JUNCTION, CO 81506-8491

2945-012-25-006 MAX CLIFFORD KENDALL

JEANNINE KENDALL 3620 BELL CT GRAND JUNCTION, CO 81506-4009 2945-012-25-009 HOWARD A RUDOLPH MINNIE J 3648 BELL CT GRAND JUNCTION, CO 81506-4009

2945-012-25-001 DEBORAH D TAYLOR 3645 27 1/2 RD GRAND JUNCTION, CO 81506-4135

2945-012-68-014 RICHARD A TOPE MELINDA S TOPE 560 E SADDLE GRAND JUNCTION, CO 81503

2945-012-68-010 PAUL G TRINKLEIN MATSUYO M TRINKLEIN 3728 CHRISTENSEN CT GRAND JUNCTION, CO 81506 2945-011-36-001 VIRGINIA JOHNSON 2285 S SEVILLE CIR GRAND JUNCTION, CO 81506-8493

2945-011-36-005 THOMAS F SHEA REBECCA T 2335 S SEVILLE CIR GRAND JUNCTION, CO 81506-8494

2945-011-37-006 DORIS E ARCIERI 2335 M SEVILLE CIR GRAND JUNCTION, CO 81506

2945-011-37-004 ARLENA R HURST 2324 S SEVILLE CIR GRAND JUNCTION, CO 81506-8456

2945-011-37-008 GARY HILTBRAND JULIE L 2311 N SEVILLE CIR GRAND JUNCTION, CO 81506-8491

2945-012-25-007 WILLIAM K JOHNSON LINDA L 3636 BELL CT GRAND JUNCTION, CO 81506-4009

2945-012-25-004 M L RAY SMITH RUTH M 1836 RIDGE DR GRAND JUNCTION, CO 81506-4070

2945-012-25-002 JOHN J GLISAN PAMELA K GLISAN 3635 27 1/2 RD GRAND JUNCTION, CO 81506-4135

2945-012-68-015 RICHARD A TOPE MELINDA S TOPE 560 E SADDLE GRAND JUNCTION, CO 81503

2945-012-68-008 RUFUS JONES FLORENCE M JONES 3716 CHRISTENSEN CT GRAND JUNCTION, CO 81506-5250 96-217 2945-011-36-003 ROBERT R SPROWELL LUCRETIA 2311 S SEVILLE CIR GRAND JUNCTION, CO 81506-8494

2945-011-37-002 COLORADO NATIONAL BANK DONNA M GREGORY REV LIVING TRST PO BOX 5168 DENVER, CO 80217-5168 2945-011-37-001 PATRICE HOWEY 3936 S PIAZZA PL GRAND JUNCTION, CO 81506-8440

2945-011-37-009 WILLIAM D POTTER CHRISTINA C 2297 N SEVILLE CIR GRAND JUNCTION, CO 81506-8490

2945-011-37-005 LUANNE M ANTRONICA 3933 S SEVILLE CIR GRAND JUNCTION, CO 81506-8495

2945-012-25-008 BARBARA A LACY 3644 BELL CT GRAND JUNCTION, CO 81506-4009

2945-012-25-005 DOROTHY B GULLEY 1820 RIDGE DR GRAND JUNCTION, CO 81506-4070

2945-012-25-003 HERBERT M WHEELER H LOUISE WHEELER 3625 27 1/2 RD GRAND JUNCTION, CO 81506-4135

2945-012-68-009 FORREST HOLGATE 2936 G RD GRAND NUNCTION, CO 81504

2945-012-68-012 LORI A NELSON 3740 CHRISTENSON CT GRAND JUNCTION, CO 81506-5250

96-217

2945-012-68-013 SHERRY HEPBURN 3748 CHRISTENSON CT GRAND JUNCTION, CO 81506-5250 2945-012-68-011
 STEVE C VOYTILLA
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 GRAND JUNCTION, CO 81506-8325

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City of Grand Junction Community Development Dept. 250 N 5th St. Grand Junction, C0 81501 2945-012-00-052
 JACK A BROWN
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David Chase Banner Associates 2777 Crossroads Blvd. Grand Junction, C0 81506

# POSTING OF PUBLIC NOTICE SIGNS

The posting of the Public Notice Sign is to make the public aware of development proposals. The requirement and procedure for public notice sign posting are required by the City of Grand Junction Zoning and Development Code.

To expedite the posting of public notice signs the following procedure list has been prepared to help the petitioner in posting the required signs on their properties.

- 1. All petitioners/representatives will receive a copy of the Development Review Schedule for the month advising them of the date by which the sign needs to be posted. IF THE SIGN HAS NOT BEEN PICKED UP AND POSTED BY THE REQUIRED DATE, THE PROJECT WILL <u>NOT</u> BE SCHEDULED FOR THE PUBLIC HEARING.
- 2. A deposit of \$50.00 per sign is required at the time the sign is picked up.
- 3. You must call for utility locates before posting the sign. Mark the location where you wish to place the sign and call 1-800-922-1987. You must allow two (2) full working days after the call is placed for the locates to be performed.
- 4. Sign(s) shall be posted in a location, position and direction so that:
  - a. It is accessible and readable, and
  - b. It may be easily seen by passing motorists and pedestrians.
- 5. Sign(s) MUST be posted at least **10 days** before the Planning Commission hearing date and, if applicable, shall stay posted until after the City Council Hearing(s).
- 6. After the Public Hearing(s) the sign(s) must be taken down and returned to the Community Development Department within FIVE (5) working days to receive a full refund of the sign deposit. For each working day thereafter the petitioner will be charged a \$5.00 late fee. After eight working days Community Development Department staff will retrieve the sign and the sign deposit will be forfeited in its' entirety.

The Community Development Department staff will field check the property to ensure proper posting of the sign. If the sign is not posted, or is not in an appropriate place, the item will be pulled from the public hearing agenda.

I have read the above information and agree to its terms and conditions.

SIGNATURE DATE FILE #INAME PDR-96-217 The Knolls RECEIPT #4748PETITIONER/REPRESENTATIVE: D.P. Development LLC PHONE #241-2373 POST SIGN(S) BY: 10/25 DATE OF HEARING:\_\_ 10/22/96 RETURN SIGN(S) BY: 1/13 DATE SIGN(S) PICKED-UP\_\_\_\_ DATE SIGN(S) RETURNED 11/12/9/ RECEIVED BY: 54 1/# 40009079



Lincoln DeVore

1000 West Fillmore St. Colorado Springs, Colorado 80907 (303) 632-3593 Home Office

August 17, 1981

Gingery & Associates 1310 Ute Avenue Grand Junction, CO 81501

RE:

#### PRELIMINARY

#### SUBSURFACE SOILS INVESTIGATION

ONION HILL SUBDIVISION

GRAND JUNCTION, COLORADO

Gentlemen:

Transmitted herein are the results of a Preliminary Subsurface Soils Investigation and Foundation Recommendations for the proposed Onion Hill Subdivision of 27½ Road and F3/4 Road in Grand Junction, Colorado.

Respectfully submitted,

LINCOLN-DeVORE TESTING LABORATORY, INC.

By: Gary Krzisnik, М GE D. Grand Juncti Off on Reviewed by GMK/jb LDTL Job No. 40644J

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P.O. Box 1427 Glerwood Springs, Colo 81601 (303) 945-6020 86 Rosemoni Plaza Montrose, Colo 81401 (303) 249-7838 P.O. Box 1882 Grand Junction, Colo 81501 (303) 242-8968 P.O. Box 1643 Rock Springs, Wyo 82901 (307) 382-2649

#### ABSTRACT:

The contents of this report are a Preliminary Subsurface Soils Investigation and Foundation Recommendations for the proposed Onion Hill Subdivision at 27<sup>1</sup>/<sub>2</sub> Road and F 3/4 Road in Grand Junction, Colorado.

Topographically, the site is approximately level, with a general southwesterly gradient, and is located on an alluvial plain of the Colorado River.

The foundation soils underlying the site were found to consist of silty clays interbedded with layers of fine grained sands. The upper 8 to 26 feet of the soil profile are of lower moisture, medium density and are mildly expansive. The soil below this is wet, soft and of low density in the southwest portion of the site. At other areas, the medium density fine-grained soils are underlain by Mancos Shale. In general, shallow foundation systems are recommended for most types of structures at this site, using maximum and minimum allowable pressures of 3500 and 2000 psf, respectively. Local variations in these pressures should be expected. Several foundation options are available for use in this site, depending on the design of the structure and the magnitude of the foundation loads anticipated.

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Because of the expansive nature of the foundation materials, we would recommend that the foundation system be well balanced and heavily reinforced.

All floor slabs on grade must be constructed to act independently of other structural portions of the buildings.

Adequate drainage must be provided at all times. Water must never be allowed to pond above the foundation soils.

Surface and subsurface drainage must be carefully designed and controlled. A perimeter drain would be recommended around the building exterior.

A Type II Cement would be recommended in all concrete in contact with the soil on this site. More detailed recommendations can

be found within the body of this report. All recommendations will be subject to the limitations set forth herein.

The information herein has been obtained to obtain a general and preliminary indication of the soils which will probably be found under presently unknown types of structures proposed for the site. Site specific information must be obtained beneath each proposed structure after its exact location is determined, since the soil types

and conditions differ across the overall site and the type of structure proposed is not known.

This report is intended to identify general soil conditions on the site, as requested. Nine test borings spread over a 30 acre site, can only be used as an overview of the soil conditions and not for site specific design purposes. The purpose of this investigation was to determine the general suitability of the site for construction of a 30 acre residential subdivision southeast of the intersection of  $27\frac{1}{2}$  and F 3/4 Roads in Grand Junction, Colorado. Characteristics of the individual soils found within the test borings were examined for use in designing foundations on this site.

Although Lincoln-DeVore has not seen a set of construction drawings for any of the multiple family dwelling units proposed, we believe that they will be basically frame structures of more or less conventional design. Foundation loads for structures of this nature are normally light to medium weight in magnitude.

The topography of the site is relatively flat, being located on an alluvial plain of the Colorado River. The ground surface in the vicinity of the site has an overall gradient to the southwest towards the river. The exact direction of surface runoff on this site will be controlled to an extend by the proposed construction, and therefore, will be variable. In general, however, surface runoff will travel to the south and southwest, eventually entering the ©lorado River. Surface and subsurface drainage on this site can be described as poor.

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The foundation soils encountered on this site consisted predominantly of alluvial and some colluvial deposits. The deposits are placed by past flooding action from the Colorado River and, more recently (in geological time) by slope wash from the Book Cliffs located north and northeast of the site. These soils were deposited over bedrock of the Mancos Shale Formation.

The Mancos Shale can broadly be described as a thin-bedded, drab, light to dark gray marine shale, with thinly interbedded fine grain sandstone and limestone layers. Some portions of the Mancos Shale are bentonitic, and therefore, are highly expansive. The majority of the shale, however, has only a moderate expansion potential. Formational shale was encountered in most of the borings at depths varying from 8 to 22 feet. It is anticipated that this formational shale in some areas could affect the construction and the performance of the foundations on the site.

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#### BORINGS, LABORATORY TESTS AND RESULTS:

Nine test borings were drilled across the subdivision site and are located approximately as shown on the attached Test Boring Location Diagram. The test borings were placed in such a manner as to obtain a reasonably good profile of the subsurface soils. All test borings were drilled with a power-driven, continuous auger drill. Samples were taken with a standard split-spoon sampler and by bulk methods.

The precise gradational and plasti-

city characteristics associated with the soils encountered during drilling can be found on the attached summary sheets. The representative number for each soil group is indicated in a small circle immediately below the sampling point on the Drilling Logs. The following discussion of the soil groups will be general in nature.

The site soils profile varied somewhat but may be generalized into 3 layers. The first layer consists of medium density silty and sandy clays and silty sand. The second layer, occurring in the southwest part of the property, is of very low density, soft silty clay. The underlying Mancos Shale bedrock would constitute the third and final layer of the profile.

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Soil Type No. 1 classified as a silty sand (SM) of medium to very fine grain size. Soil Type No. 1 is of very low plasticity, low moisture content and of low to moderate density. In themselves, these soils will have virtually no tendency to expand upon the addition of moisture nor to long-term consolidate under applied foundation stresses. Granular materials, such as these, do have a tendency to rapidly settle under the initial application of static foundation pressures. However, these settlements are characteristically fairly rapid in nature and should be virtually complete by the end of construction. In any event, if the allowable bearing values given in this report are not exceeded, and if recommendations pertaining to inspection, reinforcing, balancing and drainage are followed, it is felt that differential movement can be held to a tolerable magnitude. At shallow foundation depths across the site, these soils were found to have an average allowable bearing capacity on the order of 1200 to 3500 psf. In general, foundations located on a minimum of 3 feet of this fine granular deposit could be designed for a minimum pressure of 250 psf.

Soil Type No. 2 classified as a silty clay (CL) of fine grain size. Soil Type No. 2 is of moderate plasticity and water content and of moderate density.

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These soils have a tendency to expand upon the addition of moisture with swell pressures on the order of 1715 psf being considered typical. While this magnitude of expansion should not be sufficient to affect the heavy structural members of the building, it can cause some movement beneath light structural members and floor slabs on grade. These soils will have a slight tendency to long-term consolidate under applied foundation pressures. However, if the allowable bearing values given are not exceeded, we feel that differential movement would be tolerable. This soil group was found to have an allowable bearing value on the order of 2500 to 3500 In order to resist the remaining potential swell psf maximum. of these soils at the existing 13 to 19 percent water content range, a minimum pressure of 1500 psf will be required for design of the foundations. Please note that in the southwest part of the site soils of this group occur in such a low density state that we cannot recommend directly bearing footings on them.

Soil Type Nos. 3 and 4 also classified as a silty clay (CL), like Soil Type No. 2 previously described. However, the sand content of these soils varied considerably as shown on the soil summary sheets. The expansion and settlement characteristics of these soil groups will be

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nearly identical to those previously described for Soil Type No. 2. Allowable bearing values on the order of 1500 to 3500 psf maximum would be associated with this soil group. Required minimum contact pressures could range from 1500 to 2000 psf for these soils.

Soil Type No. 5 classified as silty clay (CL) of fine to very fine grain size. Soil Type No. 5 is typical of the formational shale which underlies the site and serves as bedrock in the area. Soil Type No. 5 is plastic, of very low permeability and of high to very high density. The shales are expansive in nature with swell pressures on the order of 1330 psf being measured. Should drilled piers be used for the building, the expansive nature of the fine grained bedrock must be given consideration. Owing to its initial high density condition, these soils would have virtually no tendency to long-term consolidate. At a penetration of 5 feet into the shale layer, tip bearing capacities on the order of 15,000 psf could be achieved. Where the shale occurs at suitable depths for shallow type foundations under full basements or shallower structures, maximum allowable pressures varying from 2000 psf (in the severely weathered zone) to 6000 psf are recommended. Minimum contact pressures

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of 1300 to 1500 psf are likely. Soil Type No. 5 was found to contain sulfates in detrimental quantities.

Free water was found in the majority of the test borings placed on the site. The depth to this free water table varied from 12 to 18 feet over the site. Each building site should be investigated to determine the depth to free water, if any, prior to planning basements on the sites. In general, this free water is believed to be associated with seepage from area irrigation ditches and from nearby irrigated properties, and can therefore, be expected to continue to exist for the foreseeable future.

#### CONCLUSIONS AND RECOMMENDATIONS:

Since the exact magnitude and nature of the foundation loads are not precisely known at the present time, the following recommendations must be somewhat general in nature. Any special loads or unusual design conditions should be reported to Lincoln-DeVore so that changes in these recommendations may be made, if necessary. However, based upon our analysis of the soil conditions and project characteristics previously outlined, the following recommendations are made.

In general, the soils found across the subdivision will form a reasonably good base of the proposed residential structures. Silty sands of low to moderate density were encountered at or near the present ground surface in the region of the majority of the test borings drilled. For these non-expansive (or low expansive) areas, spread footings of various widths, in conjunction with a reinforced concrete grade beam stem wall, will probably be the most suitable foundation type, if the higher expansive clays are not located within 3 feet of the bottom of the foundations.

For those areas of the subdivision where the clays are encountered, foundations must be designed

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with the expansive potential of the subsurface soils in mind. The foundation configuration which can be used on the expansive clays will depend upon the magnitude of foundation loads exerted by the residential units as well as the exact degree of expansion anticipated from the soils. Several foundation types are acceptable for use on these clays. These foundation configurations would include, but are not limited to:

- 1) The first option would consist of the engineered no footing design, with the stem wall resting directly on the ground surface. The judicious use of voids would be employed to balance the structure and to increase the contact stresses beneath any very light walls. For most moderately loaded foundation systems, this voided stem wall design would probably prove satisfactory considering the magnitude of expansion pressures encountered across the subdivision, and the anticipated foundation loads for these single family dwelling units. We would anticipate that the majority of the foundation systems used on the clays across the subdivision will fall into this category.
- 2) A balanced pad and grade beam type of foundation system would form the second general foundation option. This alternative would involve the use of small bearing pads beneath a reinforced concrete grade beam. The grade beam would be continually voided between pads with the foundation loads being transferred by the pads only, and not the grade beam between pads. This foundation alternative will probably be suitable for very light structures on clays of high expansion potential. This configuration generally allows the designer to maintain a fairly high minimum dead load pressure.

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3)

The third option would consist of a drilled pier and grade beam system. The expansive clays do have side frictional effects which must be taken into account when designing the drilled piers. The diameter and length of the pier must be balanced so that the appropriate load carrying capacity is developed while maintaining enough minimum pressure to prevent upward movement of the piers as a result of expansive action. The grade beam would span from pier to pier and be continually voided between these bearing points. This foundation type would be required where the structural tolerance of differential movement is very small, or where full basement construction would locate foundations of significant loads close to or in soft soils.

- 4) The fourth foundation system could consist of a structural slab thickened under areas of bearing walls and concentrated loads. This type, basically a modified mat foundation, would be used in areas of low expansive, low density soils to support light and moderate weight residential structures. The use of the thickened slab foundation could aid in minimizing excavation, filling and recompaction of existing soils. Careful proportioning of thickened areas to balance and distribute loads and the use of more extensive reinforcing steel than is usual in residential slabs would be imperative with this foundation option.
- 5) The fifth and final foundation configuration would essentially be a combination of one of the preceding alternatives in conjunction with an overexcavated, compacted, granular pad. The depth of overexcavation would be related to the expansion potential of the clays as well as the nature of the residential units. Typical depths of overexcavation should range from about 3 to 10 feet. After overexcavation, a compacted granular pad using non-expansive, non-free draining soils could be constructed, maintaining a minimum of 90% of the soil's modified maximum Proctor dry density, ASTM D-1557. The purpose of this compacted pad is not entirely

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overcome the expansive potential of the clays, but rather to provide a "buffer" zone between the clays and the foundations. A designed foundation system, similar to one of the preceding alternatives, would then be constructed on top of the granular pad. Frequent density tests would be required during pad construction to ensure that an adequate density level is being maintained. This option would also be used if any areas of uncontrolled fill are encountered during the excavation process.

At the present time, it is difficult

to establish the exact maximum and minimum allowable design parameters for each residential building site across the subdivision. As noted earlier, the foundation soils are somewhat variable in terms of their classification and engineering characteristics. The engineering properties given in this report were based upon those soil materials encountered in our subsurface exploration program. While it is unlikely that drastically different soil types will be encountered during excavation for foundations, the possibility exists that intermediate variations between several of the soil types outlined here could be encountered.

It must, therefore, be recommended that the open foundation excavation be inspected prior to the placing of forms to establish the appropriate design parameters for each individual building site. Further exploration on a building site to building site basis may be warranted. At

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the time of inspection or further investigation, the maximum and minimum bearing values can be established and recommendations made as to the suitable foundation type for that particular building site. Also, this inspection will ensure that no debris, soft spots, or areas of unusually low density are located within the foundation region. Any changes in the recommendations included in this report can easily be made at the time of such inspection.

Regardless of the foundation type used, it is recommended that the foundation components be balanced to lower the possibility of differential movement. This balancing will help the buildings move more or less as single units, rather than in a differential manner. The foundation system should be proportioned such that the pressure on the soil is approximately the same throughout the building. The judicious use of voids beneath very light walls will help balance the structure, as well as to develop the minimum design pressures dictated by the expansive clays. Using the criterion of dead load plus approximately one-half the live load, the contact pressures should be balanced to within +300 psf beneath all load bearing walls throughout the residential units. For the sandier soils, isolated interior column pads should be designed for pressures of slightly less than the average selected for the bearing

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walls. On the clays, isolated pads should be designed for pressures of slightly more than the exterior wall average. Using whichever criterion is applicable, we would recommend balancing these internal pads on pressures of approximately 150 psf more or less than the average of the exterior walls.

To help ensure that the structure moves more or less as a single unit rather than in a differential manner, we would recommend that all stem walls be supported by a grade beam capable of spanning at least 15 feet. This grade beam would apply to both interior and exterior load bearing walls. Such a grade beam should be horizontally reinforced continuously around the structure with no gaps or breaks in reinforcing steel unless they are specially designed. Beams should be reinforced at both the top and the bottom with the major reinforcement being located at the top where foundations bear on the more expansive soils. Otherwise, major reinforcing should be approximately equally distributed between the top and bottom of the stem wall section. All interior bearing walls should rest on a grade beam and foundation system of their own and should not be allowed to rest on a thickened slab section or "shovel" footing except

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where the entire foundation system of a structure is of the thickened slab type.

Where the stem walls are relatively shallow, vertical reinforcing will probably not be necessary. However, where the walls retain soil in excess of about 5 feet in height such as partial or full basement walls, vertical reinforcing may be necessary to resist the active pressure of the soils along the wall exterior. To aid in designing such vertical reinforcing, the following equivalent fluid pressures can be utilized:

40 pcf for wall backfill (at least 2 feet thick) consisting of pitrun sand and gravel or other well draining granular material.

It should be noted that the above values should be modified to take into account any surcharge loads applied at the top of the walls as a result of stored goods, live loads on the floor, machinery, or any other externally applied forces. The above equivalent fluid pressures should also be modified for the effects of any free water table.

The bottom of all foundation com-

ponents should rest a minimum of  $l\frac{1}{2}$  feet below finished grade or as required by the local building codes. Foundation components must not be placed on frozen soils.

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Where floor slabs are used, they may be placed directly on grade or over a compacted gravel blanket of 4 to 6 inches in thickness. Under no circumstances should this gravel pad be allowed to act as a water trap beneath the floor slab. In areas where very expansive soils occur at grade, it could be necessary to overexcavate in slab-on-grade areas in order to provide a minimum of 2 feet of compacted granular, non-expansive fill under the slabs. A vapor barrier is recommended beneath any and all floor slabs on grade which will lie below the finished exterior ground surface. All fill placed beneath the interior floor slabs must be compacted to at least 90% of its maximum Proctor dry density, ASTM D-698.

All floor slabs on grade must be constructed to act independently of the other structural portions of the building. These floor slabs should contain deep construction or contraction joints to facilitate even breakage and to help minimize any unsightly cracking which could result from differential movement. Floor slabs on grade should be placed in sections no greater than 20 feet on a side. In some of the areas where 2 feet of non-expansive fill has been placed, it may be possible to delete this "floating" slab construction from the design if the fill is not underlain by highly expansive soil. Prior to constructing

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slabs on grade, all existing topsoil and organics must be removed from the building interior. Likewise, all foundations must penetrate the topsoil layer.

Any interior, non-load bearing partitions which will be constructed to rest on the floor slab should be constructed with a minimum space of 1½ inches at either the top or bottom of the wall. The bottom of the wall would be the preferred location for this space. This space will allow for any future potential expansion of the subgrade soils and will prevent damage to the wall and/or roof section above which could be caused by this movement.

in the foundation area both during and after construction to prevent the ponding of water. The ground surface around the building should be graded so that surface water will be carried quickly away from the structure. The minimum gradient within 10 feet of the building will depend upon surface landscaping. Bare or paved areas should maintain a minimum gradient of 2%, while landscaped areas should maintain a minimum gradient of 5%. Roof drains must be carried across all backfilled areas and discharged well away from the structure.

Adequate drainage must be provided

The existing drainage in the area must either be maintained or improved. Water should be drained away from the structures as rapidly as possible and should not

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be allowed to stand or pond in the area of the buildings. The surface drainage across the entire subdivision must be carefully controlled to prevent infiltration and saturation of the foundation soils. All backfill around the buildings should be compacted to a minimum of 90% of its maximum Proctor dry density, ASTM D-698. Roof drains must be carried across all backfilled regions and discharged well away from the structure.

A subsurface peripheral drain, including an adequate gravel collector, sand filter and perforated drain pipe, should be constructed around the outside of the building at foundation level. Dry wells should not be used anywhere on this site. The discharge pipe should be given a free gravity oulet to the ground surface. If "daylight" is not available, a sealed sump and pump should be used.

Due to the varying condition of the soil materials encountered, construction of basements may be difficult and dewatering techniques may be necessary during construction. Additionally, problems with basement foundations may be encountered during periods of strong seepage due to uplift against the foundation and the possibility of seepage into the basement. While we would not

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entirely recommend against the construction of basements on this site, it is strongly recommended that basement or half basement foundations be well sealed and that they be provided with the peripheral drains and underslab drainage layers described in this report. It is extremely important that the subsurface drains be properly installed and in good working order. We also strongly recommend that a subsurface soils investigation tailored to basement construction be performed on a site specific basis where such construction is planned.

Samples of the typical surficial soils were evaluated using the Hveem-Carmany method to determine their support characteristics. These soils (unstable unless confined, according to the test) were found to have a Hveem (R) value of 9. For a multiple family subdivision of this type, we believe a reasonable traffic mix would include 70-75% passenger cars, 20-25% pickup trucks and 5% or less of single - or multiple - axle medium and heavy trucks. For such a traffic mix, we have evaluated the Hveem-Carmany characteristics of the soil at several levels of traffic volume. The table below indicates the recommended pavement section at each traffic volume:

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ADT	Aggregate Base For Alternate			
	<u>3"</u>	<u>4"</u>	<u>5"</u>	
Under 500	12	9	5	
500 <del>,</del> 1000	14	11	8	下にたね
Over 1000	15	12	9	「大学校学生

We suggest that the aggregate used for the hot-mix bit develop course and the base course conform to Colorado DOT gradies and class 6 gradation requirements, respectively. The bit minous mixture used should develop a Total Resistance File  $(R_t)$  of at least 87.

In general, no major excavation difficulties are anticipated. In some areas, isolated **concles** could occur in the Type No. 4 Soils. If encountered in **wis** or full basement excavations, the Mancos Shale is generally rippable for the upper several feet that is highly weakered. Deeper (basement) excavations may also require bracing sloping of sidewalls. The extent of such safety provider. if needed, must be determined from the results of site

The soils on this site we't to contain sulfates in detrimental quantities. The Type II Cement would be recommended in all concrete with the soil. Under no circumstances should calcin

-22-

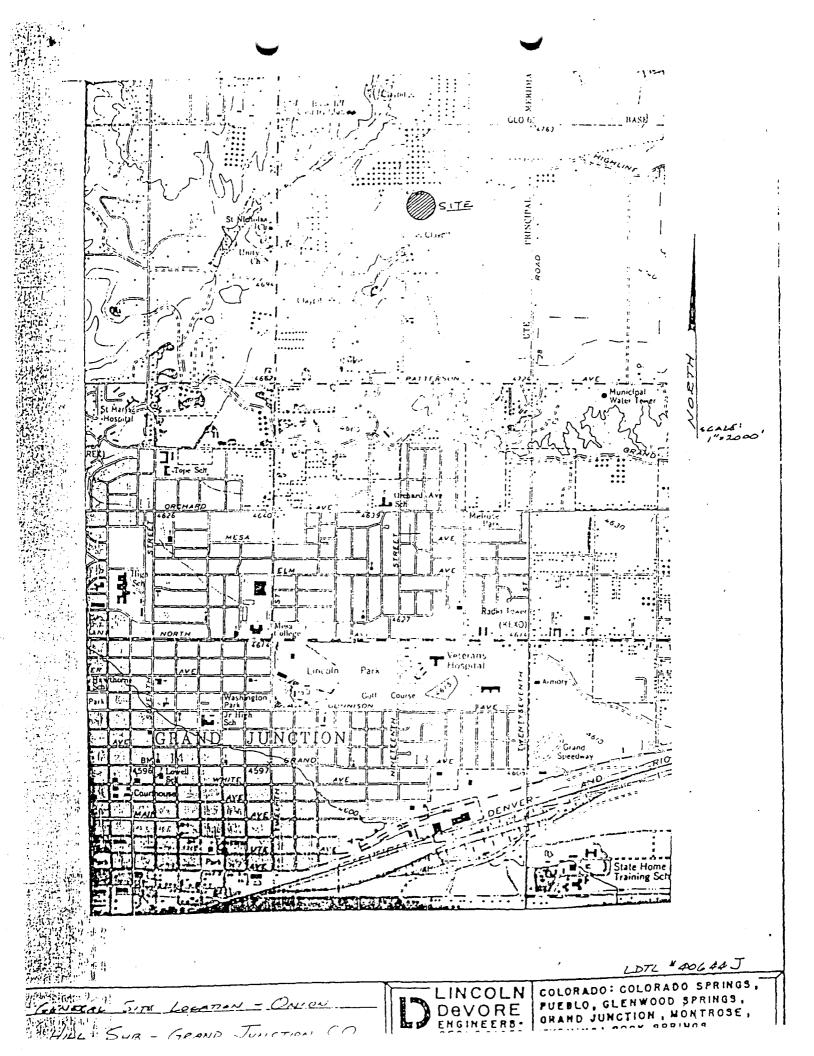
ever be added to a Type II Cement. In the event that Type II Cement is difficult to obtain, a Type I Cement may be used, but only if it is protected from the soils by an impermeable membrane.

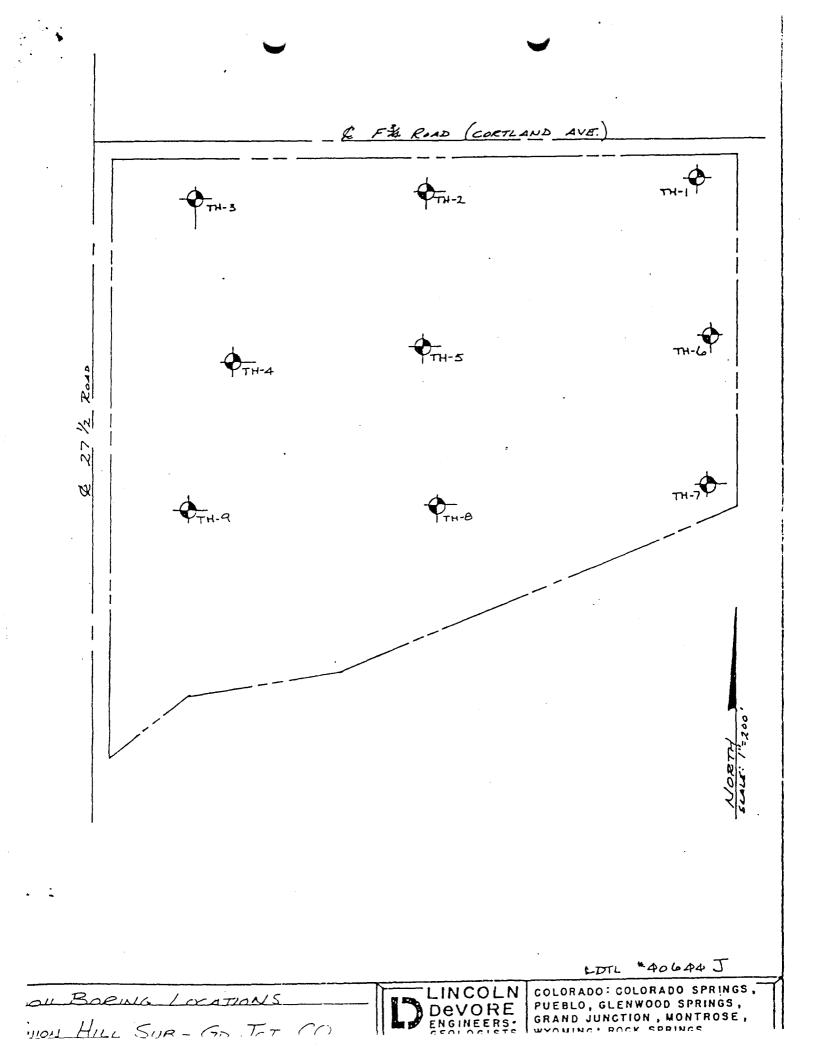
The open foundation excavation must be inspected prior to the placing of forms and pouring of concrete to establish that adequate design bearing materials have been reached and that no debris, soft spots or areas of unusually low density are located within the foundation region. All fill placed below the foundations must be fully controlled and tested to ensure that adequate densification has occurred.

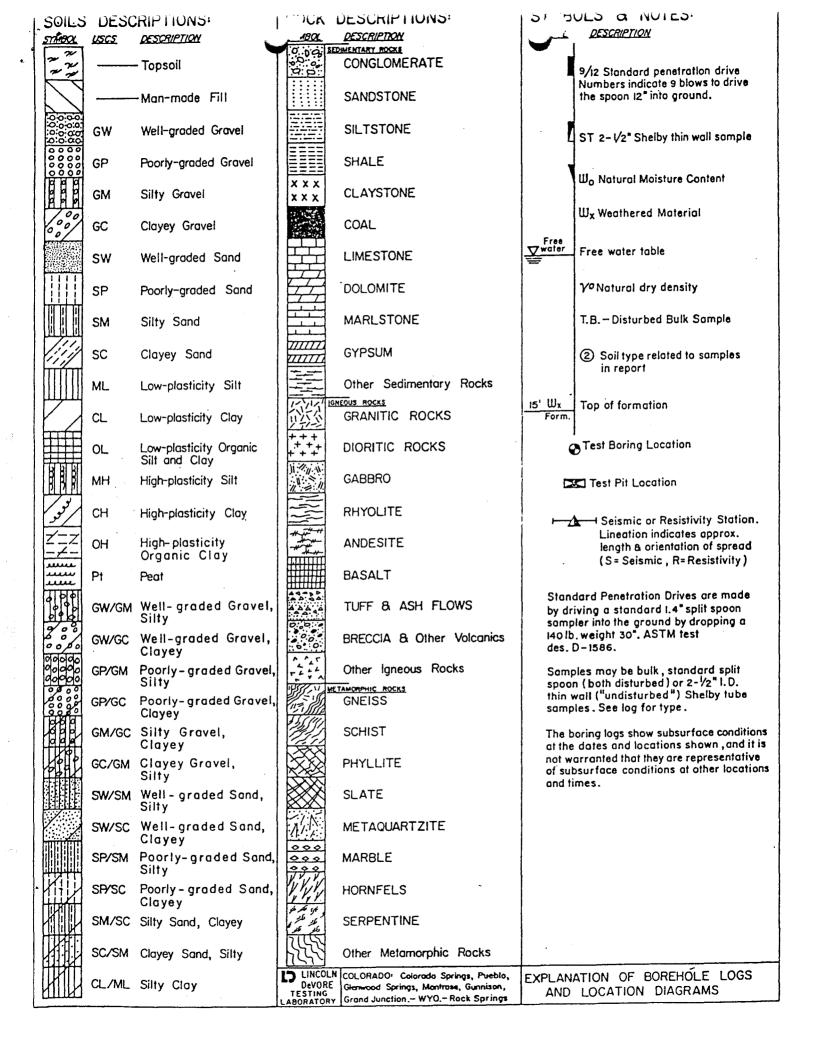
It is extremely important due to the nature of data obtained by the random sampling of such a heterogeneous material as soil that we be informed of any changes in the subsurface conditions observed during construction from those outlined in the body of this report. Construction personnel should be made familiar with the contents of this report and instructed to relate any differences immediately if encountered.

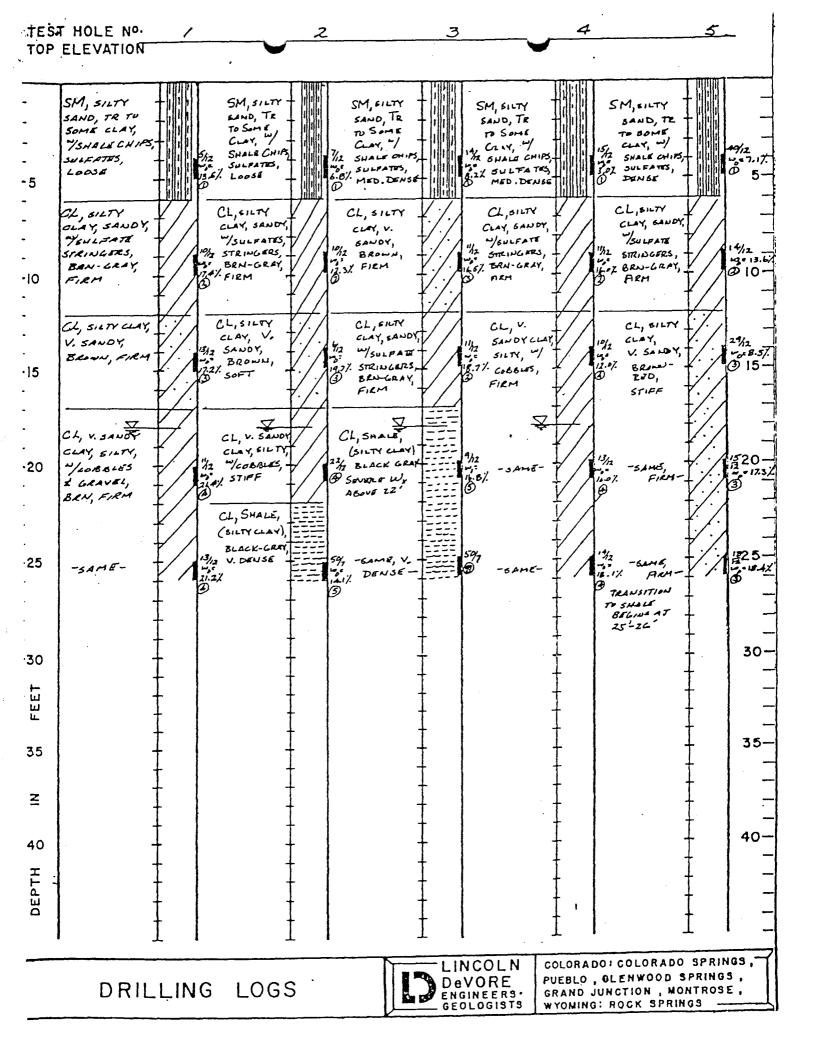
It is believed that all pertinent points concerning the subsurface soils on this site have been covered in this report. If questions arise or further information is required, please feel free to contact Lincoln-DeVore at any time.

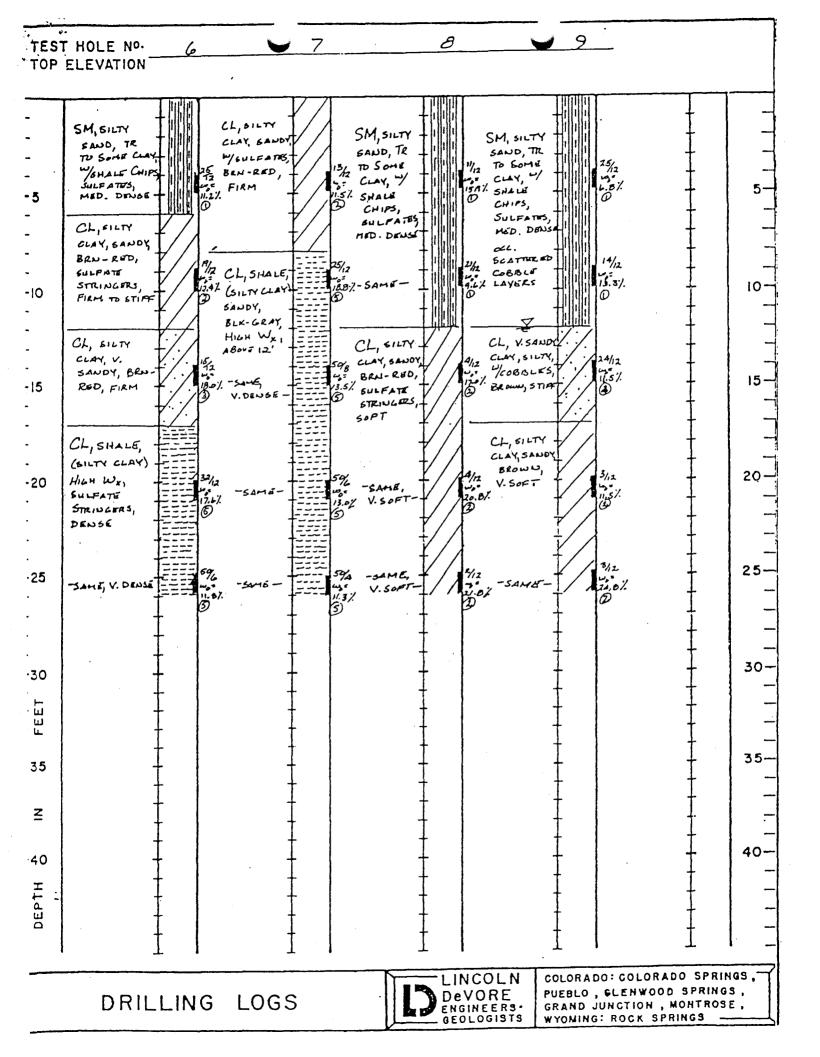
-23-











SUM	MARY SHEET
oil Sample5M	
ocation ONION HILL SUBDIVISION- GD. JET.	CO Date 8-11-81
ocation <u>Own Hill Suspivision</u> -Go. Jer., pring NoDepth ample No1	
	·
Natural Water Content (w)% Specific Gravity (Gs)	In Place Density (70)pcf
IEVE ANALYSIS:	
ieve No. % Passing	Plastic Limit P.L <u>17.4</u> %
1/2"	Liquid Limit L. L. 21.2 %
11	Plasticity Index P.1. <u>3.8</u> % Shrinkage Limit%
/2 <sup>11</sup> /2 <sup>10</sup> /00.0	Flow Index
V8 " <u>97.3</u> 94.0	Shrinkage Ratio% Volumetric Change%
0	Lineal Shrinkage%
07.4	,
0 <u>66.6</u> 00 <u>52.4</u>	
0041.0	MOISTURE DENSITY: ASTM METHOD
	Optimum Moisture Content
	Maximum Dry Density -7dpcf
	California Bearing Ratio (av)% Swell:Days%
· · · · · · · · · · · · · · · · · · ·	Swell against <u>/zz</u> psf Wo gain <u>/5.0</u> %
YDROMETER ANALYSIS:	
rain size (mm) %	BEARING:
0.02 21.3	Housel Penetrometer (av)psf
0,005 13.3	Unconfined Compression (qu)psf
	Plate Bearing:psf
	Inches Settlement Consolidation % under psf
	PERMEABILITY:
	K ( + 202C)
•	K (at 20°C) Void Ratio
•	Sulfates ppm.

.

. SUM	IMARY SHEET
Soil SampleCL	Test No 40644 J
•	
Boring No Depth	
Location_ <i>Owion_Hill_Sug - Go_Tct, CO</i> Boring NoDepth Sample No2	Test by ADD
Natural Water Content (w)% Specific Gravity (Gs)	In Place Density (70)pcf
SIEVE ANALYSIS:	
Sieve No. % Passing	Plastic Limit P.L%
1 1 /2*	Liquid Limit L. L. 25.8%
1 1/2 <u>"</u> ]"	Plasticity Index P.1. <u>10.1</u> % Shrinkage Limit
3/4"	
1/2".	Flow Index
1/2" 4	Volumetric Change%
1099.7	Lineal Shrinkage%
20	,
4096.6	
10087.2	MOISTURE DENSITY: ASTM METHOD
20078.7	
	Optimum Moisture Content
	Maximum Dry Density -rdpcf
	California Bearing Ratio (av)%
	Swell:Days%
HYDROMETER ANALYSIS:	Swell against <u>1715</u> psf Wo gain <u>14</u> 1 %
Grain size (mm) %	
	BEARING:
Grain size (mm) %	
	Housel Penetromèter (av)psf
0.02 42.5	
0.02 42.5	Housel Penetromèter (av)psf Unconfined Compression (qu)psf Plate Bearing:psf Inches Settlement
0.02 42.5	Housel Penetrometer (av)psf Unconfined Compression (qu)psf Plate Bearing:psf
0.02 42.5	Housel Penetrometer (av)psf Unconfined Compression (qu)psf Plate Bearing:psf Inches Settlement
0.02 42.5	Housel Penetrometer (av)psf Unconfined Compression (qu)psf Plate Bearing:psf Inches Settlementpsf Consolidation % under psf
0.02 42.5	Housel Penetrometer (av)psf Unconfined Compression (qu)psf Plate Bearing:psf Inches Settlement
0.02 42.5	Housel Penetrometer (av)psf Unconfined Compression (qu)psf Plate Bearing:psf Inches Settlementpsf Consolidation % under psf PERMEABILITY:
0.02 42.5	Housel Penetrometer (av)psf Unconfined Compression (qu)psf Plate Bearing:psf Inches Settlementpsf Consolidation % under psf PERMEABILITY: K (at 20°C)
0.02 42.5	Housel Penetrometer (av)psf Unconfined Compression (qu)psf Plate Bearing:psf Inches Settlementpsf Consolidation % under psf PERMEABILITY:
0.02 42.5	Housel Penetrometer (av)psf         Unconfined Compression (qu)psf         Plate Bearing:psf         Inches Settlement         Consolidation % under psf         PERMEABILITY:         K (at 20°C)         Void Ratio
0.02 42.5	Housel Penetrometer (av)psf Unconfined Compression (qu)psf Plate Bearing:psf Inches Settlementpsf Consolidation % under psf PERMEABILITY: K (at 20°C)
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0.02 42.5	Housel Penetrometer (av)psf         Unconfined Compression (qu)psf         Plate Bearing:psf         Inches Settlement         Consolidation % under psf         PERMEABILITY:         K (at 20°C)         Void Ratio
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0.02 42.5	Housel Penetrometer (av)psf         Unconfined Compression (qu)psf         Plate Bearing:psf         Inches Settlement         Consolidation % under psf         PERMEABILITY:         K (at 20°C)         Void Ratio
0.02 42.5	Housel Penetrometer (av)psf         Unconfined Compression (qu)psf         Plate Bearing:psf         Inches Settlement         Consolidation % under psf         PERMEABILITY:         K (at 20°C)         Void Ratio

SU	IMMARY SHEET
Soil SampleCL	Test No 20644 J
Location_Owen Hill Sus Go. JEr., C Boring NoDepth	0 Dote <i>B-11-B1</i>
Sample No	Test by ADD
Natural Water Content (w)% Specific Gravity (Gs)	In Place Density (70)pcf
SIEVE ANALYSIS:	
Sieve No.       % Passing         1       1/2"	Plastic Limit P.L.       16.4       %         Liquid Limit L. L.       25.2       %         Plasticity Index P.I.       8.8       %         Shrinkage Limit       %       %         Flow Index       %       %         Shrinkage Ratio       %
4     99.1       10     97.7       20     92.9       40     87.9       100     78.5	Volumetric Change% Lineal Shrinkage% MOISTURE DENSITY: ASTM METHOD
200 <u>66.3</u> HYDROMETER ANALYSIS:	Optimum Moisture Content
Grain size (mm) %	BEARING:
0.02 <u>36.7</u> 0.005 <u>22.9</u>	Plate Bearing:psf Inches Settlementpsf
	PERMEABILITY:
• •	K (at 20 <sup>o</sup> C) Void Ratio
·	Sulfates ppm.
SOIL ANALYSIS	LINCOLN-DeVORE TESTING LABORATORY COLORADO SPRINGS, COLORADO

SUMN	ARY SHEET
oil SampleCL	Test No 40644 J
ocation Dwon Hill SUB- Go JET. CO	
pring No Depth pring No Depth pring No	
Natural Water Content (w)% Specific Gravity (Gs)	In Place Density (70)pcf
SIEVE ANALYSIS:	
Sieve No.       % Passing         1/2"	Plastic Limit P.L.       19.9       %         Liquid Limit L. L.       28.8       %         Plasticity Index P.I.       9.0       %         Shrinkage Limit       %       %         Flow Index       %       %         Shrinkage Ratio       %       %         Volumetric Change       %       %         Volumetric Change       %       %         MOISTURE DENSITY: ASTM METHOD       Optimum Moisture Content
Grain size (mm) %	BEARING:
<u>0.02</u> <u>28.9</u> <u>0.005</u> <u>20.7</u>	Housel Penetrometer (av)psf Unconfined Compression (qu)psf Plate Bearing:psf Inches Settlement Consolidation % under psf
· · · · · · · · · · · · · · · · · · ·	PERMEABILITY:
	K (at 20°C) Void Ratio
	Sulfates ppm.
	LINCOLN-DeVORE TESTING LABORATORY

· SUM/	MARY SHEET
Dil SampleCL	Test No. 406 44 J
protion Onion Hill Sug - Gp. Jer., C	0 Date <u>8-11-81</u>
ample No	Test by <u>ADD</u>
Natural Water Content (w)% Specific Gravity (Gs)	In Place Density (70)pcf
IEVE ANALYSIS:	
ieve No.       % Passing         1/2"	Plastic Limit P.L       20.4       %         Liquid Limit L. L       43.6       %         Plasticity Index P.I.       23.2       %         Shrinkage Limit       %       %         Flow Index       %       %         Shrinkage Ratio       %       %         Volumetric Change       %       %         Lineal Shrinkage       %       %         MOISTURE DENSITY: ASTM METHOD       Optimum Moisture Content       %         Maximum Dry Density -7d       pcf         California Bearing Ratio (av)       %         Swell:
rain size (mm) %	BEARING:
· 0.005 52.7	Housel Penetrometer (av)psf Unconfined Compression (qu)psf Plate Bearing:psf Inches Settlement Consolidation % under psf
	PERMEABILITY:
	K (at 20 <sup>0</sup> C) Void Ratio
	Sulfates ppm.

### GENERAL PROJECT REPORT THE KNOLLS SUBDIVISION

#### A. Project Description

The proposed Knolls Subdivision is located at the southeast corner of  $27\frac{1}{2}$  Road and Cortland Avenue. The project will consist of approximately 33.8 acres and is more particularly described as being located in the SW<sup>1</sup>/<sub>4</sub> of the NE<sup>1</sup>/<sub>4</sub> of Section 1, Township 1 South, Range 1 West, of the Ute Principle Meridian. This proposal will be to rezone this entire area into a Planned Residential development consisting of 51 single family homesites and 23 patio homes platted on common open space. Filing One of The Knolls Subdivision, which approval of the Final Plan is also being requested with this application, will contain nine of these single family lots. These lots in Filing One, ranging in size from 0.31 acres to 0.64 acres, will be situated on the extension of the existing Ridge Drive into a cul-de-sac.

As part of this application, it is being proposed to include Lot 2 of the St. Matthews Episcopal Church Subdivision into the development. Lot 2 of this subdivision, which was platted in May of 1988 and contains approximately 5.53 acres, will be replatted into single family lots. In return, St. Matthews Episcopal Church will be deeded a 4.80 acre tract at the corner of 27½ Road and Cortland Avenue. This is shown as Tract A on the Final Plat.

#### B. Public Benefit

The housing market for the Grand Junction vicinity still demands new homesites. This area is attractive to buyers due to its proximity to Horizon Drive, Patterson Road, Bookcliff Country Club and the upper-class developments that surround the site. This development will be an "in-fill" project on vacant land that currently has no use. It does provide a frequently used walking and jogging area, which will be maintained in the proposed development plan.

#### C. Project Compliance, Compatibility, and Impact

Recent history of this project is that a Preliminary Plan was heard before the Grand Junction Planning Commission and the City Council on July 9 and August 7, 1996, respectively. In short, the applicant received approval to eliminate the connection of Ridge Drive from Spring Valley Subdivision to 27½ Road and preliminary plan approval for Filing One. However, a new and revised Preliminary Plan was required and resubmitted. Therefore, this submittal of The Knolls Subdivision consists of a new Preliminary Plan and the Final Plan/Plat for Filing One. Along with this, a rezone of a portion of site is being sought to bring the entire site into a PR-4 zoning.

As touched on briefly, this site will be an "in-fill" development. Spring Valley Subdivision is located at the east boundary of the site, Crown Heights Subdivision is located directly to the north across Cortland Avenue, and Ptarmigan Ridge North and Bell Ridge Subdivisions are located directly to the west across  $27\frac{1}{2}$  Road. To the south of this parcel is one single family tract, 2.9 acres in size, and a large undeveloped parcel approximately 27 acres in size. Access to the project will be via Cortland Avenue. Frontage with Cortland will be improved to a collector street standard as detailed in the City of Grand Junction Major Street Standards. For Filing One, the improvements to Ridge Drive will be to match existing improvements which will consist of a vertical curb and gutter along with a detached 4½ foot wide sidewalk. Remaining interior streets that will be constructed in future filings will be consistent with the urban residential street standard (44 ft. R.O.W.) also as detailed by the City of Grand Junction. In addition, the Applicant is seeking approval to construct a "private street" section in a future phase. This private street is being proposed with a right-of-way width corresponding to 33 feet and will be comprised of a 26 foot asphalt mat with a 2<sup>1</sup>/<sub>2</sub> foot concrete curb and gutter. No sidewalk is be proposed with this section.

As existing developments are currently situated around this site, all utilities are available for connection into the proposed Knolls Subdivision. The proposed routing for the sanitary sewer and domestic water lines are depicted on the revised Preliminary Plan, along with the fire hydrant locations. There will be no special or unusual demands on these utilities. As this project has been reviewed recently, there has been no indication of any adverse impact to public facilities.

Included as part of this submittal is soil information gathered both from the Soil Conservation Service and a Subsurface Soils Investigation prepared by Lincoln Devore in 1981. Data contained in this information is typical of the area and does not appear to pose any risk to developing at this site. This information has been submitted as required. During the previous application and subsequent review, there was an area of the site that was identified as potential wetlands. The Applicant has since employed the services of a wetland consultant, Bio Environs, to delineate possible wetlands for the planning of this project. This information has been included in the Preliminary Drainage Report.

#### D. Development Schedule and Phasing

. . .

 $k \in \mathcal{A}$ 

At this time it is anticipated that there will be four phases, or filings, associated with this development. Filing One, which approval of the Final Plan/Plat is being requested for, will be the nine lots fronting Ridge Drive. Construction of Filing One will be completed in the spring of 1997. Subsequent filings will be submitted for approval and constructed at six to 12 month intervals with the entire project being completed by the fall of 1999.

# FINAL DRAINAGE REPORT

## **FILING ONE**

## THE KNOLLS SUBDIVISION

## 27<sup>1</sup>/<sub>2</sub> ROAD & CORTLAND AVENUE

## **CITY OF GRAND JUNCTION**

Prepared For:

O. P. DEVELOPMENT COMPANY, L.L.C. c/o Robert C. Knapple 2421 Applewood Circle Grand Junction, Colorado 81506

September 1996

# **BANNER**

Banner Associates, Inc. • Consulting Engineers & Surveyors 2777 Crossroads Blvd. • Grand Junction, CO 81506 • (970)243-2242 605 E. Main • Suite 6 • Aspen, CO 81611 • (970)925-5857

# FINAL DRAINAGE REPORT

## FILING ONE

## THE KNOLLS SUBDIVISION

## 27<sup>1</sup>/<sub>2</sub> ROAD & CORTLAND AVENUE

## **CITY OF GRAND JUNCTION**

Prepared For:

O. P. DEVELOPMENT COMPANY, L.L.C. c/o Robert C. Knapple 2421 Applewood Circle Grand Junction, Colorado 81506

Prepared By:

**BANNER ASSOCIATES, INC.** 2777 Crossroads Boulevard Grand Junction, Colorado 81506

September 1996

## **CERTIFICATION**

I hereby certify that this Final Drainage Report for Filing One of The Knolls Subdivision was prepared under my direct supervision.

9. Ż David E. Chase Registered Professional Engineer State of Colorado, #24991 David E. Chase 24991

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# **I.** GENERAL LOCATION AND DESCRIPTION

## FINAL DRAINAGE REPORT THE KNOLLS SUBDIVISION

### SITE AND MAJOR BASIN LOCATION

Filing One of the Knolls Subdivision, being proposed by O. P. Development Co., is located in the southeast corner of the subdivision. The subdivision is located in the southeast corner of the intersection of 27<sup>1</sup>/<sub>2</sub> Road and Cortland Avenue, as shown on the Vicinity Map that is included in Appendix A of this report. Filing One is bounded to the east by Spring Valley Subdivision, and to the south, west, and north by undeveloped land. Development in the vicinity also consists of Crown Heights Subdivision in the north, single family homes and undeveloped land to the southwest, and Belle and Ptarmigan Ridge Subdivisions in the west.

### SITE AND MAJOR BASIN DESCRIPTION

The proposed Filing One of the Knolls Subdivision is approximately 4.4 acres in size. This area consists mostly of weeds with grass understory with surface grades ranging from 1 - 4% sloping downward to the southwest. Vegetation covers approximately 50 - 70% of the ground as observed in this region.

In researching the soils on the site, reference was made to the Soil Survey of the Grand Junction Area as issued by the U.S. Department of Agriculture, Soil Conservation Service, November 1955. The soil in the northern 20% of the filing is Fruita clay loam (Fe) and the southern 80% is Avalon loam (AvC) as described in Appendix A of this report. Both of these soils are classified as hydrologic soil type B, having moderate infiltration rates when thoroughly wetted.

# **II. EXISTING DRAINAGE CONDITIONS**

### MAJOR BASIN

In researching the floodplain hazard for the area, reference was made to the Flood Insurance Rate Map for the City of Grand Junction as produced by the Federal Emergency Management Agency, revised July, 1992. The existing site lies approximately 2,200 feet southeast of the 100-year flood delineation for Horizon Drive Channel. Therefore, no part of the proposed filing is within the 100-year flood limits.

### <u>SITE</u>

The northern boundary is adjacent to undeveloped land that drains to the southwest. This area may contribute some runoff to Filing One. The irregular eastern boundary is adjacent to developed land of Spring Valley Subdivision. Approximately 200 feet of Ridge Drive drains northwest into Filing One across a part of this eastern boundary. The southern boundary consists of an irrigation ditch that flows westward, preventing runoff from being introduced from any south areas. The existing topography of the area of Filing One slopes downward to the southwest, therefore no runoff is introduced from the west. The ultimate outfall point of the entire subdivision consists of a 12" corrugated metal pipe that drains westward under 27 1/2 Road into Belle Ridge Subdivision's Irrigation pond system. This CMP is approximately 1000 feet southwest of the western boundary of Filing One.

# **III. PROPOSED DRAINAGE CONDITIONS**

8.0

### **CHANGES IN DRAINAGE PATTERNS**

No change in drainage patterns is proposed for the lands adjacent to and surrounding Filing One. Proposed drainage patterns within the site will be modified, as is customary, to accommodate development and to better control surface flows to designed collection areas. A Preliminary Drainage Map is included in Appendix B that illustrates the existing drainage basin. Upon development, inlet and storm drain structures will be constructed under Ridge Drive for storm water runoff. Flows from this storm drain line will ultimately reach the outfall point of the entire subdivision and be discharged at historic levels into the existing 12" drain.

### MAINTENANCE ISSUES

Access to drainage and outlet structures are provided, by design, to be directly from the streets that border them. The Knolls Subdivision Homeowners Association will claim ownership and maintenance responsibilities for the drainage basin. IV. DESIGN CRITERIA & APPROACH

### **GENERAL CONSIDERATIONS**

Due to the isolation of the site on the north and west, the development to the east, and natural topography affecting runoff patterns to the south, larger scale master planning for drainage is difficult. Strategic location of detention ponds within future development of the entire subdivision site lends itself as an attractive and effective layout for stormwater collection. No constraints should be imposed on future adjacent development due to the development of this filing.

### HYDROLOGY

Hydrology calculations will be based on the 2 and 100-year rainfall events and precipitation based on the Depth-Duration-Frequency (DDF) Table "A-2" as obtained from the City of Grand Junction Stormwater Management Manual (SWMM), June 1994. Runoff calculations will be performed using the SCS Curve Number method. Detention basin design will be accomplished by the Modified Rational Method using Haestad Methods software for maximum volume required with historic flow release rates. Parameter selection and design procedures will be based on using a composite Curve Number, an IDF value corresponding to the largest time of concentration (Tc) obtained for each drainage basin and the respective basin area obtained by use of a planimeter or computer.

### HYDRAULICS

Hydraulic calculations will be accomplished by Manning's equation for gravity flow in circular channels using Haestad Methods FlowMaster Professional Edition and/or StormCAD software. Detention pond outlet structure design will be based on use of Haestad Methods Pond-2 software. Parameter selection will be determined by the pipe material selected, accompanying pipe characteristics and the City of Grand Junction standards and specifications for storm sewer construction. Analysis and design procedures will be based on individual and combined subcatchments within the development using Manning's formula and the Rational Method for storm sewer sizing. Again, pipeline sizing may be determined using Haestad Methods StormCAD software.

# V. RESULTS & CONCLUSIONS

#### **RUNOFF RATES**

Historic runoff rates for the entire parcel are tabulated below.

2 year storm:0 cfs100 year storm:1 cfs

The 0 cfs value for the 2-year storm event is qualified by noting the large basin area, relatively flat slope, and existing soil conditions. See appendix C for these calculations.

#### **COMPLIANCE**

Developing Filing One of this parcel will insignificantly affect its total runoff. The Composite Runoff Curve Number (CN) for this parcel does not change after Filing One's development. The hydraulically most distant point from the parcel's outfall point is used in determining the Time of Concentration, (Tc). This path does not change after developing Filing One, either. These calculations are in appendix D.

A developed Filing One, analyzed independently, produces the runoff rates shown below:

2 year storm:	0 cfs
100 year storm:	1 cfs

These flows will be released from Filing One's outfall point, a 12" diameter HDPE in Outlot A. Approximately 1000 feet of gently sloping, moderately vegetated terrain lies between this outfall point and the outfall point for the entire parcel. Therefore, the flows released from Filing One will insignificantly affect the flows released from the entire subdivision.

# APPENDIX A

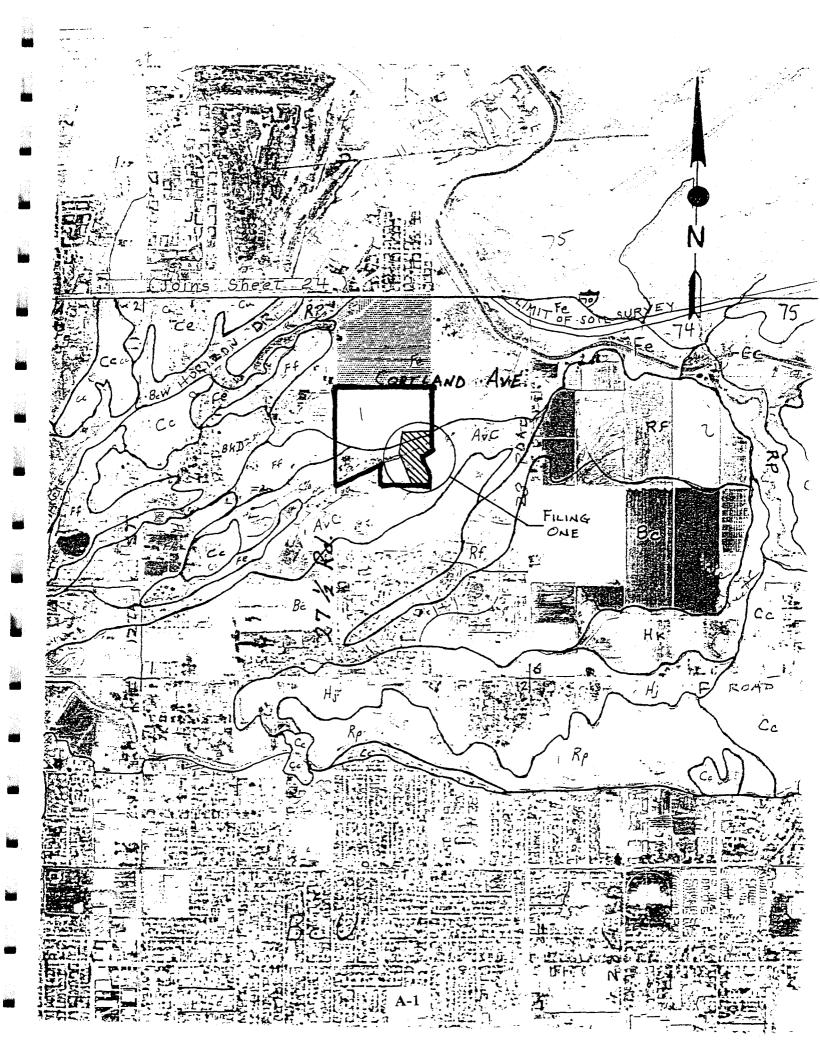
and a second

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No.ed

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. Site



## NONTECHNICAL SOILS DESCRIPTION REPORT

Map Symbol	Soil name and description
AVC	Avalon loam, 5 to 25 percent slopes
	This unit is unsuited for row crops due to slope. This unit is best suited to a permanent cover crop such as irrigated pastureland. Because of the slope, sprinkler or drip irrigation is most suitable for the less sloping areas. Irrigation water needs to be applied at a rate that insures optimum production without increasing deep percolation, runoff, and erosion.
	This unit consists of very deep, well drained soils on intermediate valley terraces. These soils formed in loess modified alluvium derived dominantly from mixed shale and sandstone sources. The surface layer is sandy loam about 3 inches thick. The upper 14 inches of the subsoil are loam, and the lower 13 inches are clay loam. The upper 12 inches of the substratum are clay loam, and the lower part to a depth of more than 60 inches is gravelly loam. Permeability of this soil is moderate. Available water capacity is high. Effective rooting depth is 60 inches or more. Runoff is rapid, and the hazard of water erosion is high.
	Capability Subclass 7C; nonirrigated
	Capability classification is the grouping of soils to show, in a general way, their suitability for most kinds of farming. It is a practical classification based on limitations of the soils, the risk of damage when they are used, and the way they respond to treatment. The soils are classified according to degree and kind of permanent limitation, but without consideration of major and generally expensive landforming that would change the slope, depth, or other characteristics of the soils; without consideration of possible unlikely major reclamation projects.
	Class VII - Not suited for cultivation. Very severe limitations. Suited for range, woodland or wildlife uses if carefully managed. Usually cannot apply physical practices such as pitting, furrowing, seeding, etc.

Marrie

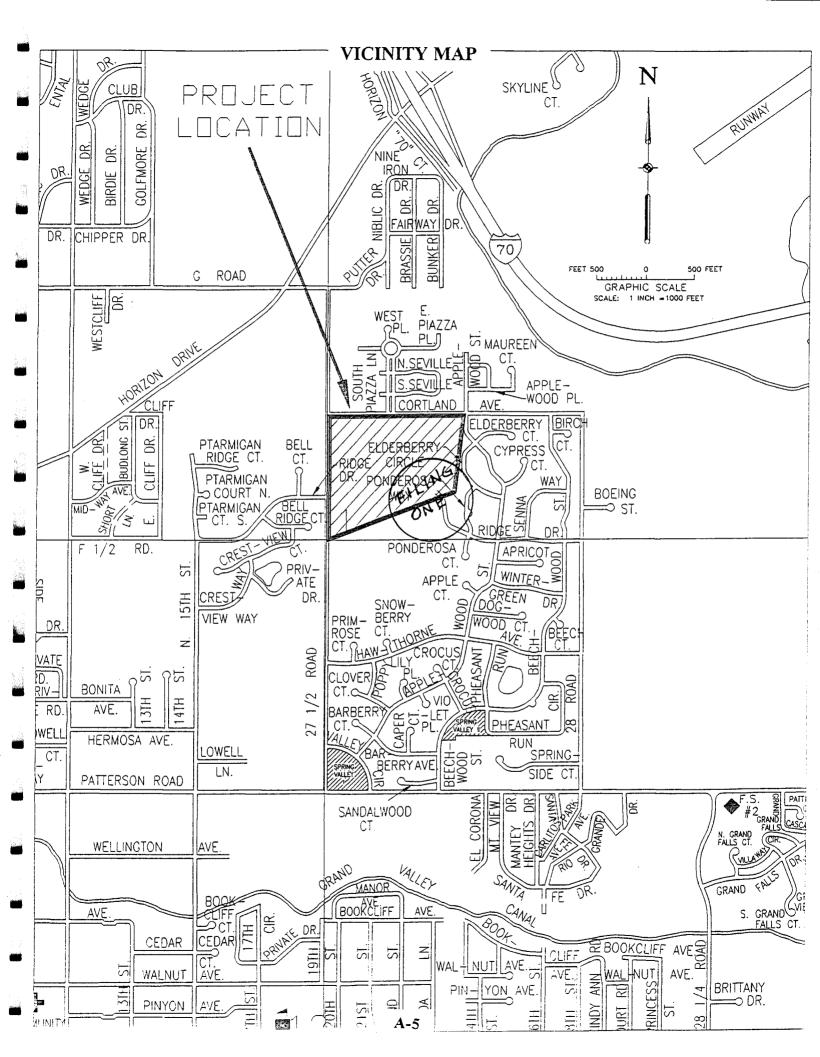
#### NONTECHNICAL SOILS DESCRIPTION REPORT DAvid Hartman

Map Symbol	Soil name and description
	C - Climate is the major hazard. Growing season may be very short; there is a shortage of rainfall or both.
 Fe	Fruita clay loam, 0 to 2 percent slopes
	This unit is suited for irrigated crops. It has few limitations. Furrow and sprinkler irrigation is suited to this soil. Irrigation water needs to be applied at a rate that insures optimum production without increasing deep percolation, runoff, and erosion. Use of pipe or ditch lining reduces water loss and deep percolation. Tilth and fertility can be improved by returning crop residue to the soil and using a suitable rotation. Excessive cultivation can result in the formation of a tillage pan. This pan can be broken by subsoiling when the soil is dry. Because of the undulating topography, onsite investigations may be needed before leveling.
	This unit consists of deep, well drained soils on old terraces. These soils formed in residuum derived dominantly from mixed calcareous sedimentary deposits. The surface layer is clay loam about 4 inches thick. The upper 16 inches of the subsoil are clay loam, and the lower 10 inches are loam. The substratum to a depth of 60 inches or more is brown sandy loam. Permeability of this soil is moderate. Available water capacity is high. Effective rooting depth is 60 inches or more. Runoff is slow, and the hazard of water erosion is slight.
	This unit is considered prime farmland.
	Capability Subclass 2E; irrigated; 7C; nonirrigated
1	

#### NONTECHNICAL SOILS DESCRIPTION REPORT DAvid Hartman

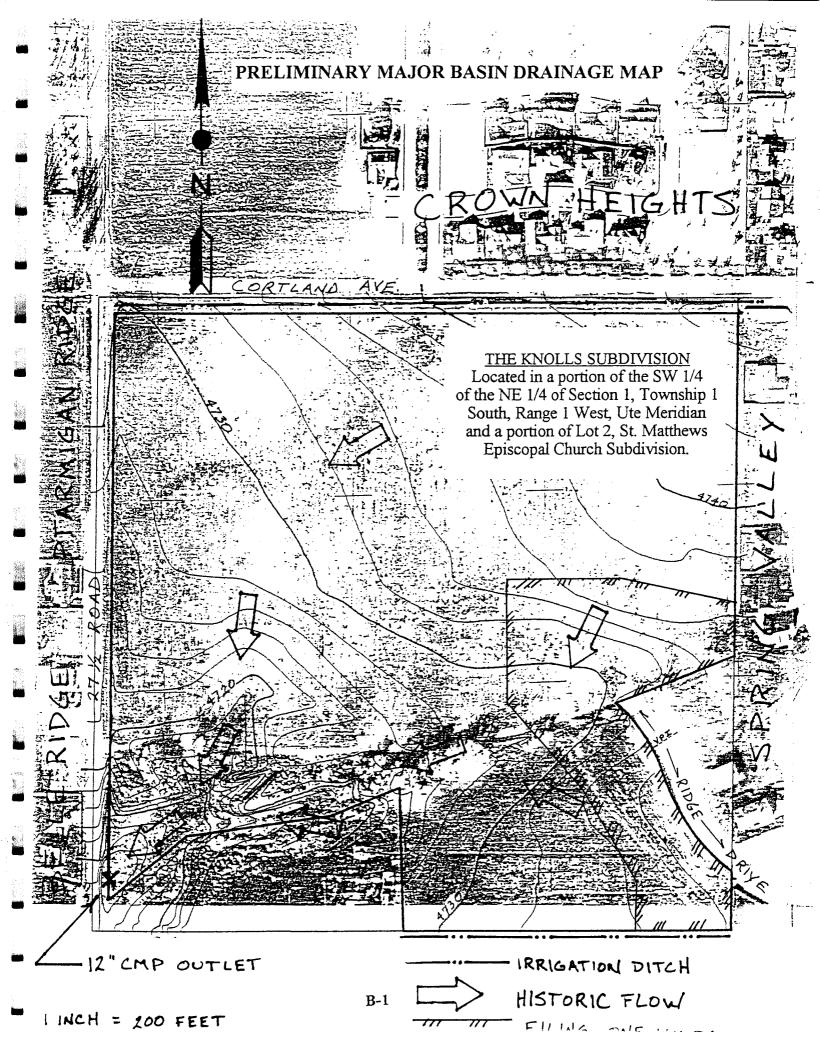
Capability classification is the grouping of soils to show, in a general way, their suitability for most kinds of farming. It is a practical classification based on limitations of the soils, the risk of damage when they are used, and the way they respond to treatment. The soils are classified according to degree and kind of permanent limitation, but without consideration of major and generally expensive landforming that would change the slope, depth, or other characteristics of the soils; without consideration of possible unlikely major reclamation projects. Class II - Some limitations that reduce the choice of crops or require moderate conservation measures. Class VII - Not suited for cultivation. Very severe limitations. Suited for range, woodland or wildlife uses if carefully managed. Usually cannot apply physical practices such as pitting, furrowing, seeding, etc. E - Erosion by wind of water is the major problem.	Map Symbol	Soil name and description
crops or require moderate conservation measures. Class VII - Not suited for cultivation. Very severe limitations. Suited for range, woodland or wildlife uses if carefully managed. Usually cannot apply physical practices such as pitting, furrowing, seeding, etc.		show, in a general way, their suitability for most kinds of farming. It is a practical classification based on limitations of the soils, the risk of damage when they are used, and the way they respond to treatment. The soils are classified according to degree and kind of permanent limitation, but without consideration of major and generally expensive landforming that would change the slope, depth, or other characteristics of the soils; without consideration of possible unlikely major reclamation
limitations. Suited for range, woodland or wildlife uses if carefully managed. Usually cannot apply physical practices such as pitting, furrowing, seeding, etc.		
E - Erosion by wind of water is the major problem.		limitations. Suited for range, woodland or wildlife uses if carefully managed. Usually cannot apply physical practices such as pitting, furrowing, seeding,
		E - Erosion by wind of water is the major problem.
C - Climate is the major hazard. Growing season may be very short; there is a shortage of rainfall or both.		C - Climate is the major hazard. Growing season may be very short; there is a shortage of rainfall or both.

100



# APPENDIX B

(interior



APPENDIX C

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Quick TR-55 Ver.5.46 S/N:1315430326 Executed: 14:23:03 09-20-1996

#### THE KNOLLS SUBDIVISION HISTORIC RUNOFF CONDITIONS

# RUNOFF CURVE NUMBER DATA

Composite Area:

SURFACE DESCRIPTION	AREA (acres)	CN	
ARID, HERBACIOUS, FAIR, B AG, WOODS, GOOD, B ATTACHED ASPHALT, RIDGE DRIVE	25.00 8.80 0.20	71 55 98	
COMPOSITE AREA>	34.00	67.0 :::::::	(67)

/ENDFILE/

Quick TR-55 Ver.5.46 S/N:1315430326 Executed: 14:23:03 09-20-1996

> THE KNOLLS SUBDIVISION HISTORIC RUNOFF CONDITIONS

RUNOFF CURVE NUMBER SUMMARY

Subarea	Area	CN
Description	(acres)	(weighted)
	34.00	67

### Quick TR-55 Ver.5.46 S/N:1315430326 Executed: 16:29:06 09-20-1996 PRE-KNOL.TCT

THE KNOLLS SUBDIVISION HISTORIC RUNOFF CONDITIONS

#### TC COMPUTATIONS FOR:

SHEET FLOW (Applicable to Tc only) Segment ID Surface description Manning's roughness coeff., n Flow length, L (total < or = 300) Two-yr 24-hr rainfall, P2	ft in	AB 0,WEEDS 0.1500 300.0 0.700 0.0083			
Land slope, s 0.8 .007 * (n*L) T =	·				1 00
T =	nrs	1.20		=	1.20
SHALLOW CONCENTRATED FLOW Segment ID Surface (paved or unpaved)? Flow length, L Watercourse slope, s		1104.0	DF Unpaved 444.0 0.0270		
0.5 Avg.V = Csf * (s) where: Unpaved Csf = 16.1345 Paved Csf = 20.3282	ft/s	2.2123	2.6512		
T = L / (3600*V)	hrs	0.14	+ 0.05	=	0.19
CHANNEL FLOW Segment ID					
Cross Sectional Flow Area, a Wetted perimeter, Pw	sq.ft ft				
Hydraulic radius, $r = a/Pw$	ft	0.000			
Channel slope, s Manning's roughness coeff., n	ft/ft	0.0000 0.0000			
2/3 $1/21.49 * r * s$					
v =n	ft/s	0.0000			
Flow length, L	ft	0			
T = L / (3600*V)	hrs	0.00		=	0.00
	::::::		::::::::: IME (hrs)	::::	1.38

Quick TR-55 Ver.5.46 S/N:1315430326 Executed: 16:29:06 09-20-1996 PRE-KNOL.TCT

SUMMARY SHEET FOR Tc or Tt COMPUTATIONS (Solved for Time using TR-55 Methods)

#### THE KNOLLS SUBDIVISION HISTORIC RUNOFF CONDITIONS

Subarea descr. Tc or Tt Time (hrs) Tc 1.38

n 1

>>>> GRAPHICAL PEAK DISCHARGE METHOD <<<<<

THE KNOLLS SUBDIVISION HISTIORIC DRAINAGE CONDITIONS

#### CALCULATED DISK FILE: PRE-KNOL.GPD

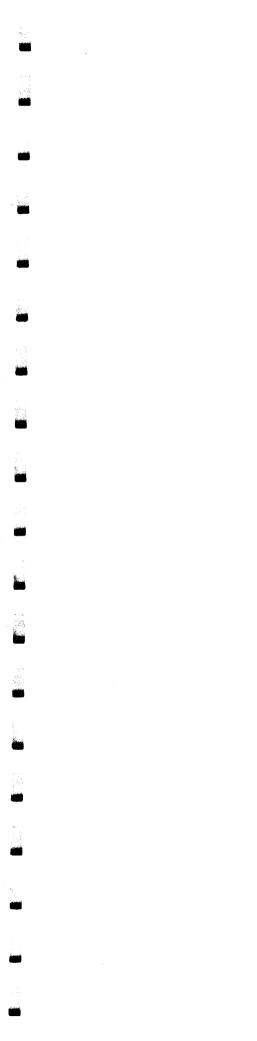
Drainage Area (acres) Runoff Curve Number (CN) Time of Concentration,Tc (hrs) Rainfall Distribution (Type) Pond and Swamp Areas (%)	33.8 67 1.38 II .2	> 0.0528 > 0.1	_
	Storm #1	Storm #2	Storm #3
Frequency (years) Rainfall, P, 24-hr (in)	2	100 2.01	
Initial Abstraction, Ia (in) Ia/p Ratio Unit Discharge, * qu (csm/in) Runoff, Q (in) Pond & Swamp Adjustment Factor	1.407	0.985 0.490 141 0.18 0.97	0.000
PEAK DISCHARGE, qp (cfs)	0	1	0
Summary of Computations for qu			
		0.450	
		2.292	
		-0.570	
		-0.023	
qu (csm) #1	135.020	163.003	0.000
Ia/p #2	0,500	0.500	0.000
CO #2	2.203	0.500 2.203	0.000
CO #2 C1 #2	-0.516	-0.516	0.000
C2 #2	-0.013	-0.013	0.000
qu (csm) #2	135.020	135.020	0.000
	135	141	0
* Interpolated for computed Ia/p rati		n Ia/p #1 & Ia	a/p #2)

If computed Ia/p exceeds Ia/p limits, bounding limit for Ia/p is used.

2

log(qu) = C0 + (C1 \* log(Tc)) + (C2 \* (log(Tc)))qp (cfs) = qu(csm) \* Area(sq.mi.) \* Q(in.) \* (Pond & Swamp Adj.)

- ----



# APPENDIX D

#### Quick TR-55 Ver.5.46 S/N:1315430326 Executed: 10:01:40 09-24-1996

#### DEVELOPED RUNOFF CONDITIONS THE KNOLLS SUBDIVISION IMPACT ON ENTIRE PARCEL FROM DEVELOPMENT OF FILING ONE

# RUNOFF CURVE NUMBER DATA

Composite Area:

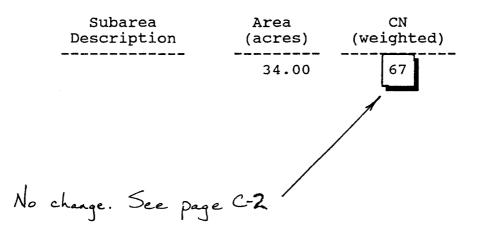
SURFACE DESCRIPTION	AREA (acres)	CN	
IMPERVIOUS, ROADS, ROOFS, SW	1.23	98	
DEVELOPED LAWNS, OPEN SPACE	3.16	61	
AG, WOODS, GOOD, B	8.60	55	
ARID, HERBACIOUS, FAIR, B	20.81	71	
ATTACHED ASPHALT, RIDGE DRIVE	0.20	98	
COMPOSITE AREA>	34.00	67.2	(67)

COMPOSITE AREA ---> 34.00 67.2 (

Quick TR-55 Ver.5.46 S/N:1315430326 Executed: 10:01:40 09-24-1996

#### DEVELOPED RUNOFF CONDITIONS THE KNOLLS SUBDIVISION IMPACT ON ENTIRE PARCEL FROM DEVELOPMENT OF FILING ONE

# RUNOFF CURVE NUMBER SUMMARY



N-7

Quick TR-55 Ver.5.46 S/N:1315430326 Executed: 08:32:50 09-24-1996

#### DEVELOPED RUNOFF CONDITIONS FILING ONE -- THE KNOLLS SUBDIVISION

# RUNOFF CURVE NUMBER DATA

Composite Area:

SURFACE DESCRIPTION	AREA (acres)	CN	
IMPERVIOUS LOTS, ROOFS, DRIVES PERVIOUS LOTS, YARDS ROADS, ASPHALT ROADS 13' OF GRASS IN R.O.W. OPEN SPACE	1.00 2.99 0.23 0.06 0.11	98 61 98 61 61	
COMPOSITE AREA>	4.39	71.4	(71)

~

Quick TR-55 Ver.5.46 S/N:1315430326 Executed: 08:32:50 09-24-1996

#### DEVELOPED RUNOFF CONDITIONS FILING ONE -- THE KNOLLS SUBDIVISION

# RUNOFF CURVE NUMBER SUMMARY

Subarea	Area	CN	
Description	(acres)	(weighted)	
	4.39	71	

Quick TR-55 Ver.5.46 S/N:1315430326 Executed: 09:39:25 09-24-1996 POST-FI.TCT

> DEVELOPED RUNOFF CONDITIONS FILING ONE -- THE KNOLLS SUBDIVISION

### TC COMPUTATIONS FOR:

SHEET FLOW (Applicable to Tc only) Segment ID		АВ	BC	
Surface description	LAWN		SIDEWALK	
Manning's roughness coeff., n	LICAN	0.2400		
Flow length, L (total < or = 300)	ft	165.0		
Two-yr 24-hr rainfall, P2			0.700	
Land slope, s			0.0250	
0.8	10/10	0.0240	0.0250	
.007 * (n*L)				
T =	hrs	0.71	+ 0.01	= 0.71
0.5 0.4				
P2 * s				
SHALLOW CONCENTRATED FLOW				
Segment ID		CD		
Surface (paved or unpaved)?		Unpaved		
Flow length, L	ft			
Watercourse slope, s	ft/ft	0.0250		
0.5				
Avg.V = Csf * (s)	ft/s	2.5511		
where: Unpaved Csf = 16.1345	•			
Paved $Csf = 20.3282$				
T = L / (3600 * V)	hrs	0.00		= 0.00
$\mathbf{I} = \mathbf{H} / (300000)$	111.5	0.00		- 0.00
CHANNEL FLOW				
Segment ID		de <del>*</del>	$_{\rm EF}$ * *	
Cross Sectional Flow Area, a	sq.ft			
Wetted perimeter, Pw	ft			
Hydraulic radius, $r = a/Pw$			0.250	
Channel slope, s		0.0210		
Manning's roughness coeff., n	/	0.0130		
,				
2/3 1/2				
1.49 * r * s				
V =	ft/s	6.2269	3.7995	
n				
Flow length, L	ft	265	75	
T = L / (3600 * V)	hrs	0.01	+ 0.01	= 0.02
* Curb's wither El : Ell I I'		TOTAL T	IME (hrs)	0.73
* Curb & gutter Flowing full to road's crow	パ.			
× × well the same of the				

Quick TR-55 Ver.5.46 S/N:1315430326 Executed: 09:39:25 09-24-1996 POST-FI.TCT

SUMMARY SHEET FOR Tc or Tt COMPUTATIONS (Solved for Time using TR-55 Methods)

DEVELOPED RUNOFF CONDITIONS FILING ONE -- THE KNOLLS SUBDIVISION

Subarea descr.	Tc or Tt	Time (hrs)
	TC	0.73

>>>> GRAPHICAL PEAK DISCHARGE METHOD <<<<<

DEVELOPED RUNOFF CONDITIONS FILING ONE -- THE KNOLLS SUBDIVISION

#### CALCULATED DISK FILE: POST-F1 .GPD

Drainage Area (acres) Runoff Curve Number (CN) Time of Concentration,Tc (hrs) Rainfall Distribution (Type) Pond and Swamp Areas (%)	71 .73 II		-
	Storm #2	1 Storm #2	Storm #3
Frequency (years) Rainfall, P, 24-hr (in)	2 .7	100 2.01	
Initial Abstraction, Ia (in) Ia/p Ratio Unit Discharge, * qu (csm/in) Runoff, Q (in) Pond & Swamp Adjustment Factor	0.817 1.167 188 0.00 1.00	273 0.27	0.817 0.000 0 0.00 1.00
PEAK DISCHARGE, qp (cfs)	0	1	0
Summary of Computations for qu			
C0 #1 C1 #1 C2 #1	2.203 -0.516	-0.599 -0.056	0.000 0.000 0.000 0.000 0.000
CO #2 C1 #2 C2 #2	2.203 -0.516 -0.013	0.450 2.292 -0.570 -0.023 234.351	0.000 0.000 0.000
* qu (csm)	188	273	0

\* Interpolated for computed Ia/p ratio (between Ia/p #1 & Ia/p #2) If computed Ia/p exceeds Ia/p limits, bounding limit for Ia/p is used.

2  $\log(qu) = C0 + (C1 * \log(Tc)) + (C2 * (\log(Tc)))$ qp (cfs) = qu(csm) \* Area(sq.mi.) \* Q(in.) \* (Pond & Swamp Adj.)

# **REVIEW COMMENTS**

Page 1 of 5

**FILE #PDR-96-217** 

TITLE HEADING: The Knolls

**LOCATION:** SE corner 27 Road & Cortland Avenue

**PETITIONER:** Robert C. Knapple

**PETITIONER'S ADDRESS/TELEPHONE:** 

O.P. Development Company, LLC 2421 Applewood Circle Grand Junction, CO 81506 241-2373

PETITIONER'S REPRESENTATIVE:

**Banner** Associates

STAFF REPRESENTATIVE:

Bill Nebeker

**NOTE: THE PETITIONER IS REQUIRED TO SUBMIT FOUR (4) COPIES OF WRITTEN RESPONSE AND REVISED DRAWINGS ADDRESSING ALL REVIEW COMMENTS ON OR BEFORE 5:00 P.M., OCTOBER 24, 1996.** 

# **CITY COMMUNITY DEVELOPMENT**

Bill Nebeker

244-1447

NOTE: In the future, please list engineer (Banner) as your representative on the application form so comments and inquiries regarding this project can be directed towards him

#### **REZONE**:

- 1. Although your narrative states that the site is to be rezoned PR-4, in accordance with the final decision (#PP-96-111), the overall density of the site is 2.18 dwellings per acre (including the church site). Prior to the Planning Commission hearing staff will determine the appropriate density of the residential portion of the site, and the appropriate zoning classification for the church site.
- 2. Are there any estimates on when the church will develop? Approval of this plan will limit the use of the church parcel in the future if it is decided not to build a church here.

# FINAL PLAT:

- 1. To achieve a consistency of platting terms, please redesignate Tract A as a lot. Redesignate Outlot A as a Tract. Outlot B & C shall be designated as lots for future development.
- 2. What are setbacks for filing #1
- 3. Cortland Road improvements for the portion adjacent to the church site shall be installed during filing #2
- 4. Revise plat dedication statement for the pedestrian easement to include the following: "pedestrian easements to the City of Grand Junction as perpetual easement for ingress and egress use by the general public pedestrian."
- 5. A 10' wide concrete pedestrian path shall be required in Tract A (outlot A). The path shall be shown on improvement plans with an appropriate ramp onto Ridge Drive. Show where drainage will go in relation to the pedestrian path.

# PDR-96-217 / REVIEW COMMENTS / page 2 of 5

# PRELIMINARY PLAN:

- 1. Regarding Jody's comment (#5) that the street system on the preliminary plan exceeds the maximum 250 ADT for a single outlet street, do you have any idea of the likelihood or timeline that Willow Glen Drive will be extended to the parcel to the south and connect to 27 ½ Road? Any other suggestions for an alternate access to this subdivision?
- 2. See attached draft administrative regulations regarding private street standards, for use in design of the patio homes phase.
- 3. Additional pedestrian/bicycle connections are needed from North Knoll Circle to Cortland Avenue; and from Willow Glen Drive or Spring Court to the church site. Without these connections this isn't much of a planned residential subdivision.
- 4. The plan needs better definition of the turnaround in Spring Court.
- 5. Is street or private access no longer needed for the home on the parcel in the southwest corner of the site?
- 6. By building the patio homes in filing 3 you risk opposition to the final plan approval from all persons who buy homes in filings 1 & 2. It will be important to notify all home buyers in filings 1 & 2 that patio homes are proposed for phase 3 of this development. What will you tell them and how will you get the message across?
- 7. Provide more detail regarding the nature overlook.
- 8. I didn't see any active recreation areas that was stressed so much during the first preliminary review. I suggest you eliminate lot 1, block 1 in filing 3 and provide some.
- 9. Place the airport critical zone boundary on the preliminary plan, and final plat if applicable.
- 10. Are any provisions proposed for soundproofing homes that lie in the airport critical zone boundaries?

NOTE: Please submit reduced copies (11" X 17") of all revised plans that are resubmitted with response to comments.

CITY DEVELOPMENT ENGINEER	10/14/96
Jody Kliska	244-1591

- 1. The submitted geotechnical report was done in 1981 and does not meet current pavement design requirements. A new pavement design must be submitted.
- 2. The final drainage report does not appear to have the time of concentration calculations for the 100 year storm.
- 3. The preliminary plan indicates a sidewalk connection to filing 1. The filing 1 plans do not show the sidewalk and in fact show a drainage discharge where the sidewalk should be. Construction of the sidewalk will be required with the filing, and drainage needs to be designed for the ultimate sidewalk extension. The sidewalk must be handicap accessible.
- 4. There appears to be minimal cover over the storm sewer pipe in the street. Please explain why HDPE is specified for this application. The manufacturer's literature for this product does not appear that this is the best choice of materials.
- 5. The preliminary plan as shown does not met the TEDS standards for single outlet streets. The proposal for 42 single family and 23 townhomes exceeds the traffic generation of 250 ADT on a maximum length cul-de-sac of 1000 feet.
- 6. Willow Glen Drive needs to be analyzed for future traffic needs. It may need to be an urban residential collector street section.

## PDR-96-217 / REVIEW COMMENTS / page 3 of 5

CITY UTILITY ENGINEER	10/16/96	
Trent Prall	244-1590	

PRELIMINARY PLAN:

- A. 10' Wide Concrete Pedestrian shall be 6" thick between 27 ½ Rd to manhole south of Lots 19 and 20, Filing 3 to allow City sewer cleaning trucks access.
- B. Please reconfigure manhole in front of Lots 6 and 7, Block 1, Filing 2 westward to eliminate possible interference with water line.

FINAL PLAN:

- 1. Final Plans shall have City and Ute signoff blocks on all water and sewer related construction drawings.
- 2. All lots not able to sewer by gravity such as Lot 5, Filing 1, shall have note on the plat stating "pump required for sewer service."

CITY PROPERTY AGENT	10/15/96
Steve Pace	256-4003

- 1. Outlot B should be labeled Lot 1, Block 2 and Outlot C should be labeled Lot 1, Block 3.
- 2. Tract "A" should be addressed in the dedication.
- 3. Remove verbage referring to drainage and detention / retention easements from the dedication.
- 4. Building set-back lines?
- 5. Outer monumentation needs to be set or reset in concrete, plus the outer monuments for each block.

CIT	Y PARK & RECREATION	10/7/96
<u>Shav</u>	vn Cooper	256-3869
1.	Is Outlot A intended for public pedestrian use?	This route is identified on the "pending" Urban
	Trails Plan. Connections to future filings must l	be required. This should be identified as a public

- pedestrian easement to avoid confusion for area property owners in the future.
- 2. Parks & Open Space fees 9 lots @ \$225 = \$2,025.

<b>CITY FIRE DEPAR</b>	ГMENT	10/8/96
Hank Masterson		244-1414

The private drives proposed as Willow View Court and Spring Court are acceptable. The "T" turn around area of Spring Court must be posted as a no parking zone.

Make the following changes to the utility composite: Minimum fire line sizes are 6". Line sizes must be shown on drawing. Move the hydrant shown at southwest corner of Lot 1, block one of Filing Two to the corner of Cortland and Willow Glen Drive. Move the hydrant shown at Lot 1, block one of Filing four to the intersection of Willow Glen and Hollow Court. Delete the hydrants proposed at the end of Hollow Court and the end of Spring Court. Petitioner must submit a revised Utility Composite showing these changes.

CITY ATTORNEY	10/11/96
Dan Wilson	244-1505
ISSUES	

1. Street improvements for Tract A

2. "Outlot B" should be redesignated as noted, as well as "C".

## PDR-96-217 / REVIEW COMMENTS / page 4 of 5

- 3. I'll need to see / review proposed homeowners documents creating the association and providing for liens, maintenance, etc. along with provisions for integrating this filing with future filings.
- 4. See notes on the plat sheets (red-line attached).
- 5. The Development Improvements Agreement doesn't show guarantee for landscaping of "outlots".

CITY POLICE DEPARTMENT	10/7/96
Lisa Dicamillo	244-3587
The was of out do good follows the trend in arime prov	ventione prestigen

The use of cul-de-sacs follows the trend in crime preventions practices.

MESA COUNTY PLANNING	10/14/96
Richard Goecke	244-1744

1. Would meet County standards for setbacks, parking, etc.

2. This "in-fill" project encourages creative design for new single family homes on varied lot sizes/shapes.

WALKER FIELD AIRPORT	10/14/96
Dennis Wiss	244-9100

- 1. The proposed subdivision lies approximately on e mile southwest of the approach end of Runway 04 at Walker Field and as such lies within the Airport's Area of Influence (AOI). Therefore, this subdivision may be subjected to overflight of aircraft and the associated noise from aircraft. It is recommended that additional soundproofing measures be taken on the residential structures in this subdivision, to include additional sound-deadening insulation and planned landscaping in order to help mitigate noise level perceptions.
- 2. The planned church in this area is a compatible land use with the Airport and no special measures are recommended for its construction.
- 3. The Airport Authority requests that an Avigation Easement be recorded at or before the filing of the subdivision plat and further requests that a copy of the easement be forwarded to the Airport Authority after filing.

GRAND VALLEY WATER USERS	10/16/96
Richard Proctor	242-5065

Grand Valley Project Lateral 2B crosses the full width of the northern edge of the proposed development south of Cortland Avenue (F 3/4 Road). Lateral 2B is an underground pipeline with one manhole located in the northwest corner of the property and two associated manholes located in the northeast corner of the property. The south manhole located in the northeast corner contains a headgate from which the property will take delivery of its irrigation water.

The Association requires a 30 foot wide right-of-way, 15 feet either side of the pipeline. The manhole containing the headgate requires a described right-of-way of 20 feet surrounding it. Said right-of-way shall be free of building structures and trees.

Also, located in the southeast corner of the proposed subdivision, in Lot 1, Filing 1 is a portion of Lateral 2C pipeline. Said Lateral 2C pipeline is located within the proposed Lot 1 adjacent to the eastern north/south property line. Said property line is shown to be 121.89 feet long. The Association will require a 20 foot wide right-of-way over the Lateral 2C pipeline.

#### PDR-96-217 / REVIEW COMMENTS / page 5 of 5

The Grand Valley Project is a federal reclamation irrigation project managed by the Grand Valley Water Users Association. The Grand Valley Project also includes drainage ditch channels managed by the Association.

The Knolls Subdivision plan states that a storm water detention facility will be located in the southwest corner of the property adjacent to the east side of 27 Road in an existing low lying drainage channel. This drainage channel is not part of the Grand Valley Project. However, storm water released from said detention facility will eventually will eventually be drained into a Grand Valley Project drainage channel more than a 1/4 mile southwest of the detention pond's location. The Bureau of Reclamation's policy is that a license agreement must be obtained from them before any storm water run-off is discharged into a Grand Valley Project drainage channel. The developers will be provided with a license agreement application.

U S WEST	10/8/96
Max Ward	244-4721
For timely telephone service, as soon as you have a pl please	at and power drawing for your housing development,

MAIL COPY TO:	AND	CALL THE TOLL FREE NUMBER FOR:
U.S. West Communications		Developer contact group
P.O. Box 1720		1-800-526-3557
Denver, CO 80201		

We need to hear from you at least 60 days prior to trenching.

PUBLIC SERVICE COMPANY	10/11/96
John Salazar	244-2781

GAS: No objections

ELECTRIC: Request that Outlot A between lots 4 & 5 also be designated as a utility easement. Additional utility easements may be required later depending on design of electric facilities.

# **COMMENTS RECEIVED LATE**

UTE	WATER	10/16/96
<u>Gary</u>	R Mathews	242-7491
1.	Water mains shall be c-900, class 150.	Installation of pipe fittings, valves and services including
	testing and disinfection shall be in accord	dance with Ute Water standard specification and drawings.

2. Developer will install the meter pits and yokes. Ute will furnish the pits and yokes.

3. Construction plans required 48 hours before development begins.

4. Policies and fees in effect at the time of application will apply.

# **RESPONSE TO REVIEW COMMENTS**

FILE: #PDR-96-2	17 <b>TITL</b>	E HEADING: The	Knolls
LOCATION:	SE Corner of 27 <sup>1</sup> / <sub>2</sub> Road a	and Cortland Avenue	RECEIVED GRAND JUNCTION PLANNING DEPARTMENT
PETITIONER:	Robert C. Knapple		DCT 2 4 1996
PETITIONER'S AI	DDRESS/TELEPHONE:	O.P. Development ( 2421 Applewood Ci Grand Jct., CO 813 241-2373	rcle
PETITIONER'S RI	EPRESENTATIVE:	Banner Associates, 2777 Crossroads Blv 243-2242	
STAFF REPRESEN	ITATIVE:	Bill Nebeker	

# COMMUNITY DEVELOPMENT DEPARTMENT

# **REZONE:**

- 1. Comment noted, no response necessary.
- 2. It is not known when St. Matthews Episcopal Church may develop on this site. The Petitioner has no objection to limiting the use of the church site with this plan if St. Matthews does not decide to build.

## FINAL PLAT:

- 1. Redesignation of the tract and outlots has been done.
- 2. Setbacks for Filing #1 are 25' Front, 10' Side and 25' Rear. These setbacks have been added to the Final Plat.
- 3. Comment noted, no response necessary.
- 4. Verbage in plat dedication has been modified as requested.

5. It has always been the intention to construct the 10 ft. wide pedestrian path in Tract A shown as part of Filing 1. Additional details regarding construction and the relationship with storm drainage has been added to the Grading and Drainage Plan.

# PRELIMINARY PLAN:

- 1. Regarding the development of the property to the south, we do not have a time line on when that will happen. However, there has been discussions with the owner and representatives of that parcel that would indicate that development of this site is being seriously considered. If the Petitioner were to estimate a time frame, 5-years would be suggested for development of this parcel to begin. There are no other suggestions for an alternate access to this subdivision other than through this parcel.
- 2. Comment noted, no response necessary.
- 3. We do not feel as though a pedestrian/bicycle connection is warranted between North Knoll Circle and Cortland Avenue since the intersection of Willow Glen Drive and Cortland provides this connection. Concerns such as maintenance and security from crime are examples on why a connection should not be provided. The Petitioner is agreeable to providing a connection from the townhome area to the church site, but was not shown since the final configuration of buildings and their exact location is not known.
- 4. To better define the turnaround in Spring Court, an enlarged detail has been added to Sheet 2 of 3 of the Preliminary Plan.
- 5. After receiving comments from the previous submittal, it does not appear that providing access to the Davis parcel at the southwest corner of the project was as critical as providing an access point to the larger parcel to the south. Although we have discussed several different alternatives for providing a new driveway into the Davis parcel, nothing has been decided on where it might be placed. The Petitioner has no objection to providing access if required to do so.
- 6. The Knolls is set up to be a development where the developer will also be involved in constructing the homes. Home buyers will choose their lot and floor plan in conjunction with the entire planned development, including the townhomes shown as Filing 3. Lots will not be sold individually.

PDR-96-217 Response to Review Comments Page 3

- 7. At this time we do not anticipate any major structure being provided for the Nature Overlook, although some sort of gazebo may provide a nice ammenity to the area. The location planned for the Nature Overlook does not lend itself to any new developed use due to it's size and proximity to the possible wetlands. To leave the area as a natural open space providing access to it by the pedestrian trails seems to be the logical choice. Additional improvements will be to grade the area to a possible amphitheater-type setting overlooking the wetlands and ponds which to view the open space and wildlife that will use it. Several weather-proof benches would be proposed which would provide individuals the opportunity to sit for longer periods of time. This area has several existing mature trees that would be left in tact which would add to the nature and rural feel.
- 8. The Petitioner is still unsure what is meant by "active recreation areas". This site is currently used extensively by people jogging and walking in the area, in the area that is planned to be open space with trails. These trails can provide active recreation such walking, jogging, and possibly fitness stations that are seen in some City parks. This development will be marketed to a clientel that will that will be using this type of activity. Although other clientel wanting other types of activities will not be discouraged, these activities are found nearby at the country club and City parks. The Petitioner does not feel that providing usable space for something that won't be used is good planning.
- 9. The airport critical zone has been added to the Preliminary Plan and the Final Plat for Filing One where applicable.
- 10. No sound-proofing provisions are being planned for Filing One as it falls either outside the airport critical zone or on the outer limits of the zone. Future construction of homes may include additional insulation to mitigate noise if necessary.

# CITY DEVELOPMENT ENGINEER

1. In recognizing that the geotechnical report submitted was performed in 1981 and does not address the possible wetlands area, the Petitioner is in the process of having a updated soils investigation performed by Lambert and Associates that will include a pavement design. This investigation and design will be completed prior to any construction taking place and be submitted to the City staff for approval.

- 2. On pages D-5 and D-6 of Appendix D in the Final Drainage Report, the calculations for the Time of Concentration is shown.
- 3. Refer to Response #5 under CITY COMMUNITY DEVELOPMENT, FINAL PLAT.
- 4. Many times High Density Polyethylene (HDPE) pipe is specified for construction due to its' ease of placement. We would agree that HDPE would not be the best choice of material in making a crossing of Ridge Drive. This section of pipe has been changed to Reinforced Concrete Pipe (RCP).
- 5. Refer to Response #1 under CITY COMMUNITY DEVELOPMENT, PRELIMINARY PLAN.
- 6. Previous investigations by **Banner Associates** indicate that approximately 55 single family lots could be placed on the vacant ground to the south. Obviously an access onto 27½ Road would be necessary with this development that would tie into Willow Glen Drive. It is not possible to estimate exact traffic projections, however, using the Residential Trip Generation Rates given by the City, the total ADT for both developments would be in the order of 1060 trips per day. If it is approximated that half of these trips will be using each of the two access points, this would correspond to 530 ADT, still well below the 1000 ADT limit for a Urban Residential Street. Therefore, it is felt that streets within The Knolls can remain as shown on the Preliminary Plan.

# CITY UTILITY ENGINEER

# PRELIMINARY PLAN:

- 1. The concrete pedestrian path will be constructed as stipulated.
- 2. The manhole in front of Lots 6 and 7, Block 1, Filing 2 has been reconfigured to avoid possible conflict with the water line.

# FINAL PLAN:

1. Sign-off blocks for both the City and Ute have been added.

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2. There is no intention to develop lots that will require sewage pumps for their service. It is proposed to construct homesites at the necessary elevation to avoid pumping.

# CITY PROPERTY AGENT

- 1. Refer to Response #1 under CITY COMMUNITY DEVELOPMENT, FINAL PLAT.
- 2. Refer to Response #4 under CITY COMMUNITY DEVELOPMENT, FINAL PLAT.
- 3. Verbage referring to drainage and detention/retention easements has been removed from the dedication as requested.
- 4. Refer to Response #2 under CITY COMMUNITY DEVELOPMENT, FINAL PLAT.
- 5. Monumentation shall be set in concrete as stated.

# CITY PARK & RECREATION

- 1. Refer to Response #4 under CITY COMMUNITY DEVELOPMENT, FINAL PLAT.
- 2. Comment noted, no response necessary.

# CITY FIRE DEPARTMENT

Spring Court shall be posted as a "no parking zone".

Sizes for proposed water lines have been added to the Preliminary Plan. Locations of fire hydrants have been modified as requested.

PDR-96-217 Response to Review Comments Page 6

# **CITY ATTORNEY**

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- 1. Refer to Response #5 under CITY COMMUNITY DEVELOPMENT, FINAL PLAT.
- 2. Refer to Response #1 under CITY COMMUNITY DEVELOPMENT, FINAL PLAT.
- 3. Homeowners documents are being finalized and will be submitted for review as soon as they are available.
- 4. Comment noted, no response necessary.
- 5. The Total Estimated Cost of Improvements shown on the Development Improvements Agreement will be increase by \$6,500 to account for constructing the 10' wide concrete pedestrian path and placement of grass in of Tract A of Filing 1.

# CITY POLICE DEPARTMENT

Comment noted, no response necessary.

# MESA COUNTY PLANNING

Comment noted, no response necessary.

# WALKER FIELD AIRPORT

- 1. Refer to Response #10 under CITY COMMUNITY DEVELOPMENT, PRELIMINARY PLAN.
- 2. Comment noted, no response necessary.
- 3. An Avigation Easement was completed and submitted as part of this application. A copy of the recorded easement will be provided to the Airport Authority.

PDR-96-217 Response to Review Comments Page 7

1 1

## **GRAND VALLEY WATER USERS**

Easements for Laterals 2B and 2C will be provided for as requested.

We do not dispute that drainage from this site will ultimately reach irrigation canals that are part of the Grand Valley Project. However, it is our estimate that the distance required to travel is greater than a <sup>1</sup>/<sub>4</sub> mile in addition to traveling through other developments prior to this discharge. It should be stated that this storm drainage is <u>not</u> a direct discharge into the Grand Valley Project. If the license agreement is required for only direct discharges into a Grand Valley Project channel, then it is our opinion that this application may not be necessary. Although, if making this license agreement application is typical of any and all developments that may be upstream from any Grand Valley Project channel, then the Petitioner has no objection with completing this process.

### **U S WEST**

Comment noted, no response necessary.

## PUBLIC SERVICE COMPANY

GAS: No response necessary.

ELECTRIC: Tract A (Outlot A) will also be designated as a utility easement as requested.

### **UTE WATER DISTRICT**

Comments noted, no response necessary.

#### PDR-96-217 / ADDITIONAL REVIEW COMMENTS / page 1 of

CITY DEVELOPMENT ENGINEER	10/28/96
Jody Kliska	244-1591

Response to response to comments:

- 1. The updated geotechnical report is required prior to approval of construction plans.
- 2. The drainage report pages D-5 and D-6 only have calculations for the 2 year storm time of concentration. The original comment was for the 100 year storm, and this still has not been addressed.
- 3. The final plans for filing 1 while showing 200' feet of pipe and what appears to be the pedestrian path, do not contain sufficient detail for the pedestrian path including the size, length, cross-section, material, and ramp connection.
- 4. The question of this project providing only a single outlet for the development has not been addressed. The City TEDS section 6.14 allows cul-de-sacs of length up to 1000' and maximum ADT of 250. This project essentially functions as a cul-de-sac and as such exceeds these requirements. The response reads "obviously an access onto 27 1/2 Road would be necessary...", leading to the conclusion the petitioner thinks the next development should be the responsible party for providing the necessary access.

# THE KNOLLS SUBDIVISION

# ADDENDUM TO FINAL DRAINAGE REPORT

A critical step in calculating historic and developed runoff was overlooked in preparing the original Final Drainage Report. The Time of Concentration (Tc) will have different values for the 2 year and 100 year storm events in this TR-55 method of analysis. The equations on page E-2 of the Grand Junction SWM Manual produce the following relationship for the sheet flow time (To) portion of the Tc equation:

 $To_{100} = 0.6 * To_2$ 

The drainage calculations were run again and the runoff results are tabulated below. Please note the only change from page 5 of the original Final Drainage Report is the historic 100-year runoff is now 2 cfs instead of 1 cfs.

Historic Conditions

2-year runoff:0 cfs100-year runoff:2 cfs

Filing One, developed, analyzed independently

2-year runoff: 0 cfs 100-year runoff: 1 cfs

This 1 cfs released from Filing One will insignificantly affect the flows released from the entire parcel, as approximately 1000 feet of gently sloping, moderately vegetated terrain lies between Filing One's outfall point and the outfall point for the entire parcel.

The calculations showing this proper method of Tc computation are attached as part of this addendum.

RECEIVED GRAND JUNCTION PLANNING DEPARTMENT OCT 3 0 1996 Quick TR-55 Ver.5.46 S/N:1315430326 Executed: 16:35:10 10-29-1996 PRE-KNOL.TCT

> THE KNOLLS SUBDIVISION HISTORIC RUNOFF CONDITIONS

### TC COMPUTATIONS FOR:

SHEET FLOW (Applicable to Tc only)		15			
Segment ID	1070	AB			
Surface description	ARID	,WEEDS			
Manning's roughness coeff., n		0.1500			
Flow length, L (total $< \text{ or } = 300$ )					
Two-yr 24-hr rainfall, P2		0.700			
Land slope, s	ft/ft	0.0083			
0.8					
.007 * (n*L)					
T =	hrs	1.20		=	1.20
0.5 0.4					,
P2 * s			6	= 0.	6(1.20)
			100	-	6 (1.20) 0.72
SHALLOW CONCENTRATED FLOW				-	0.12
Segment ID		BD	DF		
Surface (paved or unpaved)?		Unpaved	Unpaved		
Flow length, L	ft	1104.0			
Watercourse slope, s	ft/ft				
	20/20	010100	010270		
0.5					
Avg.V = Csf * (s)	ft/s	2.2123	2.6512		
where: Unpaved $Csf = 16.1345$	10/3	<i>4</i> • <i>4</i> ± <i>4</i> J	2.0312		
Paved $Csf = 20.3282$					
Paveu CSI - 20.3282					
T = L / (3600 * V)	hrs	0.14	+ 0.05	=	0.19
CHANNEL FLOW					
Segment ID					
Cross Sectional Flow Area, a	sq.ft	0.00			
Wetted perimeter, Pw	ft	0.00			
Hydraulic radius, $r = a/Pw$	ft	0.000			
	ft/ft	0.0000			
Channel slope, s	10/10				
Manning's roughness coeff., n	,	0.0000			
2/2 1/2					
2/3 $1/21.49 * r * s$					
1.49 * r * s V =	£+ /~	0 0000			
•	ft/s	0.0000			
n					
Elevelensth I	<b>5L</b>	~			
Flow length, L	ft	0			
T = L / (3600 * V)	hrs	0.00		=	0.00
	::::::			::::	
		TOTAL T	'IME (hrs)		1.38

Tc 100

= 0.91 hrs

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Quick TR-55 Ver.5.46 S/N:1315430326 Executed: 16:35:10 10-29-1996 PRE-KNOL.TCT

> SUMMARY SHEET FOR TC or Tt COMPUTATIONS (Solved for Time using TR-55 Methods)

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#### THE KNOLLS SUBDIVISION HISTORIC RUNOFF CONDITIONS

Subarea descr.	Tc or Tt	Time (hrs)
	Тс	1.38
	T. =	0.91 hrs

#### Quick TR-55 Version: 5.46 S/N: 1315430326

#### >>>>> GRAPHICAL PEAK DISCHARGE METHOD <<<<<

#### THE KNOLLS SUBDIVISION HISTIORIC DRAINAGE CONDITIONS 2 YEAR STORM

#### CALCULATED DISK FILE: PRE-KNOL.GPD

Drainage Area (acres Runoff Curve Number (CN) Time of Concentration,Tc (hrs Rainfall Distribution (Type Pond and Swamp Areas (%)	67 1.38 II	0.0528 sq. 0.1 acr	
	Storm #1 S	torm #2 S	torm #3
Frequency (years) Rainfall, P, 24-hr (in)	2 .7		
Initial Abstraction, Ia (in) Ia/p Ratio Unit Discharge, * qu (csm/in) Runoff, Q (in) Pond & Swamp Adjustment Factor	1.407 135 0.00	0.000 0	0.985 0.000 0 0.00 0.97
PEAK DISCHARGE, qp (cfs)	0	0	0
Summary of Computations for qu			
Ia/p #1 C0 #1 C1 #1 C2 #1 qu (csm) #1	2.203 -0.516 -0.013	0.000 0.000 0.000	0.000 0.000 0.000 0.000 0.000
Ia/p $#2$ C0 $#2$ C1 $#2$ C2 $#2$ qu (csm) $#2$	2.203 -0.516 -0.013	0.000 0.000 0.000	0.000 0.000 0.000 0.000 0.000
* qu (csm)	135	0	0

\* Interpolated for computed Ia/p ratio (between Ia/p #1 & Ia/p #2) If computed Ia/p exceeds Ia/p limits, bounding limit for Ia/p is used.

log(qu) = C0 + (C1 \* log(Tc)) + (C2 \* (log(Tc)))qp (cfs) = qu(csm) \* Area(sq.mi.) \* Q(in.) \* (Pond & Swamp Adj.)

#### Quick TR-55 Version: 5.46 S/N: 1315430326

>>>>> GRAPHICAL PEAK DISCHARGE METHOD <<<<<

#### THE KNOLLS SUBDIVISION HISTIORIC DRAINAGE CONDITIONS 100 YEAR STORM

#### CALCULATED DISK FILE: PRE-KNOL.GPD

	Runoff Cu Time of C Rainfall	Area rve Number oncentration, Distribution Swamp Areas	Tc (hrs)	67 0.91 II	•	0528 sq 0.1 ac	
		-					
				Storm #	1 Storm	n #2	Storm #3
Frequer	ncy (years	١		100			
	1, P, 24-1			2.01			
	• •						
Tnitial	Abstract	ion, Ia (in)		0.985	0.98	5	0.985
Ia/p Ra		1011, 14 (111)		0.490			0.000
		* qu (csm/in)		175			0
	Q (in)	1 ( ) /		0.18		0	0.00
Pond &	Swamp Adju	ustment Facto	r	0.97	0.9	7	0.97
דת עגשת	SCHARGE,	m (afa)		2		0	0
FLAK DI				2			0
Cummo mu	of Comput	tations for q			•		
			-				
	Ia/p	#1 <sup>.</sup>		0.450	0.00	0	0.000
	CO	#1	-	2.292	0.00		0.000
	C1	#1		-0.570	0.00		0.000
	C2	#1		-0.023	0.00		0.000
	qu (csm)	#1	2	206.867	0.00	0	0.000
	Ia/p	#2		0.500	0.00	0	0.000
	CO	#2		2.203	0.00	0	0.000
	C1	#2		-0.516	0.00	0	0.000
	C2	#2		-0.013	0.00	0	0.000
	qu (csm)	#2	]	67.469	0.00	0	0.000
*	qu (csm)			175		0	0
* Inter	polated fo	or computed Ia	a/p ratio	) (betwee	en Ia/p #1	& Ia/p	#2)

\* Interpolated for computed Ia/p ratio (between Ia/p #1 & Ia/p #2) If computed Ia/p exceeds Ia/p limits, bounding limit for Ia/p is used.

2

log(qu) = C0 + (C1 \* log(Tc)) + (C2 \* (log(Tc)))qp (cfs) = qu(csm) \* Area(sq.mi.) \* Q(in.) \* (Pond & Swamp Adj.) Quick TR-55 Ver.5.46 S/N:1315430326 Executed: 07:51:10 10-30-1996 POST-FI.TCT

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DEVELOPED RUNOFF CONDITIONS FILING ONE -- THE KNOLLS SUBDIVISION

### TC COMPUTATIONS FOR:

SHEET FLOW (Applicable to Tc only) Segment ID Surface description Manning's roughness coeff., n Flow length, L (total < or = 300) Two-yr 24-hr rainfall, P2 Land slope, s 0.8 .007 * (n*L) T =	in	0.2400 165.0 0.700 0.0240 0.71	0.700 0.0250 + 0.01	
P2 * s		0,00 = 0.6 7	52 = 0.6 (0.71) =	0.43
SHALLOW CONCENTRATED FLOW Segment ID Surface (paved or unpaved)? Flow length, L Watercourse slope, s	ft ft/ft	CD Unpaved 12.0		
0.5 Avg.V = Csf * (s) where: Unpaved Csf = 16.1345 Paved Csf = 20.3282	ft/s	2.5511		
T = L / (3600 * V)	hrs	0.00		= 0.00
CHANNEL FLOW Segment ID Cross Sectional Flow Area, a Wetted perimeter, Pw Hydraulic radius, r = a/Pw Channel slope, s Manning's roughness coeff., n	sq.ft ft ft ft/ft			
$V = \frac{1.49 * r * s}{n}$	ft/s		3.7995	
Flow length, L	ft	265	75	
T = L / (3600 * V)	hrs	0.01	+ 0.01	= 0.02
		TOTAL T	IME (hrs)	0.73
		Te	100 =	0.45

Quick TR-55 Ver.5.46 S/N:1315430326 Executed: 07:51:10 10-30-1996 POST-FI.TCT

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SUMMARY SHEET FOR Tc or Tt COMPUTATIONS (Solved for Time using TR-55 Methods)

#### DEVELOPED RUNOFF CONDITIONS FILING ONE -- THE KNOLLS SUBDIVISION

Subarea descr.	Tc or Tt	Time (hrs)
	TC	0.73
	T_100 =	0.45
	-100	

#### Quick TR-55 Version: 5.46 S/N: 1315430326

>>>> GRAPHICAL PEAK DISCHARGE METHOD <<<<<

DEVELOPED RUNOFF CONDITIONS FILING ONE -- THE KNOLLS SUBDIVISION 2 YEAR STORM EVENT

#### CALCULATED DISK FILE: POST-F1 .GPD

	Runoff Cu Time of C Rainfall	Area rve Number oncentration, Distribution Swamp Areas	(CN) Tc (hrs)	71 .73	>	0.0069	sq.mi. acres
•	Poliu aliu	Swamp Areas	(*)	U	/	0.0	acres
				Storm	#1 :	Storm #2	Storm #3
	ncy (years ll, P, 24-			2 .7			
Ia/p Ra Unit Di Runoff,	atio Ischarge, Q (in)	ion, Ia (in) * qu (csm/in)		0.817 1.167 188 0.00		0.817 0.000 0 0.00	0.817 0.000 0 0.00
Pond &	Swamp Adj	ustment Facto	r	1.00		1.00	1.00
PEAK DI	SCHARGE,	qp (cfs)		0		0	0
Summary	v of Compu	tations for q	1				
	Ia/p CO C1 C2 qu (csm)	#1 #1 #1		0.500 2.203 -0.516 -0.013 87.546		0.000 0.000 0.000 0.000 0.000	0.000 0.000 0.000 0.000 0.000
	Ia/p CO C1 C2 qu (csm)	#2 #2 #2		0.500 2.203 -0.516 -0.013 .87.546		0.000 0.000 0.000 0.000 0.000	0.000 0.000 0.000 0.000 0.000
*	qu (csm)			188		0	0
* Tastas				11. a to a .	T-	/ #1 с та	1

\* Interpolated for computed Ia/p ratio (between Ia/p #1 & Ia/p #2) If computed Ia/p exceeds Ia/p limits, bounding limit for Ia/p is used.

2

log(qu) = C0 + (C1 \* log(Tc)) + (C2 \* (log(Tc)))qp (cfs) = qu(csm) \* Area(sq.mi.) \* Q(in.) \* (Pond & Swamp Adj.)

# Quick TR-55 Version: 5.46 S/N: 1315430326

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>>>>> GRAPHICAL PEAK DISCHARGE METHOD <<<<<

#### DEVELOPED RUNOFF CONDITIONS FILING ONE -- THE KNOLLS SUBDIVISION 100 YEAR STORM EVENT

#### CALCULATED DISK FILE: POST-F1 .GPD

Drainage Area Runoff Curve Number Time of Concentration,To Rainfall Distribution Pond and Swamp Areas	(CN) 71 c (hrs) 0.45		sq.mi. acres
Fond and Swamp Areas	(*)	> 0.0	acres
	Storm #2	1 Storm #2	Storm #3
Frequency (years) Rainfall, P, 24-hr (in)	100 2.01		
Initial Abstraction, Ia (in) Ia/p Ratio	0.817 0.406		0.817 0.000
Unit Discharge, * qu (csm/in)	359		0
Runoff, Q (in)	0.27		0.00
Pond & Swamp Adjustment Factor	1.00	1.00	1.00
PEAK DISCHARGE, qp (cfs)	1	0	0
Summary of Computations for qu		-	
Ia/p #1	0.400	0.000	0.000
CO´ #1	2.364	0.000	0.000
C1 #1	-0.599		0.000
C2 #1	-0.056		0.000
qu (csm) #1	367.203	0.000	0.000
Ia/p #2	0.450	0.000	0.000
C0 #2	2.292	0.000	0.000
C1 #2	-0.570		0.000
C2 #2	-0.023	0.000	0.000
qu (csm) #2	307.131	0.000	0.000
* qu (csm)	359	0	0

\* Interpolated for computed Ia/p ratio (between Ia/p #1 & Ia/p #2) If computed Ia/p exceeds Ia/p limits, bounding limit for Ia/p is used.

2

log(qu) = C0 + (C1 \* log(Tc)) + (C2 \* (log(Tc)))qp (cfs) = qu(csm) \* Area(sq.mi.) \* Q(in.) \* (Pond & Swamp Adj.)

# STAFF REVIEW - PLANNING COMMISSION REPORT - NOVEMBER 5, 1996 HEARING

FILE:	PDR-96-217
DATE:	October 30, 1996
STAFF:	Bill Nebeker
REQUEST:	Final Plat and Plan for The Knolls, Filing #1
	Revised Preliminary for The Knolls
	Rezone from RSF-4 and PR 7.2 to PR 2.6 and PR
	Special Use Permit for Low Density Development in the Airport Critical
	Zone
LOCATION:	Southeast corner of 27 1/2 Road and Cortland Avenue (F 3/4 Road)
APPLICANT:	Robert C. Knapple

EXECUTIVE SUMMARY: The applicant proposes a planned residential development consisting of 51 single family homes, 23 townhomes and a 4.8 acre site reserved for a future church. The site is located in the Airport Critical Zone which requires a special use permit for low density residential uses and churches. The site is proposed to be rezoned from PR 7.2 and RSF-4 to PR 2 on the church site and PR 2.6 on the residential portion of the site. Preliminary approval was previously approved for phase I of the subdivision which consists of the 9 lots located on Ridge Drive. Final plat approval is requested for phase I, and preliminary approval is requested for the remainder of the subdivision, including the church site. The entire site is located on 33.84 acres. Staff recommends approval with conditions

EXISTING LAND U	SE.	Vacant
EAISTING LAND C	51.	vacant
PROPOSED LAND	USE:	single family lots and church site
SURROUNDING LA	AND USE: NORTH: SOUTH: EAST: WEST:	Single Family homes & Church Vacant Single Family homes Single Family homes
EXISTING ZONING	i:	PR 7.2 & RSF-4
PROPOSED ZONIN	G:	church site - PR 2 remainder - PR 2.6
SURROUNDING ZO	DNING: NORTH: SOUTH: EAST:	RSF-4 & PR-8 RSF-4 RSF-4

#### WEST: PR-4, RSF-4, PR 1.9

RELATIONSHIP TO COMPREHENSIVE PLAN: The approved Growth Plan shows this area developing as Residential Medium-Low (2-3.9 dwellings per acre).

STAFF ANALYSIS: The applicant proposes to develop a planned residential development consisting of 51 single family homes, 23 townhomes and a 4.8 acre site reserved for a future church. The site is located in the Airport Critical Zone which requires a special use permit for low density residential uses and churches. The site is proposed to be rezoned from PR 7.2 and RSF-4 to PR 2 on the church site and PR-2.6 on the residential portion of the site. Preliminary approval was previously approved for phase I of the subdivision which consists of the 9 lots located on Ridge Drive. Final plat approval is requested for phase I, and preliminary approval is requested for the remainder of the subdivision, including the church site. The entire site is located on 33.84 acres.

**Rezone:** This site was formerly known as "Onion Hill" which received a change of zoning and preliminary plan approval during the late 1980's. The plan was never completed and lapsed. The PR 7.2 zoning remains on the site. The Onion Hill site is being added to Lot 2 of the St. Matthew's Episcopal Church Subdivision which is zoned RSF-4. Since that time the surrounding area has developed at a density much less than 7.2 dwellings per acre. The average overall surrounding density appears to be at about 4 dwellings per acre. The Growth Plan recommends that the density not exceed 3.9 dwellings per acre. The plan is based on surrounding densities and the fact that most of this site is located within the Airport Critical Zone boundaries. Residential densities higher than 4 units per acre are compatible within the Critical Zone boundaries.

The applicant is proposing a density of approximately 2.6 dwellings per acre over the residential portion of the site, including the townhomes. By themselves the townhome density is approximately 3.85 dwellings per acre which is still in conformance with the Growth Plan and the Critical Zone boundaries. Because this proposal is a Planned Residential Development, the overall density including single family homes, townhomes, open space and roads, is used to calculate the 2.6 units per acre zoning. The church site is excluded from this calculation. The church site is assigned it own zoning of PR-2. This site is limited for use as a future church.

Staff finds that the proposed rezone meets the criteria established in Section 4-4-4 of the Grand Junction Zoning and Development Code as noted below:

- A. **Was the existing zone an error at the time of adoption?** No. The zoning reflected an approved development plan with a higher density not desirable at this time due to the proximity of the airport and lower surrounding densities.
- B. Has there been a change in character in the area due to the installation of public facilities, other zone changes, new growth trends, deterioration, development

**transitions, etc.?** Yes. As mentioned in A above, the majority of the surrounding area as developed at a much lower density. Also the Airport has identified that densities higher than 4 dwellings per acre are incompatible within the Critical Zone.

C. Is there an area of community need for the proposed rezone? The project is a response to an anticipated market demand for the proposed residential use which includes single family homes and townhomes.

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- D. Is the proposed rezone compatible with the surrounding area or will there be adverse impacts? Yes. The density of the townhomes is still within the average density of surrounding uses. The townhomes are located between open space and the church site, adjacent to the heavier traveled 27 1/2 Road. The density of the single family homes in below the density of surrounding uses.
- E. Will there be benefits derived by the community, or area, by granting the proposed rezone? This site has been a constant nuisance for Code Enforcement over the past years due to uncontrolled weed growth. Development of this site to residential uses will result in City resources being spent in other areas of the community. The proposal also infills a vacant parcel almost surrounded by development. Benefits derived by the community also include the widening of Cortland Avenue and the increase in the property tax base.
- F. Is the proposal in conformance with the policies, intents and requirements of this Code, with the City Master Plan (Comprehensive Plan), and other adopted plans and policies? Yes. The zoning is in conformance with the Growth Plan Map, which shows this area developing as residential 2-3.9 dwellings per acre.
- G. Area adequate public facilities available to serve development for the type and scope suggested by the proposed zone? Yes. Utilities are available to serve this development. There will be a lesser impact on area schools based on the down zoning of this parcel.

**Special Use Permit:** A Special Use Permit is required for low density residential uses (less than 4 units/acre) and churches to locate within Airport Critical Zones. The Airport Critical Zone is a rectangular-shaped zone located directly off the end of a runway's primary surface, beginning 200 feet from the end of the pavement, which is critical to aircraft operations (i.e. more apt to have accidents within it because of the takeoff and landing mode of aircraft in that particular area). The Airport has recommended that additional soundproofing measures be taken on the residential structures in to subdivision, to include additional sound-deadening insulation and planned landscaping in order to help mitigate noise level perceptions.

The applicant has incorrectly shown the location of the Airport Critical Zone on the preliminary plat and final plat. The Critical Zone encompasses all of the townhomes and about 28 of the single family homes. The majority of the lots in Filing 1 are outside the Critical Zone boundaries. Staff recommends that as part of the approval of the Special Use Permit that soundproofing measures and

planned landscaping be taken for the affected residential dwellings. The church will be required to apply for its own Special Use Permit during a future site plan review.

**Final Plat**: The final plat proposes 9 lots, ranging in size from 13,547 square feet (0.311 acres) to 27,965 square feet (0.642 acres). Proposed setbacks are 25 feet front, 20 feet rear, and 10 feet sides. Ridge Drive in Spring Valley will be extended about 175 feet and terminated in a cul-de-sac. A detached sidewalk matching those on the continuation of Ridge Drive will be constructed. A pedestrian path located in an open space tract will connect Filing 1 with the remainder of the subdivision. Although plans showed the pedestrian path in Tract A there were no details given. Construction plans shall be revised to show the size, length, cross-section, material and ramp connection for the path. The path shall be concrete, a minimum of 10 feet wide. A portion of the subdivision will drain through a pipe in the open space tract. An updated geotechnical report with pavement design for Ridge Drive shall be required before construction plans are approved.

**Preliminary Plan:** The remainder of the preliminary plan consists a 4.8 acre church site, 42 single family homes on individual lots, 23 townhomes clustered together around common open space, and an open space area with wetlands, irrigation ponds and nature areas.

<u>Church Site</u>: Lot 2 of St. Matthew's Episcopal Church Subdivision is included in this development. The applicant is trading the church's 5.53 acre lot located interior to the site, with a 4.8 acre lot at the corner of Cortland and 27 1/2 Road. The lot the church currently owns is located approximately where Hollow Court and adjacent lots on Ridge Drive are proposed. There are advantages and disadvantages to moving the church site. A large church is better suited at the intersection of two collector streets. It routes traffic off of residential streets and provides more exposure for the church. On the other hand the church has moved into the Airport Critical Zone boundaries. A church is allowed in the Critical Zone with a Special Use Permit, but it is not allowed to have a school as an accessory use because of the conflict with the congregation of children on a regular basis.

The church site will be platted with Filing 1 of The Knolls. A timeline for construction of the church is unknown. Street improvements on Cortland Avenue adjacent to the church will be required at the same time that improvements on the remainder of the street are constructed in conjunction with the platting of Filing 2. 27 1/2 Road in on the City's Capital Improvement Project and is scheduled for construction in 2003, although there are proposals to move it to 2000.

Planning Commission approval will be required for the church prior to construction because of its location in a planned zone.

<u>Single Family Homes</u>: Forty-two single family lots about 12,000 square feet in size (0.27 acres) are proposed in three remaining phases. Willow Glen Drive will be extended to the south property line to connect with future development to the south. It is anticipated that this road will eventually connect with 27 1/2 Road to provide an additional outlet for this subdivision. Without this

connection, this subdivision exceeds the TEDS (Transportation Engineering Design Standards) requirement of 250 maximum ADT (average daily traffic) for a subdivision with only one outlet.

During preliminary review of this subdivision the applicant stressed the importance of providing an alternate access to the single family home on the large lot directly south of the irrigation ponds. The home on this lot has access only on 27 1/2 Road in a location with a limited sight distance. A street stub was proposed to this location to provide additional access. Staff felt that the street stub was needed to extend to the parcel to the south, which had a better chance of redevelopment. A single driveway over a private ingress-egress easement would be sufficient to provide an alternate access to this home. Staff recommends that a private ingress-egress easement be provided for this lot with access to Willow Glen Drive.

<u>Townhomes</u>: Twenty-three townhomes clustered around private open space and served by a private street are proposed in Filing 3. Staff is in the process of preparing administrative guidelines for developments with private streets. Listed below are some revisions needed for the townhome development that are proposed by those administrative guidelines:

- 1. Pedestrian connections to Willow Glen Drive, 27 1/2 Road, the pedestrian path in the open space area and to the church site to the north will be required.
- 2. The "T" turnaround in Spring Court shall be at least 20 feet wide.
- 3. Additional off-street parking may be required within the development.
- 4. A pedestrian trail system may be substituted for an attached sidewalk if in the opinion of the Director, properties adjacent to the street section could easily access the trail and trail system links other trails and facilities. A pedestrian trail system will be required to be shown during final approval.
- 5. Street trees will be required.

A detailed analysis of the proposed townhome development will be made when Filing 3 plat is reviewed. The townhomes are detached with individual garages and a shared driveway. Some of the shared driveways exceed 50 feet in width. These driveways should be narrowed to reduce the expanse of asphalt in front of the homes.

<u>Open Space</u>: The applicant is proposing 2.8 acres of open space, located largely within an existing draw that is unsuited for development. A wetlands delineation has been performed and wetlands vegetation will be retained on the site. Two man-made ponds for storage of irrigation water and to provide storm runoff detention are proposed. A 10 foot wide pedestrian path connecting 27 1/2 Road with Ridge Drive runs just north of the open space area. A 5 foot wide nature trail is also proposed. A nature overlook is provided.

An area for active recreation has not been provided within the development. Typically planned residential developments are required to provide at a minimum, open flat grassy areas for a variety of active sports or play. Residents that live within the townhomes need active recreation areas, especially due to the small lots associated with the townhomes. Staff recommends that Lot 1, block

1 within Filing 3 be eliminated and this area be used as a park for this development. This would be an appropriate place for a sidewalk connection to the church located on the corner.

<u>Phasing</u>: A 4 phased plan is proposed for construction over a 3 year period. The townhomes are proposed for construction in the third phase. By building single family homes in the first two phases, the developer risks opposition to the final plat and plan for the townhomes from home buyers in filings 1 and 2. Particularly home buyers in phase 2 should be made aware of the proposal to construct townhomes within this subdivision. Staff recommends that a note be placed on the plat for filings 1 and 2 notifying potential lot owners that the townhomes are proposed as part of this subdivision.

STAFF RECOMMENDATION: Approval with the following conditions:

Special Use Permit:

- 1. Soundproofing measures shall be taken on the residential structures in Filings 2-4 located in the Airport Critical Zone to include additional sound-deadening insulation and planned landscaping in order to help mitigate noise level perceptions. A note shall be placed on the final plat and in the development's CC&Rs showing this requirement.
- 2. A Special Use Permit for the church to locate in the Airport Critical Zone shall be filed at the time construction is planned for the church.

## Final Plan:

- 3. Construction plans shall be revised to show the size, length, cross-section, material and ramp connection for the pedestrian path in Tract A. The path shall be concrete, a minimum of 10 feet wide.
- 4. An updated geotechnical report with pavement design for Ridge Drive shall be required before construction plans are approved.

Preliminary Plan:

- 5. Cortland Avenue improvements including the portion in front of the church shall be constructed during filing #2.
- 6. A private ingress-egress easement shall be provided between Willow Glen Drive and Lot 2, St. Matthew's Church Subdivision, to provide an alternate access for the home on this lot.
- 7. A pedestrian connection shall be made between the church site and the townhomes or Willow Glen Drive.
- 8. The townhome development shall comply with administrative guidelines for private streets.
- 9. Shared driveways in the townhome development shall be narrowed to reduce the expanse of asphalt in front of the homes.
- 10. Lot 1, block 1, Filing 3 shall be eliminated and this area used as a park for residents of The Knolls subdivision.

- 11. A note shall be placed on the plat for Filings 1 and 2 notifying potential lot owners that the townhomes are proposed as part of this subdivision.
- 12. The Airport Critical Zone Boundary shall be correctly identified on the plat.

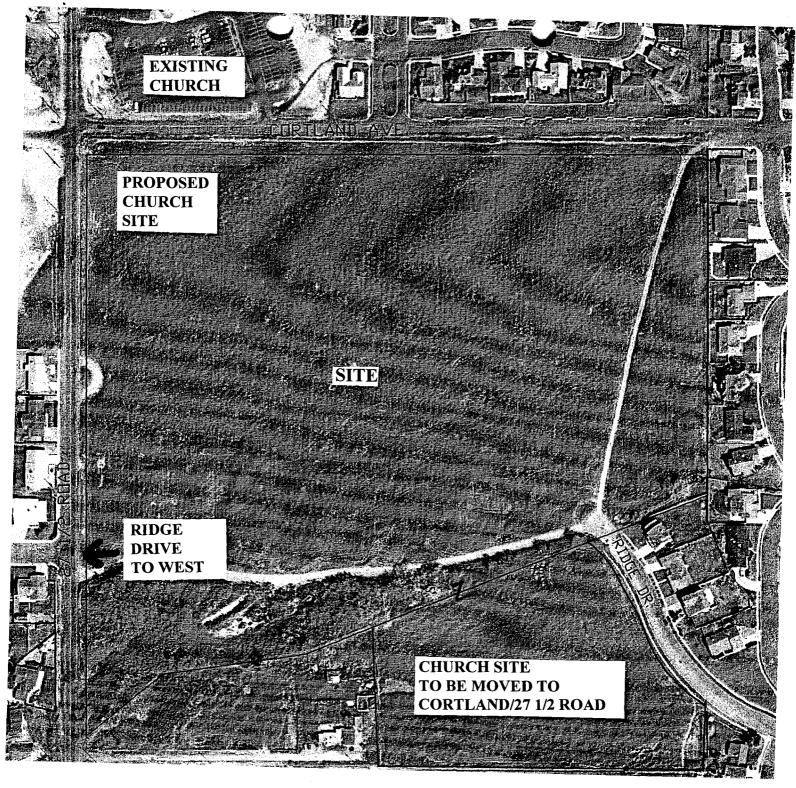
## RECOMMENDED PLANNING COMMISSION MOTION:

Mr. Chairman, on item 96-217 I move that we:

- 1. Forward a recommendation of approval to the City Council for the rezoning of the church site from PR 7.2 to PR 2; and the remainder of the subdivision from PR 7.2 and RSF-4 to PR 2.6.
- 2. Approve The Knolls Filing #1, the revised preliminary plan for The Knolls and the Special Use Permit per staff's recommendation.

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PDR-96-217 THE KNOLLS

## CITY OF GRAND JUNCTION PLANNING COMMISSION

FOR

### FINAL DECISION

PDR-96-217

Robert Knapple O.P. Development Co. LLC 2421 Applewood Circle Grand Junction, CO 81506

An application by O.P. Development Co., requesting the following;

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- 1. Rezone from Pr 7.2 to PR 2.2;
- 2. Approval of a revised preliminary plan for 51 single family lots, 23 patio home lots and 1 church site;
- 3. Approval of Filing #1 for 9 single family lots;
- 4. Approval of a special use permit for a church and residential development in an Airport Critical Zone;

affecting the parcel at the southeast corner of Cortland Avenue and 27 1/2 Road as described in the file referenced above, was considered by the City of Grand Junction Planning Commission on November 5, 1996.

After considering all the pertinent testimony and reviewing various data, the Planning Commission made the following actions:

- A. Approved the special use permit upon a finding that the proposal complies with Section 4-8-1 of the City of Grand Junction Zoning and Development Code, with the following conditions:
  - Soundproofing measures shall be taken on the residential structures in Filings 2-4 located in the Airport Critical Zone to include additional sound-deadening insulation and planned landscaping in order to help mitigate noise level perceptions. A note shall be placed on the final plat and in the development's CC&Rs showing this requirement.
  - 2. A Special Use Permit for the church to locate in the Airport Critical Zone shall be filed at the time construction is planned for the church.

- B. Approved the final plat for filing #1 with the following conditions:
  - 3. Construction plans shall be revised to show the size, length, cross-section, material and ramp connection for the pedestrian path in Tract A. The path shall be concrete, a minimum of 10 feet wide.
  - 4. An updated geotechnical report with pavement design for Ridge Drive shall be required before construction plans are approved.
- C. Accepted a withdrawal from the applicant for the preliminary plan and rezone request.

l, Nehh

Bill Nebeker Senior Planner

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<u>11-6-96</u> date

c: Banner Associates, Inc.

# Memorandum

DATE: December 6, 1996

TO: David Chase, Banner

FROM: Bill Nebeker, City Planning

RE: The Knolls

David - attached to the plat is the Memorandum of Improvements Agreement & Guarantee. Please have Bob Knapple sign and return with the plat.

I'll need the following before the plat can be recorded:

2 full size mylars of plat

1 reduced 11" X 17" mylar of plat

computer disk with plat info

\$21 recording fee for plat + \$6 recording fee for Memorandum of Improvements Agreement

signed Memorandum of Improvements Agreement

letter of credit for Development Improvements Agreement

Please also note that a homeowner's association will be required to be formed for maintenance of the Tract A.

If you have any questions please call me at 244-1447.

CITY OF GRAND JUNCTION FILE **#PDR-96-217 PLANNED DEVELOPMENT REVIEW - THE KNOLLS, FILING #1** LOCATED AT SE CORNER OF CORTLAND AVENUE & 27 ½ ROAD HAS BEEN REVIEWED AND APPROVED BY THE UTILITY COORDINATING COMMITTEE.

Butiand CHAIRMAN

<u>12-11-96</u> DATE

### CITY OF GRAND JUNCTION DEPARTMENT OF PUBLIC WORKS & UTILITIES 250 NORTH 5TH STREET GRAND JUNCTION, CO 81501 (970) 244-4003

1785315 0925AM 01/17/97 MONIKA TOOD CLEARED MESA COUNTY CO TO THE MESA COUNTY CLERK & RECORDER: THIS IS TO CERTIFY that the herein named Subdivision Plat, KNOLDS SUBDIVISION, TILING NO. 1 Situated in the  $N \in 1/4$  of Section Township | SOUTH, Range | WEST of the 👘 🕔 Meridian in the City of Grand Junction, TE County of Mesa, State of Colorado, has been reviewed under my direction and, to the best of my knowledge, satisfies the requirements pursuant to C.R.S. 38-51-106 and the Zoning and Development Code of the City of Grand Junction for the recording of subdivision plats in the office of the Mesa County Clerk and Recorder. This certification makes no warranties to any person for any purpose. It is prepared to establish for the County Clerk and Recorder that City review has been obtained. This certification does not warrant: 1) title or legal ownership to the land hereby platted nor the title or legal ownership of adjc and/or omissions, including, but not limited to, rights-of-ways and/or easements, whether or no liens and encumbrances, whether or not of qualifications, licensing status and/or any representation(s) made by the surveyor who prepar IMP AURIDUCENT subdivision plat. Dated this 6 day of Brember, 1996 243-244 City of Grand Junction, Department of Public Works & Utilities X ROAL 2294 16931 By: S L. Shanks, P.E., P.L.S. Director of Public Works & Utilities Recorded in Mesa County Date: Plat Book: 15 Page: 243 7 244 Drawer: CC/35

g:\special\platcert.doc

# TYPE LEGAL DESCRIPTION(S) BELOW, USING ADDITIONAL SHEETS AS NECESSARY. USE SINGLE SPACING WITH A ONE INCH MARGIN ON EACH SIDE.

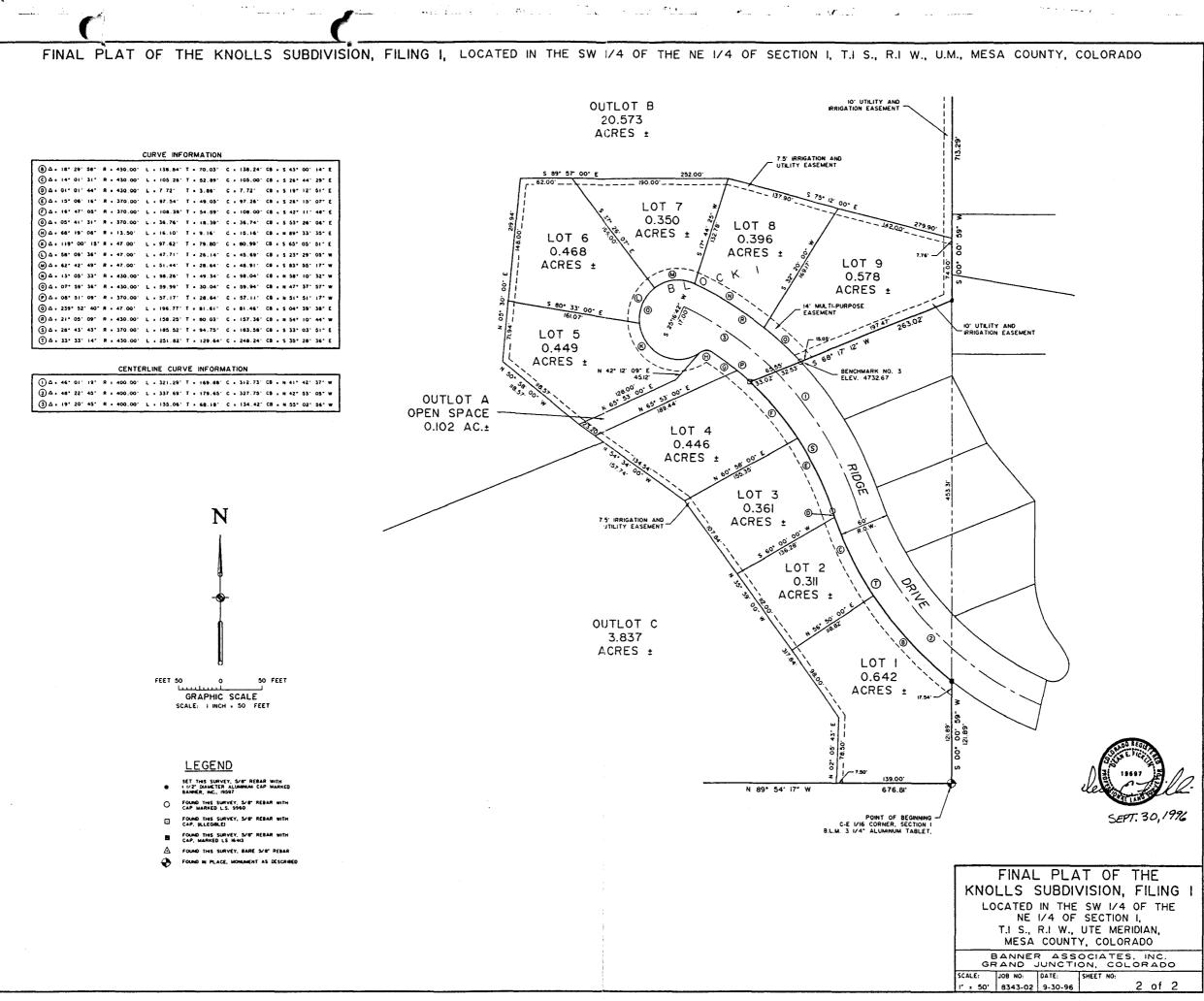
### **DESCRIPTION OF THE KNOLLS SUBDIVISION, FILING 1**

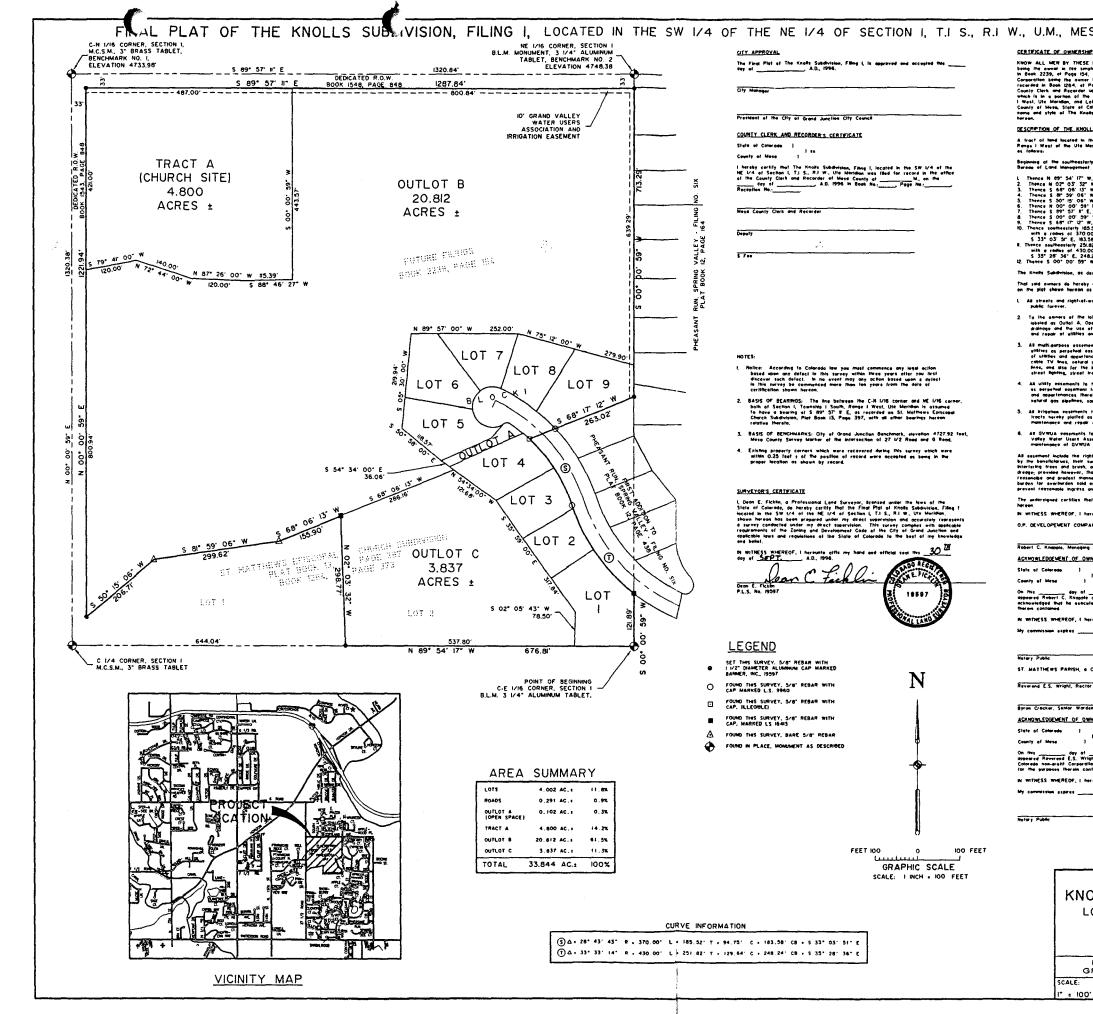
A tract of land located in the SW<sup>1</sup>/<sub>4</sub> of the NE<sup>1</sup>/<sub>4</sub> of Section 1, Township 1 South, Range 1 West of the Ute Meridian, County of Mesa, State of Colorado more fully described as follows:

Beginning at the southeasterly corner of The Knolls Subdivision, Filing 1, being a Bureau of Land Management Monument for the C-E 1/16 Corner of Section 1, Township 1 South, Range 1 West, Ute Principal Meridian.

- 1. Thence N 89° 54' 17" W, 676.81 feet;
- 2. Thence N 02° 03' 32" W, 298.77 feet;
- 3. Thence S 68° 06' 13" W, 155.90 feet;
- 4. Thence S 81° 59' 06" W, 299.62 feet;
- 5. Thence S 50° 15' 06" W, 206.71 feet;
- 6. Thence N 00° 00' 59" E, 1221.94 feet;
- 7. Thence S 89° 57' 11" E, 1287.84 feet;
- 8. Thence S 00° 00' 59" W, 713.29 feet;
- 9. Thence S 68° 17' 12" W, 263.02 feet;
- 10. Thence southeasterly 185.52 feet along the arc of a circular curve to the right with a radius of 370.00 feet, a delta of 28° 43' 43", and a chord bearing S 33° 03' 51" E, 183.58 feet;
- 11. Thence southeasterly 251.82 feet along the arc of a circular curve to the left with a radius of 430.00 feet, a delta of 33° 33' 14", and a chord bearing S 35° 28' 36" E, 248.24 feet;
- 12. Thence S 00° 00' 59" W, 121.89 feet to the Point of Beginning.

The Knolls Subdivision, as described above contains 33.844 acres more or less.



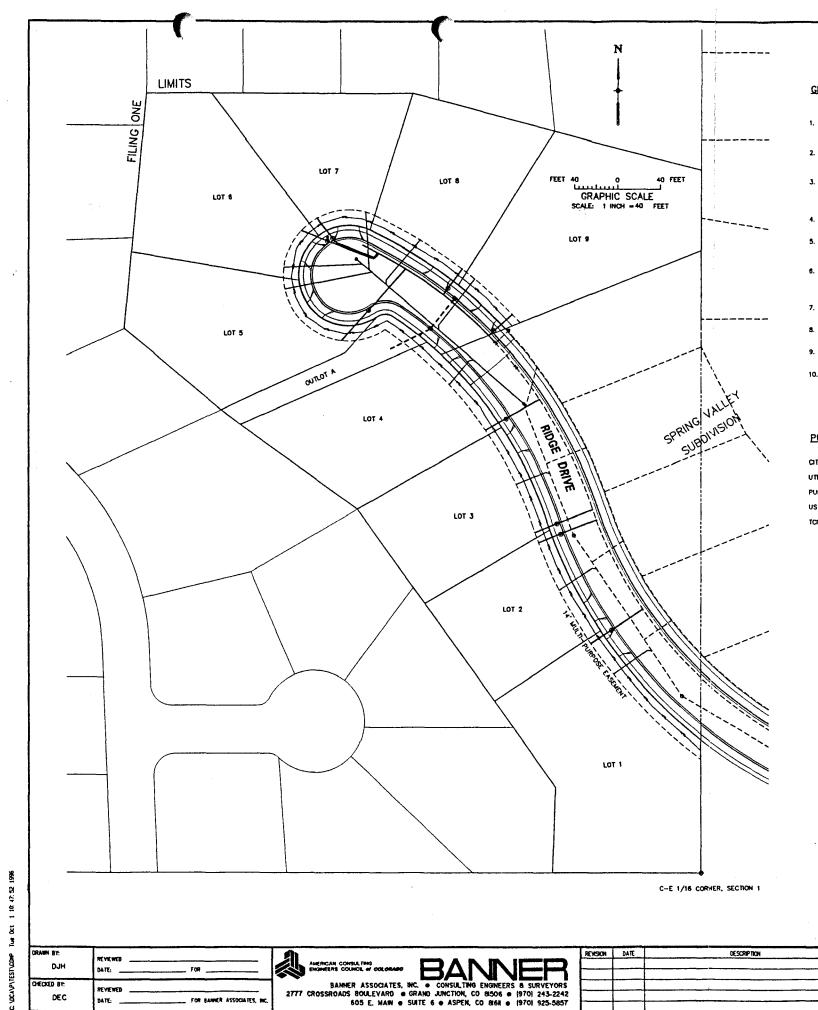


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., MESA COUNTY, COLC	ORADO
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CERTIFICATE OF OWNERSHIP AND DEDICATION <u>MARTIFICATE UF UFINERISTER AND PERCATOR</u> KNOW ALL MEN BY THESE PRESENTS that O.P. Development Company, LLC being the owner in the sample of that forestry as described in the instrument recorded in Book 2235, of Page 154, and that 51 Marthews Parish, a Calcode non-uraft Corrections there the control for the simple of that property as described in the instrument for the sample of the sample of that property as described in the instrument County Clerk and Eccuder Wash Which The Knots Subdivision, Films I is seciled in the sporting of the SW I/4 of the KI/4 of School Theorem Subdivision, at in the County of Markes Sites at Colorado do Subdivision for the sport of the the News Market State at Colorado do Subdivision for the sport of the shown horemain and style of The Knots Subdivision, Films I, in eccerdance with the Pasi shown horemain DESCRIPTION OF THE KNOLLS SUBDIVISION FILMS I A tract of hand located in the SW 1/4 of the NE 1/4 of Section L Texmiship i South. Ramee i West of the Ute Markhan, County of Masa, State of Colorado more hully described Beginning at the southeesterty cerner of The Knafs Subdivision, Filing I, being a Bureau of Land Management Manument for the C-E 1/16 Cerner at Section I, TJ S., R.I W., U.M.; The Knolls Subdivision, as described above contains 33.844 acres more or less That sold owners do hereby dealcate and set apart real property as shown and labeled on the plat shown hereon as fallows: All streets and right-of-way to the City of Grand Junction for the use of the o the ammers of the lots, their successors and assigns forever, the real property upsied as Quitol A. Open Saace as perpetiud essement for pedestrion ingress and egress, archinge and the use public utilities for the instalation, operation, maintenance and reader at utilities and appointamences. All multi-autors essements to the City of Grand Junction for the use at the Public willing as persetted essements for the installation, operation, methicances and regul-control of the second second second second second second second second control V these installations, control y second second second formed and second sec An utility eesements to the City of Grand Junction for the use of the public effettes as perpetual eesement for the installation, operation, maintenance and report of statis and appertunces thereis including, but not Ministel to effortic lines, cable TV thes, hatward gas playshes, contary source lines, water lines, lefephane lines. 18 krigation assements to the Homeowners Association and to the owners of the lots and tracts hereby platted as perpatua assements for the instability, operation, maniformers and repair of private irrigation systems, AT DVWUA resements to the City of Grand Juncilon for the use of the public and to the Gran, Valley Weter Usert Association, its successors and assigns, for the installation and maintenance of OVWUA integration fieldhese. menni luctude the right of ingress and spress an, along, over, under, through, and across beneficiewas, their successors, or estions, logether with the right is tim er remove and free and branch, and it Drakange and Delanfor/Feishin a sessmets). The right to provide havever, that the beneficients of total estimates that within the some in a 36 and prudent moment. Furthermore, the anometric of tota of their the some in a 36 and suckets and another the sometric of total writes and write the sestmetic total estimation by eracting on slocing any wardswenests thereon which m risesandow they are and another to another the saments. The undersigned certifles that no lending institution holds any ancumbrance on the property shown n withess whereof, I herewito set my hand this \_\_\_\_\_ day of \_ O.P. DEVELOPEMENT COMPANY, LLC Robert C. Knappie, Managing Directo ACKNOWLEDGEVENT OF OWNERSHIP . } ! # On his \_\_\_\_\_\_ day at \_\_\_\_\_\_ A.D., 1996, before me the undersigned atticer, personal appeared Robert C. Knopple as Monoging Okrector of O.P. Developement Company, LLC., and acknowledges May the securide the longradius certificate of Ownership. (or the purpose) IN WITNESS WHEREOF, I hereunte attis my have and official seal ST. MATTHEWS PARISH, a Coloredo non-profit Corporation Barne Cracker Senior Worden ACKHOWLEDGEWENT OF OWNERSHIP , <sup>| 16</sup> On the \_\_\_\_\_\_ day of \_\_\_\_\_\_ AD, 1996, before me the undersigned officers, per operated Reversed E.S. Wright is Rector dod Byran Cocker or Some Wriefen of S. Malthew Coloredge non-welf Corporation and echanologied that they ascuted the foregoing Certificate o for the purposes Thermit Containing. n witness whereor, I hereunic attiz my hand and atticid seal FINAL PLAT OF THE KNOLLS SUBDIVISION, FILING I LOCATED IN THE SW 1/4 OF THE NE 1/4 OF SECTION I, T.I S., R.I W., UTE MERIDIAN,

	MESA	COUNT	Y, COLORADO				
BANNER ASSOCIATES, INC. GRAND JUNCTION, COLORADO							
SCALE:	JOB NO:	DATE:	SHEET NO:				
1" = 100'	JOB NO: 8343-02	9-30-96	<u>    of 2</u>				



#### GENERAL NOTES:

- 1. CONSTRUCTION, INSPECTION, AND TESTING FOR INSTALLATION OF SAMITARY SEWER WILL BE IN ACCORDANCE WITH THE "SPECIFICATIONS FOR CONSTRUCTION OF SAMITARY SEWER SYSTEMS" AS DEVELOPED BY THE CITY OF GRAND JUNCTION.
- CONSTRUCTION, INSPECTION, AND TESTING FOR INSTALLATION OF DOMESTIC WATER WILL BE IN ACCORDANCE WITH THE "SPECIFICATIONS FOR WATERLINE CONSTRUCTION" AS DEVELOPED BY THE UTE WATER CONSERVANCY DISTRICT.
- SANITARY SEWER LINES TO BE CONSTRUCTED WITH SDR-35 PVC (ASTM 3034) SERVICE LINE CONNECTIONS TO THE NEW SEWER MAIN SHALL BE ACCOMPLISHED WITH FULL BODY WYES OR TEES. TAPPING SADDLES WILL BE ALLOWED ONLY WHERE CONNECTING SERVICES TO EXISTING SEWER MAIN.
- 4. DOMESTIC WATER MAIN TO BE CONSTRUCTED WITH 6"# PVC (AWWA C-900, CLASS 150) WATER SERVICE LINES TO BE 1"# SOFT TEMPER COPPER PIPE.
- 5. THE CONTRACTOR SHALL HAVE ONE SIGNED COPY OF THE PLANS AND A COPY OF THE CITY OF GRAND JUNCTION STANDARDS AND SPECIFICATIONS AND A COPY OF UTE WATER CONSERVANCY DISTRICT STANDARDS AND SPECIFICATIONS ON THE JOB SITE AT ALL TIMES.
- 8. CONTRACTOR IS RESPONSIBLE FOR INSTALLING WATER METER PITS AND YOKES. UTE WATER CONSERVANCY DISTRICT WILL SUPPLY THE PITS AND YOKES. WATER SERVICES WILL BE EXTENDED TO THE MULTIPURPOSE EASEMENT LINE, AND MARKED WITH A METAL OR WOOD POST PAINTED BLUE. METER PITS TO BE LOCATED 2 FEET BACK OF CURB.
- ALL SEWER SERVICE LINES SHALL BE EXTENDED TO THE MULTIPURPOSE EASEMENT LINE AND MARKED WITH A METAL OR WOOD POST PAINTED GREEN.
- 8. THE CITY OF GRAND JUNCTION AND UTE WATER CONSERVANCY DISTRICT SHALL BE NOTIFIED 48 HOURS IN ADVANCE OF ANY CONSTRUCTION ACTIVITIES.
- 9. CONTRACTOR IS RESPONSIBLE FOR OBTAINING THE NECESSARY UNDERGROUND UTILITY PERMITS PERMITS REQUIRED FOR WORK WITHIN THE EXISTING RIDGE DRIVE RIGHT-OF-WAY.
- 10. FINAL LAYOUT, ROUTING, AND LOCATION OF TRANSFORMERS OR PEDESTALS TO BE DETERMINED BY INDIVIDUAL UTILITY COMPANIES.

#### PUBLIC FACILITIES

CITY OF GRAND JUNCTION (SANITARY SEWER AND STORM SEWER) UTE WATER CONSERVANCY DISTRICT (DOMESTIC WATER)

PUBLIC SERVICE COMPANY OF COLORADO (GAS AND ELECTRIC)

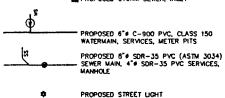
US WEST COMMUNICATIONS (TELEPHONE)

TCI-UNITED ARTISITS CABLE OF WESTERN COLORADO (CABLE TV)

### LEGEND

- A -- H -- EXISTING WATER MAIN, FIRE HYDRANT, VALVE O- --- EXISTING SEWER MAIN, SERVICES, MANHOLE





COMMON UTILITIES TRENCH (ELEC, GAS, TV, PHONE)

2	ORAWN BY:	REVENCE		REVISION	DATE	DESCRIPTION	BY	CHD	O.P. DEVELOPMENT CO., L.L.C.
291	DJH	DATE: FOR			ł				· · · · · · · · · · · · · · · · · · ·
o/TES	CHECKED BY:		BANNER ASSOCIATES, INC. • CONSULTING ENGINEERS & SURVEYORS						сомро
3	050	REVIEWED	2777 CROSSROADS BOULEVARD . GRAND JUNCTION, CO 8506 . (970) 243-2242						
3	500	DATE: FOR BANNER ASSOCIATES, INC.	605 E. MAIN . SUITE 6 . ASPEN, CO 8(6) . (970) 925-5857						THE KNOL

· · ·	GRAND	JUNCTION,	COLORADO	SCALE: Hunte: 1" = 40" Verte	Project Hec 8343
MPOSITE PLAN				OATE:	SHEET NO:
NOLLS SUBDIVISION				9-30-96	4 OF 11

## **File Close-out Summary**

**File #:** PDR-96-217

**Name**: The Knolls - revised preliminary plan, final plat for filing #1; special use permit & rezone

Staff: Bill Nebeker

Action: revised preliminary withdrawn by applicant; filing #1 approved; special use permit for residential portion of site approved (SUP for church not approved at this time because no development proposal was submitted), rezoning requests withdrawn

**Comments**: revised revised preliminary submitted and approved (file # RSF-1997-033)

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**File Turned In:** 04-07-97