Table of Contents

File <u>RZP-1996-157</u> Name: <u>Horizon Village – SE Corner of 7th Street / Horizon Drive – Rezone/Preliminary Plan</u>							
P r e s e n t	S c a n n e d	A few items are denoted with an asterisk (*), which means they are to be scanned for permanent record on the ISYS retrieval system. In some instances, items are found on the list but are not present in the scanned electronic development file because they are already scanned elsewhere on the system. These scanned documents are denoted with (**) and will be found on the ISYS query system in their designated categories. Documents specific to certain files, not found in the standard checklist materials, are listed at the bottom of the page. Remaining items, (not selected for scanning), will be listed and marked present. This index can serve as a quick guide for the contents of each file.					
X	X	Table of Contents					
		*Review Sheet Summary					
X	X	*Application form					
X		Review Sheets					
		Receipts for fees paid for anything					
X	X	*Submittal checklist					
X	X	*General project report					
		Reduced copy of final plans or drawings			`		
X		Reduction of assessor's map.			and the state of t		
		Evidence of title, deeds, easements			\.\		
X	X	*Mailing list to adjacent property owners			en e		
		Public notice cards					
		Record of certified mail					
X	X	Legal description					
		Appraisal of raw land					
	\neg	Reduction of any maps – final copy			to the second		
	\neg	*Final reports for drainage and soils (geotechnical reports)			7 (74) (14 (4 (1 4))		
	\neg	Other bound or non-bound reports					
		Traffic studies					
X	X	*Review Comments					
		*Petitioner's response to comments					
X	X	*Staff Reports					
\dashv	\dashv	*NI					
		*Planning Commission staff report and exhibits					
-	-	*City Council staff report and exhibits *Summary sheet of final conditions					
!	i	DOCUMENT DES	CDI	IDT	TON.		
		BOCCIMENT BES	CI		TON:		
x	X	Correspondence	X	1	Parking Detail - Sheet 2		
X		Preliminary Drainage Report – 6/27/96		-	1 arking Detail - Sheet 2		
X		Photos / Brochures/Illustrations of constructed interior/exterior	+	\vdash			
	1	sites					
X	X	Surficial Geology Investigation – 6/28/96	+				
X	X	Subsurface Soils Exploration – 6/29/96	1				
X	X	Wetlands Report – 7/96	\top				
X X X		Posting of Public Notice Signs – 7/26/96	1				
X		Planning Commission Minutes / Agenda – 9/3/96 - **		П			
X		Warranty Deed – Bk 1033 / Pg 246 – not conveyed to City	1	\Box			
X		Parking Detail	T				
X		Preliminary Plan					
X		Location Map					
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DEVELOPMENT APPLICATION

Community Development Department 250 North 5th Street, Grand Junction, CO 81501 (303) 244-1430

Receipt	 		
Date			
Rec'd By		 47.	
File No			

	situated in Me		ndersigned, being the ow te of Colorado, as descr	ners of property ibed herein do hereby pe	tition this:		
PETITION	PHASE	SIZE	LOCATION	ZONE		LAND USE	
Subdivision Plat/Plan	☐ Minor Major ☐ Resub	9.2 dc	SE CORNER OF 7th HORIZOH			RESIDENTUL	
X Rezone	To the second			From: PR 6.2 To:	PR-7-4		
Planned Development	ODP Prelim Final	9.24c	SE CORNER OF 7th HORIZON			PESIDENTUL	
☐ Conditional Use							
☐ Zone of Annex	1						
☐ Variance						·	
☐ Special Use							
☐ Vacation						☐ Right-of Way	
☐ Revocable Permit		******					
□ PROPERTY OWNER		CU	DEVELOPER CUNNINGHAM INVESTMENT CO.,INC. MAC CUNNINGHAM Name Name				
<u>(12 26/z Ro.</u> Address	4P	lz Ad	121 S. GALGNA STREET SHITE ZOI 259 GRAND AVE. Address Address				
SPAND JUNCTION, City/State/Zip	CO 81501	_	SPEN, CO 8 (61) y/State/Zip		GRAND JUNCTION, CO 81501 City/State/Zip		
742 - 2464 Business Phone No.			76) 925-8803 siness Phone No.		245-		
Business Phone No. Business Phone No. Business Phone No. NOTE: Legal property owner is owner of record on date of submittal.							
We hereby acknowledge that we have familiarized ourselves with the rules and regulations with respect to the preparation of this submittal, that the foregoing information is true and complete to the best of our knowledge, and that we assume the responsibility to monitor the status of the application and the review comments. We recognize that we or our representative(s) must be present at all required hearings. In the event that the petitioner is not represented, the item will be dropped from the agenda, and an additional fee charged to cover rescheduling expenses before it can again be placed on the agenda.							
Signature of Person Completing Application Date							
Viele VI Wahlere 6/24/96							
Heen 1/1 aplece 6/20/96							

Signature of Property Owner(s) - attach additional sheets if necessary

Date



MAJOR SUBDIVISION: PRELIMINARY

Location: SE Corner 7th & Horizon Project Name: **ITEMS** DISTRIBUTION Date Received <u>N-1-94</u> TOTAL REQ'D. Corps of Engineer SSID REFERENCE Receipt # File # **DESCRIPTION** Application Fee \$1,035 VII-1 Submittal Checklist VII-3 VII-3 Review Agency Cover Sheet* VII-1 Application Form* 8 Reduction of Assessor's Map VII-1 Evidence of Title VII-2 VII-2 Names and Addresses Legal Desdription VII-2 General Project Report X-7 8 IX-21 Location Map 6 Preliminary Plan IX-26 O 11"x17" Reduction of Prelim, Plan IX-26 Preliminary Drainage Report X-12 · Geotechnical Report 11 X-08 Wetlands Studing · Traffic Impact Study 1 21-X

NOTES: * An asterisk in the item description column indicates that a form is supplied by the City.

APRIL 1995

PRE-APPLICATION CONFERENCE

Date: 6 17 96 Conference Attendance: B. Hart, M. Drollinger Proposal De Corner 7478 Horizon							
Tax Parcel Number: 2945 - 024 - 00 - 048 Review Fee: \$1,035 (Fee is due at the time of submittal. Make check payable to the City of Grand Junction.)							
Additional ROW required? As per engage Adjacent road improvements required? Area identified as a need in the Master Plan of Parks and Recreation?							
Parks and Open Space fees required?	IES						
Recording fees required?		Estimated Amount:					
Half street improvement fees/TCP requ	uired? TCP or as per ens.	Estimated Amount:					
Revocable Permit required? No							
State Highway Access Permit required	? No						
On-site detention/retention or Drainage	e fee required? On - 5)+e						
Applicable Plans, Policies and Guideli	nes Devel-Code						
Located in identified floodplain? FIRM panel # YES Located in other geohazard area?							
Located in established Airport Zone? Clear Zone, Critical Zone, Area of Influence? Area of Toblogical Avigation Easement required?							
While all factors in a development proposal require careful thought, preparation and design, the following "checked" items are brought to the petitioner's attention as needing special attention or consideration. Other items of special concern may be identified during the review process.							
O Access/Parking	O Screening/Buffering	O Land Use Compatibility					
O Drainage	O Landscaping	O Traffic Generation					
O Floodplain/Wetlands Mitigation	O Availability of Utilities	O Geologic Hazards/Soils					
O Other							
Related Files:	A STATE OF THE STA						
Veigien Liles,							
It is recommended that the applicant inform the neighboring property owners and tenants of the proposal prior to the public hearing and preferably prior to submittal to the City.							
PRI	E-APPLICATION CONFERE	NCE					

WE RECOGNIZE that we, ourselves, or our representative(s) must be present at all hearings relative to this proposal and it is our responsibility to know when and where those hearings are.

In the event that the petitioner is not represented, the proposed item will be dropped from the agenda, and an additional fee shall be charged to cover rescheduling expenses. Such fee must be paid before the proposed item can again be placed on the agenda. Any changes to the approved plan will require a re-review and approval by the Community Development Department prior to those changes being accepted.

WE UNDERSTAND that incomplete submittals will not be accepted and submittals with insufficient information, identified in the review process, which has not been addressed by the applicant, may be withdrawn from the agenda.

WE FURTHER UNDERSTAND that failure to meet any deadlines as identified by the Community Development Department for the review process may result in the project not being scheduled for hearing or being pulled from the agenda.

Signature(s) of Petitioner(s)

Signature(s) of Representative(s)

RZP-96-157

2945-024-10-015 THOMAS D GRAVES PATRICIA L 2719 8TH CT GRAND JUNCTION, CO 81506-8203

2945-024-20-012 WARREN LEE MCELVAIN CAROLE A 2123 NATAHOA CT FALLS CHURCH, VA 22043-1948

2945-024-20-057 ERIN J JOHNSON 2750 REED ST LAKEWOOD, CO 80215-6832

2945-024-20-011 RONALD WILLIAM HALL PO BOX 3949 GRAND JUNCTION, CO 81502-3949

2945-024-20-034 DOROTHY E HOWARD 636 HORIZON DR APT 809 GRAND JUNCTION, CO 81506-0901

2945-024-20-037
JOY E EISENHAUER
VIKI L SIMMONS
636 HORIZON DR APT 812
GRAND JUNCTION, CO 81506-0901

2945-024-20-052 RALPH R POWERS ELIZABETH ANNE POWERS - TRUST

636 HORIZON DR APT 903 GRAND JUNCTION, CO 81506-0902 2945-024-20-055 JOAN NESTLER 636 HORIZON DR APT 906 GRAND JUNCTION, CO 81506-0903

2945-024-20-060 WAYNE W NELSON MARIE NELSON 636 HORIZON DR APT 911 GRAND JUNCTION, CO 81506-0904

2945-024-20-059 TERRY G BROOM MARY JANE BROOM 2678 CONTINENTAL DR GRAND JUNCTION, CO 81506-1801 2945-024-10-016 NORMAN A CRAIG HARRIETT V 2721 8TH CT GRAND JUNCTION, CO 81506-8203

2945-024-20-009 MICHAEL R BIEBER MARGUERITE M 4202 24TH ST #508 LUBBOCK, TX 79410

2945-024-20-024
COLORADO NATIONAL BANK
CNDT2311
DORA PERLMUTTER TRUST
PO BOX 5168
DENVER, CO 80217-5168
2945-024-21-002
RONALD LYNN UNFRED
LEE ANN UNFRED
614 30 RD
GRAND JUNCTION, CO 81504-5560

2945-024-20-035 PHYLLIS L SAFFORD KAWNA L 636 HORIZON DR APT 810 GRAND JUNCTION, CO 81506-0901

2945-024-20-050 ETHEL E ARENDSEE 636 HORIZON DR APT 901 GRAND JUNCTION, CO 81506-0902

2945-024-20-053 CHESTER J CARTER PHYLLIS A 636 HORIZON DR APT 904 GRAND JUNCTION, CO 81506-0902

2945-024-20-056 KAWNA L SAFFORD 636 HORIZON DR APT 907 GRAND JUNCTION, CO 81506-0903

2945-024-20-061 ALLAN L WORLEY 636 HORIZON DR APT 912 GRAND JUNCTION, CO 81506-0904

2945-024-20-025 GERALD J ASHBY ELIZABETH 636 HORIZON DR -UNIT 304 GRAND JUNCTION, CO 81506-1979 2945-024-10-017 WALTER H HATMAKER ETHEL P 2656 PATTERSON RD GRAND JUNCTION, CO 81506-8838

2945-024-20-028 GARY J CUCAROLA MARY E CUCAROLA 14655 W 56TH DR ARVADA, CO 80002

2945-024-20-041 BEVERLY J KIRBY PO BOX 4332 GRAND JUNCTION, CO 81502

2945-024-21-003 RONALD LYNN UNFRED LEE ANN UNFRED 614 30 RD GRAND JUNCTION, CO 81504-5560

2945-024-20-036 HENRIETTA W HAY 636 HORIZON DR APT 811 GRAND JUNCTION, CO 81506-0901

2945-024-20-051 TERRY LEE SOMMERFIELD

ROBERTA SUE
636 HORIZON DR APT 902
GRAND JUNCTION, CO 81506-0902
2945-024-20-054
ELIZABETH L BENTJEN
636 HORIZON DR APT 908
GRAND JUNCTION, CO 81506-0903

2945-024-20-058
ELEANOR ANDERSON
BETH E VOKOUN - SYLVIA K CONN
636 HORIZON DR APT 909
GRAND JUNCTION, CO 81506-0904

2945-024-20-023 LAWRENCE D CAPPS TRUSTEE 1111 HORIZON DR APT 606 GRAND JUNCTION, CO 81506-1454

2945-024-20-001 NOLA A MORRISSEY 636 HORIZON DR APT 101 GRAND JUNCTION, CO 81506-1980 2945-024-20-003 RUTH A BENNETT 636 HORIZON DR APT 103 GRAND JUNCTION, CO 81506-1980

2945-024-20-007 JESSE REAGAN STONE 636 HORIZON DR APT 202 GRAND JUNCTION, CO 81506-1981

2945-024-20-038 MOLLY L STUCKER TRUSTEE 636 HORIZON DR APT 401 GRAND JUNCTION, CO 81506-1983

2945-024-20-042 EARLE B WAGAMAN MILDRED I 636 HORIZON DR APT 501 GRAND JUNCTION, CO 81506-1984

2945-024-20-045

JANE S QUIMBY
636 HORIZON DR APT 504

GRAND JUNCTION, CO 81506-1984

2945-024-20-048 K B LATHAM 636 HORIZON DR APT 603 GRAND JUNCTION, CO 81506-1985

2945-024-20-014 GLADYS R PHILLIPS JOHN B 636 HORIZON DR APT 705 GRAND JUNCTION, CO 81506-1987

2945-024-20-017 SHARON DANIELS 636 HORIZON DR APT 708 GRAND JUNCTION, CO 81506-1987

2945-024-20-026 DIANA W CHOTVACS 636 HORIZON DR APT 801 GRAND JUNCTION, CO 81506-1989

2945-024-20-032 LORELL E CHAPMAN 636 HORIZON DR APT 807 GRAND JUNCTION, CO 81506-1990 2945-024-20-004 ARTHUR HENKE MARGERY O 636 HORIZON DR APT 104 GRAND JUNCTION, CO 81506-1980

.2945-024-20-008 HOWARD J NESBITT MILDRED A-TRUSTEES 636 HORIZON DR APT 203 GRAND JUNCTION, CO 81506-1981

2945-024-20-039 ROBERT L HOOVER RHEA JEAN 636 HORIZON DR APT 402 GRAND JUNCTION, CO 81506-1983

2945-024-20-043 A J LETEY MARGARET 636 HORIZON DR APT 502 GRAND JUNCTION, CO 81 506-1984

2945-024-20-046 J DAN POWELL DOROTHY J POWELL 636 HORIZON DR APT 601 GRAND JUNCTION, CO 81506-1985

2945-024-20-049 MARILYNN J DORN 636 HORIZON DR APT 604 GRAND JUNCTION, CO 81506-1985

2945-024-20-015 MARGE RICHERT 636 HORIZON DR APT 706 GRAND JUNCTION, CO 81506-1987

2945-024-20-019 JOHN C LAFFERTY DONNA J 636 HORIZON DR APT 710 GRAND JUNCTION, CO 81506-1988

2945-024-20-027 VIVIEN M GLAZE 636 HORIZON DR APT 802 GRAND JUNCTION, CO 81506-1989

2945-024-20-033 F BING JOHNSON ROSE W 636 HORIZON DR APT 808 GRAND JUNCTION, CO 81506-1990 2945-024-20-006 EARL P JONES MARGARET G 636 HORIZON DR APT 201 GRAND JUNCTION, CO 81506-1981

2945-024-20-022 LILLIAN S MOORE 636 HORIZON DR APT 301 GRAND JUNCTION, CO 81506-1982

2945-024-20-040 RUTH ALLINE HALL 636 HORIZON DR APT 403 GRAND JUNCTION, CO 81506-1983

2945-024-20-044 ROBERT W STRAIN MARY S 636 HORIZON DR APT 503 GRAND JUNCTION, CO 81506-1984

2945-024-20-047 ROBERT F LINNEMEYER CAROLYN A 636 HORIZON DR APT 602 GRAND JUNCTION, CO 81506-1985

2945-024-20-010 ROBIN L KENDRICK 636 HORIZON DR APT 701 GRAND JUNCTION, CO 81506-1986

2945-024-20-016 LAVINA E SUMMERS 636 HORIZON DR APT 707 GRAND JUNCTION, CO 81506-1987

2945-024-20-021 NORMA F HERMAN TRUSTEE 636 HORIZON DR APT 712 GRAND JUNCTION, CO 81506-1988

2945-024-20-030 WILLIAM PAUL CASH GERALDINE MARIE 636 HORIZON DR APT 805 GRAND JUNCTION, CO 81506-1990

2945-024-20-002 EDWARD M GARDNER LOIS K 935 LAKESIDE CT GRAND JUNCTION, CO 81506-2815 2945-024-20-020 MELVIN L SCOTT DONNA M 1025 LAKESIDE DR GRAND JUNCTION, CO 81506-2823

2945-024-20-013 RUDY A RODRIGUEZ CHRISTINE A 1636 HASLAM TER LOS ANGELES, CA 90069-1305

2945-023-00-023 JOHN I GORDON SHARON A 629 1/2 26 1/2 RD GRAND JUNCTION, CO 81506-1903

2945-023-00-029
MILDRED M VANDOVER
TRUSTEE
604 MEANDER DR
GRAND JUNCTION, CO 81505-1414

2945-023-13-002 WDM CORPORATION 2525 N 8TH ST GRAND JUNCTION, CO 81501-8845

2945-023-13-008 GORDON R GILBERT VICTORIA L 628 SAGE CT GRAND JUNCTION, CO 81506-1955

GRAND JUNCTION, CO 81502-1628

2945-023-15-001 ROBERT B CHRISTENSEN TRUSTEE PO BOX 3025

Mac Cunningham Cunningham Investments Co.,Inc 121 S Galena St., Suite 201 Aspen, CO 81611 2945-024-20-018

ROGER C HEAD

TRUST

2713 8TH CT

GRAND JUNCTION, CO 81506-8203

2945-024-20-029 RUDY A RODRIGUEZ CHRISTINE A 1636 HASLAM TER LOS ANGELES, CA 90069-1305

2945-023-00-027 MERCEDES CAMERON 621 26 1/2 RD GRAND JUNCTION, CO 81506-1904

2945-023-00-948 CITY OF GRAND JUNCTIO \

250 N 5TH ST GRAND JUNCTION, CO 81: 01-2628

2945-023-13-005 MICHAEL R HEUTON JUDITH M 630 SAGE CT GRAND JUNCTION, CO 81506-1955

2945-023-14-006 WM R PATTERSON 662 26 RD GRAND JUNCTION, CO 81506-1405

GRAND JUNCTION, CO 81502-3025

2945-023-15-002 R M O LAND CO LLC 550 PATTERSON RD GRAND JUNCTION, CO 8150

Brian Hart Landesign 259 Grand Ave. Grand Junction, CO 81501 2945-024-20-031
WAYNE P HARRIS
ELIZABETH J HARRIS
36 N MEADOW VIEW CT
GLENWOOD SPRINGS, CO
81601-9224
2945-023-00-001
SHIRLEY A HOWARD
ETAL - C/O CLARENCE L FILES
631 26 1/2 RD
GRAND JUNCTION, CO 81506-1961

2945-023-00-028 C W MOTTRAM R D 609 26 1/2 RD GRAND JUNCTION, CO 81506-1904

2945-023-13-001/ WDM CORPORATION 2525 NATH ST GRAND JUNCTION, CO 81501-8845

2945-023-24-002 MESA VIEW RETIREMENT RESIDENCE PO BOX 14111 SALEM, OR 97309-5026

2945-023-14-007 SISTERS OF CHARITY OF LEAVENWORTH HEALTH SERVICES CORPORATION

PO BOX 1628

R M O LAND CO LLC 550 PATTERSON RD GRAND JUNCTION, CO 81506

City of Grand Junction Community Development Dept. 250 N 5th St. Grand Junction, CO 81501

2945-024-00-015 2945-024-00-019 . 2945**-**024-00-022 DEBORAH L SHOWALTER JOHN D HYRE **RUTH C EDFAST** V 604 26 1/2 RD 606 26 1/2 RD 2674 PATTERSON RD GRAND JUNCTION, CO 81506-1905 GRAND JUNCTION, CO 81506-8839 GRAND JUNCTION, CO 81506-1905 2945-024-00-023 2945-024-00-037 2945-024-00-043 GENE O TAYLOR **NICK H MAHLERES** KENNETH H ALLEN ANNIE L MUHR HELEN C MAHLERES ISABELLE E 633 FLETCHER LN 612 26 1/2 RD **603 VIEWPOINT DR** GRAND JUNCTION, CO 81505-1403 GRAND JUNCTION, CO 81506-1905 GRAND JUNCTION, CO 81506-8222 2945-024-00-044 2945-024-00-045 2945-024-00-053 KENNETH H ALLEN ROBERT ALSTATT GEORGE A DUNHAM ISABEL E 2670 PATTERSON RD LYN DUNHAM 603 VIEWPOINT DR GRAND JUNCTION, CO 81506-8839 126 KYLE LN GRAND JUNCTION, CO 81506-8222 BECKLEY, WV 25801-9562 2945-024-00-010 2945-024-00-054 2945-024-00-011 EUGENE L HANSEN JAMES R DANBURY WILLIAM G BUSH VIRGINIA M AMELIA J COLLEEN M 610 26 1/2 RD 620 VIEWPOINT DR 619 VIEWPOINT DR GRAND JUNCTION, CO 81506-1905 GRAND JUNCTION, CO 81506-8204 GRAND JUNCTION, CO 81506-8222 2945-024-03-003 2945-024-03-001 2945-024-03-002 STANLEY D CARLSON ROBERT C BISHOP JOHN I SCHUMACHER NS CYNTHIA K KL606 VIEWPOINT DR 612 VIEWPOINT DR 608 VIEWPOINT DR GRAND JUNCTION, CO 81506-8223 GRAND JUNCTION, CO 81506-8223 GRAND JUNCTION, CO 81506-8223 2945-024-05-001 2945-024-05-002 2945-024-05-003 JAMES R DANBURY ALLEN J MUNRO STEPHEN R MEACHAM AMELIA J MARY B 2525 N 8TH ST 620 VIEWPOINT DR 617 VIEWPOINT DR GRAND JUNCTION, CO 81501-8845 GRAND JUNCTION, CO 81506-8222 GRAND JUNCTION, CO 81506-8204 2945-024-05-005 2945-024-05-004 2945-024-05-006 RAYMOND C BECKNER MAURICE BRASETTE WILLIAM G BUSH **609 VIEWPOINT DR** CC WILMA R GRAND JUNCTION, CO 81506-8222 619 VIEWPOINT DR 611 VIEWPOINT DR GRAND JUNCTION, CO 81506-8222 GRAND JUNCTION, CO 81506-8222 2945-024-10-009 2945-024-10-011 2945-024-10-010 ABBIE KAY MARSHNER IBX, INC RICHARD C POND 640 S 12TH ST PATRICIA M 299 BOOKCLIFF CT **GRAND JUNCTION, CO 81501** GRAND JUNCTION, CO 81501-3750 2714 8TH CT GRAND JUNCTION, CO 81506-8202 2945-024-10-002 2945-024-10-003 2945-024-10-001 STEVEN R RUTTER ROBERT A LUBINSKI OLGA J HENRY TERRILL A **GRETCHEN L DAVIS** JOHN N HENRY 2705 8TH CT 2709 8TH CT 2711 8TH CT GRAND JUNCTION, CO 81506-8203 GRAND JUNCTION, CO 81506-8203 GRAND JUNCTION, CO 81506-8203 2945-024-10-004 2945-024-10-005 2945-024-10-006 ROGER C HEAD MARY A ROBINSON WILLIAM R LATHAM 2713 8TH CT 2715 8TH CT FAYE G & KAY BARRY LATHAM

GRAND JUNCTION, CO 81506-8203

2717 8TH CT

GRAND JUNCTION, CO 81506-8203

GRAND JUNCTION, CO 81506-8203

GENERAL PROJECT REPORT

HORIZON VILLAGE SUBDIVISION

June 27, 1996 Revised July 25, 1996

INTRODUCTION:

The accompanying narrative and maps will provide sufficient data to assess the merits of the requested Preliminary Application for a Major Subdivision. Information gained as the result of the review process will be utilized in the preparation of the Final Plans.

PROJECT DESCRIPTION:

Horizon Village Subdivision is located on the southeast corner at the intersection of Horizon Drive and North 7th Street. The subject property contains approximately 9.2 acres. The Tax Parcel Number is 2945-024-00-048.

The proposed Horizon Village Subdivision calls for the ultimate development of 17 Four-plex Multi-family buildings, creating 68 units. This will yield a density of 7.39 units per acre for the development. The accompanying preliminary plan depicts the relationship of each building to the property boundary, roadway access, waterways and neighboring developments.

The following Preliminary Land Use chart breaks down the entire subject property into specific uses under developed conditions:

PRELIMINARY LAND USE SUMMARY CHART					
USE	AREA IN ACRES	% OF TOTAL			
Four-plex Units	2.1	22.8			
Street R.O.W.	0.8	8.7			
Open Space	1.8	19.6			
Driveways	0.9	9.8			
Common Area	3.6	39.1			
Total	9.2	100			
Resulting Density = 7.39 units per acre					
Total Number of units = 68 units					

EXISTING LAND USE:

The site is currently vacant of any structures and is being used for the production of hay. The City of Grand Junction has a 15 inch sanitary sewer line which crosses through the property from the southeast corner of the site, towards the west to North 7th Street. There are numerous mature trees located on the property. The topography of the site is considered to be "rolling" in nature, and historically drains to the northwest into the Independent Ranchmen's Ditch which ultimately conveys water to the Colorado River.

PUBLIC BENEFIT:

The proposed Horizon Village Subdivision will provide the residents of the area with a quality land development product which will be designed, constructed and maintained in accordance with the City of Grand Junction standards. This project does coincide with the City of Grand Junction overall plan for development. Horizon Village Subdivision will enhance the area and provide a multi-family subdivision which is compatible with the surrounding land use.

PROJECT COMPLIANCE, COMPATIBILITY AND IMPACT:

Zoning -- Currently the land is located within the City of Grand Junction and is zoned PR-6.2 (Planned Residential not to exceed 6.2 units per acre). The Overall Development Plan with the application was submitted to Community Development last year and was approved by City Council on October 4, 1995. The development has been revised to show a reduction of multi-family units from 72 to 68 and the elimination of the single-family lots. These revisions show that Horizon Village Subdivision is proposing a overall density of 7.39, which is a change in the density from the ODP approved. A Mesa County Zoning map is located at the end of this report for surrounding land use comparisons.

Surrounding Land Use — The surrounding land use consists of a number of subdivisions. This includes single-family developments Walker Heights, View Point, Northern Hills and North Acres subdivisions. Westwood Estates Condominiums and a church are also located near the proposed subdivision.

Site Access and Traffic Patterns -- Primary access will be gained from North 7th Street, as shown on the a reduction of the Preliminary Plan located at the end of this report. Major intersections in the area are 7th and Horizon to the north and 7th and Patterson to the south. Assuming an average trip generation rate of 10 trips per household per day, an average of 680 trips from the 68 units would be created and routed through the primary access point. There is no secondary access proposed for the subdivision. This is due to the constraints

from the Grand Valley Canal and the Independent Ranchmen's Ditch bordering the property on the east and north sides of the site respectively.

It is proposed to install a guard house at the entry of the development. There will not be a gate installed at this guard house, nor will their need to be a turn-around area for vehicles entering the development by mistake. This in effect would require the need to propose private roads, and send the final approval for the private roads to City Council. The right-of-way for the streets will be designated as an ingress/egress easement for the maintenance of City Sanitary Sewer and Domestic Water, as well as other dry utilities. This will be reflected on the Final Plat which will be submitted during the next phase of the review process.

The cul-de-sac at the end of the street improvements is proposed as a nonstandard design. The cul-de-sac has a larger radius and an island in the center which will be used for landscaping. This design has been approved by Community Development, City Engineering and the City Fire Department for a different development in the area.

Utilities -- With major streets near to the project, all major utilities are located near the subject property.

Sanitary Sewer -- There is a 15 inch clay sanitary sewer line which crosses through the property. This line will be abandoned and reconstructed through the property with a 20 foot easement for maintenance purposes where the line is outside street right-of-way. The new line will be 15 inch RCP and will connect to the existing 15 inch line located in North 7th Street.

Domestic Water -- Water is available from the City of Grand Junction, which owns and maintains an 8 inch line located on the west side of North 7th street.

All other utilities such as, electric, gas, phone and CATV are expected to be extended from the surrounding developments.

Effects on Public Facilities -- No unusual effects are expected on public facilities such as fire, police, sanitation, roads, parks, schools, irrigation or other facilities.

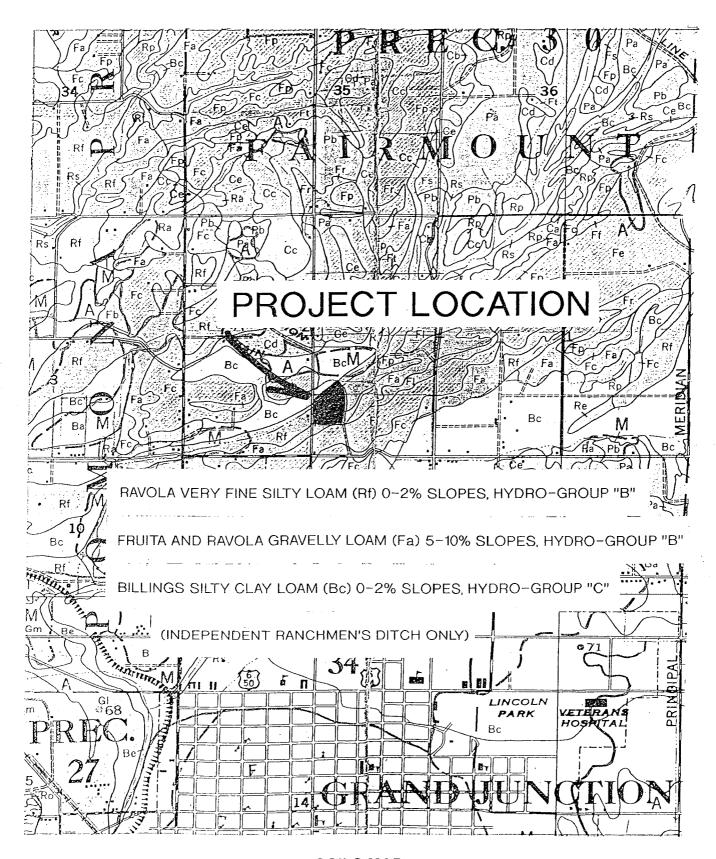
Site Soils and Geology -- A soils map is provided at the end of this report, and shows the types of soil historically found on the property. According to the U.S. Department of Agriculture Soil Survey of 1955, there are a combination of three types of soils on the site. Fruita and Ravola gravelly loams, 5 to 10 percent slopes (Fa), Billings silty clay loam, 0 to 2 percent slopes (Bc) and Ravola very fine sandy loam, 0 to 2 percent slopes (Rf). Each of these soils are common to

the Grand Junction area and are not expected to present any problems. See the attached soils map at the end of this report.

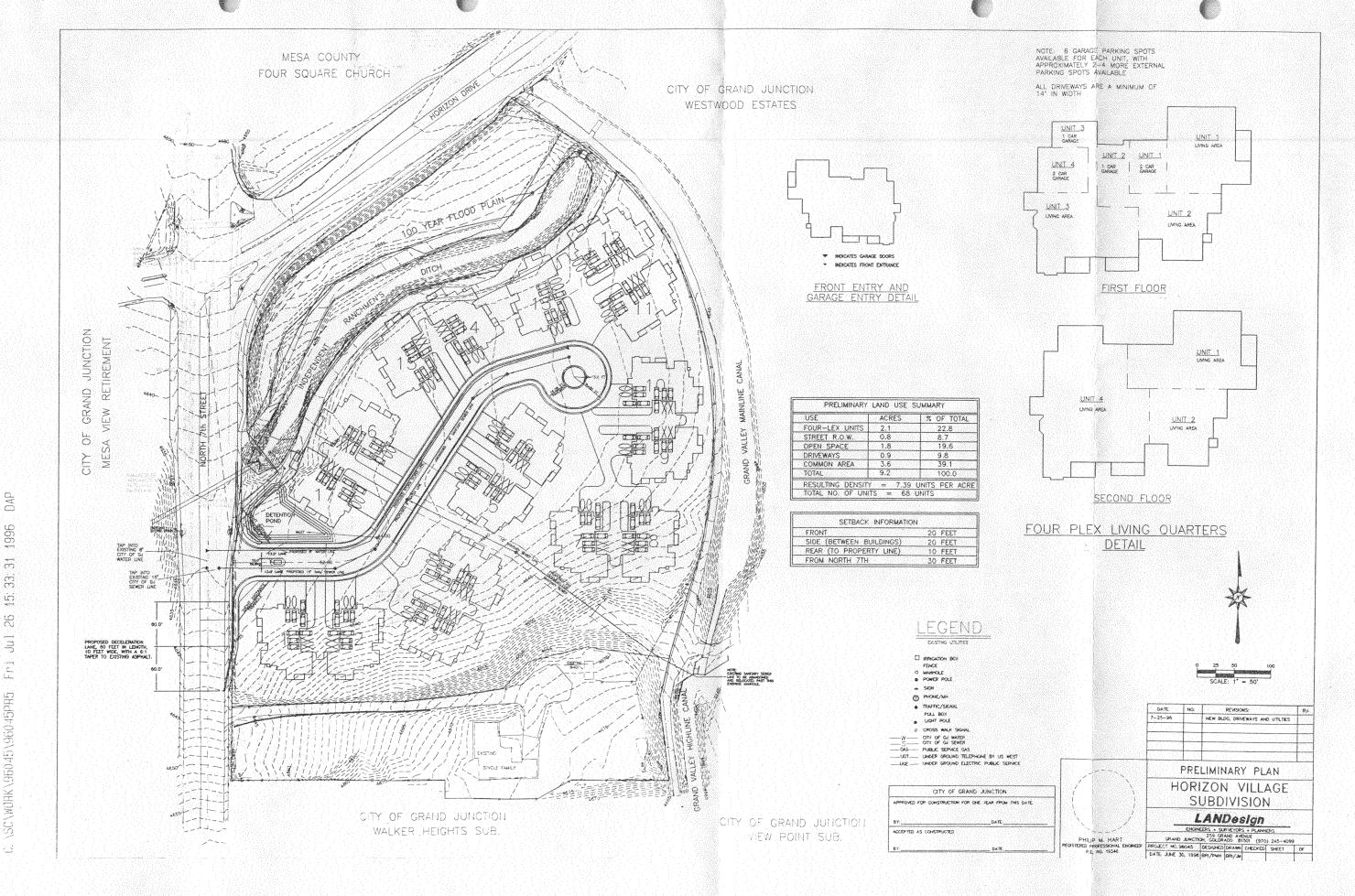
Signage Plans -- A signage plan will be provided to the City of Grand Junction during the final and construction phases of the review process.

DEVELOPMENT SCHEDULE AND PHASING:

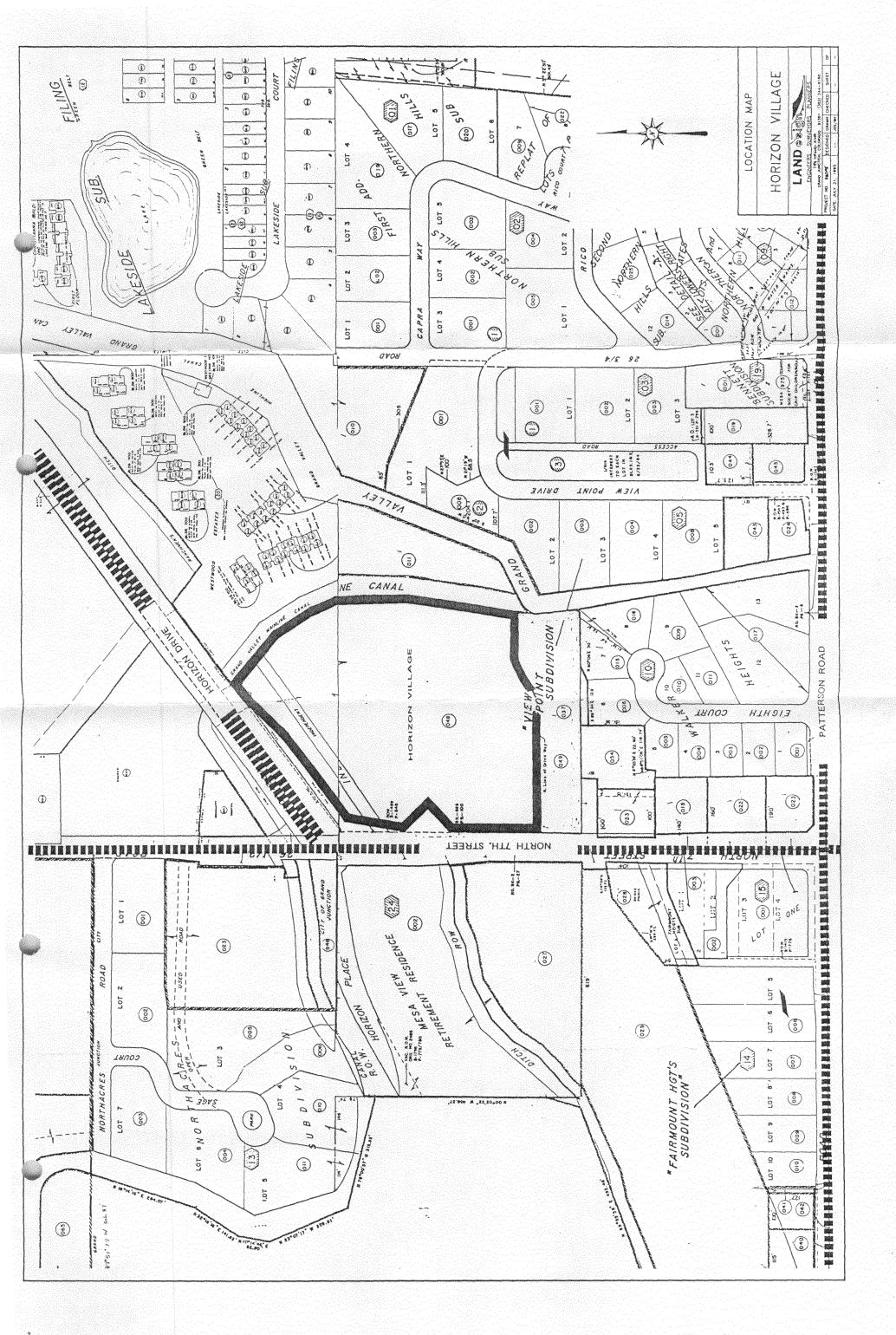
The rate at which the development of Horizon Village will occur is dependent upon the City of Grand Junction's future growth and housing needs. It is anticipated that site development will begin once the final approval from the City has been granted. A phasing plan will be submitted during the next step in the review and application process.



SOILS MAP



1996 \overline{c} 33 ij 98 = SC\WORK\96045\96045PH5







THE BEST SELLERS PORTFOLIO



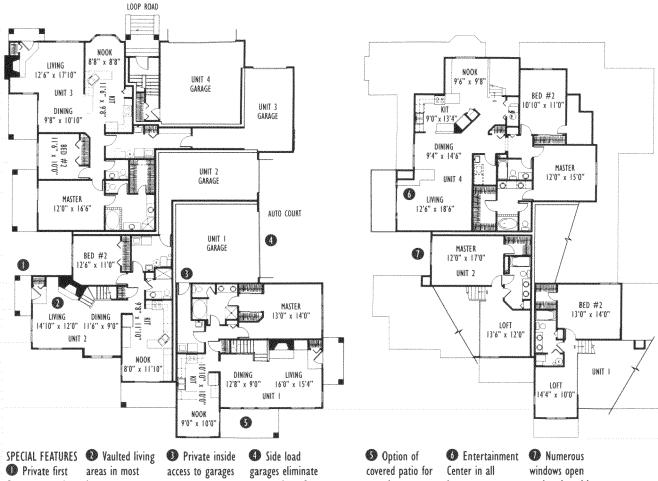
odel #91052-Four. The appeal of this manor-style, multi-family residence is its ability to blend comfortably with large, single-family designs. The unique identity of each home makes it attractive to "empty-nesters" and those seeking an active lifestyle with low home maintenance. Introduced in Chicago area in December 1992 Sales averaged 5/month for the first 12 months Entries on different sides enhance the sense of privacy and separation Manor home design maintains private home appearance and continuity in planned communities Four models provide style and price selection; 1337 sq. ft.

NOTES ON THE PROJECT

As an alternative to townhomes, the manor home fulfills the growing market desire for independent living and ownership combined with the cost efficiencies of multi-family construction.

This design creates the street appeal of a large, attractively landscaped home, free of the repetitive driveways, garages and entryways found in many multi-family designs.

The manor home is evolving as its popularity grows. New developments in Cleveland and Denver are further refining the proven appeal of this concept.



floor entry and porch for each home

homes

garage doors from street view

most homes

homes

up interior with abundant natural light

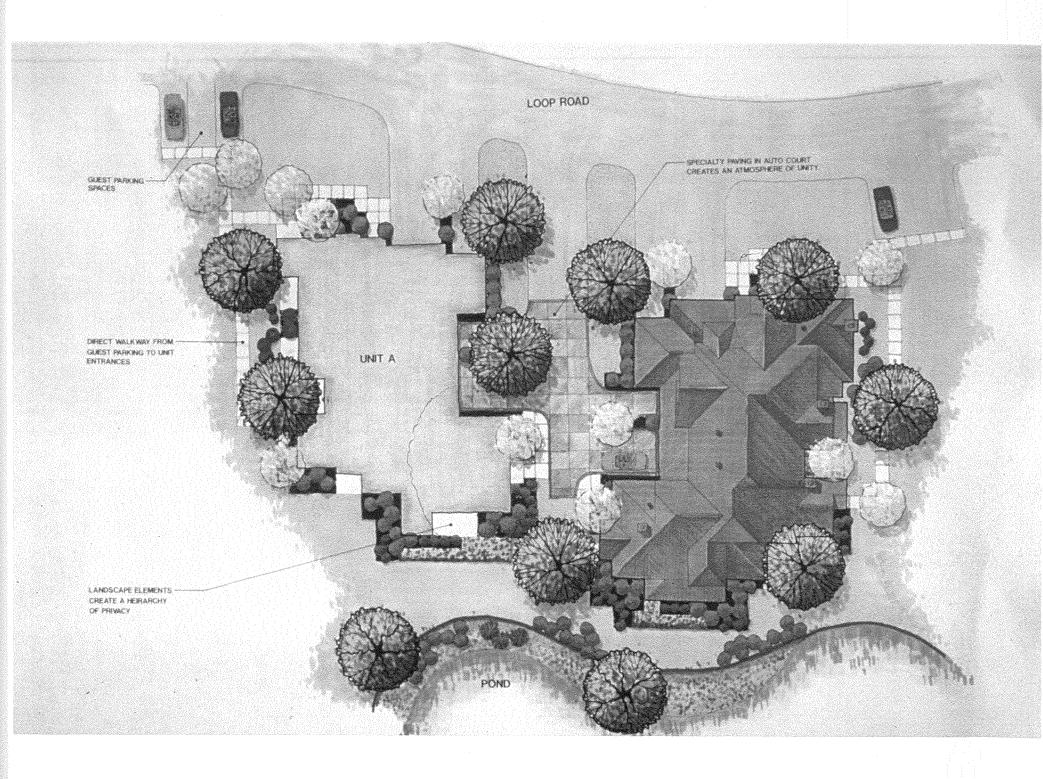


For 20 years, Kephart has been designing attractive, cost-effective homes with superior sales records. You'll find our designs in Denver, Cleveland, Palm Beach, Charlotte, Chicago, Phoenix and other locations around the country.

This model is just one example from a portfolio of best-selling homes. You'll be seeing several more this year. If you just can't wait, or would like to know more about our services, contact Mike Kephart at (303) 832-4474.



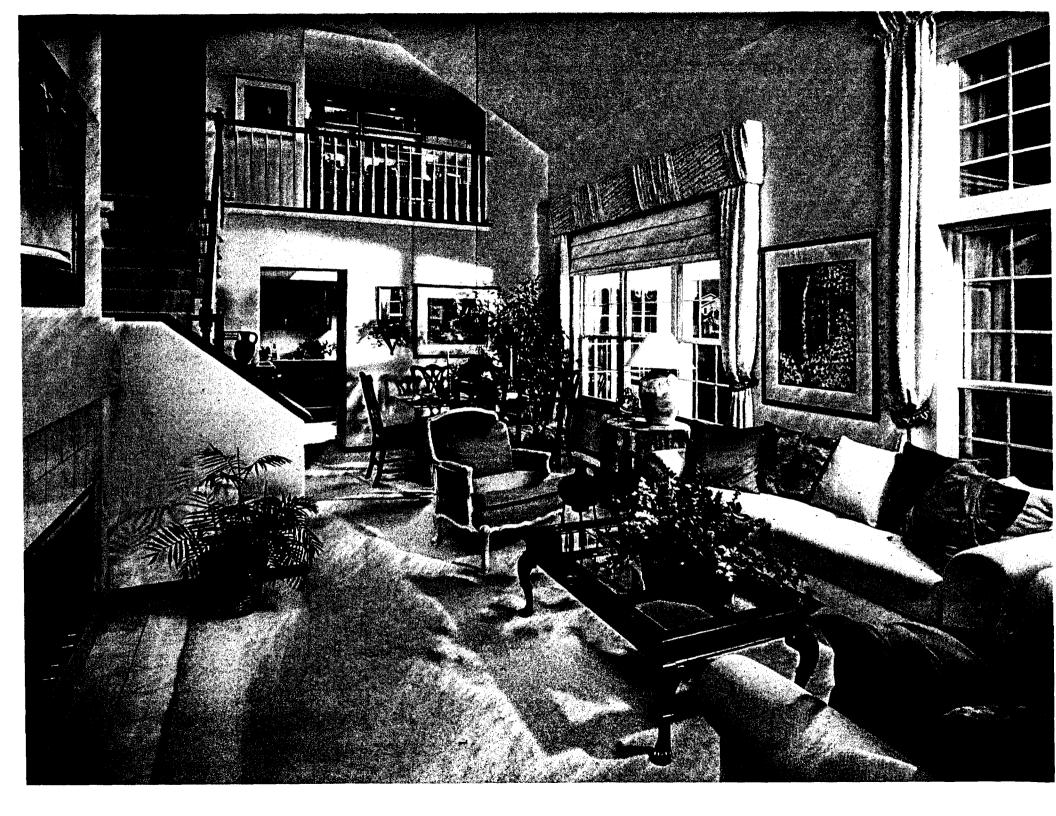






















PRELIMINARY DRAINAGE REPORT

FOR

HORIZON VILLAGE SUBDIVISION

Prepared for:

Cunningham Investment Co., Inc. c/o Mac Cunningham 121 S. Galena Street, Suite 201 (970) 925-8803

Prepared by:

LANDesign, LLC
PLANNING ENGINEERING SURVEYING
259 Grand Avenue
Grand Junction, CO 81501
(970) 245-4099

June 27, 1996

Job No. 96045

Prepared by:		•
Br	ian C. Hart, E.I.	
	that this report for the preliminary drains pared under my direct supervision."	age design of Sunset
Reviewed by:		
Ph	nilip M. Hart, P.E.	· <u>·······</u>
Sta	ate of Colorado, #19346	
	6	

Section 2

I. GENERAL LOCATION AND DESCRIPTION

A. Site and Major Basin Location

Horizon Village Subdivision is located at the southeast corner of the intersection at North 7th Street and Horizon Drive. The property tax parcel number is 2945-024-00-048. The property can otherwise be described as; a part of the N1/2 SW1/4 SE1/4 and that part of the S1/2 NW1/4 SE1/4 lying South and West of the main line canal of The Grand Valley Irrigation Company in Section 2, Township 1 South, Range 1 West of the Ute Meridian. The property tax parcel number is 2945-031-00-124.

Developments in the area near Horizon Village include, View Point Subdivision, Walker Heights Subdivision and Westwood Estates Condominiums.

B. Site and Major Basin Description

The subject property contains approximately 9.2 acres. The topography of the property can be described as "rolling" in nature and historically slopes to the northwest at an average rate of 8.0 percent.

The Independent Ranchmen's Ditch runs through the property from the northeast corner of the property to the northwest corner of the property. This ditch conveys a small amount of water year-round, but the majority of water is from irrigation water supplied by the Grand Valley Mainline Canal which runs during the irrigation season. The Grand Valley Mainline Canal defines the east boundary of the site.

Ground Cover can be described as tall grass and three small groves of trees. For the purposes of obtaining Rational "C" values, the land and ground cover can be described as a "pasture".

As shown in the appendix of this report (Reference 3.0, Exhibit 6.0), there are three soils types located on the site. Billings silty clay loam (Hydro-group "C") is located in the area of the ditch, which will not be developed, therefore this soil type will not be considered in any calculations for historic or developed conditions. The portion of the site which will be used for development contains both Ravola very fine loam (Rf) 0-2% slopes and Fruita and Ravola gravelly loams (Fr) 5-10% slopes. Both of these soils types are described as Hydro-group "C".

II. EXISTING DRAINAGE CONDITIONS

A. Major Basin

There are two major waterways which border or run through the property. The Grand Valley Mainline Canal defines the east boundary of the site, and flow from the southeast corner of the property to the northeast corner of the property. From this point the canal crosses Horizon Drive and continues to the east. The Independent Ranchmen's Ditch runs through the northern part of the site, flowing from the east to the west. From the northwest corner of the site, the ditch flows under North 7th Street and continues to the west. The Independent Ranchmen's Ditch is the only waterway which will be affected by the drainage from the site.

The area of the project to be disturbed with development is defined as being in Zone X and is not within the 100 year flood plain as shown on the, "Flood Insurance Rate Map, Mesa County Colorado" (Reference 4.0, Exhibit 5.0). It is shown on this map that the 100 year event is conveyed by the Independent Ranchmen's Ditch. This creates an area which is designated as "AE" which establishes a base flood elevation. This area is delineated in the appendix shown with the developed conditions of the site (Exhibit 4.0)

B. Project Site

Historically the property drains in a sheetflow fashion from the southeast to the northwest at an average of 8.0 percent, eventually discharging into the Independent Ranchmen's Ditch.

The property is bounded to the north by Horizon Drive and to the west by North 7th Street. The Grand Valley Mainline Canal and the accompanying maintenance road define the east boundary of the site. The south boundary of the property is defined by the north line of the driveway used for access by the parcel directly to the south. The inflow characteristics of offsite runoff are sheetflow in fashion, entering the property from the southeast.

The areas north, west and east of the property drain away from the site and will not contribute runoff to the site. The parcel to the south will contribute a small amount of runoff from the east portion of it's boundary. The historic basin for the site is shown on Exhibit 3.0 in the appendix.

III. PROPOSED DRAINAGE CONDITIONS

A. Changes in Drainage Patterns

Based on the proposed land use plan, significant changes in the existing drainage patterns are not anticipated, either to the site or the major basin.

B. Maintenance Issues

It is expected that the storm drainage such as inlets, piping and the roadway systems will be privately owned and maintained. The detention pond and outlet works will be owned and maintained by an established homeowners association for the development.

IV. DESIGN CRITERIA AND APPROACH

A. General Considerations

There has been a drainage study performed for area near the subject property by the Federal Emergency Management Agency, Reference 4.0. This study was revised July 15, 1992, and it's purpose was to establish the Flood Insurance Rate Maps for Mesa County, Colorado shown on Exhibit 5.0.

Because of the location of the proposed project, there is no other development expected which would be effected or contribute to the drainage at Horizon Village, either historic or developed.

Their are no apparent constraints imposed by the proposed site which would effect the historic or developed drainage patterns.

B. Hydrology

The "Stormwater Management Manual, City of Grand Junction, Colorado" (Reference 1) will be used and followed for the Final Drainage Report. As the project is a residential development encompassing approximately 9.2 acres, the "Rational Method" will be used for the final drainage report. The minor storm event is described as the 2 year storm and the major storm event is described as the 100 year event. It is expected that detention will be required for the 100 year storage value.

Runoff coefficients to be used in calculations are based on the most recent City of Grand Junction criteria as defined in Reference 1.0 and shown on Exhibit 7.0. With the historic ground cover described as "pasture", the 8.0% average slope and the Hydro-group for the on-site soils being "B", an average historic Rational

"C" values for the project are 0.41 for the 2 year event, and 0.49 for the 100 year event.

As the project is located within the Grand Junction Urbanized area, the Intensity Duration Frequency (IDF) Table as provided in Reference 1.0 shown on Exhibit 8.0 will be used for design and analysis.

Times of Concentration are calculated based on the Average Velocities For Overland Flow and Overland Flow Curves as provided in Reference 1 and shown on Exhibits 9.0 and 10.0.

C. Hydraulics

All site facilities and conveyance elements will be designed in accordance with the City of Grand Junction guidelines as provided in Reference 1.0.

VI. CONCLUSION

A Preliminary Plan has been included in this report to represent what this proposed development will entail, Exhibit 1.0. Exhibit 2.0 shows the Grand Junction Urbanized area obtained from Reference 2.0, and shows the relationship of the proposed development to the City of Grand Junction.

Upon Preliminary approval from the City of Grand Junction Planning Commission and the City of Grand Junction City Council, a final drainage report will be submitted during the next review phase. This report will address site specific drainage concerns in accordance with the requirements of the City of Grand Junction, Colorado.

VII. REFERENCES

- 1. <u>Stormwater Management Manual (SWMM)</u>, City of Grand Junction, Colorado, Department of Public Works, June 1994.
- 2. <u>Mesa County Storm Drainage Criteria Manual, Final Draft, Mesa County Colorado, March 1992.</u>
- 3. <u>Soil Survey. Mesa County Area, Colorado</u>, U.S. Department of Agriculture, issued November, 1955.
- 4. Flood Insurance Rate Map, Mesa County, Colorado, (Unincorporated Areas), Community Panel Number 080115 0004 E, Federal Emergency Management Agency, Map revised July 15, 1992.

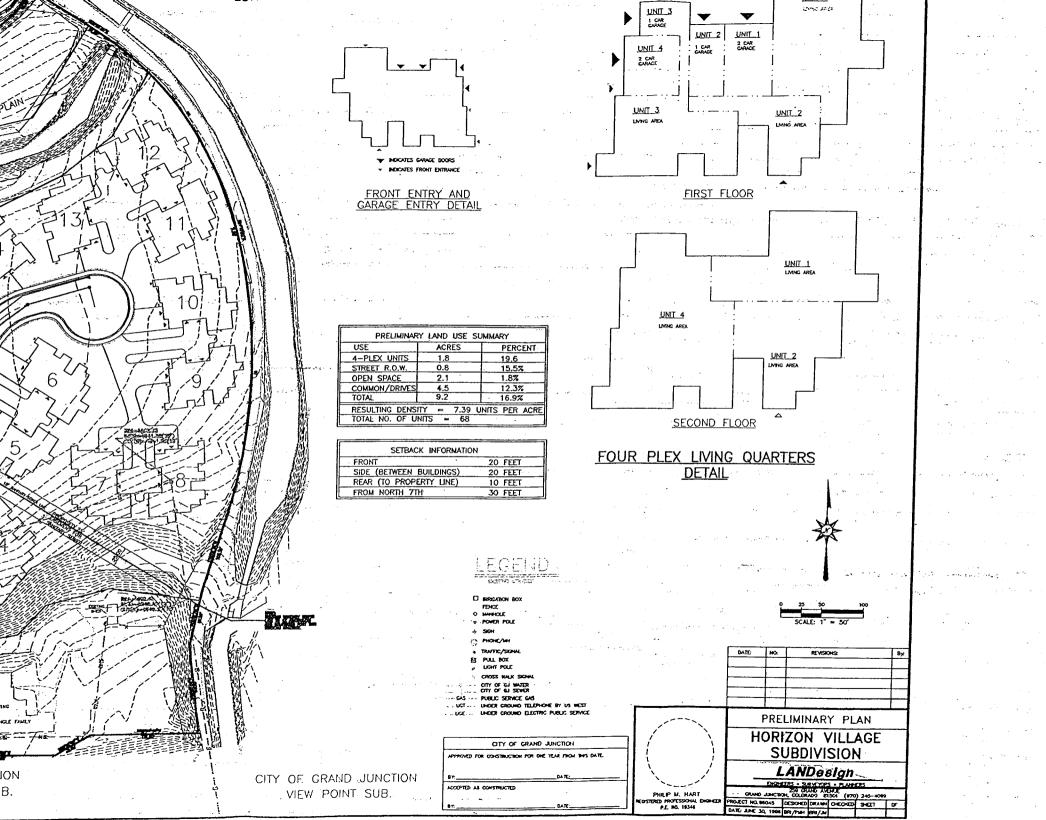
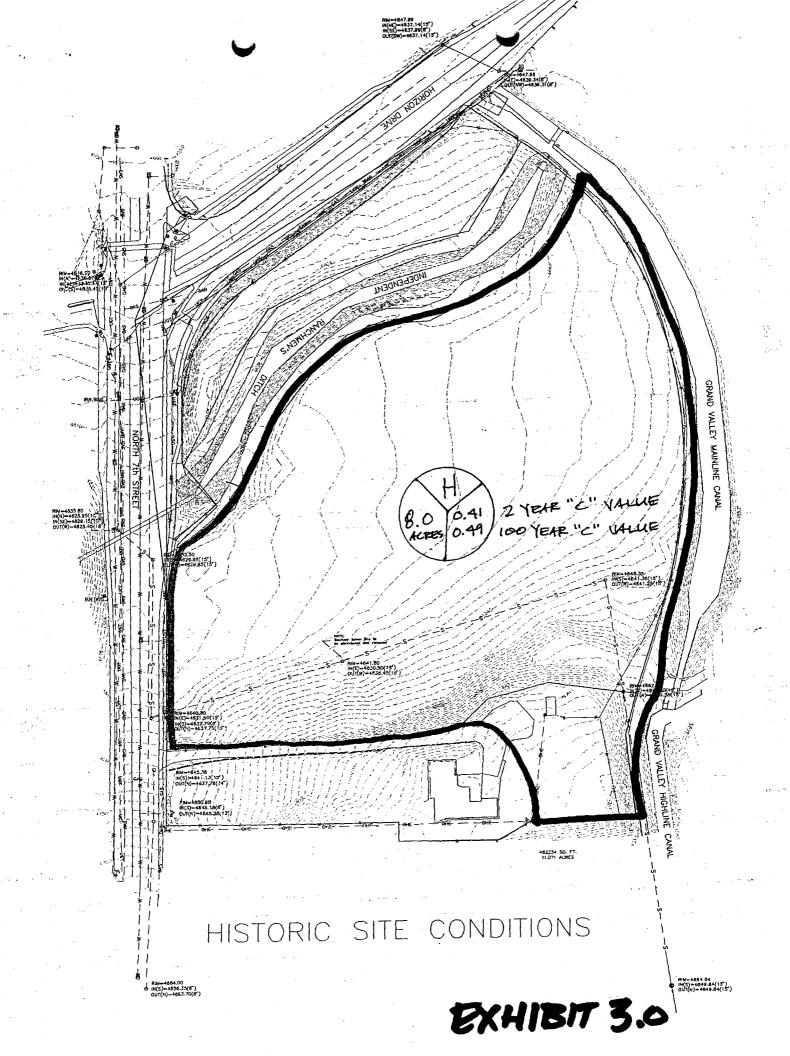


FIG 404



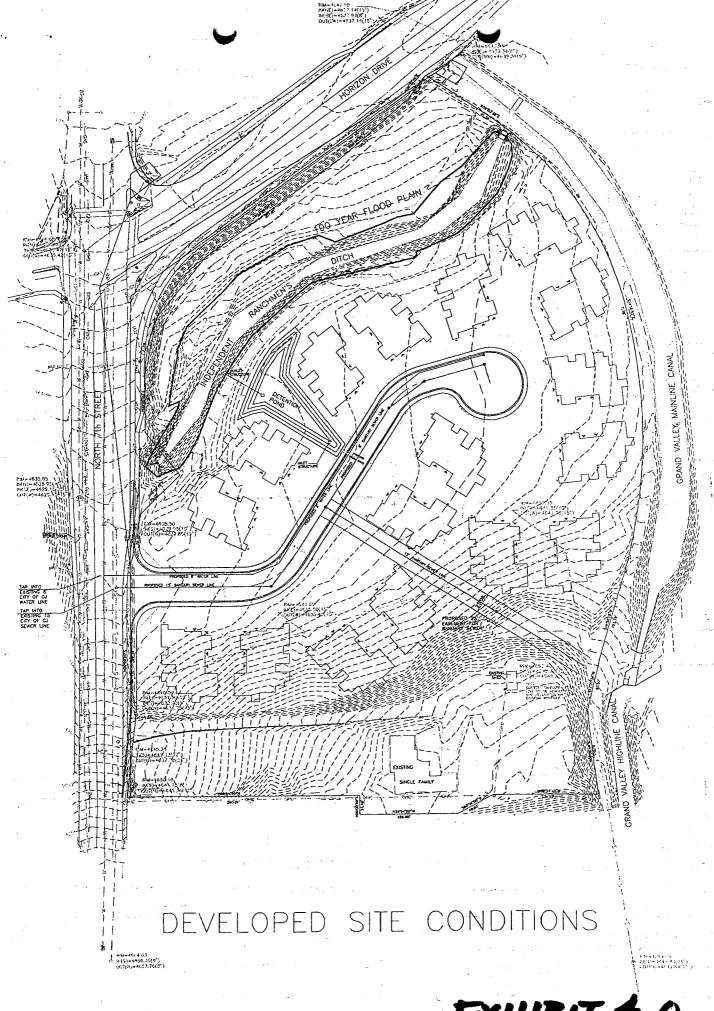
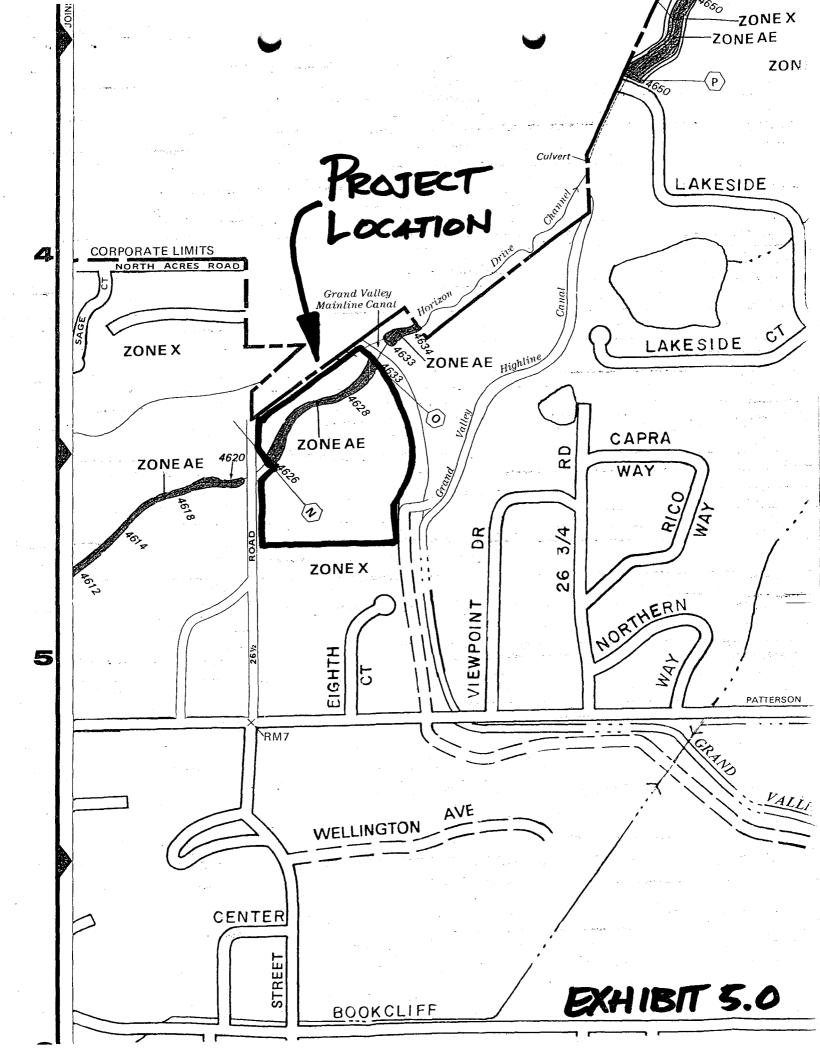
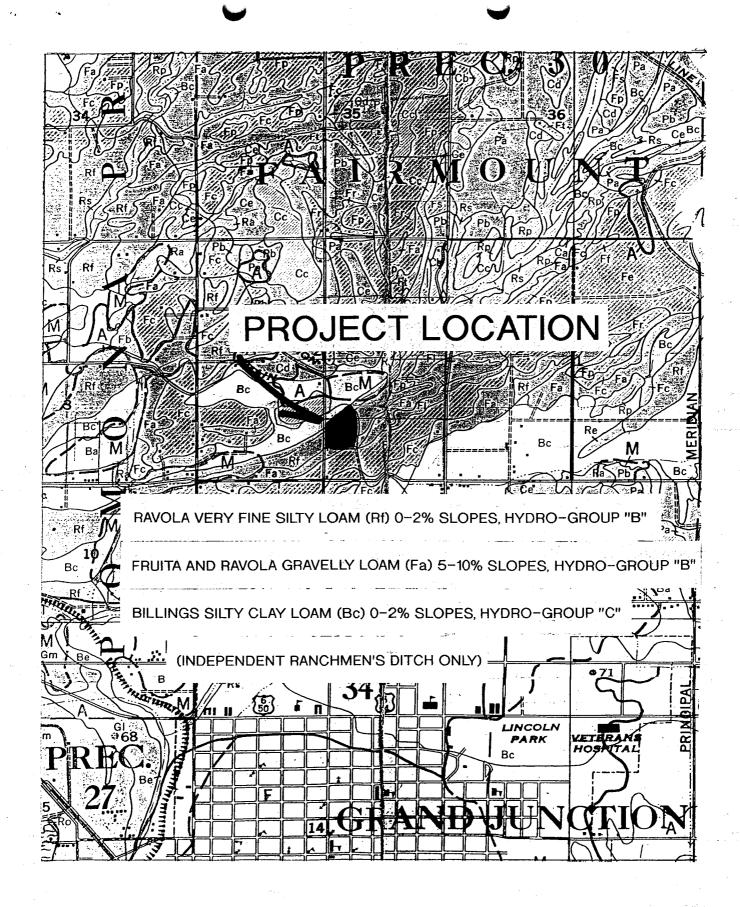


EXHIBIT 4.0





LAND USE OR		SCS	HYDROL	CS HYDROLOGIC SOIL GROUP	IL GRO	(SEE	APPENDIX "C" FOR	IX "C" F	OR DESC	DESCRIPTIONS	NS)	
SURFACE CHARACTERISTICS .		≺			Ω			O			۵	
	0.2%	2-6%	+%9	0-2%	2-6%	+%9	0-2%	2-6%	6% +	0-2%	2-6%	+%9
UNDEVELOPED AREAS Bare ground	10 - 20 14 - 24	.1626	.2535	14- 22 20-28	22 - 30 28 - 36	.3038	.20 - 28 .26 - 34	.2836 .3543	.3644	24-32	.3038	.4048
Cultivated/Agricultural	08 - 18	.13 - 23	.16 - 26	.1119 .1624	.15 - 23	* * 3	14.22 20-28		26 - 34	18-26 24-32	23 - 31	
Pasture	12:22	20-30	3040	18.26		.3745		1 1		30.38	.4048	
Meadow	10:20	16 - 26	25-35	14.22	8 9 1	30 - 38			36 - 44	* *	30 - 38	
Forest	.05 - 15	.0818		.08 - 16 .10 - 18		.1422		.1321	.2028		.1624	
RESIDENTIAL AREAS	40 - 50	43 - 53	.4656	42 - 50	.45 - 53	.5058	454.53	.4856	.5361	48.56	.5159 .6068	.5765 .6977
1/4 acre per unit	27 - 37 38 - 45	3141	3444	29 - 37		38 - 46	32 - 40	36 - 44 .4553	.5260	35 - 43	3947 .4755	.4553
1/3 acre per unit	22-33	26 - 36 35 - 45				.3341			.4856	31 - 39		
1/2 acre per unit	.16 - 26 .25 - 35	20 - 30	.2434	19.27	.2331 .3240	* * *		.3543		26-34	30 - 38	
1 acre per unit	14 - 24 22 - 32	.1929		T 4						31 - 39	3543	
MISC. SURFACES Pavement and roofs	.93 .95	8,8;	.95 79.	93	.94 .96	89. 79.	93	96. 96.	.95 797	88	28.	29. 79.
Traffic areas (soil and gravel)	.5565 6570	.70 .70	.7479 .7479	.6068 .76	.6472	.6775 .7583	24 - 72 25 - 52	.75 - 75 .75 - 83	.6977 .		.7583	.8492
Green landscaping (lawns, parks)	10.14	16-26	30 - 40	14 - 22 20 - 28	.2836	30 - 38	20 - 28	28 - 36	3644	24 - 32 30 - 38	86.38 .48	.4048
Non-green and gravel landscaping	344 044.		.5055	\$5. \$050		.5058	40 - 48	.4856	.5664	44.00	.5058	.6068
Cemeteries, playgrounds	20:30			35 - 45	3240	.4048	30 - 38	3844	.4654	34-42	.4048	.5058
NOTES: 1. Values above and below pertain to	and below pe	rtain to the 2	the 2-year and 100-year	year and 100-year storms, respectively.	s, respectivel							•

Values above and below pertain to the 2-year and 100-year storms, respectively.

The range of values provided allows for engineering judgement of site conditions such as basic shape, homogeneity of surface type, surface depression storage, and storm duration. In general, during shorter duration storms (Tc > 10 minutes), infiltration capacity is higher, allowing use of a "C" value in the low range. Conversely, for longer duration storms (Tc > 30 minutes, use a ""C value in the higher range.

For nonger duration storms (Ta > 30 minutes) use a ""C value in the higher range.

For residential development at less than 1% acre per unit or greater than 1 acre per unit, and also for commercial and industrial areas, use values under MISC SURFACES to estimate "C" value ranges for use.

TABLE "B-1"

RATIONAL METHOD RUNOFF COEFFICIENTS
(Modified from Table 4, UC-Davis, which appears to be a modification of work done by Rawls)

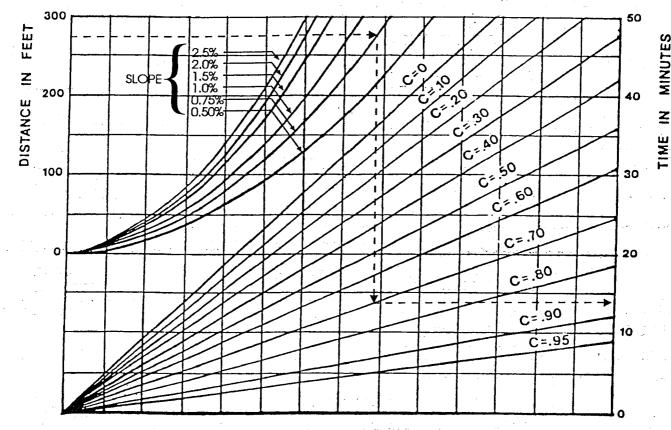
B-3

	A Commence of the Commence of		FREQUENCY		
Time (min)	2-Year Intensity (in/hr)	100-Year Intensity (in/hr)	Time (min)	2-Year Intensity (in/hr)	100-Year Intensity (in/hr)
5	1.95	4.95	33	0.83	2.15
- 6	1.83	4.65	34	0.82	2.12
7	1.74	4.40	35	0.81	2.09
8	1.66	4.19	36"	0.80	2.06
9	1.59	3.99	37	0.79	2.03
10	1.52	3.80	38	0.78	2.00
11	1.46	3,66	39	0.77	1.97
12	1.41	3.54	40	0.76	1.94
13	1.36	3.43	41	0.75	1.91
14	1,32	3.33	42	- 0.74	1.88
15	1.28	3.24	43	- 0.73	1.85
16	1.24	3.15	44	0.72	1.82
17	1.21	3.07	45	0.71	1.79
18	1.17	2.99	46	0.70	1.76
19	1.14	2.91	47	0.69	1.73
20	1.11	2.84	48	0.68	1.70
21	1.08	2.77	49	0.67	1.67
22	1.05	2.70	50	0.66	1.64
23	1.02	2.63	51	0.65	1.61
24	1.00	2.57	52	0.64	1.59
25	0.98	2.51	53	0.63	1.57
26	0.96	2.46	54	0.62	1:55
27	0.94	2.41	55	0.61	1.53
28	0.92	2.36	56	0.60	1.51
29	0.90	2.31	57	0.59	1.49
30	0.88	2.27	58	0.58	1.47
31	0.86	2.23	59	0.57	1.45
32	0.84	⁻ 2.19	60	0.56	1.43

JUNE 1994

EXHIBIT 8.0

MODIFIED FROM FIGURE 403, MESA COUNTY



THE ABOVE CURVES ARE A SOLUTION OF THE FOLLOWING EQUATION:

To =
$$\frac{1.8 (1.1 - C)\sqrt{L}}{\sqrt[3]{5}}$$

WHERE: To = OVERLAND FLOW TIME (MIN.)

S = SLOPE OF BASIN (%) C = RUNOFF COEFFICIENT (SEE TABLE "B-1" IN APPENDIX "B")

L = LENGTH OF BASIN (ft)

Exhibit 9.0

GRAPHICAL DETERMINATION OF "To:" FAA METHOD

FIGURE "E-2"

REPRODUCED FROM FIGURE 15.2, SCS 1972

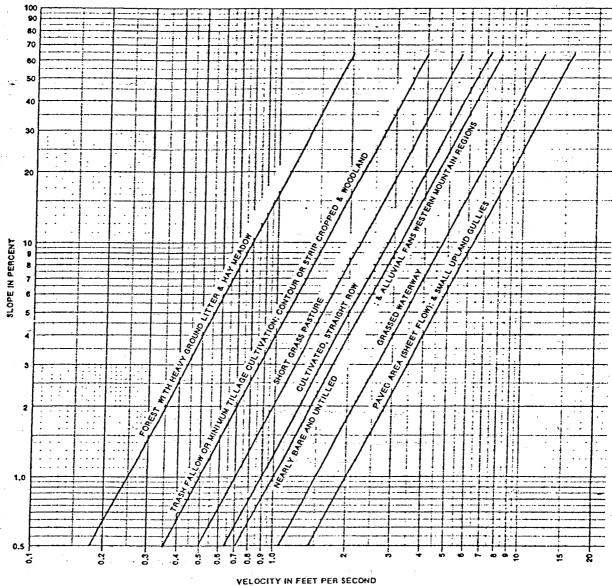


EXHIBIT 10.0

DETERMINATION OF "Ts"

FIGURE "E-3"

JUNE 1994



GPN GEO-CONSULTANTS
631 GLACIER DR.
GRAND JUNCTION, CO 81503
(970) 243-9602

Mr. Brian C. Hart E.I. LANDesign 259 Grand Avenue Grand Junction, CO 81501

RE: Surficial Geology Investigation-Horizon Village Subdivision

June 28, 1996

Dear Mr. Hart,

According to your request, I have completed a ground investigation of the above mentioned site to determine the general geologic condition and identify any geologic hazards. A site evaluation was conducted on June 25, 1996.

SITE LOCATION & DESCRIPTION

The site lies in the Southwest Quarter of the Southeast Quarter (SW1/4 SE1/4) of Section 2, Township 1 South, Range 1 West, of the Ute Meridian, Mesa County, Colorado. The site is bounded by the North 7th Street to the west, Walker Heights Subdivision to the south, Horizon Drive to the north, and The Grand Valley Canal to the east. The site contains 11.7 acres.

Topography of the site is predominantly flat (0-2% slope to the west) with steeper slopes (5-10%) to the north on the southern portion of the site. Average elevation is approximately 4630 feet above sea level, using the Grand Junction Quadrangle 7 1/2 minute series topographic map.

GENERAL GEOLOGY

The general geology of the area consists of thick deposits of shales, sands and silts of the Mancos Shale Formation, which gently dip in a northeasterly direction. Weathering of the Mancos is the origin of the soils that overlay the site. These soils are considered metastable and moderately low density.

Seismic events have occurred near, and possibly, in the Grand Valley area. These events occurred with no reported damage and having Richter Magnitudes up to and including 4.4. The Jacob's Ladder Fault Complex is approximately 5.5 miles to the south-southwest, and the Redlands Fault is approximately 6 miles southwest of the site.

SITE GEOLOGY

The bedrock that underlies the site is the Mancos Shale as mentioned above. The Mancos Shale consists of gray marine shales, and a few thin beds of sandstone and limestone. This shale has been known to exhibit swelling characteristics due to bentonitic layers within. The shale is light to medium gray in color.

The soil at the site is the Ravola Very Fine Sandy Loam, (0-2% slope) and is light brownish-gray to very pale-brown. The Ravola ranges from 4 to 20 feet deep and becomes sandier with depth according to the Soil Conservation Service survey. Disseminated lime may occur from the surface downward. The soil is usually slightly saline but may have a few strongly saline spots. This type of soil is commonly metastable and friable in nature and may be sensitive to changes in soil moisture content. The soil at the south portion of the site is the Ravola Gravely Loams (5-10% slope). This soil occurs on benches or mesas north of Grand Junction, and consists of very pale-brown to pale brown loam with a moderate accumulation of lime in the subsoil. The

Surficial Geology Investigation, Horizon Village Subdivision

Mancos Shale may occur at depth of 2 1/2 to 4 1/2 feet, but the alluvial mantle may be 10 to 12 feet thick in some places. This soil may contain sandstone gravel and semirounded stones. This type of soil is commonly metastable and friable in nature and may be sensitive to changes in soil moisture content. Severity of the metastable soils should be determined by Geotechnical Testing.

GROUND WATER

The Mancos shale is impermeable, and a poor source of groundwater. However, fluctuation in free water levels is greatly affected by external environmental conditions such as seepage moisture from irrigation. No free standing surface water was observed, however the Ravola soil occasionally has a high water table. The true water table can be determined through Geotechnical Investigation.

SURFACE WATER

Surface drainage is in a northwesterly direction which flows into the independent Ranchmen's Ditch at the northern portion of the site. The independent Ranchmen's Ditch drains to the southwest with termination at the Colorado River, located approximately 2.5 miles south of the site. The area along the ditch has been mapped by The Federal Emergency Management Agency as an area inundated by 100 year flood. Base flood elevations have been noted on the map and should be observed before any design and construction. The remainder of the site is not within a mapped flood hazard area.

The Main Line Grand Valley Canal is the eastern boundary of the site. The rapid increase of the water level due to storm runoff may cause flooding ,however the area is not mapped as a flood hazard. Water levels in the canal can be controlled.

ECONOMIC GEOLOGIC DEPOSITS

No extractable minerals, ores of deposits are believed to be present on or beneath this site. However, oil and gas fields, gravel deposits, coal deposits, uranium deposits and ornamental stone quarries exist in the surrounding areas. There may exist economic minerals deposits in this area that have not yet been investigated.

GEOLOGIC HAZARDS

Surface soils may exhibit a slight to moderate metastable condition. It is recommended that the severity be determined by Geotechnical Laboratory testing. The hezards of water erosion are high in soils with slopes of 5 percent or higher, moderate with 2-5 percent, and slight with 0-2 percent. The majority of the site is relatively flat, soil and / or slope instability is not expected to be a concern. The higher percentage slopes at the southern part of the site will have increased soil and / or slope instabilities, therefore, the Geotechnical Report should address the instability concern an make recommendations before any excavation work. The area along the Independent Ranchmen's Ditch should be investigated further to determine the area that would be inundated by 100-year flood.

Ground water in the Grand Junction area normally contains sulfates in levels detrimental to a Type I cement. The cement type should be decided by Geotechnical Testing.

It is presumed that all relevant concerns have been addressed in this report. If any further questions arise or if I can be of additional service, please feel free to call.

In conclusion, there are no serious geologic limitations to hinder the approval of the proposed development. Again, engineering investigations should be made to determined surface and subsurface soil and rock characteristics, drainage patterns, location of water table, erosional

Surficial Geology Investigation, Horizon Village Subdivision

hazards and flood hazards prior to development and construction. All statements and conclusions made herein are to my best knowledge of the investigator.

Respectfully submitted,

George P. Nichols, III Geologist

SUBSURFACE SOILS EXPLORATION
HORIZON VILLAGE SUBDIVISION
GRAND JUNCTION, COLORADO

Prepared For:

MAC CUNNINGHAM
C/O LANDesign
GRAND JUNCTION, COLORADO

Prepared By:

LINCOLN-DeVORE, INC. 1441 Motor Street Grand Junction, CO 81505

JUNE 29, 1996



Lincoln DeVore, Inc.
Geotechnical Consultants

1441 Motor St. Grand Junction, CO 81505 TEL: (970) 242-8968 FAX: (970) 242-1561

June 29, 1996

Mac Cunningham C/O LANDesign 259 Grand Ave. Grand Junction, CO

Re:

SUBSURFACE SOILS EXPLORATION

HORIZON VILLAGE SUBDIVISION

GRAND JUNCTION, COLORADO

Dear Sir:

Transmitted herein are the results of a Subsurface Soils Exploration for the proposed construction of attached and possible detached single family and condominium type residential construction within the proposed Horizon Village Subdivision.

If you have any questions after reviewing this report, please feel free to contact this office at any time. This opportunity to provide Geotechnical Engineering services is sincerely appreciated.

30590

Respectfully submitted,

LINCOLN-DeVORE, INC.

y:

Edward M. Morris, PE Western Slope Branch Manager Grand Junction, Office

LDTL Job No. 85529-J

EMM/bl

TABLE OF CONTENTS

	<u>Page</u>	No.
INTRODUCTION		1
Project Description, Scope, Field Exploration & Laboratory Testing.		
FINDINGS		5
Site Description, General Geology and Subsurface Descript: Ground Water	ion,	
CONCLUSIONS AND RECOMMENDATIONS		12
General Discussion, Open Foundation Observation, Excavation, Drainage and Gradient		
FOUNDATIONS		18
Shallow Foundations on Mancos Shale, Shallow Foundations on Compressible Soil Subgrade Improvement, Reinforced Structu Deep Foundations, Drilled Piers, Drilled Pier Observation, Grade Beams, Driven Pile Observation, Driven Piles		11,
CONCRETE SLABS ON GRADE		29
EARTH RETAINING STRUCTURES		32
REACTIVE SOILS		34
PAVEMENTS	And the second	35
Calculated Pavement Sections, Proposed Pavement Sections, Subgrade Improvement, Mechanically Stabilized Fill, Section Construction		
T T V T T A T T O V O		

INTRODUCTION

PROJECT DESCRIPTION

This report presents the results of our geotechnical evaluation performed to determine the general subsurface conditions of the site applicable to construction of attached and possible detached single family and condominium type residential construction within the proposed Horizon Village Subdivision. A vicinity map is included in the Appendix of this report.

To assist in our exploration, we were provided with a concept plan, prepared by LANDesign of Grand Junction. The Boring Location Plan attached to this report is based on that plan provided to us.

We understand that the proposed structures will probably consist of two story with the possibility of single and possibly three story, wood framed structures with the possibility of half basement and concrete floor slabs on grade. Lincoln DeVore has not seen any proposed building plans, but it is anticipated that structures of this type will develop wall loads on the order of 1000-2500 plf and column loads on the order of 8-25 kips.

The characteristics of the subsurface materials encountered were evaluated with regard to the type of construction described above. Recommendations are included herein to match the described construction to the soil characteristics found. The information contained herein may or may not be

valid for other purposes. If the proposed site use is changed or types of construction proposed, other than noted herein, Lincoln DeVore should be contacted to determine if the information in this report can be used for the new construction without further field evaluations.

PROJECT SCOPE

The purpose of our exploration was to evaluate the surface and subsurface soil and geologic conditions of the site and, based on the conditions encountered, to provide recommendations pertaining to the geotechnical aspects of the site development as previously described. The conclusions and recommendations included herein are based on an analysis of the data obtained from our field explorations, laboratory testing program, and on our experience with similar soil and geologic conditions in the area.

Specifically, the intent of this study is to:

- 1. Explore the subsurface conditions to the depth expected to be influenced by the proposed construction.
- 2. Evaluate by laboratory and field tests the general engineering properties of the various strata which could influence the development.
- 3. Define the general geology of the site including likely geologic hazards which could have an effect on site development.
- 4. Develop geotechnical criteria for site grading and earthwork.
- 5. Identify potential construction difficulties and provide recommendations concerning these problems.
- 6. Recommend an appropriate foundation system for the anticipated structure and develop criteria for foundation design.

FIELD EXPLORATION AND LABORATORY TESTING

A field evaluation was performed on 6-10-96 & 6-18-96, and consisted of a site reconnaissance by our geotechnical personnel and the drilling of 6 shallow exploration borings. These 6 exploration borings were drilled within or near the proposed building pads, near the locations indicated on the Boring Location Plan. The exploration borings were located to obtain a reasonably good profile of the subsurface soil conditions. All exploration borings were drilled using a CME 45-B, truck mounted drill rig with continuous flight auger to depths of approximately 10-25 feet. Samples were taken with a standard split spoon sampler, thin walled Shelby tubes, and by bulk methods. Logs describing the subsurface conditions are presented in the attached figures.

The boring logs and related information show subsurface conditions at the date and location of this exploration. Soil conditions may differ at locations other than those of the exploratory borings. If the structure is moved any appreciable distance from the locations of the borings, the soil conditions may not be the same as those reported here. The passage of time may also result in a change in the soil conditions at the boring locations.

The lines defining the change between soil types or rock materials on the attached boring logs and soil profiles are determined by interpolation and therefore are approximations. The transition between soil types may be abrupt or may be gradual.

The following laboratory tests were performed on representative soil samples to determine their relative engineering properties.

ASTM D-2487 Soil Classification
ASTM D-2435 One Dimensional Consolidation
ASTM D-2937 In-Place Soil Density
ASTM D-2216 Moisture Content of Soil
ASTM D-2844 R-Value of Soils (Hveem-Carmany)

Tests were performed in accordance with test methods of the American Society for Testing and Materials or other accepted standards. The results of our laboratory tests are included in this report. The in-place soil density, moisture content and the standard penetration test values are presented on the attached drilling logs.

FINDINGS

SITE DESCRIPTION

The project site is located in the West half of the Southeast Quarter of Section 2, Township 1 South, Range 1 West of the Ute Principal Meridian, Mesa County, Colorado. More specifically the site is located at the Southeast corner of the intersection of North 7th Street and Horizon Drive, within the corporate limits of the City of Grand Junction. The site contains approximately 11.7 acres.

portion of a small, Northwest facing bluff slope, with a variable slight to moderate slope to the Northwest. The exact direction of surface runoff on this site will be controlled by the proposed construction and therefore will be variable. In general, surface runoff is expected to travel to the proposed street drainage, may be temporarily detained as required by the site specific drainage plan, eventually entering the existing unimproved Independent Ranchmen's Ditch and to the Colorado River, approximately 2 miles to the South. Surface drainage on this site would be described as fair to good and subsurface drainage as poor.

On-site erosion can be a significant problem if drainage and vegetation are not carefully controlled. Vegetation will probably be maintained in the immediate area around the building sites, but special care should be taken to maintain vegetation on the steeper slopes. We recommend that runoff from these slopes be carefully controlled to prevent

erosion caused by irrigation practices, sheetwash or seepage. It may be necessary to provide culverts or drainage ways to prevent excessive erosion along steeper slopes.

GENERAL GEOLOGY AND SUBSURFACE DESCRIPTION

The geologic materials encountered under the site consist of between 2-1/2' to over 20' of unconsolidated, alluvial/colluvial and debris fan soils which overlie the Mancos Shale Formation. The Mancos Shale is part of a very thick sequence of sedimentary rocks. The geologic and engineering properties of the materials found in our 6 exploration borings will be discussed in the following sections.

The surface soils on this site consist of some debris fan deposits originating on the higher ground of the Bookcliffs to the Northeast and some colluvial (slope wash) deposits, originating on the higher ground to the Southeast. These soil materials found in the exploration borings consist of mixed soils containing silt, clay, shale fragments, sand, gravel and cobble sized fragments. Due to the method of deposition, these materials are mixed and of variable composition and consistency.

The majority of the soils on this site are derived from debris fan activity. The colluvial soils have eroded from previously deposited debris fan features forming the hill to the South & East of the site. The surface soils are generally overlain by organic silty clays and clayey silts which range in thickness from less than 1/2' to approximately 2' and

have been partially reworked by previous agricultural activities.

The majority of the soil profile have been designated as Soil

Type I for purposes of this report.

This Soil Type was classified sandy, silty clay (CL) under the Unified Classification System. This material is of low plasticity, of low to moderate permeability, and was encountered in a low density, wet condition. soil will undergo long-term consolidation upon the addition of moisture or applied construction loads. This soil will settle after being loaded. The maximum allowable bearing capacity for this soil was found to be approximately 750 psf, with 100 psf minimum dead load pressure required. Soil Type contains sulfates in detrimental quantities.

These soils, if recompacted to a moderate to high density, will exhibit expansive characteristics. The amount of soil expansion experience will depend upon the methods and amount of soil compaction and cannot be accurately predicted.

Thin to moderately thick strata of a very sandy, silty clay and clayey silt mixture was encountered throughout the soil profile. The soils have been designated Soil Type II for this report.

This Soil Type was classified as a sandy, silty clay and clayey silt (ML-CL) under the Unified Classification System. This material is of low plasticity, of low to moderate permeability, and was encountered in a low density, wet condition. This soil will undergo long-term consolidation upon the addition of moisture or applied construction loads. This soil will settle after being loaded. The maximum allowable

bearing capacity for this soil was found to be 700 psf, with no minimum dead load pressure required. Soil Type No. II contains sulfates in detrimental quantities.

Strata of compressible sandy silt (ML) was encountered, in the exploration program. These soils are designated Soil Type III and are very similar to Soil Type II. These silts are low plastic, of moderate permeability and of low density. The maximum allowable bearing capacity for these silts was found to be 700 psf, with no minimum dead load pressure required.

The surface soils are deposited over the dense formational material of the Mancos Shale of Cretaceous Age, which is designated as Soil Type IV. The Mancos Shale is described as a thinbedded, drab, light to dark gray marine shale, with thinly interbedded fine grain sandstone and siltstone layers. The majority of the shale, has a low to moderate expansion potential. The formational shale was encountered at depths ranging from 2' to 21'. It is anticipated that this formational shale will affect the construction and the performance of the foundations on the site.

The soils of the Mancos Shale was classified as a silty clay (CL) under the Unified Classification System. The Standard Penetration Tests ranged from 36 to over 100 blows per foot. Penetration tests of this magnitude indicate that the soil is quite variable and generally of medium high to very high density. The moisture content varied from 13.4% to 18.4%, indicating a relatively moist soil. This soil is plastic

and is sensitive to changes in moisture content. With decreased moisture, it may shrink, with some cracking upon desiccation. Upon increasing moisture, it will tend to expand. Expansion tests were performed on typical samples of the soil and expansive pressures on the order of 1000-2400 psf were obtained. Due to the relatively wide range of expansion pressures, a minimum deadload of 2600 psf will be required. This soil was found to contain sulfates in detrimental quantities.

The Mancos Shale Formation is often highly fractured, with fillings of soluble sulfate salts being very common, particularly in the weathered zones. The samples obtained in this drilling program indicated many of the fractured faces and bedding planes in the shale contain sulfate salt deposits. Some seams of sulfate salts up to 1/4 inch thick were observed in the upper 2' to 3' of the weathered Mancos Shale.

Sulfate Salts exhibit variable strength, depending upon surrounding moisture conditions and their chemistry as related to water. In addition, Sulfate Salts are soluble and may be physically removed from the soil by ground moisture conditions. Such removal may leave significant amounts of void areas within the Mancos Shale, which may affect the load bearing capacity of the formation. Many of the fractures in the Mancos Shale Formation are open, allowing the rapid transmission of water to occur. Some sandstone and siltstone strata within the Mancos Shale Formation also exhibit elevated permeability.

GROUND WATER:

A free water table came to equilibrium during drilling at 13-16 feet below the present ground surface in the Northern, flatter portion of the tract adjacent to the unimproved portion of the Independent Ranchmen's Ditch. This is probably not a true phreatic surface but is an accumulation of subsurface seepage moisture (perched water). In our opinion the subsurface water conditions shown are a permanent feature on this site. The depth to free water would be subject to fluctuation, depending upon external environmental effects.

No free water was encountered in the exploration borings on the Southern part of the tract, which is somewhat higher, where the Mancos Shale was encountered at fairly shallow depths.

Due to the proximity of the Mancos Shale Formation in the Southern portion of the tract, there exists a possibility of a perched water table developing in the alluvial soils which overlie the Mancos Shale and within any excavations in the Mancos Shale. This perched water would probably be the result of increased irrigation due to the presence of lawns and landscaping and roof runoff. The exploration holes indicate that the top of the Mancos Shale Formation has only a gentle slope and that subsurface drainage would probably be quite slow.

While it is believed that under the existing conditions at the time of this exploration the construction process would not be effected by any free-flow waters, it is

very possible that several years after development is initiated, a troublesome perched water condition may develop which will provide construction difficulties. In addition, this potential perched water could create some problems for existing or future foundations on this tract. Therefore it is recommended that the future presence of a perched water table be considered in all design and construction of both the proposed residential structures and any subdivision improvements.

Because of capillary rise, the soil zone within a few feet above the free water level identified in the borings will be quite wet. Pumping and rutting may occur during the excavation process, particularly if the bottom of the foundations are near the capillary fringe. Pumping is a temporary, quick condition caused by vibration of excavating equipment on the site. If pumping occurs, it can often be stopped by removal of the equipment and greater care exercised in the excavation process. In other cases, geotextile fabric layers can be designed or cobble sized material can be introduced into the bottom of the excavation and worked into the soft soils. Such a geotextile or cobble raft is designed to stabilize the bottom of the excavation and to provide a firm base for equipment.

CONCLUSIONS AND RECOMMENDATIONS

GENERAL DISCUSSION

No geologic conditions were apparent during our reconnaissance which would preclude the site development as planned, provided the recommendations contained herein are fully complied with. Based on our investigation to date and the knowledge of the proposed construction, the site condition which would have the greatest effect on the planned development is the very soft low bearing alluvial soils which overlie the expansive Mancos Shale Formation.

Since the exact magnitude and nature of the foundation loads are not precisely known at the present time, the following recommendations must be somewhat general in nature. Any special loads or unusual design conditions should be reported to Lincoln DeVore so that changes in these recommendations may be made, if necessary. However, based upon our analysis of the soil conditions and project characteristics previously outlined, the following recommendations are made.

OPEN FOUNDATION OBSERVATION

Since the recommendations in this report are based on information obtained through random borings, it is possible that the subsurface materials between the boring points could vary. Therefore, prior to placing forms or pouring concrete, an open excavation observation should be performed by representatives of Lincoln DeVore. The purpose of this observation is to determine if the subsurface soils directly below the

proposed foundations are similar to those encountered in our exploration borings. If the materials below the proposed foundations differ from those encountered, or in our opinion, are not capable of supporting the applied loads, additional recommendations could be provided at that time.

EXCAVATION:

Site preparation in any areas which are to receive structural fill should begin with the removal of all topsoil, vegetation, and other deleterious materials. Prior to placing any fill, the subgrade should be observed by representatives of Lincoln DeVore to determine if the existing vegetation has been adequately removed and that the subgrade is capable of supporting the proposed fills. The subgrade should then be scarified to a depth of 10 inches, brought to near optimum moisture conditions and compacted to at least 90% of its maximum modified Proctor dry density (ASTM D-1557). The moisture content of this material should be within + or - 2% of optimum moisture, as determined by ASTM D-1557.

In general, we recommend all structural fill in the area beneath any proposed structure or roadway be compacted to a minimum of 90% of its maximum modified Proctor dry density (ASTM D1557). This structural fill should be placed in lifts not to exceed six (6) inches after compaction. We recommend that fill be placed and compacted at approximately its optimum moisture content (+/-2%) as determined by ASTM D 1557. Structural fill should be a granular, non-expansive soil.

We recommend that the amount of cut and fill be kept to a minimum on this site. Specifically, we recommend that any cut or fill which reduces the stability of native slopes be avoided. This includes any cut at the toe of a slope and any fill placed at the top of a slope. We recommend that any cut or fill over 4 feet in height be analyzed for stability of the final slope prior to construction.

Allowable slope angle for cuts in the native soils is dependent on soil conditions, slope geometry, the moisture content and other factors. Should deep cuts be planned for this site, we recommend that a slope stability analysis be performed when the location and depth of the cut is known.

No major difficulties are anticipated in the course of excavating into the surficial soils on the site. It is probable that safety provisions such as sloping or bracing the sides of excavations over 4 feet deep will be necessary. Any such safety provisions shall conform to reasonable industry safety practices and to applicable OSHA regulations. The OSHA Classification for excavation purposes on this site is Soil Class C for the alluvial soils, Types I, II, III. The OSHA Classification for excavation purposes of the Weathered Mancos Shale (Soil Type IV) is Soil Class B, assuming free water is not encountered in the excavation.

DRAINAGE AND GRADIENT:

Adequate site drainage should be provided in the foundation area both during and after construction to prevent the ponding of water and the saturation of the subsurface

soils. We recommend that the ground surface around the structure be graded so that surface water will be carried quickly away from the building. The minimum gradient within 10 feet of the building will depend on surface landscaping. We recommend that paved areas maintain a minimum gradient of 2%, and that landscaped areas maintain a minimum gradient of 8%. It is further recommended that roof drain downspouts be carried across all backfilled areas and discharged at least 10 feet away from the structure. Proper discharge of roof drain downspouts may require the use of subsurface piping in some areas. Planters, if any, should be so constructed that moisture is not allowed to seep into foundation areas or beneath slabs or pavements.

If adequate surface drainage cannot be maintained, or if subsurface seepage is encountered during excavation for foundation construction, a full perimeter drain is recommended for this building. It is recommended that this drain consist of a perforated drain pipe and a gravel collector, the whole being fully wrapped in a geotextile filter fabric. We recommend that this drain be constructed with a gravity outlet. If sufficient grade does not exist on the site for a gravity outlet, then a sealed sump and pump is recommended. Under no circumstances should a dry well be used on this site.

The existing drainage on the site must either be maintained carefully or improved. We recommend that water be drained away from structures as rapidly as possible and not be allowed to stand or pond near the building. We recommend that water removed from one building not be directed onto the

backfill areas of adjacent buildings. We recommend that a hydrologist or drainage engineer experienced in this area be retained to complete a drainage plan for this site.

stability and to aid in the rapidity of runoff, it is recommended that all backfill around the building and in utility trenches in the vicinity of the building be compacted to a minimum of 85% of its maximum Proctor dry density, ASTM D 698. The native soils on this site may be used for such backfill. We recommend that all backfill be compacted using mechanical methods. No water flooding techniques of any type may be used in placement of fill on this site.

Should an automatic lawn irrigation system be used on this site, we recommend that the sprinkler heads be installed no less than 5 feet from the building. In addition, these heads should be adjusted so that spray from the system does not fall onto the walls of the building and that such water does not excessively wet the backfill soils.

year floodplain of the Independent Ranchmen's Ditch will be addressed as part of the overall drainage plan for the site. We recommend that construction be avoided in this area and that drainage ways be kept open and free from debris. During periods of high runoff, debris may cause damming at bridges and culverts, resulting in backwater effects which may be damaging. We recommend that this drainage plan be completed by a hydrologic or drainage engineer fully experienced in this area. Such a plan is beyond the scope of this report.

It is recommended that lawn and landscaping irrigation be reasonably limited, so as to prevent undesirable saturation of subsurface soils or backfilled areas.

Several methods of irrigation water control are possible, to
include, but not limited to:

- * Metering the Irrigation water.
- * Sizing the irrigation distribution service piping to limit on-site water usage.
- * Encourage efficient landscaping practices.
- * Enforcing reasonable limits on the size of high water usage landscaping for each lot and any park areas.

The slope areas immediately adjacent to the unimproved portion of the Independent Ranchmen's Ditch can be considered potentially unstable due to the threat of ongoing erosion. A minimum setback should be established between the proposed construction and the edge of existing slope scarps. We recommend that the setback distance be established by laboratory analysis of the shear strength and stability of specific locations along the banks. In addition, mitigation systems are recommended to control the on-going erosion caused by the creek. Such mitigation could include retaining walls, riprap, gabions or other stabilization materials.

FOUNDATIONS

The soils and weathered rock formations on this site present several difficulties for construction. overlying soils on much of the site are very soft and will probably undergo significant amounts of long-term consolidation if building loads are applied. In addition, the Mancos Shale Formation, particularly near the ground surface on the Southern portion of this tract, exhibits rather variable expansive characteristics. Some of the samples obtained from the Mancos Shale Formation were observed to be somewhat more expansive than the average encountered in the Grand Junction area. Due to the existing site topography, and ground water conditions affecting the site, it is not believed that a shallow foundation system could be placed directly on the Mancos Shale which would not experience a relatively high risk of movement. Recommendations for shallow foundation systems are given but, we would generally recommend that a deep foundation, consisting of drilled piers in the Southern portion of the tract and driven piles in the Northern portion and possibly the Southern of the tract be constructed to support the structures.

SHALLOW FOUNDATIONS ON MANCOS SHALE

A conventional shallow foundation system consisting of either a voided wall on grade or an isolated pad and grade beam system, resting on the relatively unweathered expansive clays of the Mancos Shale Formation (penetrating the

weathered portion which contains very large amounts of soluble sulfate salts), may be designed on the basis of an allowable bearing capacity of 8000 psf maximum, and a minimum dead load of 2800 psf must be maintained. Contact stresses beneath all continuous walls should be balanced to within + or - 150 psf at all points. Isolated interior column footings should be designed for contact stresses of about 250 psf more than the average used to balance continuous walls. The criteria use for balancing will depend somewhat upon the nature of the structure. Single-story, slab on grade structures and single-story crawlspace structures may be balance on the basis of dead load only. Multi-story structures may be balanced on the basis of Dead Load plus one half live load, for up to three stories.

SHALLOW FOUNDATIONS ON COMPRESSIBLE SOILS

Assuming that some amount of differential movement can be tolerated, then a conventional shallow foundation system, underlain by a reinforced structural fill, placed in accordance with the recommendations contained within this report may be utilized. The foundation would consist of continuous spread footings beneath all bearing walls and isolated spread footings beneath all columns and other points of concentrated load. Such a shallow foundation system, resting on the properly constructed structural fill, may be designed on the basis of an allowable bearing capacity of 2000 psf maximum.

Recommendations pertaining to balancing, reinforcing, drainage, and inspection are considered extremely important and must be followed. Contact stresses beneath all

continuous walls should be balanced to within + or - 200 psf at all points. Isolated interior column footings should be designed for contact stresses of about 150 psf less than the average used to balance the continuous walls. The criteria for balancing will depend somewhat on the nature of the structure. Single-story, slab-on-grade structures may be balanced on the basis of dead load only. Multi story structures may be balanced on the basis of dead load plus one half live load, for up to three stories.

SUBGRADE IMPROVEMENT, REINFORCED STRUCTURAL FILL

We recommend the following Structural Fill Sections for areas of moderately unstable subgrade (pumping), due to permanent or seasonally high Water table. Subgrade soils are assumed to be either fine grained sand (SM), Silt (ML), or Silty Clay (ML-CL). These sections assume the Subgrade Soils have an R Value >10.

The specific areas which will require placement of either the Biaxial Geogrid or the Geotextile Fabric will depend on the actual conditions encountered during construction. The subgrade and fill section construction should be monitored by representatives of the Geotechnical Engineer.

For use Beneath Structures, Walks and Non Traffic Areas

Base of Foundations and Slabs

^{4&}quot; Imported Structural Fill (Hveem-Carmany R>70)
Biaxial Geogrid

^{16&}quot; Imported Structural Fill (Hveem-Carmany R>70)
Geotextile for separation and reinforcement

All Geosynthetics to extend a minimum of 4' beyond the limits of the slabs, pads and footings, unless shown otherwise on plans.

Geotextile Fabric for separation and minor reinforcement may be either woven with a minimum Grab Strength of 180 lb., in the weakest direction (such as Mirafi 500-X) or, if free water is encountered at the level the geotextile is to be placed, a non-woven/needle punched fabric with a minimum Grab Strength of 110 lbs., in the weakest direction (such as Mirafi 140-N).

Biaxial Geogrid for reinforcement shall have a minimum Tensile Strength @ 5% Strain of 550 lb/ft., in the weakest direction (such as Tensar BX 1100).

The Imported Structural Fill (Hveem-Carmany R>70, swell not critical) is to be Granular, Medium to Coarse Grained, Very low plastic (PI<4), Non Freedraining, Compactable and within the following Gradation:

Maximum	size, by screening	<u>6"</u>
Passing	the #4 screen	20% - 85%
Passing	the #40 screen	10% - 60%
Passing	the #200 screen	3% - 15%

Imported Structural Fill and Aggregate Base Course (ABC) to be compacted to 90% of its maximum Modified Proctor dry density (ASTM-D-1557) at a moisture content within \pm 2% of optimum moisture. The use of light weight, tracked equipment will minimize subgrade degradation. Vibratory compaction

equipment is not recommended.

The finish 2" to 6" of the Structural Fill may be minus 3/4" Aggregate Base Course (ABC) to aid in obtaining the finish grading and an acceptable construction surface.

DEEP FOUNDATIONS:

Because of the possibility of relatively high foundations loads associated with these structures and the variable soil conditions under the site, we strongly recommend the use of a deep foundation system consisting of drilled piers in the area of shallow Mancos Shale and no ground water or driven piles in the areas of relatively high ground water levels, penetrating the Mancos Shale bedrock. Since the Southern portion of the site is generally dry and the overlying clayey soils are slightly to moderately stiff, problems with seepage and caving are not anticipated. Therefore, it is recommended that the use of drilled piers be considered for the Southern portion of this site.

The Northern portion of the site, adjacent to the Independent Ranchmen's Ditch, has in excess of 20' of low density, caving soils and a relatively high ground water table above the Mancos Shale Formation. It is recommended the use of driven piles be considered in this area. Driven piles could also be utilized in the Southern portion of the tract, for

which the drilled pier foundation system has been recommended. Following are complete recommendations for drilled piers for the Southern portion of the tract and driven piles for the Northern and possibly the entire tract.

DRILLED PIERS:

We recommend that drilled piers have a minimum shaft length of 7 feet and be embedded at least 7 feet into the relatively unweathered rock of the Mancos Shale Formation. At this level, these piers may be designed for a maximum end bearing capacity of 25000 psf, plus 1800 psf side support considering only the side wall area embedded in the bedrock. Due to the expansive potential of the bedrock, a minimum dead load uplift is required, consisting of a point uplift of 2600 psf and 375 psf side uplift, based on the side wall embedded in the bedrock. The overburden is soft and no supporting or uplift values are assigned to this material. The weight of the concrete in the pier may be incorporated into the required dead load.

It is recommended that the bottoms of all piers be thoroughly cleaned prior to the placement of concrete. The amount of reinforcing in each pier will depend on the magnitude and nature of loads involved. As a rule of thumb, reinforcing equal to approximately 1/2 of 1% of the gross cross-sectional concrete area should be used. Additional reinforcing should be used if structural conditions warrant. We recommend that reinforcing extend through the full length of pier.

To minimize the possibility of voids developing in the drilled piers, concrete with a slump of 5 to 6 inches is recommended. We recommend that piers be dewatered and thoroughly cleaned of all loose material prior to placing the steel cage and concrete. The pier excavation should contain no more than 2 inches of free water unless the concrete is placed by means of a tremie extending to the bottom of the pier. A free fall in excess of 5 feet is not recommended when placing concrete in drilled piers. We recommend that casing be pulled as the concrete is being placed and that a 5 foot head of concrete be maintained while pulling the casing. It is recommended that drilled piers be plumb with 2% of their length and that the shaft maintain a constant diameter for the full length of the pier and not allowed to "mushroom" at the top.

DRILLED PIER OBSERVATION:

The foundation installation for drilled piers should be continuously observed by a representative of Lincoln DeVore to determine that the recommended bearing material has been adequately penetrated and that soil conditions are as anticipated by the exploration. This observation will aid in attaining an adequate foundation system. In addition, abnormalities in the subsurface conditions encountered during foundation installation can be identified and corrective measures taken as required. Lincoln DeVore requires a minimum of one working day's notice, and a copy of the foundation plan, to schedule any field observation.

GRADE BEAMS:

A reinforced concrete grade beam is recommended to carry the exterior wall loads in conjunction with the deep foundation system. We recommend that this grade beam be designed to span from bearing point to bearing point and not be allowed to rest on the ground surface between these points. We recommend a void space be left between the bottom of the grade beam and the subgrade below due to the expansive nature of the subgrade soils.

DRIVEN PILES:

We recommend that driven piles bear in the competent materials of the underlying formation. We anticipate that pile driving refusal will be encountered within a few feet of penetration into the relatively unweathered Mancos Shale bedrock. Based on a static analysis, piles driven to refusal may be designed for an allowable tip bearing capacity of 70 to 100 To determine the bearing area of the pile, the area including the space between the flanges may be included. For example, an HP-12 pile may be assumed to have an end area of approximately 1 square foot. A round, closed-end pipe pile bearing area would be the area of the pile end plate. Pile driving refusal should be determined by our representative in the field. Generally, pile driving refusal is taken as a maximum of 15 blows If pile groups are used, the overall capacity of the pile group should be reduced in accordance with the appropriate efficiency formula (such as the Converse-Labarre method).

bearing capacities greater than those recommended above are necessary, we recommend that the pile bearing capacity be determined on the basis of static load tests.

It is anticipated that steel piling (either 'H' sections or concrete filled pipe) will be utilized in this construction. The following recommendations will assume the use of these materials. If wood or concrete piling are anticipated, recommendations can be readily provided.

Driving hammers should be of such size and type to consistently deliver effective dynamic energy suitable to the piles and materials into which they are to be driven. Hammers should operate at manufacturer's recommended speeds and pressures. We recommend that a pile driving hammer be used which is rated at least 19,000 feet pounds. However, driving energy should not be so large that pile damage occurs.

Piles must be used in groups to provide for eccentricities in loading. The group capacity will be less than the summation of the individual pile capacities, depending upon the relative spacing of the piles. A conservative estimate of group capacity is two-thirds of the summation of the individual pile capacities.

We recommend that minimum spacing of the piles be twice the average pile diameter or 1.75 times the diagonal dimension of the pile cross-section, but no less than 24 inches. It is recommended that the tops of the piles extend a minimum of 4 inches into the pile cap. Based on the exploration

borings no pile shorter than 24 feet is recommended unless proper pile capacity is verified by field inspection by the Geotechnical Engineer. Vertical piles should not vary more than 2% from the plumb position. We further recommend that eccentricity of reaction on a pile group with respect to the load resultant not exceed a dimension that would produce overloads of more than 10% in any one pile.

Since the underlying bedrock is moderately expansive, we recommend a minimum of permanent pressure be maintained on each pier. The minimum pressure should be designed based on a tip uplift pressure of 2600 psf. The area used to consider the uplift pressure should be width times the depth of the pile section used when considering H piles. Round pipe piles will require an end uplift pressure of 2600 psf and a side uplift of 650 psf for the portion of the side wall in contact with the expansive formation.

Based on our analyses, a standard 10-3/4inch diameter, 1/4 inch wall, pipe pile driven to refusal may be designed for an allowable capacity of 70 to 100 tons. On this site the capacity of the pile will probably govern allowable load. Pile driving refusal required to obtain the recommended capacity was taken as 6 blows per inch with a 19 foot kip hammer, utilizing the Jambu Pile Driving Equation. Driving hammers should be of such size and type to consistently deliver effective energy suitable to the piles and materials into which they are driven. Final pile driving refusal should be determined by

representatives of Lincoln DeVore in the field.

DRIVEN PILE OBSERVATION:

Continuous observation of the pile driving operations and a pile load test, if required, should be performed by Lincoln DeVore as a representative of the owner. A continuous log should be maintained on the number of blows per foot required to drive each pile. Driving should be completed without interruption (except for splicing) and without jetting or pre-drilling unless the geotechnical engineer has been contacted for further recommendations.

GRADE BEAMS:

A reinforced concrete grade beam is recommended to carry the exterior wall loads in conjunction with the deep foundation system. We recommend that this grade beam be designed to span from bearing point to bearing point and not be allowed to rest on the ground surface between these points in the portions of the tract where the Mancos Shale is within 4' of the bottom of the grade beam or pile cap. In the cases of shallow occurrences of Mancos Shale, we recommend a void space be left between the bottom of the grade beam and the subgrade below.

CONCRETE SLABS ON GRADE

Slabs could be placed directly on the natural soils or on a structural fill. We recommend that all slabs on grade be constructed to act independently of the other structural portions of the building. One method of allowing the slabs to float freely is to use expansion material at the slabstructure interface.

Any partitions which will be located on slabs on grade should be constructed with a minimum space of 1-1/2 inches at the bottom of the wall. This space should allow for any future potential upward movement of the floor slabs and minimize damage to the walls and roof sections above the slabs.

If the slab is to be placed directly on the expansive soils of the Mancos Shale Formation or on a thin fill (less than 3') overlying these soils, the risk of slab movement is high and stringent mitigation techniques are recommended. No design method known at this time will prevent slab movement should moisture enter the expansive soils below. Therefore, to mitigate the effects of slab movement should they occur, we recommend the following:

- 1. Control joints should be placed in such a manner that no floor area exceeding 400 square feet remains without a joint. Additional joints should be placed at columns and at inside corners. These control joints should minimize cracking associated with expansive soils by controlling location and direction of cracks.
- 2. We recommend that all slabs on grade be isolated from all structural members of the building. This is generally accomplished by an expansion joint at the floor slab / foundation interface. In addition, positive

separation should be maintained between the slab and all interior columns, pipes and mechanical systems extending through the slab.

- 3. The slab subgrade should be kept moist 3 to 4 days prior to placing the slab. This is done by periodically sprinkling the subgrade with water. However, under no circumstances should the subgrade be kept wet by the flooding or ponding water.
- 4. Any partitions which will rest on the slabs on grade should be constructed with a minimum void space of 1-1/2 inches at the bottom of the wall (see figure in the Appendix). This base should allow for future upward movement of the floor slabs and minimize movement and damage in walls and floors above the slabs. This void may require rebuilding after a period of time, should heave exceed 1-1/2 inches.

If a vapor barrier is desired beneath slabs, we recommend that it be overlain by at least 2 inches of sand to decrease the likelihood of curing problems. An alternate method of reducing finishing problems would be to place the vapor barrier beneath approximately 6 inches of a minus 3/4 inch gravel fill. This method must be very carefully accomplished to minimize excessive puncturing and tearing of the vapor barrier.

It is recommended that floor slabs on grade be constructed with control joints placed to divide the floor into sections not exceeding 360 to 400 square feet, maximum. Also, additional control joints are recommended at all inside corners and at all columns to control cracking in these areas.

Problems associated with slab 'curling' are usually minimized by proper curing of the placed concrete slab. This period of curing usually is most critical within the first 5 days after placement. Proper curing can be accomplished

by continuous water application to the concrete surface or, in some instances by the placement of a 'heavy' curing compound, formulated to minimize water evaporation from the concrete. Curing by continuous water application must be carefully undertaken to prevent the wetting or saturation of the subgrade soils.

EARTH RETAINING STRUCTURES

The active soil pressure for the design of earth retaining structures may be based on an equivalent fluid pressure of 50 pounds per cubic foot. The active pressure should be used for retaining structures which are free to move at the top (unrestrained walls). For earth retaining structures which are fixed at the top, such as basement walls, an equivalent fluid pressure of 65 pounds per cubic foot may be used. It should be noted that the above values should be modified to take into account any surcharge loads, sloping backfill or other externally applied forces. The above equivalent fluid pressures should also be modified for the effect of free water, if any.

The passive pressure for resistance to lateral movement may be considered to be 200 pcf per foot of depth. The coefficient of friction for concrete to soil may be assumed to be 0.24 for resistance to lateral movement. When combining frictional and passive resistance, the latter must be reduced by approximately 1/3.

The above recommendations assume that retaining walls are not bearing upon or retaining the Mancos Shale Formation. Retaining walls placed upon the Mancos Shale or retaining Mancos Shale must be specifically designed for the expansive characteristics of the shale. Recommendations for retaining walls founded upon or retaining expansive soils can be easily provided, if desired.

Drainage behind retaining walls is considered critical. If the backfill behind the wall is not well drained, hydrostatic pressures are allowed to build up and lateral earth pressures will be considerably increased. Therefore, we recommend a vertical drain be installed behind any impermeable retaining walls. Because of the difficulty in placement of a gravel drain, we recommend the use of a composite drainage mat similar to Exxon Battledrain or Tensar MD Series NS-1100. An outfall must be provided for this drain.

REACTIVE SOILS

Since groundwater in the Grand Junction area typically contains sulfates in quantities detrimental to a Type I cement, a Type II or Type I-II or Type II-V cement is recommended for all concrete which is in contact with the subsurface soils and bedrock. Calcium chloride should not be added to a Type II, Type I-II or Type II-V cement under any circumstances.

PAVEMENTS

Samples of the surficial native soils that may be required to support pavements have been evaluated using the Hveem-Carmany method (ASTM D-2844) to determine their support characteristics. The results of the laboratory testing are as follows:

AASHTO Classification - A-4(8) Unified Classification - CL Soil Type #I

R = 13 Expansion @ 300 psi = 86.6 psf Displacement @ 300 psi = 4.03

Displacement values higher than 4.00 generally indicate the soil is unstable and may require confinement for proper performance. The relatively high expansion value indicates that some minor swelling of the subgrade soils may be anticipated after construction. However, the swell value was not sufficiently high as to control the R Value.

Traffic Counts or volumes have not been provided to Lincoln DeVore. Information presently available to Lincoln DeVore indicates these streets will probably have a truck and passenger vehicle mix and volume which would allow a daily EAL of 5 for calculation of the pavement structure. It should be noted that if a higher EAL is determined through further traffic studies, the pavement sections recorded here may require minor modification.

Two methods of design were utilized for this project. First, the 1986 AASHTO procedure, recognized by the Colorado Department of Transportation and second, The Asphalt Institute (MS-1). A design life of 20 years was used, with an annual growth rate of 2%.

Based upon the existing topography, the anticipated final road grades and subsurface soils conditions encountered during the drilling program, a Drainage Factor of 0.6 (1986 AASHTO procedure) and a mean average annual air temperature (MAAT) of 60° Fahrenheit (Asphalt Institute Method) has been utilized for the section analysis.

<u>Calculated Pavement Sections</u>

18K EAL = 5

Soil "R" Value = 13

Drainage Coefficient = 0.6	Asphalt Institute MAAT = 60° F	
AC 3"	3" AC	
ABC 7"	6" ABC	
Subbase 0"	0" Subbase	
FULL DEPTH AC 4"	4"	

PROPOSED PAVEMENT SECTIONS

The use of full depth asphalt is generally not recommended on this site, unless significant subgrade preparation has been accomplished. In general, the Asphalt

Institute Method does not present a straight forward method of accounting for base course and subbase degradation by high ground water levels. Based on our experience in this area, it is recommended the sections obtained from the 1986 AASHTO Method be utilized for this project.

SUBGRADE IMPROVEMENT, MECHANICALLY STABILIZED FILL

Based on the soil support characteristics outlined above, We recommend the following Structural Fill Sections for areas of moderately to severely unstable subgrade (pumping), due to permanent or seasonally soil moisture. Subgrade soils are assumed to be either fine grained sand (SM), Silt (ML), or Silty Clay (ML-CL). These sections assume the Subgrade Soils have an R Value >10.

Residential Traffic, 18k EAL = 5:

3" asphaltic concrete
on 6" of aggregate base course
on Biaxial Geogrid or Geotextile for reinforcement
on 12-16" of subbase/structural fill
on Geotextile for separation and reinforcement

Full Depth Asphalt

4" asphaltic concrete
on 4" of aggregate base course
on Biaxial Geogrid or Geotextile for reinforcement
on 12" of subbase/structural fill
on Geotextile for separation and reinforcement

6" of portland cement pavement
on 4" of aggregate base course
on Biaxial Geogrid or Geotextile for reinforcement
on 12" of subbase/structural fill
on Geotextile for separation and reinforcement

Due to the probability of very high soil moisture in the subgrade soils, the use of a Geotextile Fabric for separation and minor reinforcement (such as Mirafi 500-X), placed beneath the Structural Section, may be required in many areas along these road alignments. The upper layer of Biaxial Geogrid or Geotextile for reinforcement, placed between the Aggregate Base Course and the subbase/structural fill, may not be required, depending on actual field conditions.

The additional materials and effort expended in subgrade stabilization is to provide a construction platform, so the actual Road Section can be placed and compacted. The specific areas which will require placement of either the Biaxial Geogrid or the Geotextile Fabric will depend on the actual conditions encountered during construction. The subgrade and road section construction should be monitored by representatives of the Geotechnical Engineer.

Recommended Geogrid, Geotextile and Imported Structural Fill may be found in the Subgrade Improvement, Reinforced Structural fill section of this report.

During the placement of any structural fill, it is recommended that a sufficient amount of field tests and observation be performed under the direction of the Geotechnical Engineer. The Geotechnical Engineer should determine the amount of observation time and field density tests required to determine substantial conformance with these recommendations.

Any areas of Fill or Subgrade instability encountered during construction are to be immediately brought to the attention of the Geotechnical Engineer, so recommendations for stabilization can be given.

The Subgrade Stabilization is normally considered effective if the imported structural fill materials are confined, if specified imported fill and specified asphalt densities are obtained and the final traffic surface is stable according to local practices. Some 'pumping and rolling' of the finish Base Course (ABC) surface is anticipated but, rutting should not occur.

SECTION CONSTRUCTION

We recommend that the asphaltic concrete pavement meet the State of Colorado DOT requirements for a Grade C or CX mix. If Laboratory Testing values are available, recycled asphalt may be factored and substituted for a portion of the new asphaltic concrete. In addition, the asphaltic concrete

pavement should be compacted to 92% minimum and 96% maximum of its maximum theoretical (Rice) density.

The aggregate base course should meet the requirements of State of Colorado DOT Class 5 or Class 6 material, and have a minimum R value of 78. We recommend that the base course be compacted to a minimum of 95% of its maximum Modified Proctor dry density (ASTM D-1557), at a moisture content within + or -2% of optimum moisture. The native subgrade shall be scarified and recompacted to a minimum of 90% of their maximum Modified Proctor day density (ASTM D-1557) at a moisture content within + or -2% of optimum moisture.

All pavement should be protected from moisture migrating beneath the pavement structure. If surface drainage is allowed to pond behind curbs, islands or other areas of the site and allowed to seep beneath pavement, premature deterioration or possibly pavement failure could result.

LIMITATIONS

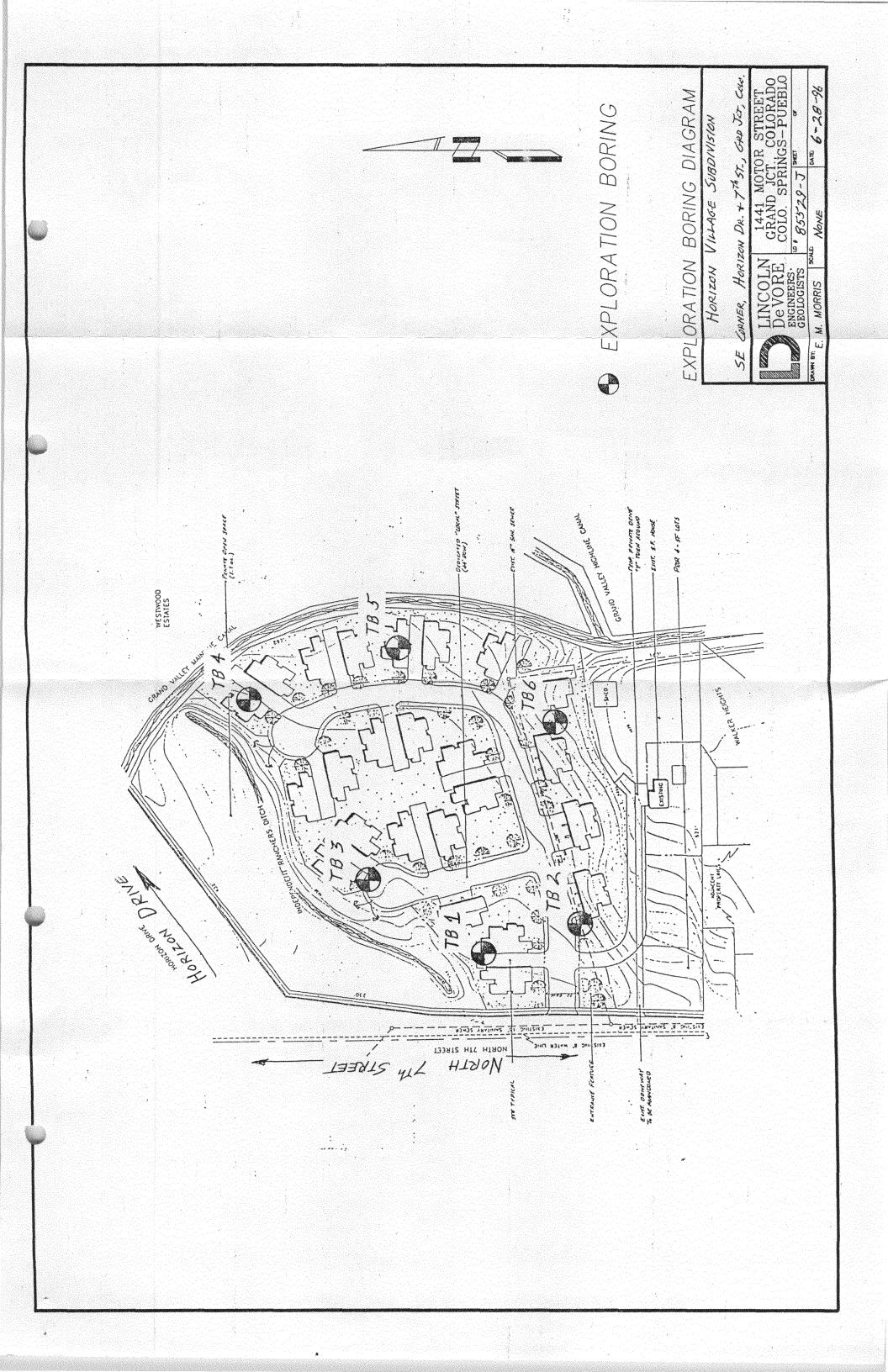
This report is issued with the understanding that it is the responsibility of the owner, or his representative to ensure that the information and recommendations contained herein are brought to the attention of the individual lot purchasers for the subdivision. In addition, it is the responsibility of the individual lot owners that the information and recommendations contained herein are brought to the attention of the architect and engineer for the individual projects and the necessary steps are taken to see that the contractor and his subcontractors carry out the appropriate recommendations during construction.

of the present date. However, changes in the conditions of a property can occur with the passage of time, whether they be due to natural processes or the works of man on this or adjacent properties. In addition, changes in acceptable or appropriate standards may occur or may result from legislation or the broadening of engineering knowledge. Accordingly, the findings of this report may be invalid, wholly or partially, by changes outside our control. Therefore, this report is subject to review and should not be relied upon after a period of 3 years.

The recommendations of this report pertain only to the site investigated and are based on the assumption that the soil conditions do not deviate from those described in this report. If any variations or undesirable conditions are encountered during construction or the proposed

construction will differ from that planned on the day of this report, Lincoln DeVore should be notified so that supplemental recommendations can be provided, if appropriate.

Lincoln DeVore makes no warranty, either expressed or implied, as to the findings, recommendations, specifications or professional advice, except that they were prepared in accordance with generally accepted professional engineering practice in the field of geotechnical engineering.



OILS	DESC uses	RIPTIONS:	SYMBOL	DESCRIPTIONS: DESCRIPTION	SYMBOL	OLS & NOTES: DESCRIPTION
2 2		Topsoil	0.06	CONGLOMERATE		9/a Ctandard manakation drive
**		-Man-made Fill	<u> </u>	SANDSTONE		9/12 Standard penetration drive Numbers indicate 9 blows to drive the spoon 12" into ground.
0000	GW	Well-graded Gravel		SILTSTONE	. 1	ST 2-1/2" Shelby thin wall sample
0000	GP	Poorly-graded Gravel		SHALE	1	Wa Natural Moisture Content
	GM	Silty Gravel	XXX	CLAYSTONE		W _X Weathered Material
000	GC	Clayey Gravel		COAL	Frae	DX Wedinered malerica
	sw	Well-graded Sand	瞬	LIMESTONE	Free Twater	Free water table
	SP	Poorly-graded Sand	纽	DOLOMITE		Y ^o Natural dry density
	SM	Silty Sand		MARLSTONE		T.B. — Disturbed Bulk Sample
	sc	Clayey Sand	7/////	GYPSUM		② Soil type related to samples in report
ЩЩ	ML	Low-plasticity Silt	틣	Other Sedimentary Rocks	15' Wx	Top of formation
	CL	Low-plasticity Clay	巡巡	GRANITIC ROCKS	Form.	1 to the mellon
讕	OL	Low-plasticity Organic Silt and Clay	+++	DIORITIC ROCKS		Test Boring Location
	МН	High-plasticity Silt		GABBRO	G	▼ Test Pit Location
الووو	СН	High-plasticity Clay		RHYOLITE		▲ Seismic or Resistivity Station.
[三]	ОН	High-plasticity Organic Clay		ANDESITE		Lineation indicates approx. length a orientation of spread (S * Seismic , R = Resistivity)
444 444	PI	Peat		BASALT		
	GW/GM	Well- graded Gravel, Silty	200	TUFF & ASH FLOWS	by dr	dard Penetration Drives are made riving a standard 1.4" split spoon pler into the ground by dropping a
000	GW/GC	Well-graded Gravel, Clayey	0.0	BRECCIA & Other Volcanics		o, weight 30°, ASTM test D-1586.
	GP/GM	Poorly-graded Gravel, Silty	1988	Offier Igneous Rocks	\$ poo	ples may be pulk, standard split n (both disturbed) or 2-1/2" I.D.
	GP/GC	Cloyey		CNEISS	thin sam;	wall ("undisturbed") Shelby tube ples. See log for type.
		Silty Gravel, Clayey		SCHIST	at the	poring logs show subsurface condition a dates and locations shown , and it it
		Clayey Gravel, Silty		PHYLLITE	of su	arranted that they are representative bsurface conditions at other location imes.
∭		Well - graded Sand, Silty		SLATE		
		Well-graded Sand, Clayey	1///	METAQUARTZITE		
膷	SP/SM	Silty	999	MARBLE		
	SP/SC	Poorly-graded Sand, Clayey	11/1	HORNFELS		
	SM/SC	Silty Sand, Clayey	Kit Kit	SERPENTINE		
1111	SC/SM	Clayey Sand, Silty	<u>REG</u>	Other Metamorphic Rocks		
	CL/ML	Silty Clay	LO LINCOL DAVOR INC			ATION OF BOREHOLE LOGS LOCATION DIAGRAMS

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		BORING NO. 1				
				BLOW	SOIL	
PTH	1	BORING ELEVATION:		COUNT	DENSITY	WATER
·.)	LOG	DESCRIPTION		/inch	pcf	%
	74 1	ORGANIC CLAYEY SILT				
	1/4	VERY LOW DENSITY DAMP				1
		BROWN, SILTY, SANDY CLAY				
		CL SANDY SILTY CLAY SULFATES WET	ST		98.3	23.6%
5		I COMPRESSIBLE LOW PLASTIC	5	01/06		
		MIL-CL SANDY, SILTY CLAY VERY SOFT TO DRILL	SPT	03/12		22.8%
		II ALLUVIAL, DEBRIS FAN DEPOSIT		04/18		
		VERY COMPRESSIBLE SAND STRATA				
		ML-CL SANDY, SILTY CLAY WET	ST		99.4	24.9%
0 7		II SULFATES	10	01/12		
		HOLE IS SQUEEZING SHUT	SPT	02/18		25.3%
\neg		•				
		FREE WATER VERY SOFT TO DRILL			44.9	
	!	ML SANDY SILT	SPT	01/12		26.6%
5	olid	III VERY COMPRESSIBLE	15		·	
	'[]]]	ALLUVIAL, DEBRIS FAN DEPOSIT				
\dashv	4344	VERY SANDY STRATA				
\dashv		SULFATES				
	"] [/]]]	VERY LOW DENSITY VERY SOFT TO DRILL	-			
	1010	VERY COMPRESSIBLE	20		•	
´—[`		GRAVELS OF SILTSTONE & SANDSTONE			**	·
	222	MANCOS SHALE THICK SULFATE DEPOSITS				
-	7774	INCREASING DENSITY W/DEPTH				
	[] [] [] [] [] [] [] [] [] [] [] [] [] [CL SILTY CLAY EXPANSIVE	SPT	37/6		17.3%
; -	= = =	IV LOW to MEDIUM PLASTICITY	25	88/12		17.5%
′— [:]	=	TV LOVE TO WILDIOW PLASTICITY		147/18		
\dashv				14//10		
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\dashv		TD @ 251				.
\backslash		TD @ 25'	30		1 + 44-1 *	
'		Plant Carrier and accommodative for and	30			
\dashv		Blow Counts are cumulative for each				
		6 inches of sampler penetration.				· · · · · · · · · · · · · · · · · · ·
		Free Water @ 13-1/2'		İ		
L		During Drilling 6-10-96				

LOG OF SUBSURFACE EXPLORATION HORIZON VILLAGE SUBDIVISION

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and the second of the second o	SE Corner, HORIZON Drive & 7th Street			
	Mr. MAC CUNNINGHAM Date			
LINCOLN - DeVORE, Inc.	. GRAND JUNCTION, COLO. 6-20-96			
Geotechnical Consultants	Job No.	Drawn		
Grand Junction, Colorado	85529-J	EMM		

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		BORING NO. 2				
	ļ		BLOW	SOIL		
DEPTH	SOIL	BORING ELEVATION:	COUNT	 	WATER	
(FT.)	LOG	DESCRIPTION	/inch	pcf	%	} }
_	170	ORGANIC, SANDY SILT SOFT WET				
	#1/	BROWN, ALLUVIAL, SILT & CLAY]
<u> </u>		DEBRIS FAN DEPOSIT SULFATES V. MOIST				
<u> </u>	1//	CL SANDY, SILTY CLAY ST		104	19.0%	
5_		I COMPRESSIBLE SULFATES 5	4		.:	
		VERY SOFT WET SPT	04/12		25.5%	
	1/2		08/18		}	
	77/2	MANCOS SHALE THICK SULFATE DEPOSITS	ļ ·			
	ZZZ	CL SANDY, SILTY CLAY MOIST ST		108.2	16.6%	
10	===	IV EXPANSIVE SULFATES 10	-{		45.00/	
] [VERY FRACTURED FIRM to VERY FIRM SPT	41/12	٠.	15.8%	::
	,		66/18			
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30—	1 1	Blow Counts are cumulative for each	1			
—	1	6 inches of sampler penetration.]			
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	1	During Drilling 6-10-96	<u> </u>			
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Geotechnical Consultants

Grand Junction, Colorado

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GRAND JUNCI	TION, COLO.	6-20-96
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						, 9
-		BORING NO. 3				
			BLOW	SOIL		İ
DEPTH	SOIL	BORING ELEVATION:	COUNT	DENSITY	 	
(FT.)	LOG	DESCRIPTION	/inch	pcf	%	·
	47	ORGANIC CLAYEY SILT				
i		VERY LOW DENSITY DAMP				
		BROWN, SILTY, SANDY CLAY	·			
	1/:	CL SANDY, SILTY CLAY SULFATES WET ST		100.4	15.7%	
5	111	I COMPRESSIBLE LOW PLASTIC 5				
		ML-CL SANDY, SILTY CLAY VERY SOFT TO DRILL SPT	03/12		21.2%	
		II ALLUVIAL, DEBRIS FAN DEPOSIT	04/18	·		,
	(m))	VERY COMPRESSIBLE SAND STRATA				
	1/	CL SANDY, SILTY CLAY WET ST		101.4	22.9%	
10	\mathbb{Z}^{\prime}	I COMPRESSIBLE SULFATES 10				
	الأرزا					, m. 1800
. ,		VERY SOFT TO DRILL				
		ML-CL SANDY, SILTY CLAY SPT	01/18		25.4%	
15		II ALLUVIAL, DEBRIS FAN DEPOSIT 15				,
		HOLE IS SQUEEZING SHUT VERY SANDY STRATA				
		FREE WATER	·			
		VERY LOW DENSITY VERY SOFT TO DRILL				
	MIN.	HIGHER DENSITY, VERY SANDY STRATA				
20	27/2	MANCOS SHALE THICK SULFATE DEPOSITS 20				
	7/2/2	INCREASING DENSITY W/DEPTH				
	7/17/2	VERY FRACTURED				
	Z Z Z					
		CL SILTY CLAY EXPANSIVE SPT	22/6		18.4%	. ,
25		IV LOW to MEDIUM PLASTICITY 25	74/12			
			148/18			
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		TD @ 25'				
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		Blow Counts are cumulative for each				
		6 inches of sampler penetration.	. New	arte in	5	. '
		Free Water @ 16'				1,00
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LOG OF SUBSURFACE EXPLORATION

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	Mr. MAC CUNNINGHAM		Date	
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Geotechnical Consultants

Grand Junction, Colorado

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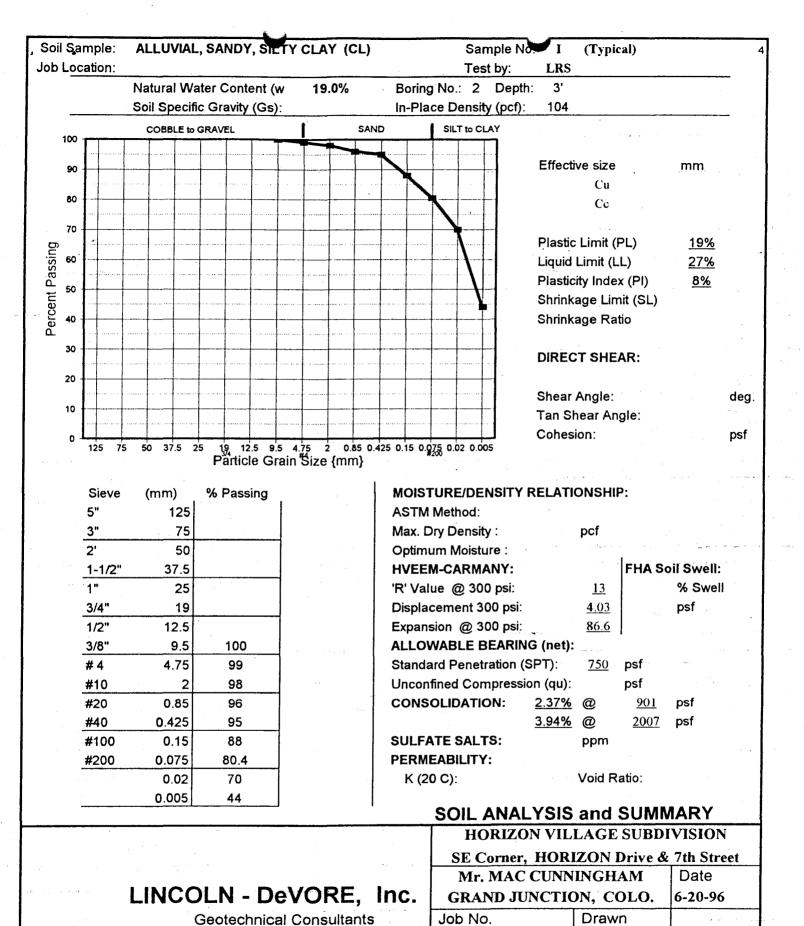
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Blow Counts are cumulative for each 6 inches of sampler penetration.

NO Free Water

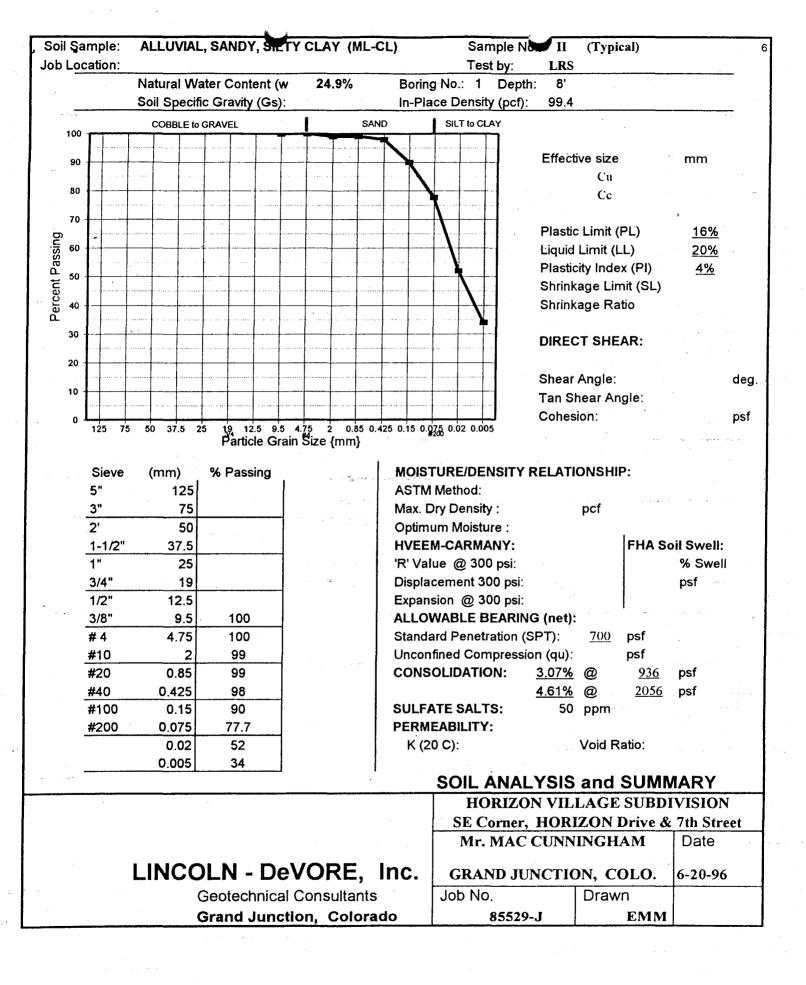
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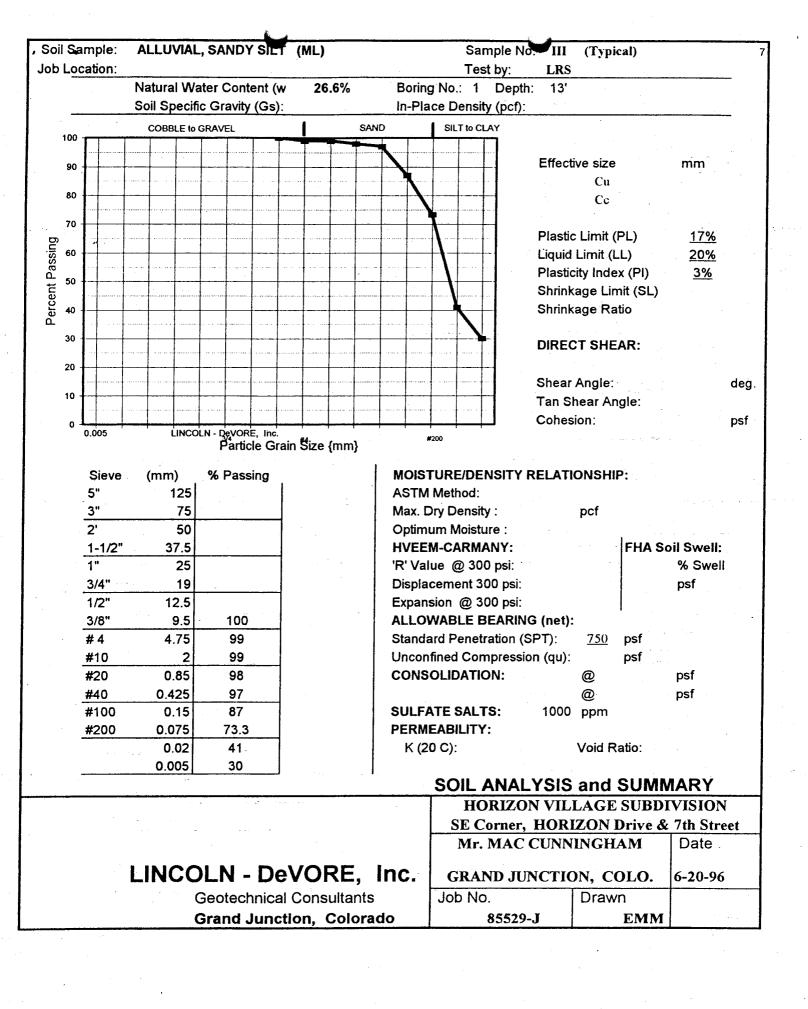


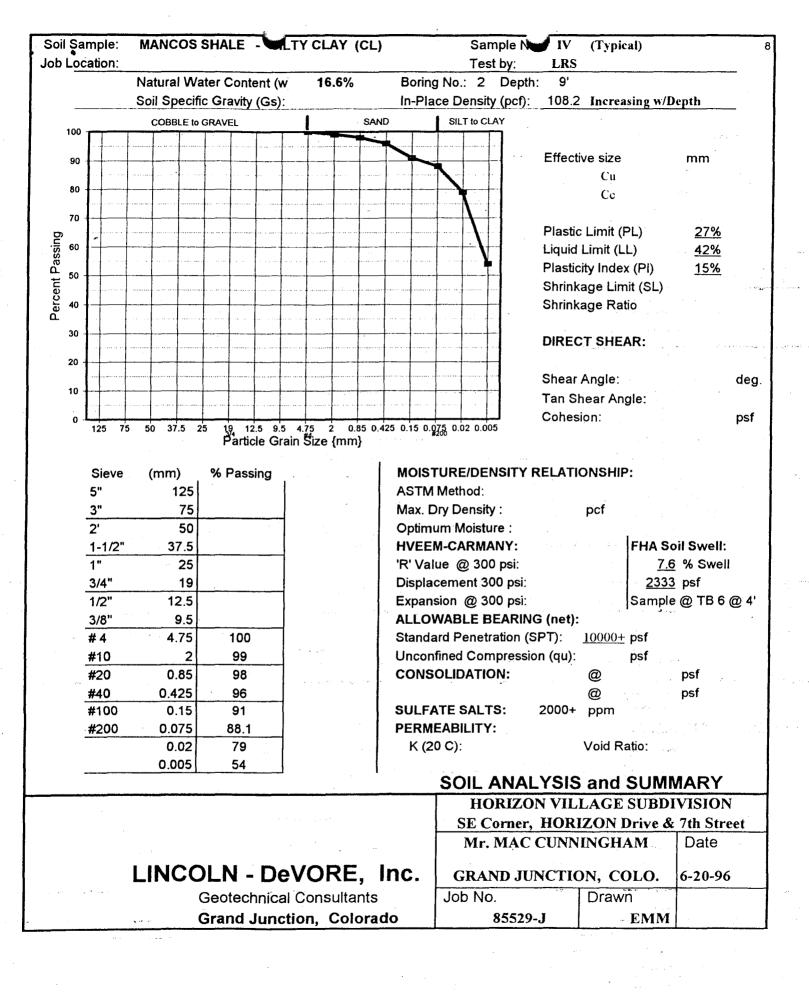
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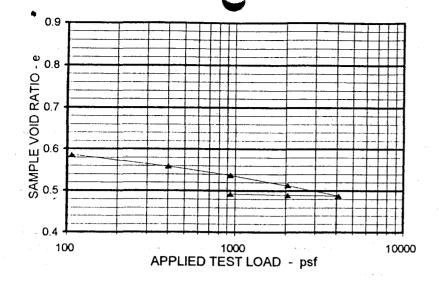
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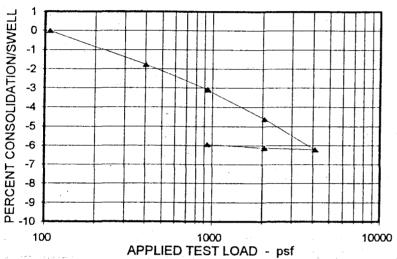
Grand Junction, Colorado











The Consolidation Test (ASTM D-2435)
Was Run By First Subjecting The Soil
Specimen To A 'Seating' Load.

The 'Seating' Load Is To Remove Slack From The Apparatus And To Provide An Accurate Point of Beginning.

The Test Begins With The Specimen At Approximately Natural Moisture Content.

The Sample is Loaded to Approximately 900 psf And Then Saturated With Water.

Any Swell Or Collapse Of The Specimen Is Noted And The Loading Is Continued.

After The Maximum Test Load, The Soil Specimen Is Unload, To Measure Rebound And Swelling Potential, After Consolidation.

LOAD SUMMARY

106	psf SEATING LOAD
936	psf SAMPLE SATURATED
0.03	% SOIL COLLAPSE
0	% SOIL EXPANSION/SWELL
0.29	% SAMPLE REBOUND @ UNLOAD
6.21	% MAXIMUM CONSOLIDATION
4116	psf MAXIMUM TEST LOAD

***** **	INITIAL	MAXIMUM	FINAL
		LOAD	LOAD
SOIL DENSITY (pcf)	104.6	111.5	111.2
SOIL MOISTURE (%)	22.7%	18.3%	18.6%
CONSOLIDATION (%)	-0-	6.21%	5.92%
VOID RATIO (e)	0.587	0.488	0.493
SATURATION (%)	103%	100%	100%

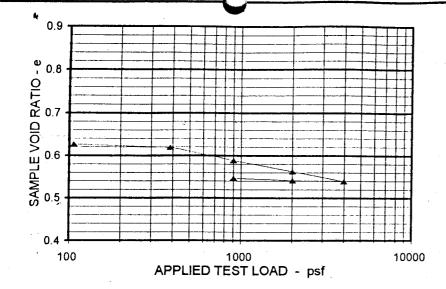
SOIL #:	11
SOIL TYPE:	ML-CL
TEST HOLE #:	1 @ 8'
SAMPLE Gs:	2.66
DIAMETER:	2.5"
AREA inchs:	.03409

SOIL CONSOLIDATION ASTM D-2435

HORIZON VILLAGE SUBDIVISION

SE Corner, HORIZON Drive & 7th Street Mr. MAC CUNNINGHAM Date GRAND JUNCTION, COLO. 6-20-96 Job No. Drawn Grand Junction, Colorado 85529-J EMM





The Consolidation Test (ASTM D-2435)
Was Run By First Subjecting The Soil
Specimen To A 'Seating' Load.

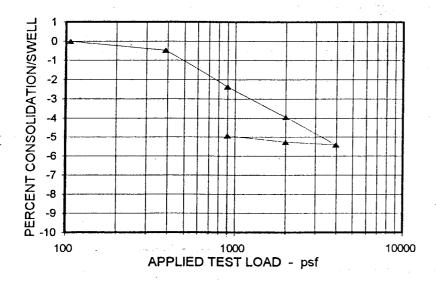
The 'Seating' Load Is To Remove Slack From The Apparatus And To Provide An Accurate Point of Beginning.

The Test Begins With The Specimen At Approximately Natural Moisture Content.

The Sample is Loaded to Approximately 900 psf And Then Saturated With Water.

Any Swell Or Collapse Of The Specimen Is Noted And The Loading Is Continued.

After The Maximum Test Load, The Soil Specimen Is Unload, To Measure Rebound And Swelling Potential, After Consolidation.



LOAD SUMMARY

400	
106	psf SEATING LOAD
901	psf SAMPLE SATURATED
. 0	% SOIL COLLAPSE
0	% SOIL EXPANSION/SWELL
0.47	% SAMPLE REBOUND @ UNLOAD
5.4	% MAXIMUM CONSOLIDATION
3990	psf MAXIMUM TEST LOAD

·	INITIAL	MAXIMUM	FINAL
		LOAD	LOAD
SOIL DENSITY (pcf)	102.0	107.8	107.3
SOIL MOISTURE (%)	20.0%	20.3%	20.5%
CONSOLIDATION (%)	-0-	5.40%	4.93%
VOID RATIO (e)	0.627	0.539	0.547
SATURATION (%)	85%	100%	100%

SOIL#:	1
SOIL TYPE:	CL
TEST HOLE #:	2 @ 3'
SAMPLE Gs:	2.66
DIAMETER:	2.5"
AREA inchs:	.03409

SOIL CONSOLIDATION ASTM D-2435

HORIZON VILLAGE SUBDIVISION SE Corner, HORIZON Drive & 7th Street Mr. MAC CUNNINGHAM Date GRAND JUNCTION, COLO. 6-20-96 Job No. Drawn 85529-J EMM

LINCOLN - DeVORE, Inc.

Geotechnical Consultants **Grand Junction, Colorado**



PRELIMINARY TRAFFIC STUDY

FOR

HORIZON VILLAGE

Prepared for:

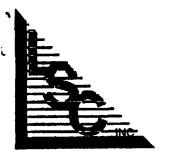
CUNNINGHAM INVESTMENT CO., INC. 121 South Galena Street, Suite 201 Aspen, CO 81611 (970) 925-8803

Prepared by:

LANDesign, LLC
PLANNING ENGINEERING SURVEYING
256 Grand Avenue
Grand Junction, CO 81501
(970) 245-4099

July 1, 1996 Revised August 13, 1996

Job No. 96045



LEGH, SCOTT & CLEARY, INC. TRANSPORTATION PLANNING & TRAFFIC ENGINEERING CONSULTANTS

1889 York Street Denver, CO 80206 (303) 333-1105 FAX (303) 333-1107

August 16, 1996

Mr. Phil Hart LANDesign P.O. Box 4506 Grand Junction, CO 81502

Re: Horizon Village (LSC #AAA962)

Dear Phil:

At your request, we have reviewed the preliminary traffic analysis for the Horizon Village development and have the following comments:

- Year 2010 Traffic Volumes: It is unclear how you calculated Year 2010 traffic volumes.
 You should indicate that background Year 2010 traffic volumes were calculated by
 increasing existing traffic volumes by 2.2 percent per year. Total Year 2010 traffic
 volumes are the sum of background 2010 traffic volumes and site-generated traffic
 volumes.
- 2. Capacity Analyses: Lane geometry used on the capacity analysis for the 7th/Horizon Drive intersection differs for the 1996 analysis from the 1996 with proposed development analysis for the westbound lanes. The former shows one left-turn lane plus a shared through lane while the latter shows two left-turn lanes plus a shared through lane. We would recommend that both analyses have one left-turn lane plus a shared through lane. We would also recommend using the traffic volumes for 1996 of 346 for the westbound left-turn lane and 93 for the shared through lane and a similar breakdown for the 1996 with the proposed development analysis. The program will prompt you for the breakdown of left/through movements and you can enter 90/10.
- 3. Gap Analysis: We recommend modification of the gap analysis as follows:

"A total of 57 available gaps for left-turn movements out of the development had been counted for a 15-minute period during the PM peak-hour. Typically, gaps of about six to nine seconds are needed to allow the critical entry of a vehicle into the traffic stream of a major street; gaps of nine to thirteen seconds will allow two vehicles to enter; and gaps of 13 or more seconds will allow entry of three vehicles. During the 15-minute period studied, there were thus a total of 111 effective gaps or 444 extrapolated to one hour. The volume of traffic projected to turn left at peak-hour is 13. If the volume of traffic projected to enter from the cross street is

Mr. Phil Hart

٦,

Page 2

August 16, 1996

less than 1/2 of the number of gaps available, then no additional traffic control is necessary. Consequently, sufficient gaps exist and additional signal analysis will not be required."

We trust that these comments will assist you in finalizing your traffic analysis of the Horizon Village development. Please call if you have any questions.

LEIGH, SCOTT & CLEARY, INC.

AJA/wd

C:\PROJECTS\AAA-96\HORIZON.REP

TRAFFIC STUDY

FOR

HORIZON VILLAGE

August, 1996

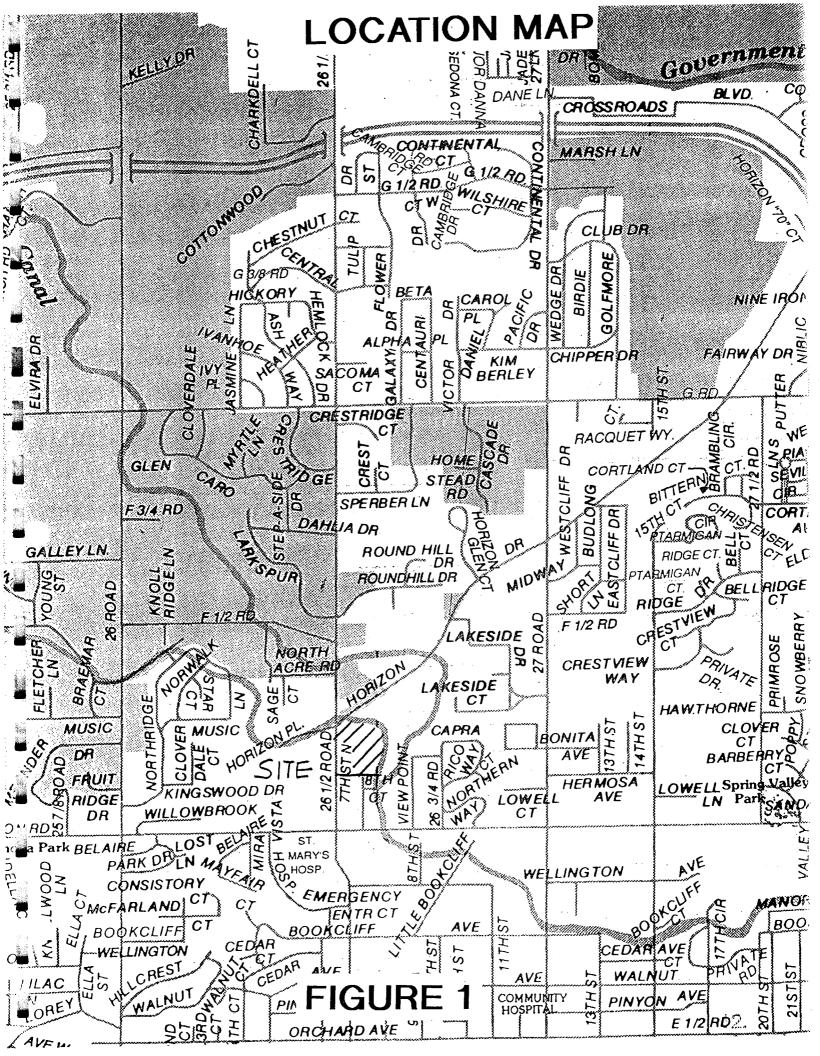
Prepared by: Jeffory P. Crane

I certify that this study has been prepared by me or under my direct supervision.

Philip M. Hart, P.E.
State of Colorado, No. 19346

TABLE OF CONTENTS

- A. INTRODUCTION
- **B.** TRIP GENERATION and DESIGN HOUR VOLUMES
- C. TRIP DISTRIBUTION and ASSIGNMENT
- D. TRAFFIC VOLUMES
- E. CAPACITY & GAP ANALYSIS
- F. CONCLUSIONS and RECOMMENDATIONS
- G. APPENDIX



A. INTRODUCTION

1. Purpose of Report

This report considers the concepts for access and the impacts of this proposed development on the current street transportation system in the general vicinity of the development and determines what improvements should be recommended to compensate for the additional traffic generated by this proposed development. Furthermore, this report may be used to assist City of Grand Junction Planners in determining future improvements of the transportation system in the area due to anticipated growth patterns.

Conditions or combinations of events other than those stated have not been analyzed and are not the responsibility of *LANDesign* or the engineer. Maintenance and construction of facilities are the responsibility of others.

2. Location & Land Use

The subject property is located within the SW 1/4 of Section 4, Township 1 South, Range 1 West, of the Ute Principal Meridian and contains 9.2 +/- acres. More specifically the site is located on the SE corner of North 7th Street and Horizon Drive. The tax ID number is 2945-024-00-048. See Figure 1 for the Location Map.

The property is presently a vacant parcel of land used primarily for grazing and hay production. The site is irrigated from the Grand Valley Mainline Canal which forms the east property line. The Independent Ranchman's Ditch traverses the northern portion of the site from east to west and discharges under North 7th Street just north of the existing access to the site.

The property immediately surrounding the proposed development consists primarily of moderate density residential communities. The Mesa View Retirement development is located on the SW corner of 7th and Horizon. Single family residences immediately surround the site while St. Mary's Hospital, professional medical offices and retail facilities exist in the vicinity of 7th and Patterson, 1/4 mile to the south.

The site is currently zoned PUD 6.2 by the City of Grand Junction. The proposed development will consist of 68 condominium units in 17 buildings located south of the Independant Ranchman's Ditch which will serve as a buffer between Horizon Drive and the development.

Proposed capital improvement projects in the vicinity include the reconstruction and widening of Horizon Drive from 7th Street to 12th Street to 5 lanes in the year 2001.

3. Access

Access to the development will be attained from 7th Street, a minor arterial, through a proposed 52' right-of-way extending 220' from 7th Street. The proposed urban residential collector road, Horizon Village Ct., will taper down to an urban residential road with a 44' right-of-way. The access to the development will be located approximately 380' south from the intersection of 7th and Horizon. The sight distance from the centerline of Horizon Village Ct. looking south on 7th Street is 520'. The design speed of 7th Street is 35 mph. See Figure 6.

B. TRIP GENERATION & DESIGN HOUR VOLUMES

1. Trip Generation

CONDOMINIUM DEVELOPMENT - The condominium development proposed calls for 68 units. The ITE manual specifies an average rate of between 5.86 vehicle trip ends per dwelling unit per day for condominiums, however, the City Development Engineer has indicated a preference to use the rate for single family developments.

68 Condominium Dwelling Units
Average Trip Ends vs. Single-Family Dwelling Units

Time Unit		tional bution	Average Rate	Trip Ends
	in	out		
weekday	50%	50%	9.55	325 in
ADT				325 out
weekday	26%	74%	0.74	13 in
AM peak				37 out
weekday	64%	36%	1.01	44 in
PM peak				25 out

2. Design Hour Volumes

Design hour volumes have been determined from traffic counts performed by LANDesign between June 6th and the 20th, 1996. This study will use the weekday peak hour volumes for analysis and design. Peak hours vary for different legs of the intersection. The northbound leg peaked between 5 and 6 PM at 7.8% of the ADT. The westbound leg of the intersection peaked between 12 and 1 PM at 8.6% of the ADT. The southbound leg peaked in the morning between 8 and 9 at 12.8% of the ADT and the eastbound leg peaked between 3 & 4 PM at 11.3% of the ADT. The northbound leg of the intersection will be the most affected leg due to the proposed development and therefore this study will assume a peak hour between 5 and 6 PM but will utilize the highest peak hour volumes at each leg for analysis of the intersection. See Figure 2 for the background peak hour volumes for each movement.

Single-Family Detached Housing (210)

Average Vehicle Trip Ends vs: Dwelling Units
On a: Weekday

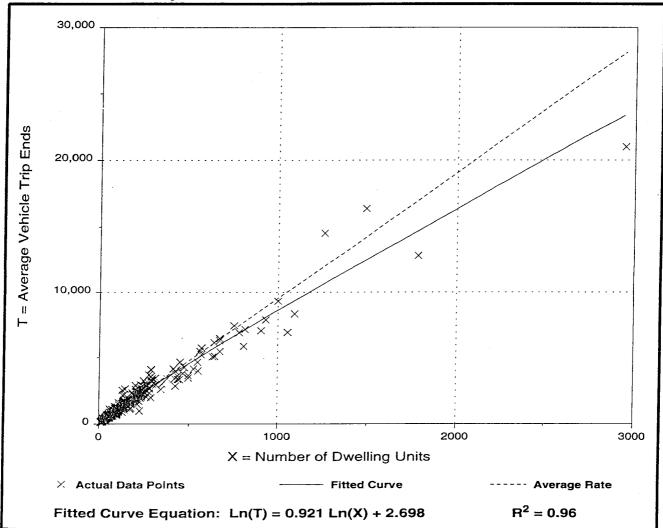
Number of Studies: 348 Average Number of Dwelling Units: 206

Directional Distribution: 50% entering, 50% exiting

Trip Generation per Dwelling Unit

Average Rate	Range of Rates	Standard Deviation
9.55	4.31 - 21.85	3.66

Data Plot and Equation



Single-Family Detached Housing (< 300 Units) (210)

Average Vehicle Trip Ends vs: Dwelling Units

On a: Weekday,

Peak Hour of Adjacent Street Traffic,

One Hour Between 7 and 9 a.m.

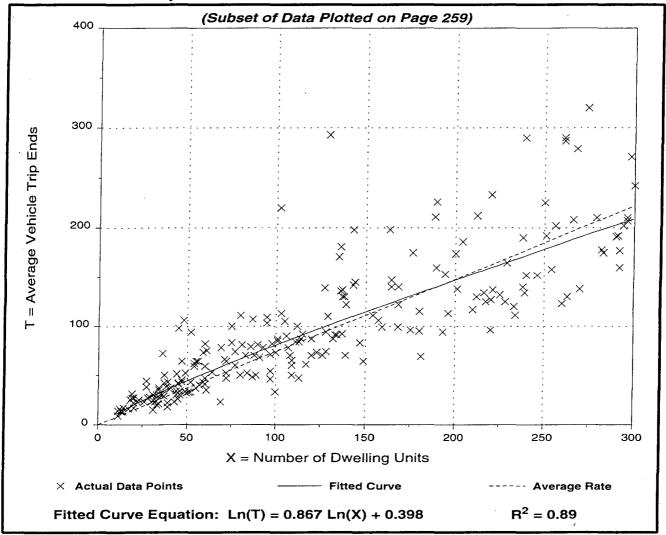
Number of Studies: 280 Average Number of Dwelling Units: 210

Directional Distribution: 26% entering, 74% exiting

Trip Generation per Dwelling Unit

Average Rate	Range of Rates	Standard Deviation
0.74	0.33 - 2.27	0.90

Data Plot and Equation



Single-Family Detached Housing (< 300 Units) (210)

Average Vehicle Trip Ends vs: Dwelling Units

On a: Weekday,

Peak Hour of Adjacent Street Traffic,

One Hour Between 4 and 6 p.m.

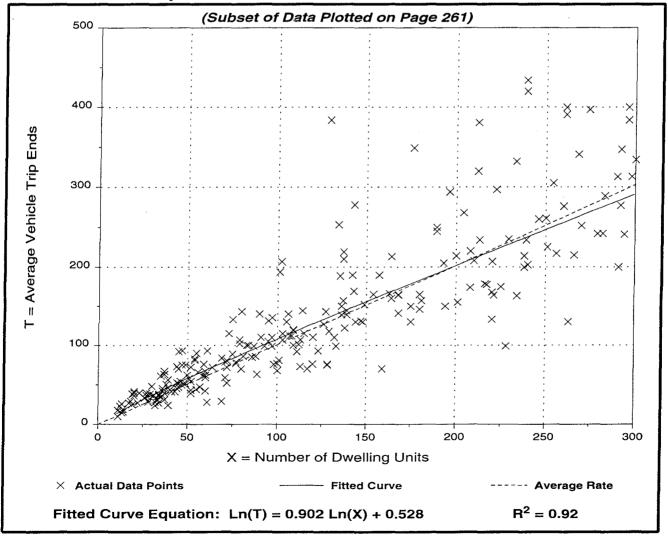
Number of Studies: 301 Average Number of Dwelling Units: 222

Directional Distribution: 64% entering, 36% exiting

Trip Generation per Dwelling Unit

Average Rate	Range of Rates	Standard Deviation
1.01	0.42 - 2.98	1.05

Data Plot and Equation



C. TRIP DISTRIBUTION and ASSIGNMENT

Directional distribution of trip ends was estimated by considering the proximity of the site to adjacent transportation facilities and the relationship to downtown Grand Junction and other major activity centers. The general distribution of trips to and from the site at build-out during the week is estimated to be 50% north and 50% south. Of that 50% of generated traffic entering or exiting the site to or from the north, It is estimated that 85% of that traffic will either turn east onto Horizon Drive or come from Horizon Drive. The remaining 15% will come from or go to 7th Street to the north of the intersection.

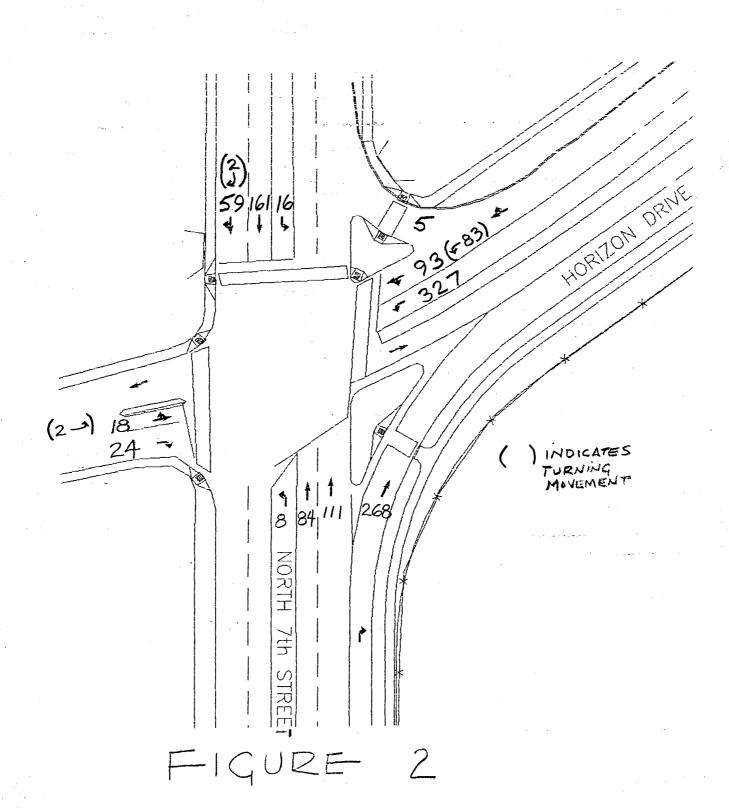
Figure 3 shows the trip end assignment for trips generated from the proposed development during the peak PM weekday hour at build-out.

D. TRAFFIC VOLUMES

Existing traffic volumes and peak hour factors have been determined by counts performed by *LANDesign* between June 6th and the 20th, 1996. *LANDesign* has utilized Peek ADR type counters to determine counts at 15 minute intervals for each lane and calculate totals and peak hour volumes. Upon determination of peak hours for each individual leg of the intersection, turning movement counts were performed by individuals in the field during the respective peak hours. See print-out of traffic counts in the end of this report.

Existing traffic volumes at the peak hours were combined with the calculated trip ends generated by the proposed development to produce a proposed total volume for analysis of the intersection. These figures were increased by 2.2% per year for analysis of the intersection in the year 2010. See Figures 4 & 5 respectively.

EXISTING PEAK HOUR VOLUMES PRE-DEVELOPMENT



TRIP ASSIGNMENT & DISTRIBUTION HORIZON DRIVE () INDICATES 15% ₈₅ (2) (10) STREET 50% (12) 50% - (13) (22) FIGURE 3

E. CAPACITY & GAP ANALYSIS

This report will investigate the impact on the existing signalized intersection at 7th and Horizon Drive due to the construction of the proposed development. The level of service of the existing intersection will be compared to the level of service attainable following full build-out of the proposed development. Furthermore, it will examine the access to the proposed development and the impact it will have on the flow of traffic on North 7th Street and delays experienced on Horizon Village Court. These analyses will look at the current conditions and the projected conditions for the year 2010.

The Highway Capacity Software (HCS) release 2.4a was utilized for analysis and determination of the level of service for the intersection of 7th Street and Horizon Drive as well as the intersection of Horizon Village Court and 7th Street. The Horizon Village Court intersection was analyzed as a simple unsignalized T-intersection while the Horizon Drive intersection was analyzed as a 3 phase isolated signalized operation.

The signalized intersection at 7th and Horizon is a fully actuated split phasing isolated operation in which the signal rests and green on 7th Street. In other words 7th Street will stay green until traffic on Horizon Drive actuates the signal. The signal operates in 3 phases. The 1st phase operates traffic on 7th Street. The 2nd phase regulates the traffic on westbound Horizon Drive while the 3rd phase operates the eastbound leg from the Mesa View Retirement Community. The cycle lengths for each leg have been measured in the field.

An analysis of the peak hour gap availability at the proposed site has been performed to determine if adequate gaps exist for left turn movements out of the development. Two directional gaps were counted in the field at peak hour in 3 categories; 6 to 9 seconds, 9-13 seconds and over 13 second gaps. A stopwatch was used to determine the length of the gaps available.

Center For Microcomputers In Transportation

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(N-S) 7th Street Streets: (E-W) Horizon Drive

Analyst: JPC File Name: EX1996.HC9

Area Type: Other 6-27-96 PM Peak

Comment: 1996 volumes

Traffic and Roadway Conditions

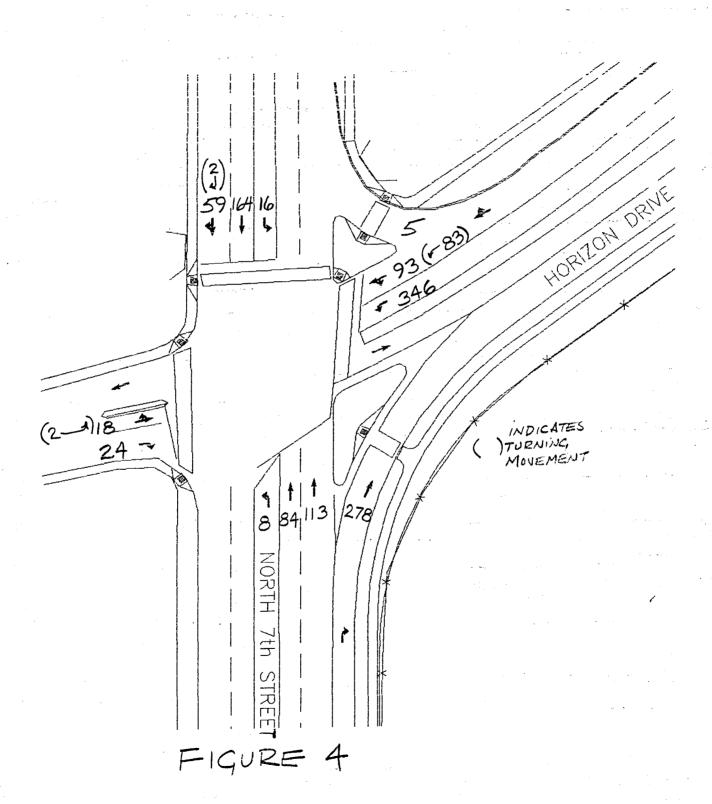
	Ea	astbo	und	Wes	stbour	nd	No	thbou	ınd	Sou	ıthboı	und
	L	${f T}$	R	L	${f T}$	R	L	T	R	L	T	R
No. Lanes	;	> 1	1	1 >	> 1		1	2		1	2 ·	<
Volumes	2	16	24	410	10		8	195		16	218	2
PHF or PK15	0.95	0.95	0.95	0.95	0.95		0.95	0.95		0.95	0.95	0.95
Lane W (ft)	ĺ	12.0	12.0	12.0	12.0		12.0	12.0		12.0	12.0	
Grade	Ì	0		ĺ	0			0			0	
% Heavy Veh	2	2	2	2	2		2	2		2	2	2
Parking	(Y/N)) N		(Y/N)) N	,	(Y/N)	N		(Y/N)	N	
Bus Stops			0			0			0			0
Con. Peds			0			0			0			0
Ped Button	(Y/N)) N		(Y/N)	N		(Y/N)	N		(Y/N)	N	
Arr Type		3	3	3	3		3	3		3	3	
RTOR Vols			0			0			0			0
Lost Time	3.00	3.00	3.00	3.00	3.00		3.00	3.00		3.00	3.00	3.00

Signal Operations

	Pha EB	se Combination Left Thru Right Peds	1	2 * * *	3	4	NB	Left Thru Right Peds	5 * *	6	7	8
1	WВ	Left Thru Right Peds	*				SB	Left Thru Right Peds	* * *			
	NB SB	Right Right					EB WB	Right Right				
	Gree Yel		.0A 15	.0A			Gre Yel	en 30 low/AR 5	.0P			

Cycle Length: 90 secs Phase combination order: #1 #2 #5

PROPOSED PEAK HOUR VOLUMES 1996



PROPOSED PEAK HOUR VOLUMES 2010

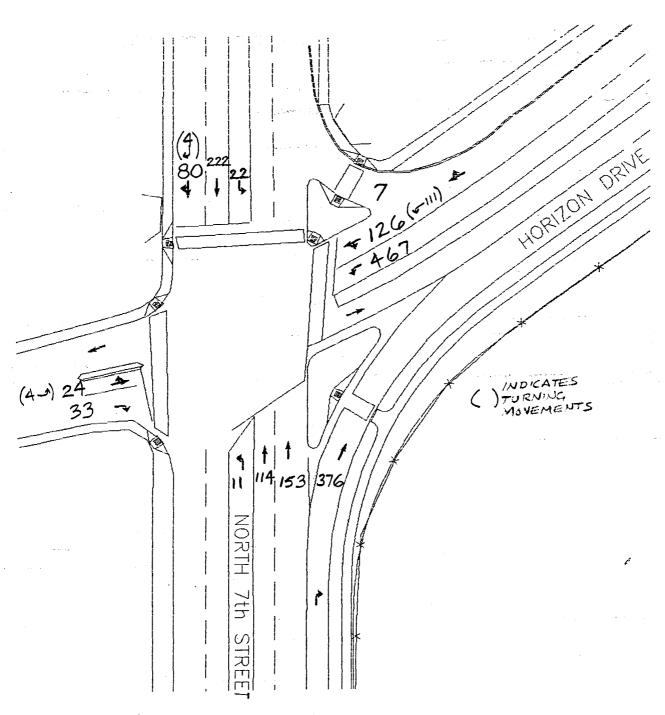


FIGURE 5

HCS: Signalized Intersection Version 2.4c

Streets: (E-W) Horizon Drive Analyst: JPC (N-S) 7th Street

File Name: EX1996.HC9 Area Type: Other 6-27-96 PM Peak

Comment: 1996 volumes

Volume Adjustment Worksheet

Direction/	Mvt Vol	PHF	Adj Vol	Lane Grp	Lane Grp Vol	No. Ln	Lane Util Fact	Growth Fact	Adj Grp Vol	Prop LT	Prop RT
EB											
Left	2	0.95	2								
Thru	16	0.95	17	${f LT}$	19	1	1.000	1.000	19	0.11	0.00
Right	24	0.95	25	R	25	1	1.000	1.000	25	0.00	1.00
WB											
Left	410	0.95	432	L	220	1	1,000	1.000	220	1.00	0.00
Thru	10	0.95	11	LT	223	1	1.000	1.000	223	0.95	0.00
NB											
Left	8	0.95	8	L	8	1	1.000	1.000	8	1.00	0.00
Thru	195	0.95	205	${f T}$	205	2	1.050	1.000	215	0.00	0.00
SB											
Left	16	0.95	17	L	17	1	1.000	1.000	17	1.00	0.00
Thru	218	0.95	229	${f T}{f R}$	231	2	1.050	1.000	243	0.00	0.01
Right	2	0.95	2								

Saturation Flow Adjustment Worksheet

	rection nGrp	Ideal Sat Flow	No. Lns	f W	f HV	f G	f p	f BB	f A	f RT	f LT	Adj Sat Flow
EB												
	$\mathbf{L}\mathbf{T}$	1900	1	1.00	0.98	1.00	1.00	1.00	1.00	1.00	0.99	1853
	R	1900	1	1.00	0.98	1.00	1.00	1.00	1.00	0.85	1.00	1583
WB												
	L	1900	1	1.00	0.98	1.00	1.00	1.00	1.00	1.00	0.95	1770
	\mathtt{LT}	1900	1	1.00	0.98	1.00	1.00	1.00	1.00	1.00	0.95	1778
NB												
	L	1900	1	1.00	0.98	1.00	1.00	1.00	1.00	1.00	0.52	969
	${f T}$	1900	2	1.00	0.98	1.00	1.00	1.00	1.00	1.00	1.00	3725
SB												
	L	1900	1	1.00	0.98	1.00	1.00	1.00	1.00	1.00	0.56	1040
	TR	1900	2	1.00	0.98	1.00	1.00	1.00	1.00	1.00	1.00	3721

Streets: (E-W) Horizon Drive

(N-S) 7th Street File Name: EX1996.HC9

Analyst: JPC Area Type: Other

6-27-96 PM Peak

Comment: 1996 volumes

Supplemental Permitted LT Worksheet

APPROACH	NB
Cycle Length, C	90
Actual Green Time for Lane Group, G	30
Effective Green Time for Lane Group, g	32
Opposing Effective Green Time, go	32
Number of Opposing Lanes, No	2
	1
Number of Lanes in Lane Group, N	
Adjusted Left-Turn Flow Rate, Vlt	8
Proportion of Left Turns in Lane Group, Plt	1.00
Left Turns per Cycle: LTC=Vlt*C/3600	0.20
Adjusted Opposing Flow Rate, Vo	243
Opposing Flow per Lane, Per Cycle: Volc=VoC/3600No	3.04
Opposing Platoon Ratio, Rpo	1
Lost time per phase, tl	3
gf=Gexp(-0.882*LTC^0.717)-t1	0.00
Opposing Queue Ratio: qro=1-Rpo(go/C)	0.64
gq = Volc * qro / (.5 - Volc * (1 - qro) / go)-tl	1.20
gu=g-gq (or g-gf)	30.80
fs=(875-0.625Vo)/1000	0.72
$Pl=Plt[1+{(N-1)g/(fsgu+4.5)}]$	1.00
El1	1.85
fmin	0.13
<pre>fm,(min=fmin;max=1.00)</pre>	0.52
flt=[fm+0.91(N-1)]/N	0.52
	0.02
APPROACH	SB
Cycle Length, C	90
Actual Green Time for Lane Group, G	30
Effective Green Time for Lane Group, g	32
Opposing Effective Green Time, go	32
Number of Opposing Lanes, No	2
Number of Lanes in Lane Group, N	ī
Adjusted Left-Turn Flow Rate, Vlt	
Proportion of Left Turns in Lane Group, Plt	1.00
Left Turns per Cycle: LTC=Vlt*C/3600	0.43
Adjusted Opposing Flow Rate, Vo	215
Opposing Flow per Lane, Per Cycle: Volc=VoC/3600No	2.69
Opposing Platoon Ratio, Rpo	1
Lost time per phase, tl	3
gf=Gexp(-0.882*LTC^0.717)-t1	0.00
Opposing Queue Ratio: qro=1-Rpo(go/C) gq = Volc * qro / (.5 - Volc * (1 - qro) / go)-tl	0.64
	0.68
gu=g-gq (or g-gf)	31.32
fs=(875-0.625Vo)/1000	0.74
Pl=Plt[1+{(N-1)g/(fsgu+4.5)}]	1.00
	1.75
fmin	0.13
<pre>fm,(min=fmin;max=1.00)</pre>	0.56

Streets: (E-W) Horizon Drive Analyst: JPC

Area Type: Other Comment: 1996 volumes (N-S) 7th Street

File Name: EX1996.HC9

6-27-96 PM Peak

Capacity Analysis Worksheet

Direction /LnGrp	Adj n Flow Rate (v)	Adj Sat Flow Rate (s)	Flow Ratio (v/s)	Green Ratio (g/C)	Lane Group Capacity (c)		
EB							
$\mathbf{L}\mathbf{T}$	19	1853	0.010	0.189	350	0.054	
R	25	1583	0.016	0.189	299	0.084	
WB							
L	220	1770	0.124	0.356	629	0.350	
${f LT}$	223	1778	0.125	0.356	632	0.353	
NB							
L	8	969	0.008	0.356	345	0.023	
${f T}$	215	3725	0.058	0.356	1324	0.162	
SB							
L	17	1040	0.016	0.356	370	0.046	
TR	243	3721	0.065 Sum (0.356 v/s) critical	1323 $1 = 0.207$	0.184	
Lost Time	e/Cycle, L =	9.0 sec		cal'v/c(x)	= 0.229		

Level of Service Worksheet

Direction /LnGrp		g/C Ratio	ď	Adj	Lane Group Cap		Delay d 2	Grp	Lane Grp LOS	Delay By App	LOS By App
EB											
LT	0.054	4 0.189	22.7	0.850	350	16	0.0	19.3	3 C	19.4	С
R	0.084	4 0.189	22.9	0.850	299	16	0.0	19.4	4 C		
WB											
L	0.350	0.356	16.2	0.850	629	16	0.1	13.9	9 B	13.9	В
${f LT}$	0.353	3 0.356	16.2	0.850	632	16	0.1	14.0	B		
NB											
${f L}$	0.023	3 0.356	14.3	0.850	345	16	0.0	12.2	2 B	12.8	В
${f T}$	0.162	2 0.356	15.1	0.850	1324	16	0.0	12.8	3 B		
SB											
L	0.046	0.356	14.4	0.850	370	16	0.0	12.3	3 B	12.9	В
TR	0.184	0.356	15.2	0.850	1323	16	0.0	12.9) B		
		Interse	ction I	Delay =	= 13.6	sec/v	eh Int	ersec	ction	LOS =	В

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Gainesville, FL 32611-2083 (904) 392-0378

Streets: (E-W) Horizon Drive (N-S) 7th Street
Analyst: JPC File Name: PROP1996.HC9

6-27-96 PM Peak Area Type: Other

Comment: 1996 volumes with proposed development

Traffic and Roadway Conditions

	l Ea	astbo	und	Wes	stbour	nd	No	rthbou	ınd	Sou	thbo	und
	L	${f T}$	R	L	${f T}$	R	L	${f T}$	R	L	${f T}$	R
No. Lanes	;	> 1	1	2 >	> 1		1	2		1	2 ·	<
Volumes	2	16	24	429	10		8	197		16	221	2
PHF or PK15	0.95	0.95	0.95	0.95	0.95		0.95	0.95		0.95	0.95	0.95
Lane W (ft)		12.0	12.0	12.0	12.0		12.0	12.0		12.0	12.0	
Grade		0			0		Į	0		ĺ	0	
% Heavy Veh	2	2	2	2	2		2	2		2	2	2
Parking	(Y/N)) N		(Y/N)) N		(Y/N)) N		(Y/N)	N	
Bus Stops			0	·		0			0			0
Con. Peds			0			0	Ì		0			0
Ped Button	(Y/N)) N		(Y/N)	N		(Y/N)) N		(Y/N)	N	
Arr Type		3	3	3	3		3	3	,	3	3	
RTOR Vols			0			0			. 0			0
Lost Time	3.00	3.00	3.00	3.00	3.00		3.00	3.00	,	3.00	3.00	3.00

Signal Operations

Pha: EB	se Combinatior Left Thru Right Peds	n 1	2 * * *	3	4	NB	Left Thru Right Peds	5 * *	6	7	8
WB	Left Thru Right Peds	*				SB	Left Thru Right Peds	* * *			
NB SB	Right Right					EB WB	Right Right				
Gree Yel		.0A 1	5.0A 5.0			Gree Yel	en 30 low/AR 5	.0P			

Cycle Length: 90 secs Phase combination order: #1 #2 #5

Streets: (E-W) Horizon Drive (N-S) 7th Street

Analyst: JPC File Name: PROP1996.HC9

Area Type: Other 6-27-96 PM Peak

Comment: 1996 volumes with proposed development

Volume Adjustment Worksheet

Direc-					Lane		Lane		Adj		
_	Mvt		Adj	Lane	Grp	No.	Util	Growth	Grp	Prop	Prop
Mvt	Vol	PHF	Vol	Grp	Vol	Ln	Fact	Fact	Vol	\mathbf{LT}^{-}	RT
EB											
Left	2	0.95	2								
Thru	16	0.95	17	\mathbf{LT}	19	1	1.000	1.000	19	0.11	0.00
Right	24	0.95	25	R	25	1	1.000	1.000	25	0.00	1.00
WB											
Left	429	0.95	452	L	231	2	1.030	1.000	238	1.00	0.00
Thru	10	0.95	11	LT	232	1	1.000	1.000	232	0.95	0.00
NB											
Left	8	0.95	8	L	8	1	1.000	1.000	8	1.00	0.00
Thru	197	0.95	207	T	207	2	1.050	1.000	217	0.00	0.00
SB											
Left	16	0.95	17	L	17	1	1.000	1.000	17	1.00	0.00
Thru	221	0.95	233	TR	235	2	1.050	1.000	247	0.00	0.01
Right	2	0.95	2								

Saturation Flow Adjustment Worksheet

	rection nGrp	Ideal Sat Flow	No. Lns	f W	f HV	f G	f p	f BB	f A	f RT	f LT	Adj Sat Flow
EB												
טט	LT	1900	1	1.00	0.98	1.00	1.00	1.00	1.00	1.00	0.99	1853
	R	1900	1	1.00	0.98	1.00	1.00	1.00	1.00	0.85	1.00	1583
WB												
	L	1900	2	1.00	0.98	1.00	1.00	1.00	1.00	1.00	0.95	3539
	LT	1900	1	1.00	0.98	1.00	1.00	1.00	1.00	1.00	0.95	1778
NB												
	L	1900	1	1.00	0.98	1.00	1.00	1.00	1.00	1.00	0.52	959
	${f T}$	1900	2	1.00	0.98	1.00	1.00	1.00	1.00	1.00	1.00	3725
SB												
	L	1900	1	1.00	0.98	1.00	1.00	1.00	1.00	1.00	0.56	1035
	TR	1900	2	1.00	0.98	1.00	1.00	1.00	1.00	1.00	1.00	3721

HCS: Signalized Intersection Version 2.4c 08-13-1996 3

Streets: (E-W) Horizon Drive (N-S) 7th Street
Analyst: JPC File Name: PROP1996.HC9
Area Type: Other 6-27-96 PM Peak

Area Type: Other

Comment: 1996 volumes with proposed development

Cumplemental Downitted III Warkshoot

Supplemental Permitted LT Worksheet		
APPROACH	NB	
Cycle Length, C	90	
Actual Green Time for Lane Group, G	30	
Effective Green Time for Lane Group, g	32	
Opposing Effective Green Time, go	32	
Number of Opposing Lanes, No	2	
Number of Lanes in Lane Group, N	1	
Adjusted Left-Turn Flow Rate, Vlt	8	
Proportion of Left Turns in Lane Group, Plt	1.00	
Left Turns per Cycle: LTC=Vlt*C/3600	0.20	
Adjusted Opposing Flow Rate, Vo	247	
Opposing Flow per Lane, Per Cycle: Volc=VoC/3600No	3.09	
Opposing Platoon Ratio, Rpo	1	
Lost time per phase, tl	3	
gf=Gexp(-0.882*LTC^0.717)-t1	0.00	
Opposing Queue Ratio: qro=1-Rpo(go/C)	0.64	
gq = Volc * qro / (.5 - Volc * (1 - qro) / go)-tl	1.27	
gu=g-gq (or g-gf)	30.73	
fs=(875-0.625Vo)/1000	0.72	
Pl=Plt[1+{(N-1)g/(fsgu+4.5)}]	1.00	
Ell fmin	1.86 0.13	
fm,(min=fmin;max=1.00)	0.52	
flt=[fm+0.91(N-1)]/N	0.52	
11C-[1m+0.91(N-1)]/N	0.52	
APPROACH	SB	
Cycle Length, C	90	
Cycle Length, C Actual Green Time for Lane Group, G	90 30	
Cycle Length, C Actual Green Time for Lane Group, G Effective Green Time for Lane Group, g	90 30 32	
Cycle Length, C Actual Green Time for Lane Group, G Effective Green Time for Lane Group, g Opposing Effective Green Time, go	90 30 32 32	
Cycle Length, C Actual Green Time for Lane Group, G Effective Green Time for Lane Group, g Opposing Effective Green Time, go Number of Opposing Lanes, No	90 30 32 32 2	
Cycle Length, C Actual Green Time for Lane Group, G Effective Green Time for Lane Group, g Opposing Effective Green Time, go Number of Opposing Lanes, No Number of Lanes in Lane Group, N	90 30 32 32 2 1	
Cycle Length, C Actual Green Time for Lane Group, G Effective Green Time for Lane Group, g Opposing Effective Green Time, go Number of Opposing Lanes, No Number of Lanes in Lane Group, N Adjusted Left-Turn Flow Rate, Vlt	90 30 32 32 2 1 17	
Cycle Length, C Actual Green Time for Lane Group, G Effective Green Time for Lane Group, g Opposing Effective Green Time, go Number of Opposing Lanes, No Number of Lanes in Lane Group, N Adjusted Left-Turn Flow Rate, Vlt Proportion of Left Turns in Lane Group, Plt	90 30 32 32 2 1 17 1.00	
Cycle Length, C Actual Green Time for Lane Group, G Effective Green Time for Lane Group, g Opposing Effective Green Time, go Number of Opposing Lanes, No Number of Lanes in Lane Group, N Adjusted Left-Turn Flow Rate, Vlt Proportion of Left Turns in Lane Group, Plt Left Turns per Cycle: LTC=Vlt*C/3600	90 30 32 32 2 1 17 1.00 0.43	
Cycle Length, C Actual Green Time for Lane Group, G Effective Green Time for Lane Group, g Opposing Effective Green Time, go Number of Opposing Lanes, No Number of Lanes in Lane Group, N Adjusted Left-Turn Flow Rate, Vlt Proportion of Left Turns in Lane Group, Plt Left Turns per Cycle: LTC=Vlt*C/3600 Adjusted Opposing Flow Rate, Vo	90 30 32 32 2 1 17 1.00 0.43 217	
Cycle Length, C Actual Green Time for Lane Group, G Effective Green Time for Lane Group, g Opposing Effective Green Time, go Number of Opposing Lanes, No Number of Lanes in Lane Group, N Adjusted Left-Turn Flow Rate, Vlt Proportion of Left Turns in Lane Group, Plt Left Turns per Cycle: LTC=Vlt*C/3600 Adjusted Opposing Flow Rate, Vo Opposing Flow per Lane, Per Cycle: Volc=VoC/3600No	90 30 32 32 2 1 17 1.00 0.43 217 2.71	
Cycle Length, C Actual Green Time for Lane Group, G Effective Green Time for Lane Group, g Opposing Effective Green Time, go Number of Opposing Lanes, No Number of Lanes in Lane Group, N Adjusted Left-Turn Flow Rate, Vlt Proportion of Left Turns in Lane Group, Plt Left Turns per Cycle: LTC=Vlt*C/3600 Adjusted Opposing Flow Rate, Vo Opposing Flow per Lane, Per Cycle: Volc=VoC/3600No Opposing Platoon Ratio, Rpo	90 30 32 32 2 1 17 1.00 0.43 217 2.71	
Cycle Length, C Actual Green Time for Lane Group, G Effective Green Time for Lane Group, g Opposing Effective Green Time, go Number of Opposing Lanes, No Number of Lanes in Lane Group, N Adjusted Left-Turn Flow Rate, Vlt Proportion of Left Turns in Lane Group, Plt Left Turns per Cycle: LTC=Vlt*C/3600 Adjusted Opposing Flow Rate, Vo Opposing Flow per Lane, Per Cycle: Volc=VoC/3600No Opposing Platoon Ratio, Rpo Lost time per phase, tl	90 30 32 32 2 1 17 1.00 0.43 217 2.71 1	
Cycle Length, C Actual Green Time for Lane Group, G Effective Green Time for Lane Group, g Opposing Effective Green Time, go Number of Opposing Lanes, No Number of Lanes in Lane Group, N Adjusted Left-Turn Flow Rate, Vlt Proportion of Left Turns in Lane Group, Plt Left Turns per Cycle: LTC=Vlt*C/3600 Adjusted Opposing Flow Rate, Vo Opposing Flow per Lane, Per Cycle: Volc=VoC/3600No Opposing Platoon Ratio, Rpo Lost time per phase, tl gf=Gexp(-0.882*LTC^0.717)-tl	90 30 32 32 2 1 17 1.00 0.43 217 2.71 1 3	
Cycle Length, C Actual Green Time for Lane Group, G Effective Green Time for Lane Group, g Opposing Effective Green Time, go Number of Opposing Lanes, No Number of Lanes in Lane Group, N Adjusted Left-Turn Flow Rate, Vlt Proportion of Left Turns in Lane Group, Plt Left Turns per Cycle: LTC=Vlt*C/3600 Adjusted Opposing Flow Rate, Vo Opposing Flow per Lane, Per Cycle: Volc=VoC/3600No Opposing Platoon Ratio, Rpo Lost time per phase, tl gf=Gexp(-0.882*LTC^0.717)-tl Opposing Queue Ratio: qro=1-Rpo(go/C)	90 30 32 32 2 1 17 1.00 0.43 217 2.71 1 3 0.00 0.64	
Cycle Length, C Actual Green Time for Lane Group, G Effective Green Time for Lane Group, g Opposing Effective Green Time, go Number of Opposing Lanes, No Number of Lanes in Lane Group, N Adjusted Left-Turn Flow Rate, Vlt Proportion of Left Turns in Lane Group, Plt Left Turns per Cycle: LTC=Vlt*C/3600 Adjusted Opposing Flow Rate, Vo Opposing Flow per Lane, Per Cycle: Volc=VoC/3600No Opposing Platoon Ratio, Rpo Lost time per phase, tl gf=Gexp(-0.882*LTC^0.717)-tl Opposing Queue Ratio: qro=1-Rpo(go/C) gq = Volc * qro / (.5 - Volc * (1 - qro) / go)-tl	90 30 32 32 2 1 17 1.00 0.43 217 2.71 1 3 0.00 0.64 0.72	
Cycle Length, C Actual Green Time for Lane Group, G Effective Green Time for Lane Group, g Opposing Effective Green Time, go Number of Opposing Lanes, No Number of Lanes in Lane Group, N Adjusted Left-Turn Flow Rate, Vlt Proportion of Left Turns in Lane Group, Plt Left Turns per Cycle: LTC=Vlt*C/3600 Adjusted Opposing Flow Rate, Vo Opposing Flow per Lane, Per Cycle: Volc=VoC/3600No Opposing Platoon Ratio, Rpo Lost time per phase, tl gf=Gexp(-0.882*LTC^0.717)-tl Opposing Queue Ratio: qro=1-Rpo(go/C) gq = Volc * qro / (.5 - Volc * (1 - qro) / go)-tl gu=g-gq (or g-gf)	90 30 32 32 2 1 17 1.00 0.43 217 2.71 1 3 0.00 0.64 0.72 31.28	
Cycle Length, C Actual Green Time for Lane Group, G Effective Green Time for Lane Group, g Opposing Effective Green Time, go Number of Opposing Lanes, No Number of Lanes in Lane Group, N Adjusted Left-Turn Flow Rate, Vlt Proportion of Left Turns in Lane Group, Plt Left Turns per Cycle: LTC=Vlt*C/3600 Adjusted Opposing Flow Rate, Vo Opposing Flow per Lane, Per Cycle: Volc=VoC/3600No Opposing Platoon Ratio, Rpo Lost time per phase, tl gf=Gexp(-0.882*LTC^0.717)-tl Opposing Queue Ratio: qro=1-Rpo(go/C) gq = Volc * qro / (.5 - Volc * (1 - qro) / go)-tl gu=g-gq (or g-gf) fs=(875-0.625Vo)/1000	90 30 32 32 2 1 17 1.00 0.43 217 2.71 1 3 0.00 0.64 0.72 31.28 0.74	
Cycle Length, C Actual Green Time for Lane Group, G Effective Green Time for Lane Group, g Opposing Effective Green Time, go Number of Opposing Lanes, No Number of Lanes in Lane Group, N Adjusted Left-Turn Flow Rate, Vlt Proportion of Left Turns in Lane Group, Plt Left Turns per Cycle: LTC=Vlt*C/3600 Adjusted Opposing Flow Rate, Vo Opposing Flow per Lane, Per Cycle: Volc=VoC/3600No Opposing Platoon Ratio, Rpo Lost time per phase, tl gf=Gexp(-0.882*LTC^0.717)-tl Opposing Queue Ratio: qro=1-Rpo(go/C) gq = Volc * qro / (.5 - Volc * (1 - qro) / go)-tl gu=g-gq (or g-gf) fs=(875-0.625Vo)/1000 Pl=Plt[1+{(N-1)g/(fsgu+4.5)}]	90 30 32 32 2 1 17 1.00 0.43 217 2.71 1 3 0.00 0.64 0.72 31.28 0.74 1.00	
Cycle Length, C Actual Green Time for Lane Group, G Effective Green Time for Lane Group, g Opposing Effective Green Time, go Number of Opposing Lanes, No Number of Lanes in Lane Group, N Adjusted Left-Turn Flow Rate, Vlt Proportion of Left Turns in Lane Group, Plt Left Turns per Cycle: LTC=Vlt*C/3600 Adjusted Opposing Flow Rate, Vo Opposing Flow per Lane, Per Cycle: Volc=VoC/3600No Opposing Platoon Ratio, Rpo Lost time per phase, tl gf=Gexp(-0.882*LTC^0.717)-tl Opposing Queue Ratio: qro=1-Rpo(go/C) gq = Volc * qro / (.5 - Volc * (1 - qro) / go)-tl gu=g-gq (or g-gf) fs=(875-0.625Vo)/1000	90 30 32 32 2 1 17 1.00 0.43 217 2.71 1 3 0.00 0.64 0.72 31.28 0.74 1.00 1.76	
Cycle Length, C Actual Green Time for Lane Group, G Effective Green Time for Lane Group, g Opposing Effective Green Time, go Number of Opposing Lanes, No Number of Lanes in Lane Group, N Adjusted Left-Turn Flow Rate, Vlt Proportion of Left Turns in Lane Group, Plt Left Turns per Cycle: LTC=Vlt*C/3600 Adjusted Opposing Flow Rate, Vo Opposing Flow per Lane, Per Cycle: Volc=VoC/3600No Opposing Platoon Ratio, Rpo Lost time per phase, tl gf=Gexp(-0.882*LTC^0.717)-tl Opposing Queue Ratio: qro=1-Rpo(go/C) gq = Volc * qro / (.5 - Volc * (1 - qro) / go)-tl gu=g-gq (or g-gf) fs=(875-0.625Vo)/1000 Pl=Plt[1+{(N-1)g/(fsgu+4.5)}] El1	90 30 32 32 2 1 17 1.00 0.43 217 2.71 1 3 0.00 0.64 0.72 31.28 0.74 1.00	

Streets: (E-W) Horizon Drive

(N-S) 7th Street

Analyst: JPC

File Name: PROP1996.HC9

Area Type: Other

6-27-96 PM Peak

Comment: 1996 volumes with proposed development

Capacity Analysis Worksheet

Direction /LnGrp	Adj n Flow Rate (v)	Adj Sat Flow Rate (s)	Flow Ratio (v/s)	Green Ratio (g/C)	Lane Group Capacity (c)		
EB							
${f LT}$	19	1853	0.010	0.189	350	0.054	
R	25	1583	0.016	0.189	299	0.084	4
WB							
L	238	3539	0.067	0.356	1258	0.189	
${f LT}$	232	1778	0.130	0.356	632	0.367	×
NB							
L	8	959	0.008	0.356	341	0.023	
${f T}$	217	3725	0.058	0.356	1324	0.164	
SB							
L	17	1035	0.016	0.356	368	0.046	
TR	247	3721	0.066 Sum (0.356 v/s) critical	1323 $= 0.213$	0.187	*
Lost Time	e/Cycle, L =	9.0 sec		cal v/c(x)	= 0.236		

Level of Service Worksheet

Direction /LnGrp			Delay d 1	Adj	Lane Group Cap	d	Delay d 2	Grp	Lane Grp LOS		LOS By App
EB											
LT	0.054	4 0.189	22.7	0.850	350	16	0.0	19.3	3 C	19.4	С
R	0.084	1 0.189	22.9	0.850	299	16	0.0	19.4	l C		
WB											
${f L}$	0.189	0.356	15.2	0.850	1258	16	0.0	13.0) B	13.5	В
LT	0.367	7 0.356	16.3	0.850	632	16	0.2	14.1	L B		
NB											
${f L}$	0.023	3 0.356	14.3	0.850	341	16	0.0	12.2	2 B	12.8	В
${f T}$	0.164	0.356	15.1	0.850	1324	16	0.0	12.8	3 B		
SB											
${f L}$	0.046	0.356			368	16	0.0	12.3	В	12.9	В
TR		0.356		0.850		16	0.0		_		
	3	nterse	ction I	Delay =	= 13.4	sec/v	eh Int	ersec	tion	Los =	В

Center For Microcomputers In Transportation

University of Florida

512 Weil Hall

Gainesville, FL 32611-2083 (904) 392-0378

Streets: (E-W) Horizon Drive

Analyst: JPC

(N-S) 7th Street File Name: PROP2010.HC9 6-27-96 PM Peak Area Type: Other

Comment: 2010 volumes

Traffic and Roadway Conditions

	E	astbo	und	Wes	stbour	nd	No	rthbou	ınd	Sou	ıthbo	und
	L	${f T}$	R	L	${f T}$	R	L	${f T}$	R	L	${f T}$	R
No. Lanes] :	> 1	1	2 >	> 1		1	2		1	2	<
Volumes	4	20	33	578	15		11	268		22	298	4
PHF or PK15	0.95	0.95	0.95	0.95	0.95		0.95	0.95		0.95	0.95	0.95
Lane W (ft)	ĺ	12.0	12.0	12.0	12.0		12.0	12.0		12.0	12.0	
Grade		0			0			0			0	
% Heavy Veh	2	2	2	2	2		2	2		2	2	2
Parking	(Y/N) N		(Y/N)) N		(Y/N)) N		(Y/N)	N	
Bus Stops			0			0			0			0
Con. Peds			0			0	į		0			0
Ped Button	(Y/N)) N		(Y/N)	N		(Y/N)) N		(Y/N)	N	
Arr Type		3	3	3	3		3	3		3	3	
RTOR Vols			0			0			0			0
Lost Time	3.00	3.00	3.00	3.00	3.00		3.00	3.00		3.00	3.00	3.00

Signal Operations

Pha EB	se Combination Left Thru Right Peds	on 1	2 * * *	3	4	NB	Left Thru Right Peds	5 * *	6	7	8
WB	Left Thru Right Peds	*				SB	Left Thru Right Peds	* * *			
NB SB	Right Right					EB WB	Right Right				
Gre Yel	en 3 low/AR	30.0A 15 5.0 5	.0A .0			Gree Yel	en 30 low/AR 5	.0P .0			

Cycle Length: 90 secs Phase combination order: #1 #2 #5

Streets: (E-W) Horizon Drive

Left 22 0.95 23 L Thru 298 0.95 314 TR

Right 4 0.95 4

Analyst: JPC

SB Left (N-S) 7th Street File Name: PROP2010.HC9

23

1.00 0.00

334 0.00 0.01

Area Type: Other

6-27-96 PM Peak

Comment: 2010 volumes

23 1 1.000 1.000 318 2 1.050 1.000

Lane Lane Adj Direc-Adj PHF Vol Lane Grp No. Util Growth Grp Grp Vol Ln Fact Fact Vol tion/ Mvt Prop Prop Mvt Vol ${f LT}$ $\mathbf{E}\mathbf{B}$ Left 4 0.95 4 Thru 20 0.95 21 LT 25 1 1.000 Right 33 0.95 35 R 35 1 1.000 1.000 25 1.000 35 0.16 0.00 0.00 1.00 WB Left 578 0.95 608 L 310 2 1.030 1.000 319 Thru 15 0.95 16 LT 314 1 1.000 1.000 314 1.00 0.00 0.95 0.00 NB Left 11 0.95 12 L 12 1 1.000 1.000 12 1.00 0.00 Thru 268 0.95 282 T 282 2 1.050 1.000 296 0.00 0.00

Volume Adjustment Worksheet

Saturation Flow Adjustment Worksheet

	rection nGrp	Ideal Sat Flow	No. Lns	f W	f HV	f G	f p	f BB	f A	f RT	f LT	Adj Sat Flow
EB												
~-	LT	1900	1	1.00	0.98	1.00	1.00	1.00	1.00	1.00	0.99	1848
	R	1900	1	1.00	0.98	1.00	1.00	1.00	1.00	0.85	1.00	1583
WB												
	L	1900	2	1.00	0.98	1.00	1.00	1.00	1.00	1.00	0.95	3539
	${f LT}$	1900	1	1.00	0.98	1.00	1.00	1.00	1.00	1.00	0.95	1778
NB												
	L	1900	1	1.00	0.98	1.00	1.00	1.00	1.00	1.00	0.42	780
	${f T}$	1900	2	1.00	0.98	1.00	1.00	1.00	1.00	1.00	1.00	3725
SB												
	L	1900	1	1.00	0.98	1.00	1.00	1.00	1.00	1.00	0.46	852
	TR	1900	2	1.00	0.98	1.00	1.00	1.00	1.00	1.00	1.00	3718

Streets: (E-W) Horizon Drive Analyst: JPC (N-S) 7th Street

File Name: PROP2010.HC9

Area Type: Other 6-27-96 PM Peak

Comment: 2010 volumes

Supplemental Permitted LT Worksheet		
APPROACH	NB	
Cycle Length, C	90	
Actual Green Time for Lane Group, G	30	
Effective Green Time for Lane Group, g	32	
Opposing Effective Green Time, go	32	
Number of Opposing Lanes, No	2	
Number of Lanes in Lane Group, N	1	
Adjusted Left-Turn Flow Rate, Vlt	12	
Proportion of Left Turns in Lane Group, Plt	1.00	
Left Turns per Cycle: LTC=Vlt*C/3600	0.30	
Adjusted Opposing Flow Rate, Vo	334	
Opposing Flow per Lane, Per Cycle: Volc=VoC/3600No	4.18	
Opposing Platoon Ratio, Rpo	1 3	
Lost time per phase, tl gf=Gexp(-0.882*LTC^0.717)-tl	0.00	
Opposing Queue Ratio: qro=1-Rpo(go/C)	0.64	
gq = Volc * qro / (.5 - Volc * (1 - qro) / go)-tl	2.93	
gu=g-gq (or g-qf)	29.07	
fs=(875-0.625Vo)/1000	0.67	
Pl=Plt[1+{(N-1)g/(fsgu+4.5)}]	1.00	
E11	2.17	
fmin	0.13	
fm,(min=fmin;max=1.00)	0.42	
flt=[fm+0.91(N-1)]/N	0.42	
APPROACH	an.	
	SB	
Cycle Length, C	90	
Cycle Length, C Actual Green Time for Lane Group, G	90 30	
Cycle Length, C Actual Green Time for Lane Group, G Effective Green Time for Lane Group, g	90 30 32	
Cycle Length, C Actual Green Time for Lane Group, G Effective Green Time for Lane Group, g Opposing Effective Green Time, go	90 30 32 32	
Cycle Length, C Actual Green Time for Lane Group, G Effective Green Time for Lane Group, g Opposing Effective Green Time, go Number of Opposing Lanes, No	90 30 32	
Cycle Length, C Actual Green Time for Lane Group, G Effective Green Time for Lane Group, g Opposing Effective Green Time, go	90 30 32 32 2	
Cycle Length, C Actual Green Time for Lane Group, G Effective Green Time for Lane Group, g Opposing Effective Green Time, go Number of Opposing Lanes, No Number of Lanes in Lane Group, N	90 30 32 32 2 1	
Cycle Length, C Actual Green Time for Lane Group, G Effective Green Time for Lane Group, g Opposing Effective Green Time, go Number of Opposing Lanes, No Number of Lanes in Lane Group, N Adjusted Left-Turn Flow Rate, Vlt	90 30 32 32 2 1 23	
Cycle Length, C Actual Green Time for Lane Group, G Effective Green Time for Lane Group, g Opposing Effective Green Time, go Number of Opposing Lanes, No Number of Lanes in Lane Group, N Adjusted Left-Turn Flow Rate, Vlt Proportion of Left Turns in Lane Group, Plt Left Turns per Cycle: LTC=Vlt*C/3600 Adjusted Opposing Flow Rate, Vo	90 30 32 32 2 1 23 1.00	
Cycle Length, C Actual Green Time for Lane Group, G Effective Green Time for Lane Group, g Opposing Effective Green Time, go Number of Opposing Lanes, No Number of Lanes in Lane Group, N Adjusted Left-Turn Flow Rate, Vlt Proportion of Left Turns in Lane Group, Plt Left Turns per Cycle: LTC=Vlt*C/3600 Adjusted Opposing Flow Rate, Vo Opposing Flow per Lane, Per Cycle: Volc=VoC/3600No	90 30 32 32 2 1 23 1.00 0.57	
Cycle Length, C Actual Green Time for Lane Group, G Effective Green Time for Lane Group, g Opposing Effective Green Time, go Number of Opposing Lanes, No Number of Lanes in Lane Group, N Adjusted Left-Turn Flow Rate, Vlt Proportion of Left Turns in Lane Group, Plt Left Turns per Cycle: LTC=Vlt*C/3600 Adjusted Opposing Flow Rate, Vo Opposing Flow per Lane, Per Cycle: Volc=VoC/3600No Opposing Platoon Ratio, Rpo	90 30 32 32 2 1 23 1.00 0.57 296 3.70	
Cycle Length, C Actual Green Time for Lane Group, G Effective Green Time for Lane Group, g Opposing Effective Green Time, go Number of Opposing Lanes, No Number of Lanes in Lane Group, N Adjusted Left-Turn Flow Rate, Vlt Proportion of Left Turns in Lane Group, Plt Left Turns per Cycle: LTC=Vlt*C/3600 Adjusted Opposing Flow Rate, Vo Opposing Flow per Lane, Per Cycle: Volc=VoC/3600No Opposing Platoon Ratio, Rpo Lost time per phase, tl	90 30 32 32 2 1 23 1.00 0.57 296 3.70 1	
Cycle Length, C Actual Green Time for Lane Group, G Effective Green Time for Lane Group, g Opposing Effective Green Time, go Number of Opposing Lanes, No Number of Lanes in Lane Group, N Adjusted Left-Turn Flow Rate, Vlt Proportion of Left Turns in Lane Group, Plt Left Turns per Cycle: LTC=Vlt*C/3600 Adjusted Opposing Flow Rate, Vo Opposing Flow per Lane, Per Cycle: Volc=VoC/3600No Opposing Platoon Ratio, Rpo Lost time per phase, tl gf=Gexp(-0.882*LTC^0.717)-tl	90 30 32 32 2 1 23 1.00 0.57 296 3.70 1 3	
Cycle Length, C Actual Green Time for Lane Group, G Effective Green Time for Lane Group, g Opposing Effective Green Time, go Number of Opposing Lanes, No Number of Lanes in Lane Group, N Adjusted Left-Turn Flow Rate, Vlt Proportion of Left Turns in Lane Group, Plt Left Turns per Cycle: LTC=Vlt*C/3600 Adjusted Opposing Flow Rate, Vo Opposing Flow per Lane, Per Cycle: Volc=VoC/3600No Opposing Platoon Ratio, Rpo Lost time per phase, tl gf=Gexp(-0.882*LTC^0.717)-tl Opposing Queue Ratio: qro=1-Rpo(go/C)	90 30 32 32 2 1 23 1.00 0.57 296 3.70 1 3 0.00 0.64	
Cycle Length, C Actual Green Time for Lane Group, G Effective Green Time for Lane Group, g Opposing Effective Green Time, go Number of Opposing Lanes, No Number of Lanes in Lane Group, N Adjusted Left-Turn Flow Rate, Vlt Proportion of Left Turns in Lane Group, Plt Left Turns per Cycle: LTC=Vlt*C/3600 Adjusted Opposing Flow Rate, Vo Opposing Flow per Lane, Per Cycle: Volc=VoC/3600No Opposing Platoon Ratio, Rpo Lost time per phase, tl gf=Gexp(-0.882*LTC^0.717)-tl Opposing Queue Ratio: qro=1-Rpo(go/C) gq = Volc * qro / (.5 - Volc * (1 - qro) / go)-tl	90 30 32 32 2 1 23 1.00 0.57 296 3.70 1 3 0.00 0.64 2.20	
Cycle Length, C Actual Green Time for Lane Group, G Effective Green Time for Lane Group, g Opposing Effective Green Time, go Number of Opposing Lanes, No Number of Lanes in Lane Group, N Adjusted Left-Turn Flow Rate, Vlt Proportion of Left Turns in Lane Group, Plt Left Turns per Cycle: LTC=Vlt*C/3600 Adjusted Opposing Flow Rate, Vo Opposing Flow per Lane, Per Cycle: Volc=VoC/3600No Opposing Platoon Ratio, Rpo Lost time per phase, tl gf=Gexp(-0.882*LTC^0.717)-tl Opposing Queue Ratio: qro=1-Rpo(go/C) gq = Volc * qro / (.5 - Volc * (1 - qro) / go)-tl gu=g-gq (or g-gf)	90 30 32 32 32 2 1 23 1.00 0.57 296 3.70 1 3 0.00 0.64 2.20 29.80	
Cycle Length, C Actual Green Time for Lane Group, G Effective Green Time for Lane Group, g Opposing Effective Green Time, go Number of Opposing Lanes, No Number of Lanes in Lane Group, N Adjusted Left-Turn Flow Rate, Vlt Proportion of Left Turns in Lane Group, Plt Left Turns per Cycle: LTC=Vlt*C/3600 Adjusted Opposing Flow Rate, Vo Opposing Flow per Lane, Per Cycle: Volc=VoC/3600No Opposing Platoon Ratio, Rpo Lost time per phase, tl gf=Gexp(-0.882*LTC^0.717)-tl Opposing Queue Ratio: qro=1-Rpo(go/C) gq = Volc * qro / (.5 - Volc * (1 - qro) / go)-tl gu=g-gq (or g-gf) fs=(875-0.625Vo)/1000	90 30 32 32 2 1 23 1.00 0.57 296 3.70 1 3 0.00 0.64 2.20 29.80 0.69	
Cycle Length, C Actual Green Time for Lane Group, G Effective Green Time for Lane Group, g Opposing Effective Green Time, go Number of Opposing Lanes, No Number of Lanes in Lane Group, N Adjusted Left-Turn Flow Rate, Vlt Proportion of Left Turns in Lane Group, Plt Left Turns per Cycle: LTC=Vlt*C/3600 Adjusted Opposing Flow Rate, Vo Opposing Flow per Lane, Per Cycle: Volc=VoC/3600No Opposing Platoon Ratio, Rpo Lost time per phase, tl gf=Gexp(-0.882*LTC^0.717)-tl Opposing Queue Ratio: qro=1-Rpo(go/C) gq = Volc * qro / (.5 - Volc * (1 - qro) / go)-tl gu=g-gq (or g-gf) fs=(875-0.625Vo)/1000 Pl=Plt[1+{(N-1)g/(fsgu+4.5)}]	90 30 32 32 2 1 23 1.00 0.57 296 3.70 1 3 0.00 0.64 2.20 29.80 0.69 1.00	
Cycle Length, C Actual Green Time for Lane Group, G Effective Green Time for Lane Group, g Opposing Effective Green Time, go Number of Opposing Lanes, No Number of Lanes in Lane Group, N Adjusted Left-Turn Flow Rate, Vlt Proportion of Left Turns in Lane Group, Plt Left Turns per Cycle: LTC=Vlt*C/3600 Adjusted Opposing Flow Rate, Vo Opposing Flow per Lane, Per Cycle: Volc=VoC/3600No Opposing Platoon Ratio, Rpo Lost time per phase, tl gf=Gexp(-0.882*LTC^0.717)-tl Opposing Queue Ratio: qro=1-Rpo(go/C) gq = Volc * qro / (.5 - Volc * (1 - qro) / go)-tl gu=g-gq (or g-gf) fs=(875-0.625Vo)/1000 Pl=Plt[1+{(N-1)g/(fsgu+4.5)}] El1	90 30 32 32 2 1 23 1.00 0.57 296 3.70 1 3 0.00 0.64 2.20 29.80 0.69 1.00 2.04	
Cycle Length, C Actual Green Time for Lane Group, G Effective Green Time for Lane Group, g Opposing Effective Green Time, go Number of Opposing Lanes, No Number of Lanes in Lane Group, N Adjusted Left-Turn Flow Rate, Vlt Proportion of Left Turns in Lane Group, Plt Left Turns per Cycle: LTC=Vlt*C/3600 Adjusted Opposing Flow Rate, Vo Opposing Flow per Lane, Per Cycle: Volc=VoC/3600No Opposing Platoon Ratio, Rpo Lost time per phase, tl gf=Gexp(-0.882*LTC^0.717)-tl Opposing Queue Ratio: qro=1-Rpo(go/C) gq = Volc * qro / (.5 - Volc * (1 - qro) / go)-tl gu=g-gq (or g-gf) fs=(875-0.625Vo)/1000 Pl=Plt[1+{(N-1)g/(fsgu+4.5)}]	90 30 32 32 2 1 23 1.00 0.57 296 3.70 1 3 0.00 0.64 2.20 29.80 0.69 1.00	

(N-S) 7th Street

Streets: (E-W) Horizon Drive Analyst: JPC File Name: PROP2010.HC9

Area Type: Other 6-27-96 PM Peak

Comment: 2010 volumes

Capacity Analysis Worksheet

Directior /LnGrp	Adj n Flow Rate (v)	Adj Sat Flow Rate (s)	Flow Ratio (v/s)	Green Ratio (g/C)	Lane Group Capacity (c)	
EB						
${f LT}$	25	1848	0.014	0.189	349	0.072
R	35	1583	0.022	0.189	299	0.117
WB						
L	319	3539	0.090	0.356	1258	0.254
${f LT}$	314	1778	0.177	0.356	632	0.497
NB						
L	12	780	0.015	0.356	277	0.043
${f T}$	296	3725	0.079	0.356	1324	0.223
SB						
L	23	852	0.027	0.356	303	0.076
TR	334	3718	0.090 Sum (0.356 v/s) critical	1322 $1 = 0.289$	0.253
Lost Time	e/Cycle, L =	9.0 sec		cal v/c(x)	= 0.321	

Level of Service Worksheet

Direction /LnGrp		g/C Ratio	d -		Group	Calib d 2	ď -	Lane Grp Del		Ву	LOS By App
EB											
LT	0.072	0.189	22.8	0.850	349	16	0.0	19.4	4 C	19.5	С
R	0.117	0.189	23.0	0.850	299	16	0.0	19.6	5 C		
WB											
L	0.254	0.356	15.6	0.850	1258	16	0.0	13.3	3 B	14.2	В
${f LT}$	0.497	0.356	17.2	0.850	632	16	0.5	15.2	2 C		
NB											
${f L}$		0.356			277	16	0.0		_	13.1	В
${f T}$	0.223	0.356	15.4	0.850	1324	16	0.0	13.1	L B		
SB											
${f L}$		0.356			303				_	13.2	В
TR		0.356						13.3			
]	interse	ction I	elay =	= 13.9	sec/v	reh Int	ersec	ction	LOS =	В

HCS: Unsignalized Intersections Release 2.1c 1996CT.HCO Page 1

Center For Microcomputers In Transportation

University of Florida

512 Weil Hall

Gainesville, FL 32611-2083

Ph: (904) 392-0378

Streets: (N-S) 7th Street (E-W) Horizon Village Ct.

Streets: (N-S) 7th Street
Major Street Direction... NS

major screet birection... Ns

Length of Time Analyzed... 60 (min) Analyst...... JPC

Date of Analysis..... 6/27/96

Other Information......1996 conditions

Two-way Stop-controlled Intersection

	No:	rthbou T	nd R	Sou L	thbou T	ind R	Ea L	stbou T	nd R	We L	stbo T	ound R
No. Lanes Stop/Yield Volumes PHF Grade MC's (%) SU/RV's (%)	0	2 471 .95 -4	1 N 22 .95	1 22 .95	2 218 .95 2	0 N	0	0	0	0 13 .95	> 0	< 0 12 .95
CV's (%) PCE's				1.40						1.10		1.10

Adjustment Factors

Vehicle Maneuver	Critical Gap (tg)	Follow-up Time (tf)
Left Turn Major Road	5.50	2.10
Right Turn Minor Road	5.50	2.60
Through Traffic Minor Road	6.50	3.30
Left Turn Minor Road	7.00	3.40

Worksheet for TWSC Intersection

Step 1: RT from Minor Street	WB	EB
Conflicting Flows: (vph) Potential Capacity: (pcph) Movement Capacity: (pcph) Prob. of Queue-Free State:	248 1037 1037 0.99	
Step 2: LT from Major Street	SB	NB
Conflicting Flows: (vph) Potential Capacity: (pcph) Movement Capacity: (pcph) Prob. of Queue-Free State:	519 903 903 0.96	
Step 4: LT from Minor Street	WB	ЕВ
Conflicting Flows: (vph) Potential Capacity: (pcph) Major LT, Minor TH Impedance Factor:	748 352 0.96	
Adjusted Impedance Factor: Capacity Adjustment Factor due to Impeding Movements Movement Capacity: (pcph)	0.96 0.96 340	

Intersection Performance Summary

Mov	ement	Flow Rate (pcph)	Move Cap (pcph)	Shared Cap (pcph)(Avg. Total Delay sec/veh)	95% Queue Length (veh)	LOS	Approach Delay (sec/veh)
WB	L	15	340 >	503	7.6	0.0		7.6
WB	R	14	1037 >		7.6	0.0	В	7.6
SB	L	32	903		4.1	0.0	A	0.4
		_						

Intersection Delay = 0.4 sec/veh

HCS: Unsignalized Intersections Release 2.1c 2010CT.HC0 Page 1

Center For Microcomputers In Transportation

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512 Weil Hall

Gainesville, FL 32611-2083

Ph: (904) 392-0378

Streets: (N-S) 7th Street (E-W) Horizon Village Ct.

Major Street Direction.... NS

Length of Time Analyzed... 60 (min)

Analyst.................................JPC

Date of Analysis..... 6/27/96

Other Information.....2010 conditions

Two-way Stop-controlled Intersection

	Nor	thbou	ind	 Sou	thbou	ind	Eas	stbour	 nd	 We	stb	ound
	L	T	R	L	T	R	L	T	R	L	\mathbf{T}	R
No. Lanes Stop/Yield	0	2	1 N	1	2	0 N	0	0	0	0	> 0	< 0
Volumes PHF Grade MC's (%)		651 .95 -4	24 .95	24 .95	302 .95 2	•				13 .95		.95 0
SU/RV's (%) CV's (%) PCE's				1.40						1.10)	1.10

Adjustment Factors

Vehicle	Critical	Follow-up
Maneuver	Gap (tg)	Time (tf)
Left Turn Major Road	5.50	2.10
Right Turn Minor Road	5.50	2.60
Through Traffic Minor Road	6.50	3.30
Left Turn Minor Road	7.00	3.40

Worksheet for TWSC Intersection

342 929 929 0.98	EB
929 929 0.98	
SB N	IB
710 713 713 0.95	
WB E	EB
1028 233 0.95 0.95 0.95	·
	WB E 1028 233 0.95 0.95

Intersection Performance Summary

Mov	ement	Flow Rate (pcph)	Move Cap (pcph)	Shared Cap (pcph)(Avg. Total Delay sec/veh)	95% Queue Length (veh)	LOS	Approach Delay (sec/veh)
WB	L	15	222 >				_	
WB	R	14	929 >	351	11.2	0.2	С	11.2
SB	L	35	713		5.3	0.0	В	0.4

Intersection Delay = 0.4 sec/veh

HORIZON VILLAGE

Two Directional Available Gaps for a 15-Minute Period Between 5 and 5:15 p.m.

6-9	Seconds	9-13 Seconds	Over 13 Seconds
	22	16	19
	22	10	19

Total Available Gaps 57

Calculated by Jeff Crane July 23, 1996

F. CONCLUSIONS and RECOMMENDATIONS

The intersection of proposed Horizon Village Court and North 7th Street has been designed to provide as much sight distance as possible. A sight zone triangle at the intersection will be designed to allow a minimum of 60' along 7th Street and 50' along Horizon Village Ct. at the flowlines with no sight obscuring signs, walls, fences or foliage more than 30" high. 7th Street is classified as a minor arterial with a design speed of 35 mph. The required safe sight distance left is 300' while the required safe sight distance right is 350'. The existing sight distance left from the proposed access looking south on 7th Street is 520' and well within City requirements. The proposed access road is located 380' south of the intersection of 7th Street and Horizon Drive, however, sight distance extends considerably beyond that. Although a 52' right-of-way at the entrance is not required, it will be constructed for added safety and ease of access.

Acceleration or deceleration lanes associated with this proposed development are also not warranted by the City's <u>Transportation Engineering Design Standards</u>. However, due to the grade and volume of traffic heading north on 7th from Patterson toward the proposed access road, a 60' right turn deceleration lane will be constructed south of the beginning of the curb return radius into the development with a 60' taper leading into that lane. The lane width will be 10' wide. The beginning of the taper into the right turn lane at the intersection of 7th Street and Horizon Drive starts approximately 20' north of the centerline of the proposed access road. Therefore, the north curb return flowline of the access road will be constructed to line up with the east flowline of the existing right turn lane to allow for a smooth transition toward Horizon Drive and still allow plenty of distance for the very small percentage of northbound trip ends exiting the development to continue north on 7th.

Analysis of the intersection of Horizon Drive and 7th Street indicates no change in the level of service due to the impacts of the proposed development. The level of service remained at a 'B' level before and after development. By projecting the increase in volumes due to a 2.2% growth rate in the area, the level of service for the westbound left turn lanes on Horizon Drive decreased to a level of 'C' for the year 2010. The remaining lanes continued a level of service of 'B'.

Analysis of the intersection of Horizon Village Court and North 7th Street indicates a comfortable level of service of 'B' for traffic exiting and a level of service of 'A' for traffic entering the development. Projected analysis for the year 2010 suggests a decrease of one level for each direction.

A total of 57 available gaps for left turn movements out of the development had been counted for a 15 minute period during the PM peak hour. The volume of traffic projected to turn left at peak hour is 13. If the volume of traffic projected to enter from the cross street is less than ½ of the number of gaps available than no additional traffic control is necessary. Consequently, sufficient gaps exist and additional signal analysis will not be required.



LANDESIGN

259 Grand Avenue GRAND JUNCTION, CO 81501 (970) 245-4099 FAX (970) 245-3076

JOB 96045.40	
SHEET NO	OF
CALCULATED BY PC	DATE 6/28/96
CHECKED BY	, ,
CENTERLINE PROFILE	7TH STREET

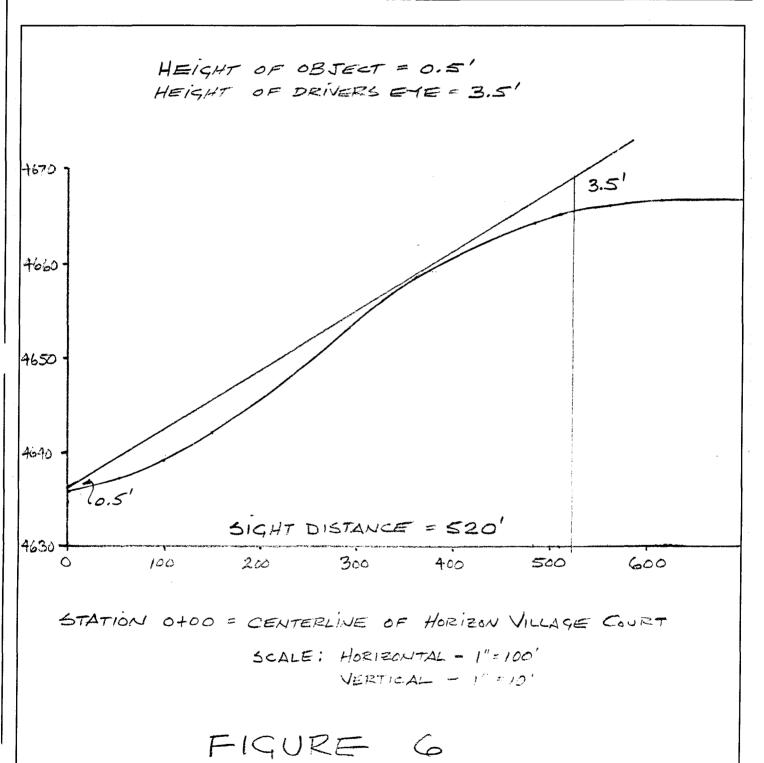


Table 16: Sight Distance (ft.) for Passenger Cars

Exiting from Private Accesses or

Public Streets onto Two-Lane Roads

Speed (MPH)	Safe Sight Distance Left (d1) *	Safe Sight Distance Right ¹ (d ²)*
20	150	130
25	240	200
30	350	260
35	430	350
40	530	440
45	610	570
50	740	700
55	830	860
60	950	1050

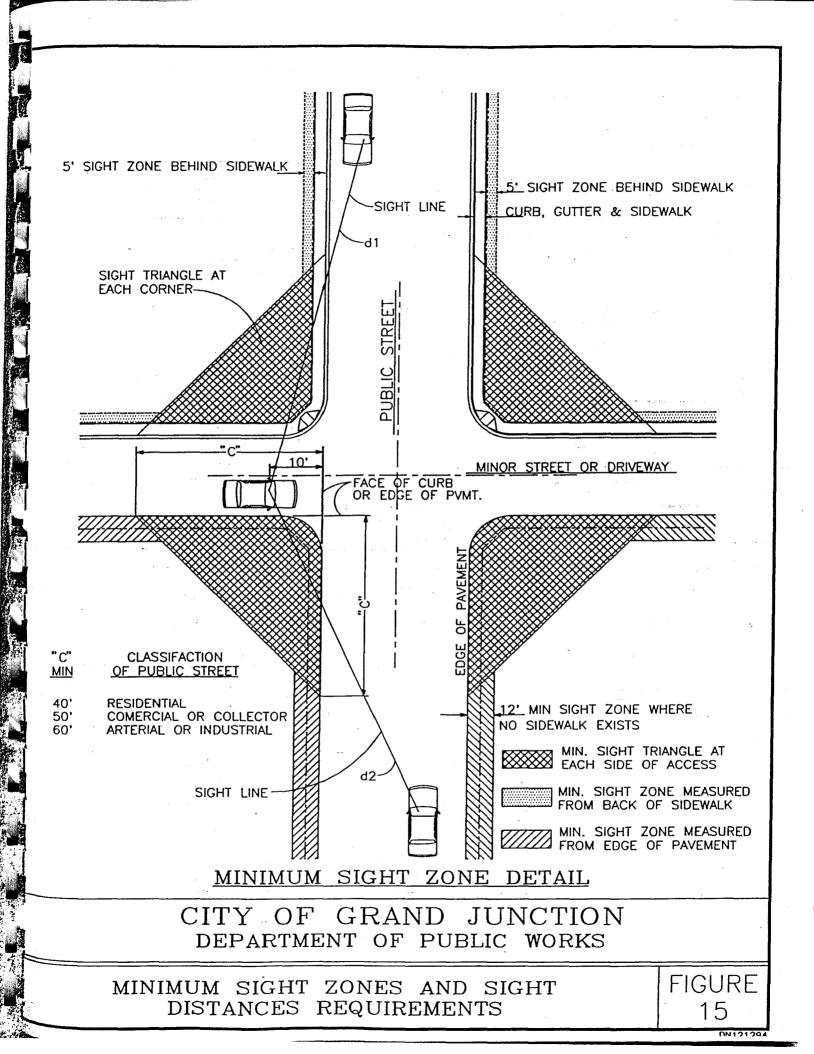
¹ Measured from the driver's eye ten feet back of the flowline or pavement edge.

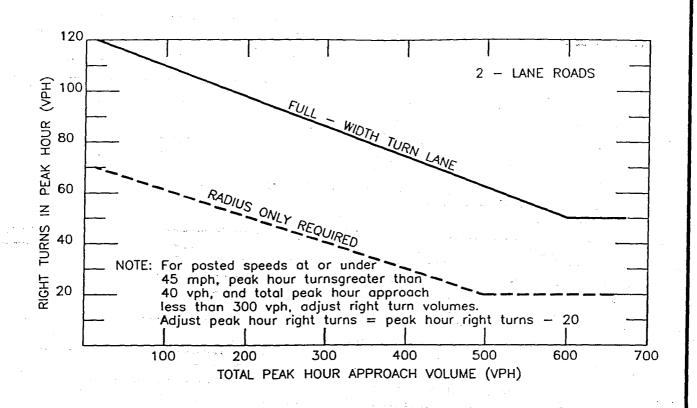
Table 17: Sight Distance (Ft.) for Passenger Cars Exiting From Private Accesses or Public Streets onto Four and Six Lane Roads

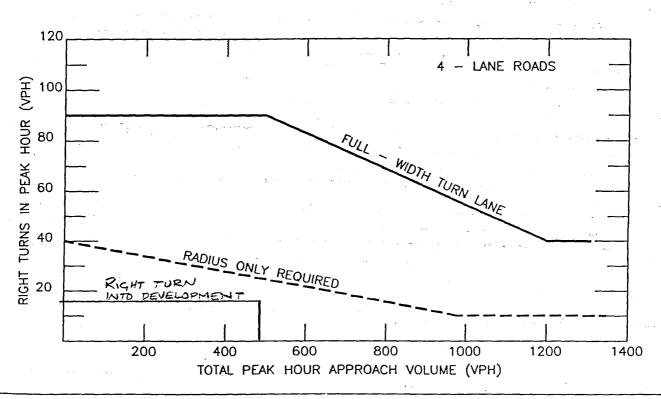
Speed (MPH)	Safe Sight Distance Left (d1)*	Safe Sight Distance Right ¹ (d ²)*
20	130	130
25	180	200
30	220	260
35	300	350
40	380	440
45	500	570
50	620	700
55	760	860
60	950	1050

¹ Measured from the driver's eye ten feet back of the flowline or pavement edge to a vehicle in the outside lane.

^{*} See Figure 15 in Appendix 11.7, Design Aids.







CITY OF GRAND JUNCTION DEPARTMENT OF PUBLIC WORKS

VOLUME WARRANTS FOR RIGHT TURN DECELERATION LANES ON CITY STREETS

FIGURE 2

2- JAN-96 T IP_PROJECT_DETAIL

Capital Improvement Project 10 Year Detail Listing

Capital Improvement Project Title

HORIZON DRIVE: 7TH ST. TO 12TH ST.

Project Number: 6000042

Public Works :partment:

Division:

Projects & Engineering

Submitted By: Don Newton: 10-yr. CIP

'oject Type: Streets, Traffic & Drain

Project Need: Expansion

Begin Date: 1/2000

End Date: 12/9999

early Expenditures	1996	1997	1998	1999	2000	2001	2002	2003	2004	2005	2006	TOTAL
Original Budget Amount	o	0	0	0	0	1,087,000	0	0	0	0	. 0	1,087,000
Adjusted Budget Amount	0	0	0	0	0	0	0	0	O	. 0	0	
Revised Budget Amount	0	0	0	0	0	0	0	0	0	0	O	

oject Narrative:

his project is the reconstruction and widening of Norizon Drive to minor arterial urban standard (5 lanes) from 7th Street to 12th Street. Adequate right of way exists or the this improvement.



NORTHBOUND THRU

This is Report Line Number One This is Report Line Number Two Volume by Lane Report - D0606001.PRN

5-1996 07:48 Pq 1 Id: 000000000010 Fmt: 300 - Imperial Int: 15 Min. Sta: 00000000000001 CId: 01 Start: Thu - Jun 06, 1996 at 10:45 End: Thu - Jun 06, 1996 at 24:00 City/Town: County: File: D0606001.PRN Location: Ln1-North Ln2-North Thu - Jun 6, 1996 Total Lane 11:00 11:15 11:30 11:45 12:00 12:15 12:30 12:45 13:00 ୀ3**:**15 13:30 13:45 14:00 14:15 14.45 15:00 15:15 15:30 15:45 16:00 . 82 16:15 16:30 16:45 **17:00** 17:15 17:30 17:45 18:00 18:15 18:30 **18:45** 19:00 19:15

19:30

19:45

20:00

This is Report Line Number One This is Report Line Number Two Volume by Lane Report - D0606001.PRN

_	
_5-1996	
fun 6	16

07:48 Pg 2

I [*] e	1	2	Total
20:15	20	23	43
2^·30	22	30	52
245 21:00	29	25	54
21:00	27	31	58
21:15	29	42	71
2 30	32	38	70
2 30 2 45	26	28	54
22:00	27	22	49
2.* 15	18	23	41
2: 15 2: 30 22:45	16	13	29
2:45	13	21	.34
3.00	7	14	21
25-15 3 -3 0	7	8	15
2∰30	10	8	18
3:45	15	16	31
?⊬)0	7	4	11
	=====	=====	22222
aily Totals	682	2986	3668
entages	18.59	81.41	

'East

This is Report Line Number One This is Report Line Number Two Volume by Lane Report - D0606001.PRN

_5-1996

07:48 Pg 3

CId: 01

Fmt: 300 - Imperial Int: 15 Min.

End: Thu - Jun 06, 1996 at 24:00

Start: Thu - Jun 06, 1996 at 10:45

County:

City/Town: Location:

File: D0606001.PRN

Ln1-North Ln2-North

Station Data Summary

Lane	1	2	Total
Grand Totals Percentages		2986	3668
Percentages	18.59	81.41	

Am/Pm Peak Hour Totals

1 2 Total Am Hour 11-12 1 324 325 entages 0.15 10.85 8.86 rm flour 17-18 4 425 429 Percentages 0.59 14.23 11.70

NORTHBOUND THRU

This is Report Line Number One This is Report Line Number Two

∠5-1996 Volume by Lane Report - D0607001.PRN

07:57 Pg 1

Sta: 000000000001 Start: Fri - Jun 07, 199 City/Town:	Id: 00000000010 6 at 00:00		300 - Imperial Int: 15 Min. End: Fri - Jun 07, 1996 at 24:0			
Ln1-North Ln2-North		rile: DU6U/UUI.PKN				
Fri - Jun 7, 1996						
Lane	1	2	Total			
00:15	8	9	17			
00 :3 0	1	3	4			
ీ∩∩ • 45	4	7	11			
01:00	<u>.</u>	2	3			
01:15	3	4	7			
01:30	3	4	7			
01:45	1	3	, A			
02:00	Ď	3	· 1			
₹ 02:15	3	2	» К			
4 02:13 4 02:30	1	2	3			
02:30 02:45	2		7			
03:00	1	τ Λ	,			
03:15	1	2	2			
03.13	1	2				
Ua:45	1	1	1			
04:00	0	1	1			
		0	1			
04:15	3	0	4			
04:30	3	0	3			
04:45	2	0	2			
05:00		3	. 9			
05:15	2	1	3			
05:30	7	3	10			
05:45	12	/	19			
06:00	14	6	20			
06:15	12	10	22			
06:30	17	13	30			
06:45	16	11	27			
07:00	29	15	44			
07:15 07:30	18	14	32			
107:30	31	19	50			
07:45	54	33	87			
08:00	91 51	35	126			
08:15	51	26	77			
08:30	52	17	69			
08:45	44	28	72			
09:00	62	32	94			
09:15	48	32	80			

Fri - Jun 7, 1996

Lane	1	2	Total
09:30	34	29	63
09:45	50	40	90
09:45 10:00	32	35	67
10:15	29	48	77
10:30	43	57	100
10:45 11:00	29	68	97
11:00	28	72	100
11:15	12	67	79
11:30 1:45	16	72	88
1:45	11	107	118
12:00	11	127	138
12:15	11	124	135
2:30 12:45	7	110	117
12:45	16	95	111
13:00	11	79	90
3:15	14	95	109
13:30	7	91	98
13:45	11	96	107
**•00	8 5 0	87	95
.5	5	95	100
14:30	0	92	92
14:45	2	93	95
5:00 5:15	6	90	96
15:15	8	76 70	84
15:30	1	79 06	80
5:45	. 0	96 26	· 96
6:00	8	96	104
16:15 46:30	3	105 89	108
	9 6		98
6:45 17:00	5	110 98	116
17:15	5 8	110	103 118
↑/:13 ↑/:30	17	98	115
7:30 7:45	26	94	120
18:00	33	77	110
£3:15	30	68	98
3:30	27	68	95
3:30 18:45	27	47	74
19:00	36	51	87
9:15	45	37	82
2 :30	32	39	71
19:45	31	31	62
):00	27	35	62

This is Report Line Number One This is Report Line Number Two lume by Lane Report - D0607001.PR

υ ο-25-1 996	Volume by Lane Report - D0607001.PRN		07:57 Pg 3
Fri - Jun 7, 1996			
Lane	1	2	Total
20:15	32	35	67
20:13	28	31	59
20:30 20:45	22	25	47
21:00	32	36	68
21:15	48	39	87
21:30	31	42	73
21:45	31	35	66
22:00	18	19	37
22:15	33	29	62
22:30	24	20	44
22:45	25	26	. 51
	19	13	32
23:00 23:15	15	23	38
23:30	15	16	31
23:45	15	15	30
24:00	9	7	16
	223222	*****	=====
raily Totals	1775	4136	5911
Jentages	30.03	69.97	

This is Report Line Number One This is Report Line Number Two Volume by Lane Report - D0607001.PRN

₩ Uo-25-1996

07:57 Pg 4

CId: 01

Fmt: 300 - Imperial Int: 15 Min.

Start: Fri - Jun 07, 1996 at 00:00

End: Fri - Jun 07, 1996 at 24:00

City/Town:

County:

File: D0607001.PRN

Location:

Ln1-North Ln2-North

Station Data Summary

Lane	1	2	Total
Grand Totals Percentages	_,,,	4136 69.97	5911

Am/Pm Peak Hour Totals

1 2 Total ²- Hour 11-12 50 373 423 entages 2.82 9.02 7.16 Pm Hour 17-18 84 379 463

4.73 9.16 7.83 Percentages

NORTHBOUND THRU

This is Report Line Number One This is Report Line Number Two Volume by Lane Report - D0608001.PRN

UU-25-1996 08:01 Pg 1 Id: 000000000010 Int: 15 Min. CId: 01 Fmt: 300 - Imperial Sta: 0000000000001 Start: Sat - Jun 08, 1996 at 00:00 End: Sat - Jun 08, 1996 at 24:00 City/Town: County: File: D0608001.PRN Location: Ln1-North Ln2-North Sat - Jun 8, 1996 2 Total 1 Lane 7 7 14 00:15 00:30 10 12 22 7 11 00:45 **01:00** 7 01:15 13 *3 01:30 9 01:45 11 02:00 8 02:15 4 02:30 1 2 02:45 2 2 03:00 ີ່^າ·15 0 03:45 04:00 04:15 04:30 1 0 04:45 1 1 305:00 **05:15** 3 05:30 3 3 6 11 * 05:45 14 06:00 12 17 7 5 12 06:15 12 12 06:30 24 7 10 17 06:45 **67:00** 17 11 28 19 7 07:15 26 07:30 13 16 29 **07:45** 25 20 45 30 19 08:00 49 28 16 908:15 44 08:30 34 22 56 08:45 24 17 41 27 09:00 30 57

26

24

50

09:15

Sat - Jun 8, 1996						
Lane	1	2	Total			
09:30	27	20	47			
09:45	26	41	67			
09:45 10:00	32	32	64			
10:15	32	41	73			
10:30	14	35	49			
10:45	23	43	66			
11:00	14	58	72			
11:15	19	50	69			
11:30	11	49	60			
11:45	10	60	70			
12:00	9	71	80			
12:15	14	68	82			
12:30	10	69	79			
12:45	2	67	69			
13:00	1	60	61			
13:15	1	67	68			
13:30	0	48	48			
13:45	3	60	63			
00	0	46	46			
.5	0	65 57	65			
14:30	1	57 57	58			
14:45	1	55 70	56			
15:00	2	70	72			
15:15 15:30	0 0	55	55			
15:45	. 0	64	64			
16:00	5	62	. 62			
16:15	13	102 59	107 72			
16:30		63	68			
16:45	5 3	70	73			
17:00	28	50	78			
17:15	33	33	66			
17:30	33 22	49	71			
17:45	17	35	52			
18:00	23	42	65			
18:15	21	41	62			
18:30	22	44	66			
18:45	32	54	86			
19:00	18	38	56			
19:15	29	36	65			
19:30	38	32	70			
19:45	31	37	68			
20:00	23	14	37			

This is Report Line Number One This is Report Line Number Two

<i>2</i> 5-1996	Volume by Lane Report	08:02 Pg 3	
Sat - Jun 8, 1996			
Lane	1	2	Total
20:15	28	23	51
∴ [®] 20•20	32	27	59
20:45	23	16	39
21:00	23	28	51
21:15	21	33	54
21:30	39	33	72
21:45	31	37	68
22:00	23	24	47
22:15	23	27	50
22:30	22	22	44
22:45	13	18	31
23:00	17	25	42
23:15	21	19	40
23:30	11	11	22
23:45	15	12	27
24:00	8	9	17
	=====	22222	=====
Daily Totals	1326	2866	4192
entages	31.63	68.37	

This is Report Line Number One This is Report Line Number Two Volume by Lane Report - D0608001.PRN

25-1996

08:02 Pg 4

Sta: 0000000000001

Id: 000000000010

CId: 01

Fmt: 300 - Imperial

Int: 15 Min.

End: Sat - Jun 08, 1996 at 24:00

Start: Sat - Jun 08, 1996 at 00:00

County:

City/Town:

File: D0608001.PRN

Location:

Ln1-North Ln2-North

Station Data Summary

1 2 Total 1326 2866 4192 Grand Totals Percentages 31.63 68.37

Am/Pm Peak Hour Totals

Lane		1	2	Total	
Am I	Hour	11-12	49	230	279
	enta	ges	3.70	8.03	6.66
ru f	Hour	12 - 13	27	264	291
Perc	centa	ges	2.04	9.21	6.94

This is Report Line Number One This is Report Line Number Two Volume by Lane Report - D0609001.PRN

25-1996 08:06 Pq 1 Fmt: 300 - Imperial Int: 15 Min. Id: 000000000010 CId: 01 Sta: 000000000001 Start: Sun - Jun 09, 1996 at 00:00 End: Sun - Jun 09, 1996 at 24:00 County: City/Town: Location: File: D0609001.PRN Ln1-North Ln2-North **Sun - Jun 9, 1996** ∃ Lane 1 2 Total 00:15 4 12 16 .00:30 9 9 18 00:45 8 10 18 01:00 7 11 18 01:15 2 10 12 0 3 01:30 3 01:45 10 02:00 5 4 9 3 -02:15 02:30 2 02:45 2 03:00 0 0 03:15 1 ,0 1 Us:45 04:00 0 2 0 04:15 0 04:30 0 1 0 04:45 05:00 2 **05:15** 6 3 05:30 2 5 05:45 4 ₫06:00 12 16 8 06:15 12 06:30 5 11 5 06:45 11 07:00 15 07:15 8 11 07:30 5 6 11 07:45 10 7 17 08:00 13 10 23 08:15 19 6 25 08:30 31 10 41 08:45 26 27 53 09:00 17 21 38

27

49

22

09:15

This is Report Line Number One This is Report Line Number Two Volume by Lane Report - D0609001.PRN

25-1996	Volume by Lane Report		08:07 Pg 3
Sun - Jun 9, 1996			
Lane	1	2	Total
20:15	20	20	40
20:30	16	32	48
20:45	13	21	34
21:00	23	29	52
	23	22	45
21:15 21:30	21	29	50
21:45	13	24	37
22:00	10	18	28
22:00 22:15	14	18	32
22:30	7	7	14
22:45	10	10	20
23:00	7	13	20
23:15	6	4	10
23:30	12	9	21
23:45 24:00	3	7	10
24:00	7	10	17
=======================================	=====	22223	=====
Daily Totals	747	2388	3135
entages	23.83	76.17	

This is Report Line Number One This is Report Line Number Two Volume by Lane Report - D0609001.PRN

25-1996

08:07 Pq 4

Sta: 000000000001

Id: 000000000010

CId: 01

Fmt: 300 - Imperial

Int: 15 Min.

Start: Sun - Jun 09, 1996 at 00:00

End: Sun - Jun 09, 1996 at 24:00

City/Town:

County:

Location:

_Ln1-North Ln2-North

File: D0609001.PRN

Station Data Summary

Lane	1	_	Total
Grand Totals Percentages		2388 76.17	3135

Am/Pm Peak Hour Totals

Lane	1	2	Tota]
Am Hour 10-11	44	229	273
entages	5.89	9.59	8.71
rm Hour 12-13	0	250	250
Percentages	0.00	10.47	7.97

Sun - Jun 9, 1996

Lane	1	2	Total
09:30	33	23	. 56
09:45	18	28	46
10:00	10	25	35
10:15	10	31	41
	.21	57	78
10:30	12	83	95
10:45	1	58	59
11:00	1 2	4 6	48
11:15	2	46	48
11:30	1	54	55
11:45	0	55	55
12:00		71	71
12:15	0	71 79	79
12:30	0	64	64
12:45	0	36	36
13:00	0		55
13:15	1	54	39
13:30	0	39	42
13:45	0	42	48
14:00	0	48	
5	0	35	35
14:30	1	60	61
14:4 5	0	43	43
15:00	0	50	50
15:15	0	33	33
15:30	2	50	52
15:45	. 3	38	. 41
16:00	0	41	41
16:15	0	50	50
16:30	0	41	41
16:45	5	49	54
17:00	11 3	60	71
17:15	3	37	40
17:30	10 7	27	37
17:45		38	45
18:00	8	45	53
18:15	14	40	54
18:30	20	36	56
18:45	10	30	40
19:00	16	35	51
9:15	9	35	44
19:30	22	25	47
19:45	18	24	42
20:00	20	28	48

NORTHBOUND THRU

This is Report Line Number One This is Report Line Number Two Volume by Lane Report - D0610001.PRN

25-1996 08:11 Pg 1 Int: 15 Min. Id: 000000000010 CId: 01 Fmt: 300 - Imperial Sta: 000000000001

Start: Mon - Jun 10, 1996 at 00:00

End: Mon - Jun 10, 1996 at 11:15

County:

City/Town: Location:

File: D0610001.PRN

Ln1-North Ln2-North

Mon - Jun 10, 1996			
Lane	1	2	Total
00:15	1	3	4
00:30	6	5	11
00:45	4	9	13
01:00	2	3	5
01:15	1	3	4
01:30	1		3
a 01:45	0	2 3	3
02:00	0	2	2
02:15	1	0	1
02:30	1	1	
02:45	0	2	2 2
03:00	2	2	4
03:15	1	0	1
0	0	0	0
∪ ∍:4 5	2	3	5
04:00	1	1	5 2
04:15	1	1	2
04:30	0	0	0
04:45	4	2	6
© 05:00	. 3	1	. 4
05:1 5	. 3 8	5	13
05:30	6	5	11
ຼ <u>ິ</u> 05 : 45	13	7	20
06:00	12	8	20
06:15	17	5	22
₃ 06:30	17	19	36 35
06:45	23	12	35
07:00	27	18	45
07:15	30	12	42
07:30	18	17	35 78
07:45	52	26	78
08:00	70	32	102
08:15	47	28	75
08:30	52	31	83
08:45	45	27	72
09:00	60	45	105
09:15	30	43	73

This is Report Line Number One This is Report Line Number Two lume by Lane Report - D0610001.PRN

25-1996	Volume by Lane Report	- D0610001.PRN	08:11 Pg 2	
Mon - Jun 10, 1996				
Lane	1	2	Total	
09:30	25	31	56	
. 09:45	8	61	69	
09:45 10:00	23	65	88	
10:15	25	69	94	
10:30	22	61	83	
10:45	15	67	82	
11:00	13	75	88	
11:15	6	82	88	
	22322	=====		
Daily Totals	695	894	1589	
Percentages	43.74	56.26		

This is Report Line Number One This is Report Line Number Two Volume by Lane Report - D0610001.PRN

25-1996

08:11 Pg 3

Sta: 000000000001

Id: 000000000010

CId: 01

Fmt: 300 - Imperial Int: 15 Min.

End: Mon - Jun 10, 1996 at 11:15

Start: Mon - Jun 10, 1996 at 00:00

County:

🔛 City/Town:

Location:

Ln1-North Ln2-North

File: D0610001.PRN

Station Data Summary

1 2 Total Lane Grand Totals 695 894 1589 Percentages 43.74 56.26

Am/Pm Peak Hour Totals

1 2 Total Am Hour 10-11 75 272 347 'entages 10.79 30.43 21.84

rm Hour None

WESTBOUND

This is Report Line Number One This is Report Line Number Two Volume by Lane Report - D0610002.PRN

25-1996

==============

Daily Totals

Percentages

ne Report - D0610002.PRN 08:11 Pg 1

=====

319

20.42

=====

1562

Sta: 000000000003 Start: Mon - Jun 10, 1996	Id: 00000000010		0 - Imperial Int: 15 Min. End: Mon - Jun 10, 1996 at 24:00
City/Town:		County:	
Location:		File: D0610002.PRN	
Ln1-North Ln2-North			***************************************
Mon - Jun 10, 1996			
Lane	1	2	Total
	= = = = = + + +		
16:15	52	15	67
16:30	65	15	80
16:45	85	26	111
17:00	70	18	88
17:15	91	30	121
17:30	59	21	80
17:45	75 50	18	93
18:00	59 50	18	77
18:15	58 50	15 11	73
18:30 18:45	50 67	15	61
19:00	74	13	82 86
19:15	46	11	57
70	47	10	57
17:45	39	10	49
20:00	32	4	36
20:15	36	8	44
20:30	27	4	31
20:45	18	5	23
³ 21:00	20	4	24
21:15	. 19	6	25
21:30	19	6	25
21:45	24	7	31
22:00	12	3	15
22:15	20	6	26
22:30	8	1	9
~22:45	12	2	14
23:00	11	3	14
23:15	18	6	24
្គ23:30	8	2	10
23:45	16	6	22
24:00	6	1	7

======

1243

79.58

This is Report Line Number One This is Report Line Number Two Volume by Lane Report - D0610002.PRN

_5-1996

08:12 Pg 2

CId: 01

Fmt: 300 - Imperial Int: 15 Min.

Start: Mon - Jun 10, 1996 at 16:00

End: Mon - Jun 10, 1996 at 24:00

County:

City/Town:

File: D0610002.PRN

Location:

Ln1-North Ln2-North

Station Data Summary

1 2 Total Grand Totals 1243 319 1562
Percentages 79.58 20.42

Am/Pm Peak Hour Totals

1 2 Total Man Hour None our 17-18 284 87 371 recentages 22.85 27.27 23.75

WESTBOUND

This is Report Line Number One This is Report Line Number Two Volume by Lane Report - D0611001.PRN

∠5-1996

08:30 Pg 1

Sta: 000000000003 Start: Tue - Jun 11, 1996	Id: 00000000010 at 00:00	End: T	Int: 15 Min. ue - Jun 11, 1996 at 24:00
City/Town:		County:	
Location:		File: D0611001.PRN	
Ln1-North Ln2-North			
Tue - Jun 11, 1996			
Lane	1	2	Total
00:15	3	0	3
00:30	4	2	6
្គ ូ00:45	5	1	6
01:00	6	2	8
01:15	5	1	6
arag 01:30	4	0	4
01:45	3	0	3
02:00	9	3	12
02:15	2	0	2
02:30	6	1	7
02:45	1	. 0	1
03:00	3	1	4
್03:15	0	0	0
'0	0	0	0
Us:45	3	1	4
04:00	1	0	1
04:15	0	0	0
04:30	0	0	0
04:45	1	0	1
_{ુંુ} 05:00	3	1	4
05:15	3	1	· 4
05:30	3	1	4
₃ 05 : 45	6	2	8
06:00	9	3	12
06:15	13	5	18
06:30	19	6	25
06:45	16	6	22
07:00	40	16	56
07:15	38	14	52
07:30	45	16	61
07:45	58	14	72
08:00	65	20	85
08:15	42	16	58
08:30	52 57	17	69
08:45		14	71
09:00	75 71	17	92
09:15	/1	22	93

20:00

46

Tue - Jun 11, 1996			***************************************
Lane	1	2	Total
09:30	60	14	74
09:45	62	14	76
10:00	58	11	69
10:15	65	19	84
10:30	77	24	101
10:45 11:00	59	15	74
11:00	86	26	112
11:15	56	14	70
11:30	75	21	96
11:45	79	21	100
12:00	87	21	108
12:15	91	26	117
12:30 12:45	64	18	82
12:45	69	15	84
13:00	97	23	120
13:15 13:30	80	14	94
13:30	76	20	96
13:45	73	22	95
	62	20	82
5	65	16	81
14:30	69	24	93
14:45	55	11	66
15:00	63	17	80
15: 15	61	20	81
15:30	63	19	82
15:45	64	16	80
16:00	84	25	109
16:15	76	25	101
16:30	86	23	109
16:45	74	25	99
17:00	58	16	74
17:15	58 76	23	99
17:30	65	22	87
17:45	55	16	71
18:00	46	14	60
*18:15	57	13	70
18:30	49	13	62
18:45	39	11	50
19:00	55	16	71
ុំ19:15	40	9	49
19: 30	25	8	33
19:45	39	10	49
20.00	20	7	10

7

39

This is Report Line Number One This is Report Line Number Two Volume by Lane Report - D0611001.PRN

08:30 Pg 3

Tue - Jun 11, 1996			
Lane	1	2	Total
20:15	40	9	49
20:3 0	34	4	38
20:30 20:45	35	5	40
21:00	27	6	33
21:15	31	8	39
21:30	26	7	33
21:45	18	4	22
	9	2	11
22:00 22:15	14	3	17
22:30	18	5	23
22:45	5	1	6
323:00	12	4	16
23:15	11	4	15
23:30	12	2	14
23 :4 5	6	2	8
24:00	4	0	4
	=====	2222	#####
Daily Totals	3752	1026	4778
entages	78.53	21.47	

This is Report Line Number One This is Report Line Number Two Volume by Lane Report - D0611001.PRN

25-1996

08:31 Pg 4

CId: 01

Fmt: 300 - Imperial Int: 15 Min.

End: Tue - Jun 11, 1996 at 24:00

Start: Tue - Jun 11, 1996 at 00:00

County: File: D0611001.PRN

City/Town:
Location:

Ln1-North Ln2-North

Station Data Summary

Lane	1	2	Total
Grand Totals	3752	1026	4778
Percentages	78.53	21.47	

Am/Pm Peak Hour Totals

1 2 Total Am Hour 11-12 297 77 374 entages 7.92 7.50 7.83 rm Hour 12-13 321 82 403 Percentages 8.56 7.99 8.43



This is Report Line Number One This is Report Line Number Two Volume by Lane Report - D0612001.PRN

∠5-1996

08:32 Pg 1

Sta: 000000000003 Start: Wed - Jun 12, 1	Id: 00000000010		al Int: 15 Min. : Wed - Jun 12, 1996 at 24:00
City/Town: Location: Ln1-North Ln2-North		County: File: DO612001.PRN	
Wed - Jun 12, 1996			
Lane	1	2	Total
00:15	4	2	6
00:30	1	0	ı
00:45	5	1	6
01:00	4	0	4
01:15	4	0	4
01:30	4	2	6
01:45	4	0	4
02:00	10	1	11
02:15	5 5	ა ე	8 7
02:30 02:45	5	2	7
03:00	3	1	, A
-03:15	2	1	3
0	3	0	3
Us:45	1	0	1
04:00	2	0	2
04:15	1	0	1
04:30	2	0	2
04:45	2	0	2
05:00	4	1	5
05:15	1	0	1
05:30	2	0	2
05:45	4	1	5
06:00	8	3	11
06:15 06:30	5 22	11	6 33
.06:45	24	7	31
07:00	28	8	36
07:15	37	18	55
97:30	40	12	52
_07 :4 5	62	21	83
08:00	75	26	101
08:15	53	15	68
08:30	54	21	75
08:45	67	23	90
09:00	79	21	100
09:15	72	21	93
and the second s			

Wed - Jun 12, 1996

Lane	1	2	Total
09:30	58	17	75
09:45	43	14	57
10:00	69	22	91
10:15	76	18	94
10:30	67	16	83
10:45	62	17	79
11:00	78	15	93
11:15	61	18	79
11:30	69	17	86
11:45	64	16	80
11:45 12:00	75	20	95
12:15	87	29	116
12:30	85	26	111
12:45	80	21	101
13:00	75	22	97
13:15	76	19	95
13:30	71	23	94
13:45	69	20	89
14:00	80	19	99
· · · · · · · · · · · · · · · · · · ·	74	24	98
1 4:30	78	43	121
14:45	60	42	102
ੂ15:00	61	28	89
15:15	76	22	98
15:30	72	19	91
₋ 15:45	58	17	75
16:00	56	13	. 69
16:15	70	22	92
16:30	61	21	82
16 : 45	71	27	98
17:00	84	26	110
17:15	67	21	88
17:30	57	19	76
17:45	49	14	63
18:00	54	15	69
18:15	58	18	76
18:30	49	10	59
18:45	43	10	53
19:00	56 51	16	72
19:15	51	13	64
19:30	51	12	63
19:45	33	7	40
20:00	25	6	31

This is Report Line Number One This is Report Line Number Two Volume by Lane Report - D0612001.PRN

25-1996

08:32 Pg 3

Wed - Jun 12, 1996			
Lane	1	2	Total
20:15	32	9	41
20:30	28	6	
	20 44	17	34
20:45 21:00			61
	30	11	41
21:15	38	11	49
21:30	25	7	32
21:45	19	5	24
22:00	25	7	32
22:15	10	1	11
22:30	10	3	13
22:45	13	2	15
23:00	14	3	. 17
23:1 5	14	6	20
23:3 0	10	2	12
23:45	10	4	14
24:00	6	3	. 9
=======================================	*****	22222	######################################
Daily Totals	3791	1156	4947
gentages	76.63	23.37	

This is Report Line Number One This is Report Line Number Two Volume by Lane Report - D0612001.PRN

_5-1996

08:33 Pg 4

Sta: 0000000000003

Id: 00000000010

Fmt: 300 - Imperial Int: 15 Min.

Start: Wed - Jun 12, 1996 at 00:00

End: Wed - Jun 12, 1996 at 24:00

County:

City/Town: Location:

Ln1-North Ln2-North

File: D0612001.PRN

Station Data Summary

1 2 Total Grand Totals 3791 1156 4947 Percentages 76.63 23.37

Am/Pm Peak Hour Totals

La	ne		1	2	Total
	Dour	10-11	283	66	349
			203 7,47	5.71	7.05
	enta	•		••••	
		12-13	327	98	425
Pe	rcenta	ges	8.63	8.48	8.59

WESTBOUND TILL 12:00 SOUTHBOUND THEREAFTER

This is Report Line Number One This is Report Line Number Two Volume by Lane Report - D0613001.PRN

∠5-1996 08:34 Pg 1 Id: 00000000010 Fmt: 300 - Imperial Int: 15 Min. Sta: 0000000000003 CId: 01 Start: Thu - Jun 13, 1996 at 00:00 End: Thu - Jun 13, 1996 at 24:00 City/Town: County: Location: File: D0613001.PRN Ln1-North Ln2-North Thu - Jun 13, 1996 Lane 1 2 Total 00:15 6 00:30 3 0 3 JO:45 01:00 3 0 01:15 1 91:30 1 0 D1:45 1 0 **-**02:00 1 02:15 2 0 ි)2:30 1 1 2 02:45 2 0 03:00 2 0 2 03:15 4 0′ 2 2 0 45ء دن 0 0 04:00 0 2)4:15 0 0 0 **4:30** 4 04:45 0 1 **)5:00** 5:15 4 05:30 6 7 **05:45** 3 3)6:00 8 12 06:15 7 10 06:30 18 22)6:45 26 8 34 7:00 38 11 49 07:15 38 15 53 77:30 43 18 61 27:45 69 19 88 08:00 76 18 94 08:15 65 17 82 #8:30 57 15 72

11

21

19

69

101

83

58

80

64

8:45

09:00

™9:15

Thu - Jun 13, 1996

Lane	1	2	Total
09:30	67	22	89
09:45	63	16	79
10:00	71	21	92
10:15	69	19	88
10:30	66	20	86
10:45	64	18	82
11:00	64	15	79
11:15	65	18	83
11:30	64	24	88
11:45	67	23	90
12:00 CHANGE LOC 12:15 SOUTH BOUN	AT/0~ 46	13	59
-10117	**	30	41
12:30	8	27	35
12:45	12	37	49
13:00	17	62	79
13:15	17	43	60
13:30	14	35 24	49
13:45	12	34	46
14:00	7 9	31 25	38 3 4
5		25 36	47
14:30 14:45	11 9	25	34
14.45 15:00	11	41	52
15:15	6	34	40
15:30	5	22	27
15:45	8	28	36
16:00	7	29	36
16:15	11	40	51
16:30	6	36	42
16:45	3	24	27
17:00	3 7	33	40
17:15	11	34	45
17:30	10	35	45
17:45	8	22	30
18:00	10	29	39
18:15	6	31	37
18:30	6	26	32
18:45	3	28	31
19:00	5	29	34
19:15	9	20	29
19:30	4	14	18
19:45	4	15	19
20:00	2	12	14

This is Report Line Number One This is Report Line Number Two Volume by Lane Report - D0613001.PRN

∠5-1996	Volume by Lane Report - D0613001.PRN		08:34 Pg 3	
Thu - Jun 13, 1996				
Lane	1	2	Total	
20:15	0	13	13	
20:30	1	14	15	
20:45	2	11	13	
21:00	2	12	14	
21:15	0	12	12	
	0	11	11	
21:30 21:45	2	11	13	
22:00	2	11	13	
22:15	2	11	13	
22:30	2	8	10	
22:45	0	8	8	
23:00	2	5	7	
23:15 23:30	0	1	1	
23:3 0	0	4	4	
23:45	0	4	4	
24:00	0	4	4	
=======================================	======	=====	=====	

1511

47.03

3213

1702

52.97

Daily Totals

entages

This is Report Line Number One This is Report Line Number Two Volume by Lane Report - D0613001.PRN

25-1996

08:35 Pg 4

CId: 01

Fmt: 300 - Imperial Int: 15 Min.

Start: Thu - Jun 13, 1996 at 00:00

End: Thu - Jun 13, 1996 at 24:00

City/Town:

County:

Location:

Ln1-North Ln2-North

File: D0613001.PRN

Station Data Summary

1 2 Total Grand Totals 1702 1511 3213 Percentages 52.97 47.03

Am/Pm Peak Hour Totals

Lane		1	2	Tota:	
Am	Hour	9-10	265	78	343
	enta	ges	15.57	5.16	10.68
Fμ	Hour	12-13	48	156	204
Per	rcenta	ges	2.82	10.32	6.35



This is Report Line Number One This is Report Line Number Two Volume by Lane Report - D0614001.PRN

_5-1996

09:15

08:39 Pg 1

35

sta: 000000000003 Start: Fri - Jun 14, 1996	Id: 00000000010 at 00:00	CId: 01	Fmt: 300 - Im	perial Int: 15 Min. End: Fri - Jun 14, 1996 at 24:00
City/Town:	40 00000		County:	2. 2. 2. 2. 2. 2. 2. 2. 2. 2. 2. 2. 2. 2
Location:		File:	D0614001.PRN	
Ln1-North Ln2-North				
Fri - Jun 14, 1996				
Lane	1		2	Total
00:15	0		3	3
00:30	0		0	0
00:45	0		0	0
01:00	0		0	0
01:15	0		1	1
01:30	0		2	2
01:45	0		0	0
02:00	0		i	1
02:15	Õ		0	0
02:30	0		1	1
02:45	0		1	1
03:00	0		1	1
03:15	0		ō	0
0	0		0	0
U3:45	0		0	0
04:00	0		Ô	0
04:15	0		1	. 1
04:30	0		0	0
04:45	0		0	0
05:00	0		6	6
05:15	. 0		1	. 1
05:30	0		3	3
,05:45	1		3	4
06:00	0		5	5
06:15	1		5	6
06:30	3		20	23
06:45	4		21	25
07:00	5		27	32
07:15	5 9		25	34
······································	13		30	43
07:45	20		47	67
08:00	18		56	74
08:15	12		47	59
08:30	10		39	49
08:45	16		49	65
09:00	18		44	62
-00+1E			20	25

29

6

19:45

20:00

Fri - Jun 14, 1996 Lane Total 09:30 09:45 10:00 **10:15** 10:30 10:45 **11:**00 11:15 ∍11:30 11:45 12:00 12:15 12:30 12:45 13:00 13:15 13:30 13:45 14:00 14:30 14:45 15:00 15:15 15:30 15:45 16:00 16:15 16:30 16:45 17:00 17:15 17:30 17:45 18:00 18:15 18:30 **18:45** 19:00 19:15 19:30

This is Report Line Number One This is Report Line Number Two Volume by Lane Report - D0614001.PRN

25-1996

08:39 Pg 3

796			
Fri - Jun 14, 1996			
Lane	1	2	Total
20:15	3	17	20
20:30	2	13	15
20:45	0	16	16
21:00	0	9	9
21:15	2	13	15
21:30	2	9	11
21:45	0	6	6
22:00	2	10	12
22:15	1	8	9
22:30	2	6	8
22:45	0	8	8
23:00	0	5	5
23:15	0	3	3
23:30	0	2	2
23:45	1	5	6
24:00	2	7	9
=======================================	*****	2222	======
Daily Totals	482	1836	2318
entages	20.79	79.21	

This is Report Line Number One This is Report Line Number Two Volume by Lane Report - D0614001.PRN

25-1996

08:39 Pg 4

Sta: 000000000003

Id: 000000000010

CId: 01

Fmt: 300 - Imperial Int: 15 Min.

End: Fri - Jun 14, 1996 at 24:00

Start: Fri - Jun 14, 1996 at 00:00

City/Town:

County:

Location:

File: D0614001.PRN

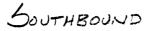
Ln1-North Ln2-North

Station Data Summary

Lane	1	2	Total
Grand Totals Percentages		1836 79.21	2318

Am/Pm Peak Hour Totals

Lane	1	2	Total
Am Hour 8-9	56	179	235
entages	11.62	9.75	10.14
⊦m Hour 12-13	40	135	175
Percentages	8.30	7.35	7.55



This is Report Line Number One This is Report Line Number Two

08:42 Pg 1

25-1996

Volume by Lane Report - D0615001.PRN

Sta: 000000000003 Start: Sat - Jun 15, City/Town: Location: Ln1-North Ln2-North	Id: 00000000010 1996 at 00:00	CId: 01 Fmt: 300 - Imperial End: Sa County: File: D0615001.PRN	Int: 15 Min. t - Jun 15, 1996 at 24:00
Sat - Jun 15, 1996			
Lane	1	2	Total
00:15	0	2	2
₂ 00:30	0	4	4
00:45	1	5	6
01:00	0	2	2
01:15	0	0	0
01:30	1	3	4
01:45	0	1	1
02:00	0	1	1
02:15 02:30	0	0	U
02:45	0	U 1	0
02.45	0	1	0
03:15	0	0	0
,0 	0	0	0
υ 3:4 5	0	0	0
04:00	0	0	0
04:15	0	0	0
04:30	0	0	ů 0
04:45	0	0	0
05:00	. 0	2	. 2
05:15	0	0	0
ୃ05:30	0	1	1
05:45	0	1	1
06:00	1	3	4
₌₌₌ 06:15	0	5	5
06:30	1	5	6
06:45	1	11	12
07:00	1	10	11
07:15	0	6	6
07:30	2	11	13
07:45	3	9	12
_08:00 _08:15	3 8	14	17
08:30	3	21 9	29
08:45	3 A	23	12 27
09:00	7	23 27	
09:15	4	22	34 26
	7	22	20

- Sat - Jun 15, 1996

Lane	1	2	Total
09:30	7	24	31
09:45	1	17	18
10:00	7	24	31
្ត 10:15	5 3 8	21	26
<u> </u>	3	23	26
10:45		27	35
11:00	8	34	42
₃ 11:15	7	27	34
11:30	6	27	33
11:45	4	22	26
§ 12:00	6	23	29
12:15	4	20	24
12:30	3	24	27
. 12:45	7	20	27
13:00	4	31	35
13:15	4	17	21
13:30	4	24	28
§13:45	6 .	20	26
14:00	9	26	35
 5	6	22	28
14:30	1	28	29
14:45	5	24	29
15:00	5	25	30
15:15	5	22	27
₂ 15:30	2	23	25
15:45	7	20	27
16:00	3	16	19
₹16:15	2	. 20	22
16:30	1	19	20
16:45	0	14	14
_17:00	3	10	13
17:15	5	20	25
17:30	6	21	27
17:45	3	23	26
18:00	1	14	15
18:15	2	16	18
18:30		19	22
18:45	3 9 5	15	24
19:00	5	20	25
19:15	0	15	15
19:30	1	15	16
19:45	0	15	15
20:00	2	11	13
-	-		-3

This is Report Line Number One This is Report Line Number Two Volume by Lane Report - D0615001.PRN

25-1996	Volume by Lane Report - D0615001.PRN		08:42 Pg 3
Sat - Jun 15, 1996			
Lane	1	2	Total
20:15	1	11	12
20:30	1	21	22
20:45	0	12	12
21:00	4	18	22
	i	8	9
21:15 21:30	0	11	11
21:45	1	14	15
22:00	0	9	9
22:15	2	9	11
22:30	2	15	17
22:45	0	9	. 9
23:00	1	5	6
23:15	1	9	10
23:30	1	7	8
23:45	0	7	7
24:00	0	7	7
=======================================	ESSEE .	=====	=====
Daily Totals	235	1269	1504
entages	15.63	84.38	

This is Report Line Number One This is Report Line Number Two Volume by Lane Report - D0615001.PRN

25-1996

08:42 Pq 4

sta: 000000000000

Id: 000000000010

CId: 01

Fmt: 300 - Imperial Int: 15 Min.

End: Sat - Jun 15, 1996 at 24:00

Start: Sat - Jun 15, 1996 at 00:00

County:

City/Town:

Location: Ln1-North Ln2-North File: D0615001.PRN

Station Data Summary

Lane	1	2	Total
Grand Totals Percentages		1269 84.38	1504

Am/Pm Peak Hour Totals

1 2 Total Am Hour 10-11 24 105 129 10.21 8.27 8.58 entages Fm Hour 14-15 17 99 116 Percentages 7.23 7.80 7.71



This is Report Line Number One This is Report Line Number Two

25-1996

08:45

09:00

09:15

Volume by Lane Report - D0616001.PRN 08:44 Pg 1

14

25

27

17

28

34

Fmt: 300 - Imperial Sta: 000000000003 Id: 000000000010 CId: 01 Int: 15 Min. Start: Sun - Jun 16, 1996 at 00:00 End: Sun - Jun 16, 1996 at 24:00 City/Town: County: File: D0616001.PRN Location: Ln1-North Ln2-North Sun - Jun 16, 1996 1 2 Total Lane 5 5 00:15 0 0 8 8 00:30 00:45 0 1 1 1 0 01:00 01:15 01:30 0 3 01:45 02:00 02:15 0 0 0 **2:30** 02:45 0 0 0 0 0 0 03:00 0 03:15, 0 0 10 Us:45 1 04:00 04:15 0 1 04:30 1 0 04:45 0 05:00 0 0 0 0 0 05:15 05:30 0 1 0 05:45 1 06:00 0 1 06:15 06:30 **06:45** 3 07:00 5 6 07:15 8 10 07:30 2 17 19 13 07:45 14 7 7 08:00 8 08:15 4 **6**08:30 13 17

3

7

Sun - Jun 16, 1996				
Lane	1	2	Total	
09:30	3	25	28	
09:45	7	19	26	
10:00	3	23	26	
10:15	5	20	25	
10:30 10:45	2	20	22	
10:45	3	30	33	
11:00 11:15	7	24	31	
11:15	7	19	26	
11:30	3	24	27	
11:45	4	20	24	
12:00 12:15 12:30	3	20	23	
12:15	3	20	23	
12:30	2	21	23	
12:45 13:00	1	13	14	
13:00	4	21	25	
13:15	4	15 12	19	
13:30	7 7	17	24	
13:45		19	26	
14:00	3	18	21	
`.5 .20	8 2	28 25	36 27	
14:30	6	25 21	27 27	
14:45 15:00	3	20	23	
15:15	1	20	23 21	
15:13 15:30		14	10	
15:45	5 2	14	. 19 16	
16:00	5	18	23	
16:15	1	15	16	
16:30	5	15	20	
16:45	6	18	24	
17:00	4	19	23	
	3	19	22	
17:30	6	17	23	
17:45	5	20	25	
18:00	7	30	37	
18:15	2	22	24	
18:30	3	15	18	
18:45	2	18	20	
19:00	3	12	15	
19:15	0	17	17	
19:30	ĺ	15	16	
19:45	2	12	14	
20:00	0	18	18	
_		- -	_•	

This is Report Line Number One This is Report Line Number Two Volume by Lane Report - D0616001.PRN

_5-1996 08:45 Pg 3 Sun - Jun 16, 1996 Lane Total 20:15 20:30 20:45 21:00 21:15 21:30 21:45 22:00 22:15 22:30 22:45 23:00 23:15 23:30 23:45 24:00 _____ Daily Totals entages 15.87 84.13

This is Report Line Number One This is Report Line Number Two Volume by Lane Report - D0616001.PRN

_5-1996

08:45 Pg 4

Id: 000000000010 Sta: 000000000003

CId: 01

Fmt: 300 - Imperial Int: 15 Min.

End: Sun - Jun 16, 1996 at 24:00

Start: Sun - Jun 16, 1996 at 00:00

City/Town:

County: File: D0616001.PRN

Location:

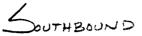
Ln1-North Ln2-North

Station Data Summary

1 2 Total Grand Totals 216 1145
Percentages 15.87 84.13 216 1145 1361

Am/Pm Peak Hour Totals

Lane	1	2	Total
Am Hour 9-10	20	94	114
entages	9.26	8.21	8.38
"rm flour 14-15	19	94	113
Percentages	8.80	8.21	8.30



This is Report Line Number One This is Report Line Number Two Volume by Lane Report - D0617001.PRN

_5-1996

08:46 Pg 1

Sta: 000000000003 Start: Mon - Jun 17, 1996 a City/Town: Location: Ln1-North Ln2-North			Int: 15 Min. Mon - Jun 17, 1996 at 24:00
Mon - Jun 17, 1996			
Lane	1	2	Total
00:15	0	1	1
00:30	1	1	2
00:45	0	0	0
01:00	0	0	0
್ಷ 01:15	0	0	0
01:30	0	1	1
01:45	0	0	0
02:00	0	2	2
02:15	0	3	3
02:30	0	0	0
02:45	0	0	0
03:00	0	0	0
03:15	0	1	1
0	0	0	0
_{ະຄ} ບ ລະ4 5	0	0	0
04:00	0	1	1
04:15	0	0	0
04:30	0	1	1
04:45	0	2	2
05:00	0	3	3
05:15	0	1	1
₅₅ 05:30	0	0	0
05:45	0	3	3
06:00	0	8	8
06:15	2	16	18
06:30	4	22	26
06:4 5	3	13	16
07:00	8	30	38
_. 07:15	8 9	30	39
2 07:30	14	41	55
07:45	10	43	53
08:00	21	56	77
08:15	11	40	51
-08:3 0	12	28	40
08:45	11	39	50
09:00	11	49	60
09:15	13	41	54
_			

Lane	1	2	Total
~;09:30	12	34	46
09:45	7	23	30
10:00	11	31	42
10:15	10	33	43
10:30	7	26	33
10:45	5	18	23
11:00	13	41	54
	14	29	43
11:30	10	35	45
11:45	9	17	26
12:00	16	33	49
12:15	12	30	42
12:30	10	29	39
12:45	4	29	33
13:00	21	40	61
13:15	14	42	56
13:30	14	35	49
13:45	14	42	56
14:00	13	37	50
5	13	25	38
14:30	6	29	35
14:45	6	29	35
15:00	11	28	39
15:15		27	36
15:30	9 7	23	30
15:45	5	27	32
16:00	8	28	36
16:15	12	25	37
16:30	11	36	47
16:45	6	24	30
17:00	13	33	46
17:15	13 9	36	45
17:30	12	36	48
17:45	9	30	39
18:00	4	25	29
18:15	4	25	29
18:30	4	18	22
18:45	2	18	20
19:00	4	26	30
19:15	9	21	30
19:30	5	23	28
19:45	2	13	15
20:00	3	22	25

This is Report Line Number One This is Report Line Number Two Volume by Lane Report - D0617001.PRN

- 5-1996	Volume by Lane Report	- D0617001.PRN	08:46 Pg 3
Mon - Jun 17, 1996			***************************************
Lane	1	2	Total
20:15		17	 17
20:30	Q	21	29
20:45	ર	28	31
21:00	0	13	13
21:15	1	12	13
21:30	4	10	14
21:45	2	10	12
22:00	0	10	10
22:15	ì	8	9
22:30	2	8	10
22:45	0	5	5
* 23:00	0	5	5
23:1 5	1	6	7
23:30	1	5	6
23:45	0	2	2
24:00	0	4	4
	=====	277222	2222
Daily Totals	543	1871	2414
entages	22.49	77.51	5.1.

This is Report Line Number One This is Report Line Number Two

£5-1996

Volume by Lane Report - D0617001.PRN

08:47 Pg 4

Sta: 000000000003

Id: 000000000010

CId: 01

Fmt: 300 - Imperial Int: 15 Min.

End: Mon - Jun 17, 1996 at 24:00

Start: Mon - Jun 17, 1996 at 00:00

County:

City/Town:

File: D0617001.PRN

Location:

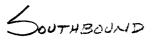
Ln1-North Ln2-North

Station Data Summary

1 2 Total Grand Totals 543 1871 2414 Percentages 22.49 77.51

Am/Pm Peak Hour Totals

La	ne		1	2	Tota]
λn	Hour	7-8	54	170	224
	enta	ges	9.94	9.09	9.28
Lm	Hour	13-14	55	156	211
	rcenta		10.13	8.34	8.74



This is Report Line Number One This is Report Line Number Two Volume by Lane Report - D0618001.PRN 08:48 Pg 1

_5-1996

Sta: 0000000000003 Start: Tue - Jun 18, 1996 a	Id: 000000000010	CId: 01 Fmt: 300 - Imperial End:	Int: 15 Min. Tue - Jun 18, 1996 at 24:00	
City/Town: Location: Ln1-North Ln2-North	•• ••••	County: File: D0618001.PRN		
Tue - Jun 18, 1996				
Lane	1	2	Total	
00:15	0	1	1	
00:30	0	1	1	
00:45	0	1	1	
01:00	0	3	3	
01:15	0	5	5	
01:30	0	1	1	
01:45	0	0	0	
02:00	0	0	0	
02:15	0	0	0	
02:30 02:45	0	0 0	0	
03:00	0	0	0	
03:15	0	0	0	
)	0	0	0	
Ua:45	0	0	0	
04:00	0	0	0	
04:15	0	0	0	
04:30	0	3	3	
04:45	0	0	0	
05:00	0	1	. 1	
05:15	0	3	3	
05:30	0	0	0	
05:45	0	6	6	
06:00 06:15	1	8	10 9	
.06:30	3	18	21	
06:45	4	18	22	
07:00	9	29	38	
07:15	13	33	46	
07:30	11	43	54	
07:45	8	41	49	
08:00	20	50	70	
08:15	22	60	82	
08:30	17	47	64	
08:45	7	30	37	
09:00 09:15	13 9	40 35	53	
M.1.17	J	30	44	

ane Lane	1	2	Total
09:30	•	36	
09:45	8 12	46	44 58
310:00	12	37	49
10:15	11	33	44
10:30	8	24	32
10:45	7	21	28
11:00	12	36	48
11:15	6	28	34
11:130 11:30	7	34	41
11:45	12	25	37
12:00	9	41	50
12:15	5	32	37
12:30	10	18	28
12:45	15	8	23
13:00	15	7	22
13:15	14	11	25
13:30	5	7	12
13:45	13	7	20
14:00	11	9	20
5	11	7	18
14:30	14	, 9	23
14:45	5	4	9
15:00	10	5	15
15:15	3	2	5
15:30	12	9	21
15:45	8	3	11
16:00	7	4	. 11
16:15	6	4	10
16:30	11	4	15
16:45	9	7	16
17:00	9	8	17
17:15	10	6	16
17:30	6	4	10
17:45	11	10	21
17:45 18:00	16	10 7 13	23
18:15	9	13	22
18:30	3	12	15
18:45	5	17	22
19:00	6	14	20
,19:15	4	11	15
19:30	6	18	24
19:30 19:45	5	16	21
20:00	2	12	14

This is Report Line Number One
This is Report Line Number Two
Volume by Lane Report - D0618001.PRN

Lane	1	2	Total

20:15	3	16	19
្ទ20:30	12	9	23
20:45	10	25	35
21:00	2	9	11
21:15	0	11	11
21:30	2	16	18
21:45	2	9	11
22:00	1	9	10
22:15	1	7	8
22:30 22:45	1	4	5
22:45	0	5	5
23:00	0	0	(
23:15	1	4	5
23:30	0	4	4
23:45	1	4	5
24:00	0	1	1
	=====	========	=====
Daily Totals	554	1285	1839
entages	30.13	69.87	

This is Report Line Number One This is Report Line Number Two Volume by Lane Report - D0618001.PRN

25-1996

08:49 Pg 4

Sta: 000000000003

Id: 000000000010

CId: 01

Fmt: 300 - Imperial Int: 15 Min.

End: Tue - Jun 18, 1996 at 24:00

Start: Tue - Jun 18, 1996 at 00:00

City/Town:

County:

Location:

Ln1-North Ln2-North

File: D0618001.PRN

Station Data Summary

Lane	1	2	Total
Grand Totals Percentages	•••	1285 69.87	1839

Am/Pm Peak Hour Totals

1 2 Total 59 177 236 Am Hour 8-9 entages 10.65 13.77 12.83 four 12-13 45 65 110 Percentages 8.12 5.06 5.98

EASTBOUND THEREAFTER

This is Report Line Number One This is Report Line Number Two Volume by Lane Report - D0619001.PRN

25-1996

9001.PRN 08:50 Pg 1

Sta: 000000000003 Start: Wed - Jun 19, City/Town: Location: Ln1-North Ln2-North	, 1996 at 00:00	County: File: D0619001.PRN	Int: 15 Min. d - Jun 19, 1996 at 24:00
Wed - Jun 19, 1996			
Lane	1	2	Total
00:15	0	2	2
00:30	0	0	0
00:45	1	5	6
01:00 01:15	0	3	3
	0	2	2
01:30	1	1	. 2
01:45 02:00	0	0	0
02:00	U	0	0
02:15 202:30	0	1	0
	0	0	0
D2:45 03:00	0	0	0
03:15	0	1	1
★ 0	0	0	0
■ 03:45	0	0	0
04:00	0	0	0
3 24:15	0	0	0
2 04:30	0	0	0
04:45	0	0	0
_{₹0} 05:00	0	3	3
05:15	. 0	3	. 3
05:30	1	1	2
05:45	2	5	7
D6:00	3	4	7
06:15	0	8	8
06:30	2 5	17 21	19 26
96:45	17	31	48
207:00 07:15	12	21	33
07:30	20	26	46
្នី)7:45	· 13	31	44
₩8:00 < CH	ANGE LOCATION 27	56	83
08:15 €A	ASTBOUYD 6	18	24
38:30	1	1	2
D8:45	2	2	4
09:00	0	0	0
09:15	1	3	4

₩ed - Jun 19, 1996

Cane	1	2	Total
09:30	1	2	3
09:45 10:00	6	7	13
10:00	0	0	0
10:15	1	3	4
10:30	5	5	10
10:45	6	7	13
11:00	3	5	8
11:15	5	6	11
11:30 11:45 12:00	6	5	11
11:45	2	4	6
12:00	2	2	4
12:15	1	3	. 4
12:30	2 2	3	5
12:4 5	2	2	4
13:00	0	0	0
13:15	3	5	8
13:15 13:30	2	2	4
13:45	8	10	18
14:00	2	5	7
14:00 5 14:30	4	3	7
14:30	7	10	17
14:45	3	3	6
15:00 15:15	2	6	8
15:15	3	4	7
15:30	2	2	4
15:45	2	2	4
16:00 16:15	2	3	. 5
—16:15	3	4	7
16:30	5	6	11
16:45	0	4	4
17:00	2	5	7
17:15	3	3	6
17:30	1	2 3	3
17:45 18:00	2	3 4	6
18:15	0	0	0
10.13	2	2	4
18:30 18:45	3		7
19:00	3	3	6
19:15	0	0	0
19:30	2	1	3
19:45	2	3	5
20:00	2	4	6
	-	7	U

::::::::::::::::::::::::::::::::::::::	Tolume by bane Repole	2001,001.1141	00.50 19 5
Wed - Jun 19, 1996			
Lane	1	2	Total
3			
20:15	0	0	0
20:30	2	2	4
20:45 21:00	4	6	10
	0	1	1
21:15	3	2	5
21:30	0	2	2
21:45	0	1	1
22:00	1	3	4
22:15	0	1	1
22:30 22:45	1	1	2
22:45	0	1	1
23:00	0	0	0
23:15	0	0	. 0
23:30	0	0	0
23:45	0	0	0
24:00	0	0	0
	=====	====	=====
Daily Totals	238	443	681
entages	34.95	65.05	

This is Report Line Number One This is Report Line Number Two Volume by Lane Report - D0619001.PRN

25-1996

08:51 Pg 4

CId: 01

Fmt: 300 - Imperial Int: 15 Min.

End: Wed - Jun 19, 1996 at 24:00

Start: Wed - Jun 19, 1996 at 00:00

County:

City/Town:

File: D0619001.PRN

Location:

Ln1-North Ln2-North

Station Data Summary

Lane	1	2	Total
Grand Totals	238	443	681
Percentages	34.95	65.05	

Am/Pm Peak Hour Totals

Lane 1 2 Total Am Hour 7-8 72 134 206 entages 30.25 30.25 30.25 ■r_m flour 14-15 16 22 38 Percentages 6.72 4.97 5.58

This is Report Line Number One This is Report Line Number Two Volume by Lane Report - D0620001.PRN

25-1996 Volume by Lane Report - D0620001.PRN 08:51 Pg 1

Sta: 00000000003 Start: Thu - Jun 20, 1996 a	Id: 000000000010	CId: 01 Fmt: 300 - Imperia End:	l Int: 15 Min. Thu - Jun 20, 1996 at 24:00
City/Town: Location: Ln1-North Ln2-North		County: File: DO620001.PRN	
Thu - Jun 20, 1996			
Lane	1	2	Total
00:15	0	0	0
00:30	0	0	0
_00:45	0	0	0
01:00	0	0	0
01:15	0	0	0
01:30	0	0	0
01:45	0	0	0
02:00	0	0	0
02:15	0	0	0
02:30 02:45	0	0	0
02:45	1	1	2
03:00	0	0	0
03:15	0	0	0
\(\hat{\text{\tin}\text{\tex{\tex	0	0	0
45	0	0	0
04:00	0	0	0
04:15	0	0	0
04:30	0	0	0
04:45	0	0	0
05:00	0	0	0
05:15	0	0	. 0
5 05:30	1	ĺ	2
05:45	0	0	0
06:00	0	0	0
06:15	1	3	4
06:30	0	0	0
.06:45	0	0	0
07:00	0	0	0
07:15	2	3	5
07:30	0	1	1
ීට7:45	5	6	11
208:00	3	2	5
08:15	0	0	0
-08:30	1	4	5
		2	3
09:00	3	5	8
09:15	2	3	5
	.	•	3

Thu - Jun 20, 1996

Lane	1	2	Total
09:30	3	4	7
09:45	1	2	3
10:00	1	2	3
10:00 10:15	3	6	9
10:30	6	10	16
10:45	2	4	6
11:00	3	5	8
11:15	4	8	12
11:30	3	6	9
11:45 12:00	5	4	9
12:00	3	5	8
12:15	3	4	7
12:30	3	4	7
12:45	1	1	2
13:00	2	1	3
13:15	0	1	1
13:30	2	1	3
13:45	2	3	5
14:00	3	2 10	5
5 	1	3	16
14:45	. 1	3 A	4 7
14.45 315:00	5 5	7	12
15:15	4	5	9
15:30	7	11	18
15:45	2	4	6
16:00	. 5	4	. 9
16:15	3	3	6
16:30	5	5	10
16:45	3	4	7
17:00	2	5	7
17:15	2	4	6
17:30	1	0	1
17:45	1	2	3
18:00	0	2	2
18:15	0	1	1
18:30	3	2	5
18:45	3	3	6
19:00	3	5	8
19:15	1	1	2
19:30	0	1	1
19:45	5	5	10
20:00	3	4	7

This is Report Line Number One This is Report Line Number Two Volume by Lane Report - D0620001.PRN

			•
Thu - Jun 20, 1996			
Lane	1	2	Total
	=====		
20:15	3	3	6
20:30	0	0	0
20:45	1	4	5
21:00	1	1	2
21:15	2	1	3
21:30	1	2	3
21:45	2	3	5
22:00	3	5	8
22:15	1	1	2
22:30	0	1	1
22:30 22:45	0	0	0
23:00	0	0	. 0
23:15	0	0	0
23:30	0	0	0
23:45	0	0	0
<u></u> 24:00	0	0	0
	=====	======	22232
Daily Totals	152	220	372
entages	40.86	59.14	

This is Report Line Number One This is Report Line Number Two Volume by Lane Report - D0620001.PRN

∠5-1996

08:53 Pg 4

Id: 000000000010 Sta: 00000000000003

CId: 01

Fmt: 300 - Imperial

Int: 15 Min.

Start: Thu - Jun 20, 1996 at 00:00

City/Town:

End: Thu - Jun 20, 1996 at 24:00

Location:

County: File: D0620001.PRN

Ln1-North Ln2-North

Station Data Summary

ane	1	2	Total
Grand Totals	152	220	372
ercentages	40.86	59.14	

Am/Pm Peak Hour Totals

aı	ne		1	2	Total
λm	Hour	10-11	14	25	39
 5.68	enta	ges	9.21	11.36	10.48
ı de	Hour	15-16	18	24	42
Per	centa	ges	11.84	10.91	11.29

This is Report Line Number One This is Report Line Number Two Volume by Lane Report - D0621001.P

∠5-1996 Volume by Lane Report - D0621001.PRN 08:54 Pg 1

Sta: 000000000003 Start: Fri - Jun 21,	Id: 00000000010 1996 at 00:00	CId: 01 Fmt: 300 - Imperi End	al Int: 15 Min. : Fri - Jun 21, 1996 at 24:00
City/Town: Location: Ln1-North Ln2-North		County: File: D0621001.PRN	
Fri - Jun 21, 1996			
Lane	1	2	Total
00:15	0	0	0
00:30	0	0	0
00:45	0	0	0
01:00 01:15	0	0	0
01:15	0	0	0
01:30	0	0	. 0
01:45	0	0	0
02:00	0	0	0
02:15	0	0	0
02:30	0	0	0
02:45 03:00	0	0	0
03:15	0	0	0
,0	0	0	0
■ 03:45	0	0	0
04:00	0	0	0
ୁ 04:15	0	0	0
04:30	0	0	0
04:45	0	0	0
05:00	0	0	0
05:15		0	. 0
05:30 05:45	1	1	2
05:45 206:00	0	0	0
06:15	1	1	2
06:30	0	0	0
06:45	2	4	6
07:00	1	1	2
07:15	0	0	0
07:30	1	1	2
07:45	1	2	3
08:00	2	2 0	4
08:15 08:30	0	U 1	υ 2
08:45	1	3	2. A
09:00	5	5	10
.09:15	0	0	0
1,4			

Lane	1	2	To
9:30	1	2	
9:45	2	7	
10:00	3	5	
0:15	4	4	
.0:30	3	4	
0:45	3	3	
1:00	4	5	
1:15	3	3	
1:30	2	3	
1:45	4	6	
2:00	3	4	
2:15	3	3	
2:30	3	3	
2:45	2	1	
3:00	0	0	
3:15	0	0	
3:30	0	0	
3:45	0	0	
4:00	0	0	
5	0	0	
30	0	0	
4:45	0	0	
5:00	0	0	
5:15	0	0	
5:15 5:30	0	0	
5:45	0	0	
6:00	. 0	0	
6:15	0	0	
6:30	0	0	
6:45	0	0	
7:00	0	0	
7:15	0	0	
7:30	0	0	
7:45	0	0	
7:45 3:00	0	0	
3:15	0	0	
3:30	0	0	
3:45	0	0	
9:00	0	0	
9:15	0	0	
9:30	0	0	
):45	0	0	
):00	0	0	

This is Report Line Number One This is Report Line Number Two Volume by Lane Report - D0621001.PRN

25-1996

08:55 Pg 3

Lane	1	2	Total
20:15		^	
20:15	0	0	(
20:30 20:45	V	0	(
20:45	U .	Ü	Ų
21:00	0	0	(
21:15	0	0	(
21:30 21:45 22:00	0	0	(
21:45	0	0	(
22:00	0	0	C
22:15	0	0	C
22:30	0	0	C
22:45	0	0	C
23:00	0	0	. 0
23:15	0	0	0
23:30	0	0	0
23:45	0	0	0
24:00	0	0	0
	=====		=====
Daily Totals	56	74	130
entages	43.08	56.92	

This is Report Line Number One This is Report Line Number Two Volume by Lane Report - D0621001.PRN

_5-1996

08:55 Pg 4

Sta: 0000000000003

Id: 000000000010

CId: 01

Fmt: 300 - Imperial Int: 15 Min.

End: Fri - Jun 21, 1996 at 24:00

City/Town:

Start: Fri - Jun 21, 1996 at 00:00

County:

Location:

File: D0621001.PRN

Ln1-North Ln2-North

Station Data Summary

Lane 1 2 Total Grand Totals 56 74 130 Percentages 43.08 56.92

Am/Pm Peak Hour Totals

La	ne		1	2	Total
— An	Hour	10-11	14	16	30
255	enta	ges	25.00	21.62	23.08
ŀш	Hour	12-13	8	7	15
Pe	ccenta	ges	14.29	9.46	11.54

LANDESIGN

259 Grand Avenue GRAND JUNCTION, CO 81501 (970) 245-4099 FAX (970) 245-3076

JOB HORIZON VILLAGE			
SHEET NO.	OF		
CALCULATED BY			
CHECKED BY	DATE		
SCALE			

TWO DIEELTIONAL AVAILABLE GAPS FOR 15 MIN PERIOD BETWEEN 5 AND 5:15 PM

6-9 sec.

9-13 500

over 13 sec.

22

16

19

TOTAL AVAILABLE GAPS = 57



TRAFFIC STUDY

FOR

HORIZON VILLAGE

Prepared for:

CUNNINGHAM INVESTMENT CO., INC. 121 South Galena Street, Suite 201 Aspen, CO 81611 (970) 925-8803

Prepared by:

LANDesign, LLC
PLANNING ENGINEERING SURVEYING
256 Grand Avenue
Grand Junction, CO 81501
(970) 245-4099

July 1, 1996

Job No. 95131

TRAFFIC STUDY

FOR

HORIZON VILLAGE

July, 1996

TABLE OF CONTENTS

- A. INTRODUCTION
- B. TRIP GENERATION and DESIGN HOUR VOLUMES
- C. TRIP DISTRIBUTION and ASSIGNMENT
- D. TRAFFIC VOLUMES
- E. CAPACITY ANALYSIS
- F. CONCLUSIONS and RECOMMENDATIONS
- G. APPENDIX

A. INTRODUCTION

1. Purpose of Report

This report considers the concepts for access and the impacts of this proposed development on the current street transportation system in the general vicinity of the development and determines what improvements should be recommended to compensate for the additional traffic generated by this proposed development. Furthermore, this report may be used to assist Mesa County or City of Grand Junction Planners in determining future improvements of the transportation system in the area due to anticipated growth patterns.

Conditions or combinations of events other than those stated have not been analyzed and are not the responsibility of *LANDesign* or the engineer. Maintenance and construction of facilities are the responsibility of others.

2. Location & Land Use

The subject property is located within the SW 1/4 of Section 4, Township 1 South, Range 1 West, of the Ute Principal Meridian and contains 9.2 +/- acres. More specifically the site is located on the SE corner of North 7th Street and Horizon Drive. The tax ID number is 2945-024-00-048. See Figure 1 for the Location Map.

The property is presently a vacant parcel of land used primarily for grazing and hay production. The site is irrigated from the Grand Valley Mainline Canal which forms the east property line. The Independent Ranchman's Ditch traverses the northern portion of the site from east to west and discharges under North 7th Street just north of the existing access to the site.

The property immediately surrounding the proposed development consists primarily of moderate density residential communities. The Mesa View Retirement development is located on the SW corner of 7th and Horizon. Single family residences immediately surround the site while St. Mary's Hospital, professional medical offices and retail facilities exist in the vicinity of 7th and Patterson, 1/4 mile to the south.

The site is currently zoned PUD 6.2 by the City of Grand Junction. The proposed development will consist of 68 condominium units in 17 buildings located south of the Independant Ranchman's Ditch which will serve as a buffer between Horizon Drive and the development.

3. Access

Access to the development will be attained from 7th Street, a minor arterial, through a proposed 52' right-of-way extending 220' from 7th Street. The proposed urban residential collector road, Horizon Village Ct., will taper down to an urban residential road with a 44' right-of-way. The access to the development will be located approximately 380' south from the intersection of 7th and Horizon. The sight distance from the centerline of Horizon Village Ct. looking south on 7th Street is 520'. See Figure 6.

B. TRIP GENERATION & DESIGN HOUR VOLUMES

1. Trip Generation

MULTI-FAMILY DEVELOPMENT - The multi-family development proposed calls for a density of 7.4 units per acre on 9.2 acres or 68 units. The ITE manual calls for an average rate of between 6 and 7 vehicle trip ends per dwelling unit per day, however, site specific studies within the Grand Valley performed by Mesa County Traffic Services indicate an average rate of 9 trips/unit/day. The average rate for average vehicle trip ends vs. dwelling units on a weekday during the PM peak hour is 0.79.

PARCEL 3
68 Multi-Family Dwelling Units
Average Trip Ends vs. Dwelling Units

Time Unit	Direc Distri	tional bution	Average Rate	Trip Ends	
	in	out			
weekday	50%	50%	9	306 in	
ADT		ĺ	<u> </u>	306 out	
weekday	65%	35%	0.79	35 in	
PM peak				19 out	

2. Design Hour Volumes

Design hour volumes have been determined from traffic counts performed by *LANDesign* between June 6th and the 20th, 1996. This study will use the weekday peak hour volumes for analysis and design. Peak hours vary for different legs of the intersection. The northbound leg peaked between 5 and 6 PM at 7.8% of the ADT. The westbound leg of the intersection peaked between 12 and 1 PM at 8.6% of the ADT. The southbound leg peaked in the morning between 8 and 9 at 12.8% of the ADT and the eastbound leg peaked between 3 & 4 PM at 11.3% of the ADT. The northbound leg of the intersection will be the most affected leg due to the proposed development and therefore this study will assume a peak hour between 5 and 6 PM but will utilize the highest peak hour volumes at each leg for analysis of the intersection. See Figure 2 for the predeveloped peak hour volumes for each movement.

C. TRIP DISTRIBUTION and ASSIGNMENT

Directional distribution of trip ends was estimated by considering the proximity of the site to adjacent transportation facilities and the relationship to downtown Grand Junction and other major activity centers. The general distribution of trips to and from the site at build-out during the week is estimated to be 50% north and 50% south. Of that 50% of generated traffic entering or exiting the site to or from the north, It is estimated that 85% of that traffic will either turn east onto Horizon Drive or come from Horizon Drive. The remaining 15% will come from or go to 7th Street to the north of the intersection.

Figure 3 shows the trip end assignment for trips generated from the proposed development during the peak PM weekday hour at build-out.

D. TRAFFIC VOLUMES

Existing traffic volumes and peak hour factors have been determined by counts performed by *LANDesign* between June 6th and the 20th, 1996. *LANDesign* has utilized Peek ADR type counters to determine counts at 15 minute intervals for each lane and calculate totals and peak hour volumes. Upon determination of peak hours for each individual leg of the intersection, turning movement counts were performed by individuals in the field during the respective peak hours. See print-out of traffic counts in the end of this report.

Existing traffic volumes at the peak hours were combined with the calculated trip ends generated by the proposed development to produce a proposed total volume for analysis of the intersection. These figures were increased by 2.2% per year for analysis of the intersection in the year 2010. See Figures 4 & 5 respectively.

E. CAPACITY ANALYSIS

The analysis of this study is divided into 2 parts. The first part will investigate the impact on the proposed intersection due to the construction of the proposed development. The second stage will examine the access to the proposed development and the impact it will have on the flow of traffic on North 7th Street and delays experienced on Horizon Village Court. These analyses will look at the current conditions and the projected conditions for the year 2010.

The Highway Capacity Software (HCS) release 2 was utilized for analysis and determination of the level of service for the intersection of 7th Street and Horizon Drive as well as the intersection of Horizon Village Court and 7th Street. The Horizon Village Court intersection was analyzed as a simple unsignalized T-intersection while the Horizon Drive intersection was analyzed as a 3 phase isolated signalized operation.

The signalized intersection at 7th and Horizon is a fully actuated split phasing isolated operation in which the signal rests and green on 7th Street. In other words 7th Street will stay green until traffic on Horizon Drive actuates the signal. The signal operates in 3 phases. The 1st phase operates traffic on 7th Street. The 2nd phase regulates the traffic on westbound Horizon Drive while the 3rd phase operates the eastbound leg from the Mesa View Retirement Community. The cycle lengths for each leg have been measured in the field.

F. CONCLUSIONS and RECOMMENDATIONS

The intersection of proposed Horizon Village Court and North 7th Street has been designed to provide as much sight distance as possible. A sight zone triangle at the intersection will be designed to allow a minimum of 60' along 7th Street and 50' along Horizon Village Ct. at the flowlines with no sight obscuring signs, walls, fences or foliage more than 30" high. 7th Street is classified as a minor arterial with a design speed of 35 mph. The required safe sight distance left is 300' while the required safe sight distance right is 350'. The existing sight distance left from the proposed access looking south on 7th Street is 520' and well within City requirements. The proposed access road is located 380' south of the intersection of 7th Street and Horizon Drive, however, sight distance extends considerably beyond that.

Accereration or deceleration lanes associated with this proposed development are not warranted by the City's <u>Transportation Engineering Design Standards</u>. However, due to the grade and volume of traffic heading north on 7th from Patterson toward the proposed access road, a 60' right turn deceleration lane will be constructed south of the beginning of the curb return radius into the development with a 60' taper leading into that lane. The lane width will be 10' wide. The beginning of the taper into the right turn lane at the intersection of 7th Street and Horizon Drive starts approximately 20' north of the centerline of the proposed access road. Therefore, the north curb return flowline of the access road will be constructed to line up with the east flowline of the existing right turn lane to allow for a smooth transition toward Horizon Drive and still allow plenty of distance for the very small percentage of northbound trip ends exiting the development to continue north on 7th.

Analysis of the intersection of Horizon Drive and 7th Street indicates no change in the level of service due to the impacts of the proposed development. The level of service remained at a 'B' level before and after development. By projecting the increase in volumes due to a 2.2% growth rate in the area, the level of service for the westbound left turn lanes on Horizon Drive decreased to a level of 'C' for the year 2010. The remaining lanes continued a level of service of 'B'.

Analysis of the intersection of Horizon Village Court and North 7th Street indicates a comfortable level of service of 'B' for traffic exiting and a level of service of 'A' for traffic entering the development. Projected analysis for the year 2010 suggests a decrease of one level for each direction.

. SIGNALIZED INTERSECTION SUMMARY Version 2.4a 06-27-1996 Center For Microcomputers In Transportation

Streets: (E-W) Horizon Drive

(N-S) 7th Street

Analyst: JPC File Name: EX1996.HC9

Area Type: Other

6-27-96 PM Peak

Comment: 1996 volumes

=========	:=====:	=====	=======	=====	=====	=====	=====	=====	=====	=====	====
	Eas	stboun	d We	stbour	nd	No	rthbou	ind	Sou	ıthbou	ınd
	L	T	R L	T	R	L	${f T}$	R	L	${f T}$	R
No. Lanes	>	1	1 1	> 1		1	2		1	2 <	(
Volumes	2	16	24 410	10		8	195		16	218	2
Lane Width	1	12.0 1	2.0 12.0	12.0		12.0	12.0	Ì	12.0	12.0	
RTOR Vols	İ		0		0			0			0
Lost Time	3.00	3.00 3	.00 3.00	3.00		3.00	3.00	ļ	3.00	3.00	3.00

Signal Operations Phase Combination 1 2 6 7 3 4 | NB Left * * EB Left * Thru * Thru Right Right Peds Peds WB Left * SB Left * Thru Thru Right Right * Peds Peds NB Right |EB Right SB Right WB Right 9.0A 15.0A Green 14.0P Green Yellow/AR 5.0 5.0 5.0 Yellow/AR Cycle Length: 53 secs Phase combination order: #1 #2 #5

	Lane	Group:	Intersect Adj Sat	ion Perf	ormance g/C	Summary		Approa	ch:
	Mvmts	Cap	Flow	Ratio	Ratio	Delay	LOS	Delay	LOS
						~ ~ ~ ~ ~			
EB	LT	594	1853	0.032	0.321	8.0	B	8.0	В
	R	508	1583	0.049	0.321	8.0	В		
WB	L	367	1770	0.599	0.208	14.2	В	14.3	В
	LT	369	1778	0.604	0.208	14.3	В		
NB	L	304	1007	0.026	0.302	8.4	В	8.8	В
	${f T}$	1125	3725	0.191	0.302	8.9	В		
SB	L	321	1063	0.053	0.302	8.5	В	8.9	В
	TR	1123	3721	0.216	0.302	8.9	В		
		Int	ercection	Dolaw -	11 3 00	c/web Int	arean	tion LOS	- B

Intersection Delay = 11.3 sec/veh Intersection LOS = B

Lost Time/Cycle, L = 9.0 sec Critical v/c(x) = 0.249

Streets: (E-W) Horizon Drive

(N-S) 7th Street

Analyst: JPC File Name: PROP1996.HC9 6-27-96 PM Peak Area Type: Other

Comment: 1996 volumes

	Ea	astbo	und	We:	stbour	nd	No:	rthbou	ınd	So	uthbou	ınd
	L	T	R	L	T	R	j L	T	R	L	T	R
					~							
No. Lanes	>	• 1	1	1 :	> 1		1	2		1	2 4	(
Volumes	2	16	24	424	10		8	196		16	221	2
Lane Width	ĺ	12.0	12.0	12.0	12.0		12.0	12.0		12.0	12.0	
RTOR Vols			0			0	ĺ		0			0
Lost Time	13.00	3.00	3.00	3.00	3.00		3.00	3.00		3.00	3.00	3.00

			Si	.gnal	Opera	atio	ns				
Phas	se Combination	1 1	2	3	4	ł		5	6	7	8
EB	Left		*			NB	Left	*			
	Thru		*			İ	Thru	*			
	Right		*			j	Right				
	Peds					İ	Peds				
WB	Left	*				SB	Left	*			
	Thru	*				i	Thru	*			
	Right					i	Right	*			
	Peds					i	Peds				
NB	Right					EB	Right				
SB	Right					WB	Right				
Gree	_	.0A 15	.0A			Gree		4.0P			
			.0				Low/AR	5.0			
	-			comb	inati	•	order:		#5		

			Intersec	tion Peri	ormance	Summary			
	Lane	Group:	Adj Sat	v/c	g/C			Approac	ch:
	Mymts	Cap	Flow	Ratio	Ratio	Delay	LOS	Delay	LOS
EB	LT	594	1853	0.032	0.321	8.0	В	8.0	В
	R	508	1583	0.049	0.321	8.0	В		
WB	L	367	1770	0.618	0.208	14.6	В	14.6	В
	LT	369	1778	0.623	0.208	14.7	В		
NB	L	302	999	0.027	0.302	8.4	В	8.9	В
	T	1125	3725	0.192	0.302	8.9	В		
SB	L	320	1061	0.053	0.302	8.5	В	8.9	В
	TR	1123	3721	0.220	0.302	9.0	В		

Intersection Delay = 11.5 sec/veh Intersection LOS = B Lost Time/Cycle, L = 9.0 sec Critical v/c(x) = 0.255

.cM: SIGNALIZED INTERSECTION SUMMARY Version 2.4a 06-27-1996

Center For Microcomputers In Transportation

(N-S) 7th Street Streets: (E-W) Horizon Drive

Analyst: JPC File Name: PROP2010.HC9

6-27-96 PM Peak Area Type: Other

Comment: 2010 volumes

=======================================	:==== E:	astbo	und	We	Westbound			rthbou	ınd	Southbound		
	į L	T	R	L	T	R	L	T	R	L	T	R
No. Lanes Volumes Lane Width RTOR Vols Lost Time			1 33 12.0 0 3.00		12.0	0	1 11 12.0 3.00		0	1 22 12.0 	2 < 298 12.0	4 0 3.00

			S	ignal	Oper	atio	ns				
Pha	se Combination	. 1	2	3	4	1		5	6	7	8
EB	Left		*			NB	Left	*			
	Thru		*			1	Thru	*			
	Right		*			ĺ	Right				
	Peds					İ	Peds				
WB	Left	*				SB	Left	*			
	Thru	*				ĺ	Thru	*			
	Right					Ì	Right	*			
	Peds					Ì	Peds				
NB	Right					EB	Right				
SB	Right					WB	Right				
Gre	en 9	.OA 15	5.0A			Gre	en 1	L4.0P			
Yel	low/AR 5	.0 5	5.0			Yel	low/AR	5.0			
		secs	Phas	e comb	inat	ion	order:	#1 #2	#5		

	Lane	Group:	Intersect Adj Sat	ion Perf.	ormance g/C	Summary		Approa	ch:
	Mvmts	Cap	Flow	Ratio	Ratio	Delay	LOS	Delay	LOS
						~~~~~			
EB	LT	593	1848	0.042	0.321	8.0	В	8.0	В
	R	508	1583	0.069	0.321	8.1	В		
WB	L	367	1770	0.838	0.208	23.8	С	24.0	С
	LT	369	1778	0.843	0.208	24.1	С		
NB	L	247	817	0.049	0.302	8.5	В	9.1	В
	${f T}$	1125	3725	0.261	0.302	9.1	В		
SB	L	272	901	0.085	0.302	8.6	В	9.2	В
	TR	1122	3718	0.298	0.302	9.2	В		
		Int	ersection	Delav =	15.9 se	c/veh Int	ersect	tion LOS	= C

Intersection Delay = 15.9 sec/veh Intersection Lost Time/Cycle, L = 9.0 sec Critical v/c(x) = 0.346

Center For Microcomputers In Transportation

University of Florida

512 Weil Hall

Gainesville, FL 32611-2083

Ph: (904) 392-0378

Streets: (N-S) 7th Street (E-W) Horizon Village Ct.

Streets: (N-S) 7th Street
Major Street Direction... NS

Length of Time Analyzed... 60 (min)

Analyst..................................JPC

Date of Analysis..... 6/27/96

Other Information.....1996 conditions

Two-way Stop-controlled Intersection

=======================================	No	rthbou T	nd R	Sou L	thbou T	ind R	=====   Еа   т.	===== stbou T	===== nd R	=====   We   T.	=== stbo T	ound R
:												
No. Lanes	0	2	1	1	2	0	0	0	0	0	> 0	< 0
Stop/Yield Volumes PHF Grade MC's (%) SU/RV's (%) CV's (%)		480 •95 -4	N 18 .95	17 .95	223 .95 2	N				10 .95		.95 0
PCE's				1.40					·	1.10		1.10

#### Adjustment Factors

Vehicle Maneuver	Critical Gap (tg)	Follow-up Time (tf)
Left Turn Major Road	5.50	2.10
Right Turn Minor Road	5.50	2.60
Through Traffic Minor Road	6.50	3.30
Left Turn Minor Road	7.00	3.40

## Worksheet for TWSC Intersection

Step 1: RT from Minor Street	WB	EB
Conflicting Flows: (vph) Potential Capacity: (pcph) Movement Capacity: (pcph) Prob. of Queue-Free State:	252 1032 1032 0.99	
Step 2: LT from Major Street	SB	NB
Conflicting Flows: (vph) Potential Capacity: (pcph) Movement Capacity: (pcph) Prob. of Queue-Free State:	524 897 897 0.97	
Step 4: LT from Minor Street	WB	EB
Conflicting Flows: (vph) Potential Capacity: (pcph) Major LT, Minor TH Impedance Factor:	758 347	
Adjusted Impedance Factor: Capacity Adjustment Factor	0.97 0.97	
due to Impeding Movements Movement Capacity: (pcph)	0.97 337	

## Intersection Performance Summary

Mov	rement	Flow Rate (pcph)	Move Cap (pcph)	Shared Cap (pcph)(	Avg. Total Delay sec/veh)	95% Queue Length (veh)	LOS	Approach Delay (sec/veh)
WB	L	12	337 >		7.0	0 0		7.0
WB	R	10	1032 >	486	7.8	0.0	В	7.8
SB	L	25	897		4.1	0.0	A	0.3
		· <b>I</b> 1	ntersect	ion Del	ay =	0.3 se	c/veh	

HCS: Unsignalized Intersections Release 2.1c 2010CT.HC0 Page 1

Center For Microcomputers In Transportation

University of Florida

512 Weil Hall

Gainesville, FL 32611-2083

Ph: (904) 392-0378

Streets: (N-S) 7th Street (E-W) Horizon Village Ct.

Major Street Direction... NS

Length of Time Analyzed... 60 (min)

Other Information......1996 conditions

Two-way Stop-controlled Intersection

=========	3	thbou		l .	Southbound			Eastbound			Westbound		
	L	T 	R 	L 	T	R 	L 	T 	R	L	T 	R	
No. Lanes Stop/Yield	0	2	1 N	1	2	O N	0	0	0	0 :	> 0	< 0	
Volumes PHF		651 •95	24 •95	24 •95	302 •95					14 .95		13 .95	
Grade MC's (%) SU/RV's (%) CV's (%)		-4			2							0	
PCE's				1.40			<u> </u>			1.10		1.10	

# Adjustment Factors

Vehicle Maneuver	Critical Gap (tg)	Follow-up Time (tf)
Left Turn Major Road	5.50	2.10
Right Turn Minor Road	5.50	2.60
Through Traffic Minor Road	6.50	3.30
Left Turn Minor Road	7.00	3.40

HCS:	Unsignalized	Intersections	Release 2.1c	2010CT.HC0	Page 2
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Workshoot	for	TWICC	Intersection
worksneet	TOL	TWSC	Intersection

Step 1: RT from Minor Street	WB	ЕВ
Conflicting Flows: (vph) Potential Capacity: (pcph) Movement Capacity: (pcph) Prob. of Queue-Free State:	342 929 929 0.98	
Step 2: LT from Major Street	SB	NB
Conflicting Flows: (vph) Potential Capacity: (pcph) Movement Capacity: (pcph) Prob. of Queue-Free State:	710 713 713 0.95	
Step 4: LT from Minor Street	WB	ЕВ
Conflicting Flows: (vph) Potential Capacity: (pcph) Major LT, Minor TH	1028 233	
Impedance Factor: Adjusted Impedance Factor: Capacity Adjustment Factor	0.95 0.95	
due to Impeding Movements Movement Capacity: (pcph)	0.95 222	

# Intersection Performance Summary

Mov	ement	Flow Rate (pcph)	Move Cap (pcph)	Shared Cap (pcph)	Avg. Total Delay (sec/veh)	95% Queue Length (veh)	LOS	Approach Delay (sec/veh)
WB	L	17	222 >		11 =	0 2	<b>a</b>	11 5
WB	R	15	929 >	345	11.5	0.3	С	11.5
SB	L	35	713		5.3	0.0	В	0.4

Intersection Delay = 0.4 sec/veh

This is Report Line Number One This is Report Line Number Two Volume by Gap Report - DO807001.PRN

**─**r^ ^7**-**1996

(°°:45 (___00 12:00 Pg 1

			12:00 Pg 1								
Sta: 000000000003 Start: Wed - Aug 07, 199	Id: 0000	000000010	CId: 01	Fmt: 300 - 1	[mperial						
City/Town: Location: .n1-North Ln2-North				County: DO807001.PRN							
Wed - Aug 7, 1996											
Sap(sec)	1-6	7-9	10-13	14-16	17-66	Total					
ു0:15	0	0	0	0	21	21					
0:30	Ô	0	0	Ô	22	22					
00:45	0	0	0	0	20	20					
01:00	0	0	0	0	9	9					
1:15	0	0	0	0	12	12					
1:30	0	0	0	0	9	9					
01:45	0	0	0	0	17	17					
32:00	0	0	0	0	8	8					
2:15	0	0	0	0	10	10					
02:30	0	0	0	0	9	9					
02:45	0	0	0	0	3	3					
3:00	0	0	0	0	1	1					
<b>v</b> 3:15	0	0	0	0	3	3					
03:30	0	0	0	0	1	1					
5	0	0	0	0	2	2					
Ó	0	0	0	0	4	4					
04:15	0	0	0	0	3	3					
€1:30	0	0	0	0	8	8					
<b>1:45</b>	0	0	0	0	2	2					
05:00	0	0	0	0	18	18					
05:15	0	0	0	0	11	11					
:30	. 0	0	0	0	11	11					
<b>45</b> :45	0	0	0	0	17	17					
06:00	0	0	0	0	26	26					
1:15	0	0	0	0	29	29					
:30	0	0	0	0	48	48					
06:45	0	0	0	0	50	50					
07:00	0	0	0	0	108	108					
:15	0	0	0	0	87	87					
<del>77:</del> 30	0	0	0	0	100	100					
07:45	0	0	0	0	123	123					
( : 00	0	0	0	0	172	172					
15	0	0	0	0	140	140					
08:30	0	0	0	0	145	145					

This is Report Line Number One This is Report Line Number Two Volume by Gap Report - D0807001.PRN

7-1996

12:00 Pa 2

( /=1990		volume by Ga	volume by Gap Report - DUSU/DUI.PRN							
Wed - Aug 7, 1996										
Gap(sec)	1-6	7-9	10-13	14-16	17-66	Total				
09:30		0	0	0	72	72				
09:45	0	0	0	0	14	14				
10:00	0	0	0	0	0	0				
10:15	0	0	0	0	0	0				
10:30	0	0	0	0	0	0				
<b>10:4</b> 5	0	0	0	0	0	0				
11:00	0	0	0	0	0	0				
11:15	0	0	0	0	0	0				
11:30	0	0	. 0	0	0	. 0				
11:45	0	0	0	0	0	0				
	=====	=====	=====	=====	=====	======				
Daily Totals	0	0	0	0	1737	1737				
Percentages	0.00	0.00	0.00	0.00	100.00					

This is Report Line Number One This is Report Line Number Two Volume by Gap Report - D0807001.PRN

7-1996

12:01 Pg 3

Sta: 000000000003

Id: 000000000010

CId: 01

Fmt: 300 - Imperial Int: 15 Min.

End: Wed - Aug 07, 1996 at 11:45

Start: Wed - Aug 07, 1996 at 00:00

City/Town:

County:

Location:

Ln1-North Ln2-North

File: D0807001.PRN

#### Station Data Summary

Gap(sec)	1-6	7-9	10-13	14-16	17-66	Total
Grand Totals	0	0		•	1737	1737
Percentages	0.00	0.00	0.00	0.00	100.00	

#### Am/Pm Peak Hour Totals

Gap(sec) 1-6 7-9 10-13 14-16 17-66 Total 0 0 0 0 561 561 Am Hour 8-9 entages 0.00 0.00 0.00 0.00 32.30 32.30

⊩ nour None

18-DEC-95 CIP_EXPHS_TRANS

45,4

Fund Code Summary of Capital Represent Project Expenditures and Transfers Report Page No. 9 of 42

		1995	1996	1997	998	1999	2000	2001	2002	7,003	2004	2005		
Yotal Ex	penses for Department 500	0	0	, 0	0	\$2,000	0	0	Q	0	0	0	52,000	2,267,800
6000004	CONTRACT STREET MAINTENANCE	1,420,000	1,325,000	1,463,900	1,451,000	1,509,000	1,569,000	1,632,000	1,697,000	1,765,000	1,636,000	1,910,000	17,577,000	
6000007	ALLEY IMPROVEMENT DISTRICT	280,000	274,000	265,000	296,000	308,000	321,000	333,000	347,000	341,000	375,000	390,000	3,570,000	
6000008	FLDOO CONTROL LEVEE	58,676	. 0	0	0	0	0	0	0	0	0	0	58,676	
6000009	CURB, GUTTER & STOEWALK REPLACEMEN	163,772	275,000	286,000	297,000	309,000	322,000	334,000	348,000	362,000	376,000	390,000	3,482,772	
6000012	•	0	0	. 0	0	0	0	Q	0	0	0	0	0	
6000013	SIDEWALK INPROVEMENTS	127,863	133,000	138,000	144,000	150,000	156,000	162,000	168,000	175,000	182,000	189,000	1,724,863	
6000016	DRAJNAGE KASTER PLAN	29,854	a	O	0	0	0	0	ø	0	6	0	29,854	
6000017	27 1/2 RD, F RD. TO G RD. RECONSTR	a	0	0	0	0	0	0	0	400,000,5	0	0	2,000,000	
6000019	GRAND AVE RECONSTRUCTION 18T TO 7T	115,532	0	0	0	0	0	0	0	D	0	0	115,532	
6000020	ACCESSIBILITY INPROVEMENTS	195,531	50,000	50,000	50,000	50,000	50,000	50,600	50,000	50,000	50,000	50,000	695,531	
6000021	WHAVEEP: HWY 50 TO 28 1/2 Road	159,000	980,000	5,639,000	Q	0	6	0	0	0	0	0	3,768,000	
6000022	NORTH - SOUTH MAJOR CORREDOR	0	35,000	0	0	0	a	0	1,715,000	0	0	0	1,750,000	14,160,000
6000023	KORTZON DRIVE: 12TH STREET TO Q R	0	D	D	0	0	0	1,300,000	0	0	0	0	1,300,000	
6000024	28 1/4 ROAD: NORTH AVE. TO ORCHAR	965,076	9	D	0	0	0	0	0	0	0	0	965,076	
6000025	25 1/2 ROAD: INDEPENDENT TO F ROA	0	D	D	0	0	1,035,600	0	D	0	0	0	1,035,000	
6000026	25 ROAD: HUY 6 4 50 TO F ROAD	9	0	D		D	0	800,000	0	0	C	0	800,000	
6000027	12TH SY BONETA TO HORIZON & YRAFF	D		D	950,000	9	0	0	D	0	0	0	950,000	
6000029	NORTH 1ST ST. ORCHARD TO PATTERSO	81,500	792,000	D	0	0	0	0	D	0	0	0	873,500	
4000030	27 ROAD: UNAMEEP TO NEY 50	0	0	0	Ð	D	Ü	U O	625,000	0	0	U	625,000	
6000031	28 RDAD: GRAND TO BELFORD	v	Ü	U	U		Ü	0	0	660,000	1 (20 020	U	660,000	
≥ 6000033 ≥ 6000033	28 1/2 ROAD: 1-708 TO ORCHARD AVE	Ů,	U	U	υ •	~~~~	v	U	0	U	1,600,000	U	1,400,000	
6000034	ERIDGE REPLACEMENT GRJ-F.4-26.7 FORESIGHT PARK: STORM SEWER IMPROV	10/ 110	120.000	U	u	250,000	, ,	0	u	U	u	U	250,000	
-2 6000035	BRIDGE REPLACEMENT GRJ-D.5-27.99	104,310	120,000	9		. 0	0	•	0	Ÿ	Š		224,310	- (235,000 1796
6000036	LAMPLITE PARK SUBSIDENCE CONTROL	0	0	0	0	0	0	v	0	U n	ų A	0	0	100,000
6000038	24 ROAD: F ROAD TO 1-70	0	0	0		1,036,000	4	,	<b>О</b>	0		0	1,036,000	100,000
6000039	CORTEND AVENUE: 27 1/2 ROAD TO 28	. 0	0			*,000,000		. ,	•	0	650,000	v	650,000	
6000042	HORIZOH DRIVEL 7TH ST. TO 12TH ST	, ,	n		0	<b>n</b>	'n	1,087,000	G.		w, w	0	1,087,000	
6000D44	28 ROAD: PATTERSON TO CORTLAND	0	0	0	'n	n	0	0.007,000	n	860,000	n	, A	000,000	
6000046	RIVERSIDE PARK/WEST AVENUE REALIGN	a	n	D.	á	0	0	133,000	253,000	0.07,0.00	ů	n	386,000	
6000069	STREET LIGHT INSTALLATIONS	152,400	73,000	76,900	79,000	82,000	85,900	89,000	92,000	96,000	100,000	104,000		
6000070	TRAFFIC SIGNAL CONTROLLERS - UPGRA	24,230	16,000	17,000			20,000	21,000	22,000		24,000	25,000		
6000072	TOURIST DIRECTIONAL SIGNS	7.975	0	0	D.,200	,300	,,,,,	_,,500	12,300	22,000	0	25,000	7,975	
6000086	COLUMBUS SCHOOL/SIGNAL RE-CONST	0	å	27,000	o	ŏ	õ	ă	ă	ŏ	ă	Ď	27,000	
6000087	ORCHARD AVE. SCHOOL/SEGHAL RECOHST	24,185	ā	0	ō	ō	ă	0	ă	ō	ō	ū	24, 185	
6000104	Bookcilff Ave Reconstruction 9th t	0	ā	ō	ò	ō	377,000	9	Õ	D	Ď	ō	377,000	
6000107	1st St.& Horth Ave right turn lane	40,000	ò	ã	ň	ň	6		ň			_	40,600	

2-JAN-96 IP_PROJECT_DETAIL

#### Capital Improvement Project 10 Year Betail Listing

# Capital Improvement Project Title

HORIZON DRIVE: 12TH STREET TO G ROAD

Projects & Engineering

epartment: Public Works

Submitted By: Don Newton: 10-yr CIP

roject Type: Streets, Traffic & Drain

Project Need: Expansion

Division:

Begin Date: 1/1999

Yearly Expenditures	1996	1997	1998	1999	2000	2001	2002	2003	2004	2005	2006	TOTAL
Original Budget Amount	0	0	0	0	0	1,300,000	0	0	0	0	0	1,300,000
Adjusted Budget Amount	0	0	0	0	0	. 0	0	0	0	- <b>Q</b>	0	
Revised Budget Amount	0	0	0	0	0	0	0	0	0	0	0	

roject Narrative:

his project is the reconstruction of Horizon Drive from 12th Street to G Road. The Principal Arterial street section would include four (4) traffic Lanes, left turn ockets, curb and gutters, sidewalks, landscaped medians and lighting. This street is a major entrance to the City from the Airport and 1-70.

# HORIZON VILLAGE

# WETLANDS REPORT

July, 1996

# Introduction

In order for an area to be classified as a wetland it must posess three essential characteristics: (1) hydrophytic vegetation, (2) hydric soils, and (3) wetland hydrology, which is the driving force creating all wetlands. These three technical criteria are mandatory and all must be met for an area to be identified as a wetland by the Unified Federal Method established by the Army Corps of Engineers, the EPA, the Natural Resources Conservation Service and the U.S. Fish & Wildlife Service.

## **Location & Land Use**

The subject property is located within the SW ½ of Section 4, Township 1 South, Range 1 West of the Ute Principal Meridian and contains 9.2 acres +/-. More specifically the site is located on the SE corner of Horizon Drive and North 7th Street in Grand Junction, Mesa County, Colorado. The tax ID number is 2945-024-00-048.

The property is presently an irrigated vacant parcel of land used primarily for grazing and hay production. The site slopes moderately to the northwest at grades ranging from 35% in the southeast corner of the property to 1.5% in the northwest. The site is irrigated from the Grand Valley Highline Canal which forms the east boundary of the property. The Independent Ranchmen's Ditch traverses the northern portion of the site from east to west. The irrigated portion of the property consists of the area south of the Independent Ranchmen's Ditch and north of the steep slopes along the southern boundary. Irrigation water is ditched from a headgate on the Highline Canal along the south and west boundaries of the irrigated field and is eventually discharged into the Ranchmen's Ditch.

The proposed development will consist of 68 condominium units in 17 buildings located south of the Ranchmen's Ditch within the existing irrigated pasture land.

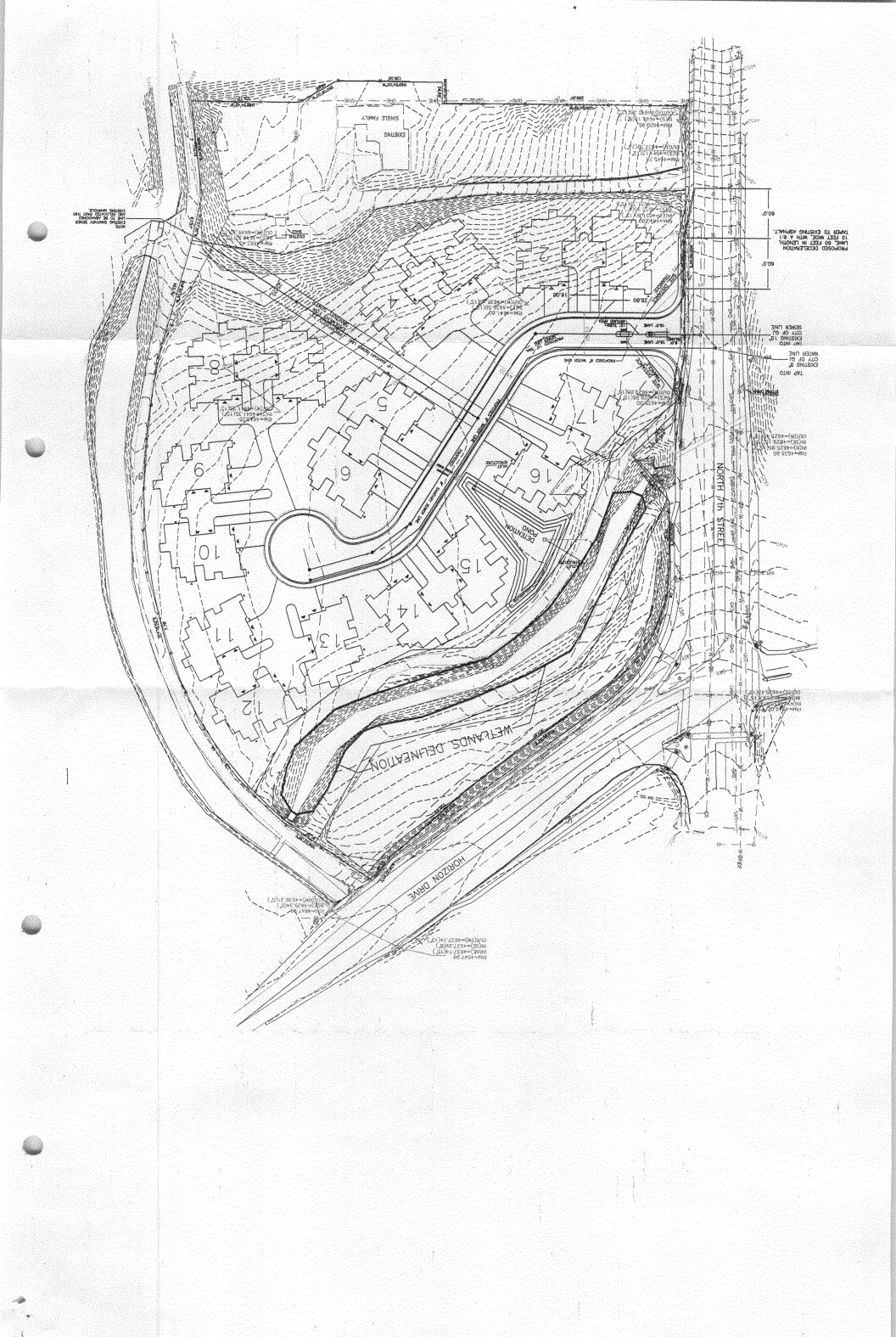
# Wetland Findings

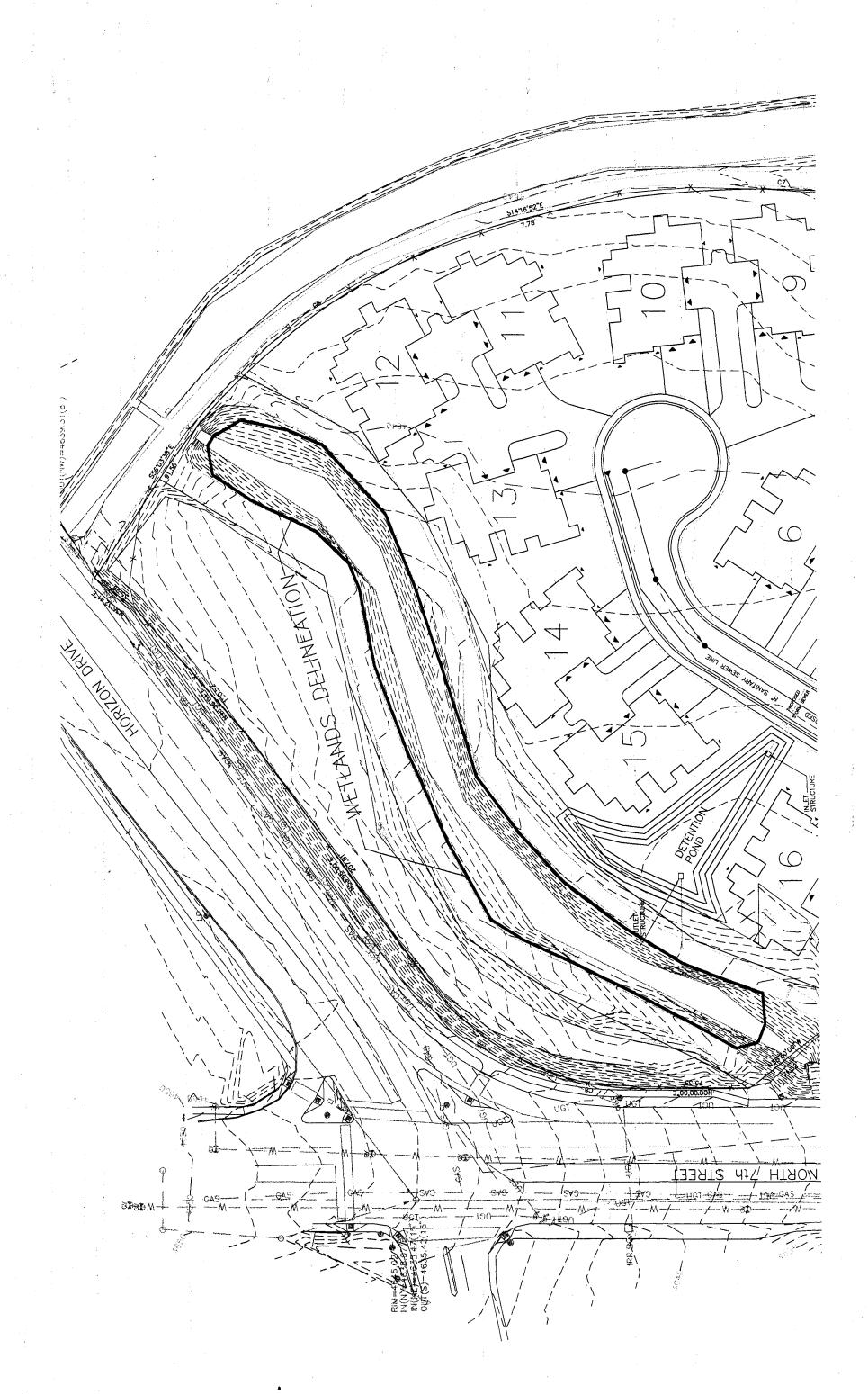
Russian olives, cottonwoods, willows and tamerisks line the irrigation ditches surrounding the property. Reeds and wild asparagus are also found along the banks of the Ranchmen's Ditch, in the northeast corner of the property at the confluence of the Ranchmen's Ditch and the Grand Valley Canal, and in some isolated areas along the east property line. These are primarily facultative and facultative wetland plant species and are predominant only in the areas described.

With the exception of the banks of the Ranchmen's Ditch, the soils are generally well drained mineral soils. The saturation level of the soil is occasionally raised to within 1' of the surface during irrigation but decreases relatively fast upon suspension of the irrigation water. The Natural Resources Conservation Service classifies the soils in the area of development as Ravola very fine silty loam (Rf) 0-2%.

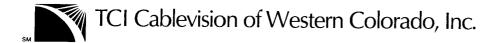
#### **Conclusions**

The only area on the site that meets all the criteria for a wetland is the area along the banks of the Independent Ranchmen's Ditch. Generally this consists of the area 10' from either bank of the ditch along its entire length. In the other areas where the predominant wetland vegetation is present, the wetland hydrology was not and therefore not determined as a wetland.



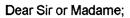


Ref. No. CON19627



July 3, 1996

Horizon Village Cunningham Investment Co. % Community Development Department 250 North 5th Street Grand Junction, CO 81501



We are in receipt of the plat map for your new subdivision, Horizon Village. We will be working with the other utilities to provide service to this subdivision in a timely manner.

RECEIVED GRAND JUNCTION

PLANNING DEPARTMENT

JUL 08 1996

I would like to take this opportunity to bring to your attention a few details that will help both of us provide the services you wish available to the new home purchasers. These items are as follows:

- We require the developers to provide, at no charge to TCI Cablevision, an open trench for cable service where 1. underground service is needed and when a roadbore is required, that too must be provided by the developer. The trench and/or roadbore may be the same one used by other utilities so long as there is enough room to accommodate all necessary lines.
- We require developers to provide, at no charge to TCI Cablevision, fill-in of the trench once cable has been installed 2. in the trench.
- We require developers to provide, at no charge to TCI Cablevision, a 4" PVC conduit at all utility road crossings 3. where cable TV will be installed. This 4" conduit will be for the sole use of cable TV.
- Should your subdivision contain cul-de-sac's the driveways and property lines (pins) must be clearly marked prior to 4. the installation of underground cable. If this is not done, any need to relocate pedestals or lines will be billed directly back to your company.
- 5. TCI Cablevision will provide service to your subdivision so long as it is within the normal cable TV service area. Any subdivision that is out of the existing cable TV area may require a construction assist charge, paid by the developer, to TCI Cablevision in order to extend the cable TV service to that subdivision.
- TCI will normally not activate cable service in a new subdivision until it is approximately 30% developed. Should 6. you wish cable TV service to be available for the first home in your subdivision it will, in most cases, be necessary to have you provide a construction assist payment to cover the necessary electronics for that subdivision.

Should you have any other questions or concerns please feel free to contact me at any time. If I am out of the office when you call please leave your name and phone number with our office and I will get back in contact with you as soon as I can.

Sincerely,

Glen Vancil.

Construction Supervisor 245-8777

Den Variet

pp.96-157



#### **DEPARTMENT OF THE ARMY**

## U.S. ARMY ENGINEER DISTRICT, SACRAMENTO CORPS OF ENGINEERS 1325 J STREET

SACRAMENTO, CALIFORNIA 95814-2922

July 16, 1996

Regulatory Branch (199675310)

RECEIVED GRAND JUNCTION PLANNING DEPARTMENT.

JUL 17 1996

City of Grand Junction Community Development Department 250 North 5th Street Grand Junction, Colorado 81501

Dear Sirs:

We are responding to your written request for a jurisdictional determination at the proposed Horizon Village Subdivision. The proposed subdivision is located within Section 2, Township 1 South, Range 1 West, Mesa County, Colorado.

Based on a site inspection by Randy Snyder of this office on July 15, 1996, we have determined that the proposed subdivision as shown on the preliminary plan "Horizon Village Subdivision, Dated June 30, 1996, will not require a Department of the Army permit.

We have assigned number 199675310 to this determination. Please contact Mr. Snyder and refer to this number if you have any questions regarding this matter and for permit requirements at (970) 243-1199 or the address below.

Sincerely,

Ken Vacobson

Chief, Southwestern Colorado

Regulatory Office

402 Rood Avenue, Room 142

Grand Junction, Colorado 81501-2563

# **REVIEW COMMENTS**

Page 1 of 6

FILE #RZP-96-157

TITLE HEADING: Horizon Village

**LOCATION:** 

SE corner 7th Street & Horizon Drive

PETITIONER:

**Cunningham Investments** 

PETITIONER'S ADDRESS/TELEPHONE:

121 S Galena Street

Suite 201

Aspen, CO 81611

925-8803

PETITIONER'S REPRESENTATIVE:

Brian Hart, LANDesign

STAFF REPRESENTATIVE:

Michael Drollinger

NOTE: THE PETITIONER IS REQUIRED TO SUBMIT FOUR (4) COPIES OF WRITTEN RESPONSE AND REVISED DRAWINGS ADDRESSING ALL REVIEW COMMENTS ON OR BEFORE 5:00 P.M., JULY 26, 1996.

# CITY COMMUNITY DEVELOPMENT

7/19/96

Michael Drollinger

244-1439

- 1. If single family residence at north end of property is no longer part of this application, the property should be rezoned back to RSF-4 as part of this process.
- 2. Please indicate location & quantity of parking spaces provided for each unit and compare with the Zoning and Development Code requirement; we are unable to determine compliance with the present drawing.
- 3. The spelling of "sight" distance triangle at the entrance drive shall be corrected.
- 4. Is there a private common recreation area to be constructed with this development; if so, where and with what amenities?

# CITY DEVELOPMENT ENGINEER

7/18/96

244-159

Jody Kliska

- 1. Please provide a drawing at a 20 scale showing the dwelling units and proposed driveways so that we can look at vehicle turning templates and see if it is possible for vehicles to get in and out of the driveways. At the 50 scale, it appears there is insufficient maneuvering room if all parking spaces are occupied.
- 2. The Wetlands Report did not indicate an author. Please sign and stamp all engineering reports.
- 3. The drainage report submitted was not signed or stamped as required by section X-1 SSID.
- 4. The Preliminary Drainage Report checklist requires a Preliminary Major Drainage Basin Map. The report included several maps as well as narrative which, taken together, include all of the information. For future reports, however, please prepare a map in accordance with checklist IX-25 so the required information is available on one drawing.
- 5. The traffic study was not stamped as required in SSID section X-1.
- 6. The specific planning commission approval of the ODP was subject to the condition the traffic study include an analysis of the peak hour gap availability at the proposed site entry to assure adequate

# RZP-96-157 / REVIEW COMMENTS / page 2 of 6

gaps exist for left turns exiting the site. If the gap analysis indicates insufficient gaps, then a signal analysis of the two signals will be required to determine if gaps can be created by revising the signal timing while still providing adequate LOS for the intersection traffic at the signals. The report did not include the gap analysis.

- 7. Enclosed is some information on gap studies for your information.
- 8. A redlined Traffic Study Checklist is enclosed. City CIP information was provided but not included in the report. Upcoming street improvements in the area need to be included in the information provided in the study.
- 9. What is the purpose of the urban residential collector section mentioned in part A.3 of the traffic study? It does not appear there is sufficient traffic to warrant this street section.
- 10. For the trip generation, using the single family rates is preferable based on Mesa County's findings. Please adjust the table to use the single family residential rates from ITE, which will increase the weekday rate to 9.55 and the pm peak rate to 1.01. Also include the am peak, as required by the checklist.
- On Figure 2, please indicate the turning movement breakdown for the shared lanes. If the turning movement count data is available, please include in the appendix.
- 12. On Figure 3, please include a legend. A separate figure for trip assignment and trip distribution is preferable.
- 13. Please label Figure 4 so it is clear that it is existing plus site traffic and indicate the hour. The same comment for figure 5. Same comment about breaking out the turning movements in the shared lanes as in comment 11.
- 14. The sight distance analysis is good.
- 15. Enclosed is the existing signal timing for the traffic signal. The HCS timing information in the report does not appear to be correct. Please include a copy of the full printout of signal analyses.
- 16. A summary of the count data in the appendix would be helpful.

#### CITY UTILITY ENGINEER

7/16/96

#### **Trent Prall**

244-1590

PLEASE NOTE: 1996 City of Grand Junction Standard Specifications shall apply for this proposed development. Copies are available for \$10 in the Public Works and Utilities office.

- 1. Please ensure the final plans have the following water notes.
  - A. Water meter pits and setters will be provided by City inspector for installation by contractor.
- 2. Please ensure the final plans have the following sewer notes.
  - A. Contractor shall have one signed copy of plans and a copy of the City of Grand Junction's Standard Specifications at the job site at all times.
  - B. All sewer mains shall be PVC SDR 35 (ASTM 3034) unless otherwise noted.
  - C. All sewer mains shall be laid to grade utilizing a pipe laser.
  - D. All service line connections to the new main shall be accomplished with full body wyes or tees. Tapping saddles will not be allowed.
  - E. No 4" services shall be connected directly into manholes.
  - F. The contractor shall notify the City inspection 48 hours prior to commencement of construction.
  - G. The Contractor is responsible for all required sewer line testing to be completed in the presence of the City Inspector. Pressure testing will be performed after all compaction of street subgrade and prior to street paving. Final lamping will also be accomplished after paving is completed. These tests shall be the basis of acceptance of the sewer line extension.
  - H. The Contractor shall obtain City of Grand Junction Street Cut Permit for all work within

# RZP-96-157 / REVIEW COMMENTS / page 3 of 6

existing City road right-of-way prior to construction.

I. A clay cut-off wall shall be placed 10 feet upstream from all new manholes unless otherwise noted. The cut-off wall shall extend from 6 inches below to 6 inches above granular backfill material and shall be 2 feet wide. If native material is not suitable, the contractor shall import material approved by the engineer.

J. Benchmark ______.

#### **CITY PROPERTY AGENT**

7/11/96

**Steve Pace** 

256-4003

No final plat to review.

## CITY FIRE DEPARTMENT

7/15/96

244-1414

- **Hank Masterson**
- 1. Driveways serving buildings 3&4 and 7&8 must be 20' wide for Fire Department access.
- 2. Submit complete utility composite with final plan. Hydrants must be spaced no more than 300' apart. One hydrant must be located at entrance to project. Minimum water line size is 8" and must provide required fire flow. Submit complete building plans to Fire Department for our plan review and to determine required fire flow.

#### CITY POLICE DEPARTMENT

7/15/96

Dave Stassen

244-3587

- 1. The plan shows a gate at the entrance, but nothing is said about it in the narrative. Is there truly a gate?
- 2. All buildings should have lights connected to photo cells installed at all pedestrian entrances and at the entrance to each garage. This will discourage both crimes against residents and cars.

#### WALKER FIELD AIRPORT

7/5/96

**Dennis Wiss** 

244-9100

The proposed building site lies outside the Airport's Area of Influence (AOI). As such, the airport has no objections to this proposal.

However, the site lies directly south of runway 4-22. It may be subject to overflight of aircraft and the noise associated with these overflights. It is our recommendation that due to this residential development's proximity to aircraft flight paths and the airport proper, additional soundproofing insulation - as well as planned landscape features - be designed into each residence and site to help mitigate potential sound-level perceptions.

#### **MESA COUNTY SCHOOL DISTRICT #51**

7/15/96

Lou Grasso

242-8500

SCHOOL - CURRENT ENROLLMENT / CAPACITY - IMPACT

Tope Elementary - 556 / 452 - 18

West Middle School - 531 / 500 - 8

Grand Junction High School - 1674 / 1630 - 11

#### **PUBLIC SERVICE COMPANY**

7/10/96

Jon Price

244-2693

1. Public Service Company would like some utility easements - 14' front lot line.

## RZP-96-157 / REVIEW COMMENTS / page 4 of 6

2. Public Service Company will require one point of service for both electric and gas meters at each building.

### **GRAND VALLEY IRRIGATION**

7/18/96

#### **Phil Bertrand**

242-2762

The proposed subdivision abuts our Mainline Canal and our Independent Ranchman Canal crosses through the subdivision (see proposed plat).

NO encroachment of our Mainline Canal will be allowed (25 feet from water's edge on both sides). Canal structures at the northeast (Rupp); the southeast (Dividers); and possible the West (7th Street) of this subdivision may need additional right-of-way for the repair, replacement and/or maintenance of these structures. This can be detailed out with the developer or engineer.

The Independent Ranchman Canal, on the northern part of the property, that flows water east to west, must be looked at closely because of its unique flows and embankment characteristics. 20 feet from top of slope, on both sides must be honored, respected and not encroached upon. More details and an understanding of how the developer plans to use this area is needed.

This is an unusual property and development. Look forward to working with the developer and design personnel.

## **GRAND JUNCTION DRAINAGE**

7/11/96

John Ballagh

242-4343

Horizon Village is wholly within the boundaries of the Grand Junction Drainage District. There are presently no known or planned drains within the site of the proposed development. The area is surrounded by sites where there are known high water table problems. The church across Horizon Drive has an extensive GJDD subsurface drain through the site. The Westwood development has two subsurface drains which cover the perimeter of the site with the exception of the property line along Independent Ranchmen's Ditch. The Mesa View Retirement Residence site had a private subsurface drain installed about the time the site was developed. The other "side" is bordered by lands that are significantly higher in elevation. It is strongly recommended that a full subsurface soils evaluation including depth to water table be required prior to construction. It is strongly recommended that the field work of the soils and water table be done during the irrigating season. Corrective measures may be designed into the plan before any other improvements are made to the site.

#### **U S WEST COMMUNICATIONS**

7/12/96

Max Ward

244-4721

For timely telephone service, as soon as you have a plat and power drawing for your development, please:

MAIL COPY TO:

U S West Communications

ATTN: Max Ward

P.O. Box 2688

Grand Junction, CO 81505

We need to hear from you at least 60 days prior to trenching.

# RZP-96-157 / REVIEW COMMENTS / page 5 of 6

#### **TCI CABLEVISION**

7/3/96

### Glen Vancil

245-8777

- 1. We require the developers to provide, at no charge to TCI Cablevision, an open trench for cable service where underground service is needed and when a roadbore is required, that too must be provided by the developer. The trench and/or roadbore may be the same one used by other utilities so long as there is enough room to accommodate all necessary lines.
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- 6. TCI will normally not activate cable service in a new subdivision until it is approximately 30% developed. Should you wish cable TV service to be available for the first home in your subdivision it will, in most cases, be necessary to have you provide a construction assist payment to cover the necessary electronics for that subdivision.

# **LATE COMMENTS**

#### **COLORADO GEOLOGICAL SURVEY**

8/21/96

James M. Soule

303-866-2611

At your request, we have reviewed the materials submitted for and made a site inspection of the proposed location of the residential development project indicated above. The following comments summarize our findings.

- 1. The original geologic conditions of this site consisted of natural residual clayey soils which were interbedded and/or admixed with stream alluvium derived from the drainage of the ancestral Colorado River. The bedrock in the area is the Mancos Shale. However, most of this site was subsequently regraded for agriculture and the contiguous roads and canals and, as a result, most of the site is now immediately underlain by man-placed fills whose composition is probably highly variable and, in that sense, uncertain. Because of irrigation in the vicinity, it is highly likely that there is a shallow perched water table in the area as well.
- 2. Before any construction takes place on this site, we recommend that a thorough geotechnical investigation, including drilling and trenching, be undertaken to determine its subsurface soils, fills, bedrock, and ground-water conditions. Data from this investigation will be absolutely critical for proper foundation designs as well as for developing methods for controlling surface and subsurface drainage across the site. Because of the possibly adverse effects of the nearby road fills and canal

# RZP-96-157 / REVIEW COMMENTS / page 6 of 6

embankments on surface drainage as well as the likely shallow ground-water conditions, a comprehensive drainage plan should be developed by a qualified drainage engineer as well. This will be especially important considering the proximity of the sit to "live" drainage channels, the effect of runoff from Horizon Drive and North 7th Street, and the amount of new impervious area which will be created by both pavements and building construction on the site.

3. Conceptually, we have no problem with the proposed building layout as shown on the site plan, and if recommendations made above are followed and made conditions of approval of this proposed project, then we have no geology-related objection to it.

#### **TO DATE, NO COMMENTS RECEIVED FROM:**

City Attorney
Ute Water
Corp of Engineers

# POSTING OF PUBLIC NOTICE SIGNS

The posting of the Public Notice Sign is to make the public aware of development proposals. The requirement and procedure for public notice sign posting are required by the City of Grand Junction Zoning and Development Code.

To expedite the posting of public notice signs the following procedure list has been prepared to help the petitioner in posting the required signs on their properties.

- 1. All petitioners/representatives will receive a copy of the Development Review Schedule for the month advising them of the date by which the sign needs to be posted. IF THE SIGN HAS NOT BEEN PICKED UP AND POSTED BY THE REQUIRED DATE, THE PROJECT WILL NOT BE SCHEDULED FOR THE PUBLIC HEARING.
- 2. A deposit of \$50.00 per sign is required at the time the sign is picked up.
- 3. You must call for utility locates before posting the sign. Mark the location where you wish to place the sign and call 1-800-922-1987. You must allow two (2) full working days after the call is placed for the locates to be performed.
- 4. Sign(s) shall be posted in a location, position and direction so that:
  - a. It is accessible and readable, and
  - b. It may be easily seen by passing motorists and pedestrians.
- 5. Sign(s) MUST be posted at least **10 days** before the Planning Commission hearing date and, if applicable, shall stay posted until after the City Council Hearing(s).
- 6. After the Public Hearing(s) the sign(s) must be taken down and returned to the Community Development Department within FIVE (5) working days to receive a full refund of the sign deposit. For each working day thereafter the petitioner will be charged a \$5.00 late fee. After eight working days Community Development Department staff will retrieve the sign and the sign deposit will be forfeited in its' entirety.

The Community Development Department staff will field check the property to ensure proper posting of the sign. If the sign is not posted, or is not in an appropriate place, the item will be pulled from the public hearing agenda.

$\sim$ $\sim$ $\sim$ $\sim$ $\sim$
I have read the above information and agree to its terms and conditions.
Branc Has 1 / 7/22/96
SIGNATURE / DATE
FILE #/NAMERZP-96-157 Norizon Wage RECEIPT # 4330
PETITIONER/REPRESENTATIVE AND #5/30/ PHONE # 245-4099
DATE OF HEARING: 8/6/96 POST SIGN(S) BY: 7/26/96
DATE SIGN(S) PICKED-UP 7/22/96 RETURN SIGN(S) BY:
DATE SIGN(S) RETURNED RECEIVED BY:

#### **GENERAL PROJECT REPORT**

#### HORIZON VILLAGE SUBDIVISION

June 27, 1996 Revised July 25, 1996

#### INTRODUCTION:

The accompanying narrative and maps will provide sufficient data to assess the merits of the requested Preliminary Application for a Major Subdivision. Information gained as the result of the review process will be utilized in the preparation of the Final Plans.

#### PROJECT DESCRIPTION:

Horizon Village Subdivision is located on the southeast corner at the intersection of Horizon Drive and North 7th Street. The subject property contains approximately 9.2 acres. The Tax Parcel Number is 2945-024-00-048.

The proposed Horizon Village Subdivision calls for the ultimate development of 17 Four-plex Multi-family buildings, creating 68 units. This will yield a density of 7.39 units per acre for the development. The accompanying preliminary plan depicts the relationship of each building to the property boundary, roadway access, waterways and neighboring developments.

The following Preliminary Land Use chart breaks down the entire subject property into specific uses under developed conditions:

PRELIMINARY LAND USE SUMMARY CHART			
USE	AREA IN ACRES	% OF TOTAL	
Four-plex Units	2.1	22.8	
Street R.O.W.	0.8	8.7	
Open Space	1.8	19.6	
Driveways	0.9	9.8	
Common Area	3.6	39.1	
Total	9.2	100	
Resulting Density = 7.39 units per acre			
Total Number of units = 68 units			

#### **EXISTING LAND USE:**

The site is currently vacant of any structures and is being used for the production of hay. The City of Grand Junction has a 15 inch sanitary sewer line which crosses through the property from the southeast corner of the site, towards the west to North 7th Street. There are numerous mature trees located on the property. The topography of the site is considered to be "rolling" in nature, and historically drains to the northwest into the Independent Ranchmen's Ditch which ultimately conveys water to the Colorado River.

#### **PUBLIC BENEFIT:**

The proposed Horizon Village Subdivision will provide the residents of the area with a quality land development product which will be designed, constructed and maintained in accordance with the City of Grand Junction standards. This project does coincide with the City of Grand Junction overall plan for development. Horizon Village Subdivision will enhance the area and provide a multi-family subdivision which is compatible with the surrounding land use.

## PROJECT COMPLIANCE, COMPATIBILITY AND IMPACT:

**Zoning** -- Currently the land is located within the City of Grand Junction and is zoned PR-6.2 (Planned Residential not to exceed 6.2 units per acre). The Overall Development Plan with the application was submitted to Community Development last year and was approved by City Council on October 4, 1995. The development has been revised to show a reduction of multi-family units from 72 to 68 and the elimination of the single-family lots. These revisions show that Horizon Village Subdivision is proposing a overall density of 7.39, which is a change in the density from the ODP approved. A Mesa County Zoning map is located at the end of this report for surrounding land use comparisons.

**Surrounding Land Use** -- The surrounding land use consists of a number of subdivisions. This includes single-family developments Walker Heights, View Point, Northern Hills and North Acres subdivisions. Westwood Estates Condominiums and a church are also located near the proposed subdivision.

Site Access and Traffic Patterns -- Primary access will be gained from North 7th Street, as shown on the a reduction of the Preliminary Plan located at the end of this report. Major intersections in the area are 7th and Horizon to the north and 7th and Patterson to the south. Assuming an average trip generation rate of 10 trips per household per day, an average of 680 trips from the 68 units would be created and routed through the primary access point. There is no secondary access proposed for the subdivision. This is due to the constraints

from the Grand Valley Canal and the Independent Ranchmen's Ditch bordering the property on the east and north sides of the site respectively.

It is proposed to install a guard house at the entry of the development. There will not be a gate installed at this guard house, nor will their need to be a turn-around area for vehicles entering the development by mistake. This in effect would require the need to propose private roads, and send the final approval for the private roads to City Council. The right-of-way for the streets will be designated as an ingress/egress easement for the maintenance of City Sanitary Sewer and Domestic Water, as well as other dry utilities. This will be reflected on the Final Plat which will be submitted during the next phase of the review process.

The cul-de-sac at the end of the street improvements is proposed as a nonstandard design. The cul-de-sac has a larger radius and an island in the center which will be used for landscaping. This design has been approved by Community Development, City Engineering and the City Fire Department for a different development in the area.

**Utilities** -- With major streets near to the project, all major utilities are located near the subject property.

Sanitary Sewer -- There is a 15 inch clay sanitary sewer line which crosses through the property. This line will be abandoned and reconstructed through the property with a 20 foot easement for maintenance purposes where the line is outside street right-of-way. The new line will be 15 inch RCP and will connect to the existing 15 inch line located in North 7th Street.

Domestic Water -- Water is available from the City of Grand Junction, which owns and maintains an 8 inch line located on the west side of North 7th street.

All other utilities such as, electric, gas, phone and CATV are expected to be extended from the surrounding developments.

**Effects on Public Facilities** -- No unusual effects are expected on public facilities such as fire, police, sanitation, roads, parks, schools, irrigation or other facilities.

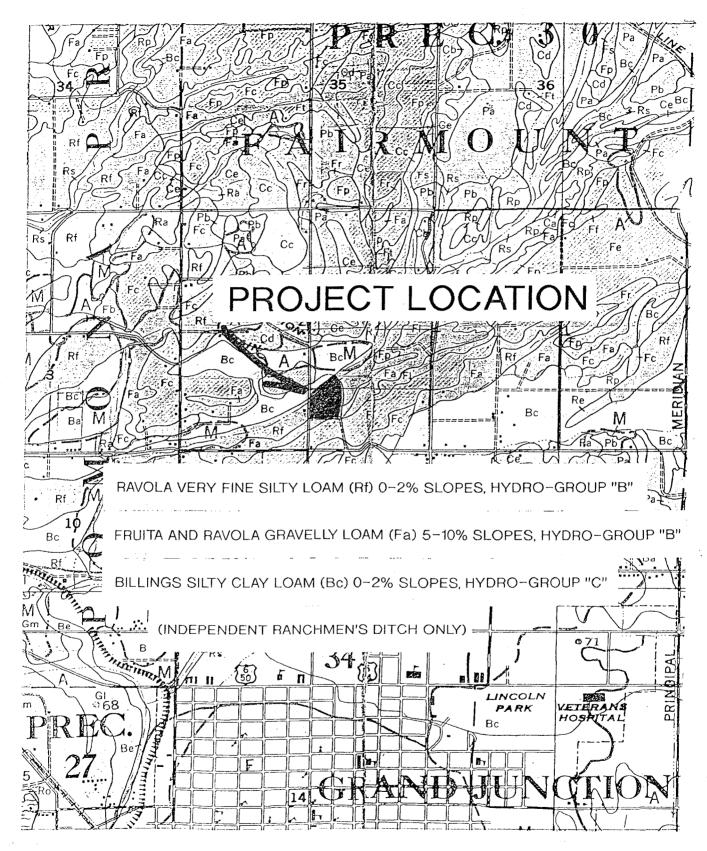
Site Soils and Geology -- A soils map is provided at the end of this report, and shows the types of soil historically found on the property. According to the U.S. Department of Agriculture Soil Survey of 1955, there are a combination of three types of soils on the site. Fruita and Ravola gravelly loams, 5 to 10 percent slopes (Fa), Billings silty clay loam, 0 to 2 percent slopes (Bc) and Ravola very fine sandy loam, 0 to 2 percent slopes (Rf). Each of these soils are common to

the Grand Junction area and are not expected to present any problems. See the attached soils map at the end of this report.

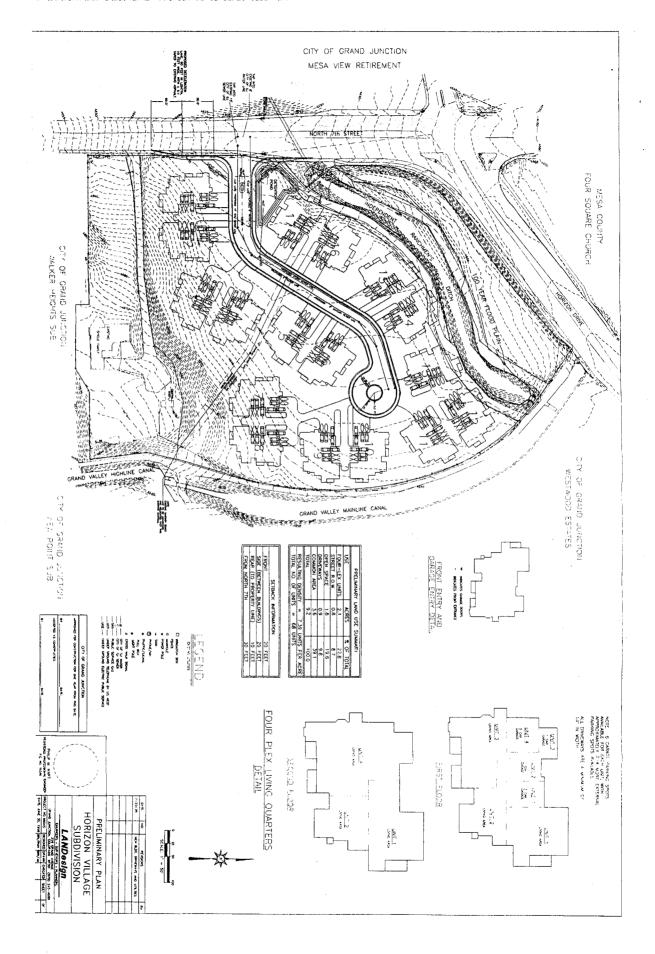
**Signage Plans** -- A signage plan will be provided to the City of Grand Junction during the final and construction phases of the review process.

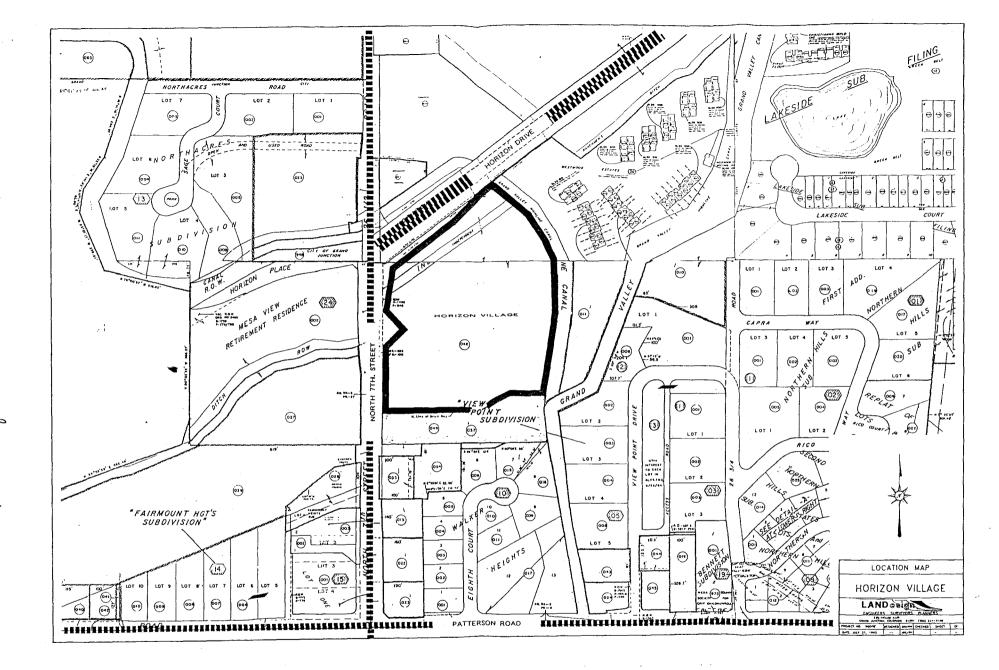
## **DEVELOPMENT SCHEDULE AND PHASING:**

The rate at which the development of Horizon Village will occur is dependent upon the City of Grand Junction's future growth and housing needs. It is anticipated that site development will begin once the final approval from the City has been granted. A phasing plan will be submitted during the next step in the review and application process.



**SOILS MAP** 





Canal Frail? - Proble access dong Ranchman's?

where is special frail suggest and claiming any interest

lufort concerns;

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Motion: Approval of following conditions

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July 25, 1996

Michael Drollinger City of Grand Junction City Community Development 250 North 5th Street Grand Junction, CO 81501

Re: Horizon Village Subdivision Preliminary Plan, File #RZP-96-157

Job # 96045.40

Dear Mr. Drollinger:

This letter is in response to comments received by our office July 19, 1996 on the above mentioned subdivision. The following items are answers to specific comments. Some comments are not answered because they are considered advisory and are taken under consideration for the Final Plan submittal.

# City Community Development

- 1. The developer for this project has no ownership or contractual rights to the south property originally included with the plan. Therefore, we cannot initiate a rezone on the property.
- 2. According to the Zoning and Development Code (section 5-5-1, page 5.36), the requirement for parking is 2 spaces per unit. Two 20 scale Parking Plan drawings have been included with this correspondence. These drawings show the parking areas available for each unit. It is important to note that the four-plex unit chosen for this development has two double space garages and two single space garages. This accounts for 6 of the 8 spaces per building. The remaining two required spaces are shown and allocated on the enclosed plans.
- 3. The spelling error mentioned has been corrected.
- 4. The area north of the Independent Ranchmen's Ditch will be designated as Private Open Space. This area is currently a barren eyesore and includes the bank side under soils from the road and sidewalk improvements made to Horizon Drive. The developer's plan includes significant landscape improvements to this area, including fertile topsoil, plantings and irrigation while allowing access for the ditch company.

# City Development Engineer

- 1. The two 20 scale drawings have been provided as requested. Please note that representative passenger cars have been placed in the parking spaces for the Engineer's benefit. We are currently working with the City Engineer to clarify any questions related to parking.
- 2. The Wetlands Report has been revised to reflect the author. The report has not been signed because it is not an engineering report, nor is any reference made to a signed and stamped Wetlands report in the City's SSID manual.
- 3. A signed and stamped copy of the Preliminary Drainage Report has been included.
- 4. We appreciate the comment and will work toward providing the necessary information.
- 5. The Traffic Study has been signed and stamped as requested.
- 6. A Peak Hour Gap study has been included with this correspondence as requested.
- 7-16. All remaining comments apply to the traffic study. These comments will be resolved with the City Development Engineer before the Planning Commission Hearing August 6th.

# City Utility Engineer

A-J. All comments from the City Utility Engineer relate to the Final Plans and are taken under advisement.

# City Fire Department

- 1. It was understood by both our office and City Staff that any buildings that set back from the street would have to have a driveway width of 14 feet. Because Mr. Masterson is unavailable, City Staff And our office agreed to keep the driveways at 14 feet until the issue can be resolved with the Fire Department.
- 2. This particular comment is related to the Final Plans and is taken under advisement.

# City Police Department

1. The narrative has been revised to reflect a guard house. There will not be a physical gate as earlier shown.

2. This comment is related to the building plans and is taken under consideration.

#### Public Service

1&2. Both comments from Public Service are considered to be typical. The details of easements and utility meter locations will be worked out with Public Service at the appropriate time.

# **Grand Valley Irrigation**

The comment from Grand Valley Irrigation Company is appreciated. Because of the unique characteristics of the property and the fact that irrigation waterways border the north and east sides of the project, the developer and the engineer look forward to working closely with the irrigation company to resolve any issues which may arise.

# **Grand Junction Drainage District**

The comment from the district is appreciated. The Subsurface Soils Report submitted to the study did mention the water table on the project site. However, the report revealed that the water table was reached at approximately 13-16 feet. It is worth noting that the soils logs were taken during the peak of irrigation season. We therefore expect no problem in dealing with the water table, or its effects on drainage, foundations or general construction of the project.

#### **US West**

The comment from US West is typical for any development and is taken under advisement.

#### TCI Cable

The comment from TCI Cable is typical for any development and is taken under advisement.

I hope this letter has served to answer any comments mentioned, and if any other issues arise, please feel free to contact me at our office.

Sincerely,

Brian C. Hart, E.I.

Brown C. How

**Project Manager** 

# MEMORANDUM

DATE:

August 10, 1996

TO:

Jody Kliska

FROM:

Michael T. Drollinger

RE:

Horizon Village

Please review the attached driveway and parking design drawings with particular attention to turning radii and parking requirements and advise in writing (e-mail OK) if the design conforms with Code requirements. I need a response no later than August 16, 1996 so that I may forward your comments to the petitioner.

Feel free to call of you have any questions.

# MEMORANDUM

DATE:

August 10, 1996

TO:

Hank Masterson

FROM:

Michael T. Drollinger

RE:

Horizon Village

Attached please find plans for the above project which detail the parking and circulation design for the development. Earlier in the design phase you had discussed permitting the petitioner to design entrance drives to the units with a width less than 20 feet (in the 12 to 14 foot range). In your review comments you stated that you will require 20 foot wide drives. Please review the attached drawings and send to me an e-mail or memo with a "final" decision on this issue (w/Code citations if appropriate) so that I may forward this on to the petitioner.

I would appreciate if you could complete your review of this issue by Friday, August 16th. This project will likely be going to Planning Commission in September. Please call if you have any questions.

#### Memorandum

DATE:

August 14, 1996

TO:

Michael T. Drollinger

FROM:

Hank Masterson ///

RE:

Horizon Village

RECEIVED GRAND JUNCTION PLANNING DEPARTMENT

AUG 15 1996

The requirement for fire department access to structures is specified in Section 902 of the 1994 Uniform Fire Code:

Section 902.2.1 states: "fire apparatus access roads shall be provided ... for every facility, building or portion of a building hereafter constructed or moved into or within the jurisdiction when any portion of the facility or any portion of an exterior wall of the first story of the building is located more than 150' from fire apparatus access as measured by an approved route around the exterior of the building or facility.

**Exceptions:** 1. When buildings are completely protected with an approved automatic fire sprinkler system, the provisions of Sections 902.2.1 and 902.2.2 may be modified by the chief.

- 2. When access roads cannot be installed due to location on property, topography, waterways, nonnegotiable grades, or other similar conditions, the chief is authorized to require additional fire protection as specified in Section 1001.9
- 3. When there are not more than two Group R, Division 3, or Group U Occupancies, the requirements of Sections 902.2.1 and 902.2.2 may be modified by the chief."

Section 902.2.2.1 states: "Fire apparatus access roads shall have an unobstructed width of not less than 20' ..."

Exception 3 of 902.2.1 applies to residential garages and single family residences. This allows us to modify access requirements for detached single family residences and duplexes. The fire department has always used this exception to exempt single family and duplex residences from access requirements for driveways or ingress/egress easements serving up to two single family lots. This exception cannot apply to Horizon Village because the buildings are four plexes.

To determine the need for a fire department access road, I measure from the most distant portion of a proposed building along the most direct path of pedestrian travel to the nearest approved access road. This distance represents the length of an attack line taken from a fire truck to the fire for an exterior attack. The fire code specifies that this distance not exceed 150' to avoid lengthy hose lays. In the case of Horizon Village, all units except 3, 4, 7, 8 and 9 are within 150' of the public street. Units 7 and 8 are about 300' from the public street at the most remote wall. Units 3, 4 and 9 are about 220' from the street. So, the entrance drives to these units need to be used by the Fire Department to park a fire apparatus within the 150' distance. These drives need to be 20' wide to accommodate fireground operations.

I apologize if I stated that all units in this subdivision were acceptable as shown. When I completed my detailed plan review I noticed the problems with access and noted them in my review comments. I generally try not to commit myself before completing a detailed review.

Also, in case fire department access policy appears inconsistent, we have an unwritten policy of not requiring access standards for single family residential houses and duplexes using exception 3 noted above. So, on plans such as Daughter's Cove, with 15' wide flag lot frontages, we do not require 20' access or turn arounds. The revised preliminary plan for Canyon View Subdivision shows a private drive easement serving two single family lots and another serving one large lot. We will not apply access standards for either easement. If we were to apply fire code standards, we would get into questions such as requiring driveways to homes be able to support the weight of our trucks, provided with 40' diameter cul-de-sacs if over 150' long, and signed no parking to ensure they are not blocked. Also, flag lots with 15' frontages could not be allowed. Another issue with single family residential having long driveways is on-site hydrants. Our general rule for commercial property is to require on-site hydrants if we need to lay a supply line longer than 250' from the hydrant to the farthest apparatus access point. If we did this on single family residential property, property owners with large lots, flag lots, or using ingress/egress easements would be restricted to locating their houses on their lots so that on-site hydrants would not be required, unless they were willing to pay the considerable cost for their very own hydrant. All this strikes me as a bit extreme for a single family residences!

Anyway, again I apologize if I put you in a difficult position with the petitioner on the Horizon Village project. Let me know if you have any questions.

RECEIVED GRAND JUNCTION
PLANNING DEPARTMENT

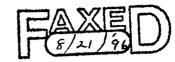
AUG 2 1998

STATE OF COLORADO

COLORADO GEÓLOGICAL SURVEY

Division of Minerals and Geology

Department of Note al Resources 1313 Sherman Street, Room 715 Denver, Colorado 80203 Phone (303) 866-2611 FAX (303) 866-2461





August 21, 1996

MA-97-0003

City of Grand Junction Community Development Department 250 North 5th Street Grand Junction, Colorado 81501 Roy Rom Governor

> James S. Lochhead Executive Director

Michael B. Long Division Director

Vicki Cowart State Geologist and Director

Re: Proposed Horizon Village Townhome Project -- Southeast of the Intersection of Horizon Drive and North 7th Street, Grand Junction

# Gentlemen:

At your request, we have reviewed the materials submitted for and made a site inspection of the proposed location of the residential development project indicated above. The following comments summarize our findings.

- (1) The original geologic conditions of this site consisted of natural residual clayey soils which were interbedded and/or admixed with stream alluvium derived from the drainage of the ancestral Colorado River. The bedrock in the area is the Mancos Shale. However, most of this site was subsequently regraded for agriculture and the contiguous roads and canals and, as a result, most of the site is now immediately underlain by man-placed fills whose composition is probably highly variable and, in that sense, uncertain. Because of irrigation in the vicinity, it is highly likely that there is a shallow perched water table in the area as well.
- (2) Before any construction takes place on this site, we recommend that a thorough geotechnical investigation, including drilling and trenching, be undertaken to determine its subsurface soils, fills, bedrock, and ground-water conditions. Data from this investigation will be absolutely critical for proper foundation designs as well as for developing methods for controlling surface and subsurface drainage across the site. Because of the possibly adverse effects of the nearby road fills and canal embankments on surface drainage as well as the likely shallow ground- water conditions, a comprehensive drainage plan should be developed by as qualified drainage engineer as well. This will be especially important considering the proximity of the site to "live" drainage channels, the effects of runoff from Horizon Drive and North 7th Street, and the amount of new impervious area which will be created by both payments and building construction on the site.
- (3) Conceptually, we have no problem with the proposed building layout as shown on the

City of Grand Junction Community Development Department August 21, 1996 Page 2

site plan, and if the recommendations made above are followed and made conditions of approval of this proposed project, then we have no geology-related objection to it.

Sincerely,

James M. Soule Engineering Geologist



August 22, 1996

Jody Kliska, P.E. City Development Engineer City of Grand Junction Grand Junction, CO 81501

Re: Horizon Village Subdivision Preliminary Plan, File #RZP-96-157

Job # 96045.40

Dear Mrs. Kliska:

Enclosed with this letter is a copy of the Parking Detail Sheets which have been revised by our office to reflect the changes mentioned in our August 21 meeting. Also enclosed is a copy of the Preliminary Plan which has also been revised to reflect the changes made to the driveways.

The most important changes made to the plan are as follows: 1) The "back-in" area for automobiles in the courtyard areas have all been removed, as they are not useable, 2) Parking in the area between units 8 & 9 has been revised to show a "No Parking" area. This option was chosen over moving units 7 & 8 to the south to avoid installing any retaining walls, 3) Parking for the double garage on Unit 12 between units 12 & 13 has been designated as "No Parking", 4) The driveways for the double garages on units 3, 4 & 7 which face the road have been revised to allow a larger area for automobile traffic, 5) The combined driveways for units 3 & 4 as well as 7 & 8 have been widened to 20 feet from 14 feet as required by Hank Masterson at the City Fire Department.

These changes were made due to the conversation with you and Michael Drollinger on August 21. If there are any other items which you or Mr. Drollinger would like to see revised, or if I am mistaken in any respect with any revisions required, please contact me so the drawings can be revised as soon as possible. Thank you for meeting with me yesterday to discuss the project.

Sincerely,

Brian C. Hart, E.I.

Project Manager

cc: Mac Cunningham, Cunningham Investment Co., Inc.

Michael Drollinger, City Senior Planner

### PLANNING COMMISSION STAFF REPORT

FILE:

#RZP-96-157

DATE:

August 28, 1996

STAFF:

Michael T. Drollinger

REQUEST:

Rezone/Preliminary Plan

HORIZON VILLAGE

LOCATION: SE Corner 7th Street & Horizon Drive

APPLICANT: Cunningham Investment Co., Inc.

121 S. Galena Street, Suite 201

**Aspen CO 81611** 

#### **EXECUTIVE SUMMARY:**

A request to (1) rezone the property at the southeast corner of 7th Street and Horizon Drive from PR-6.15 (Planned Residential - 6.15 units per acre) to PR-7.4 (Planned Residential - 7.4 units per acre) and RSF-4 (Residential Single Family - 4 units per acre) and (2) for Preliminary Plan approval for 68 units on 9.2 acres. Staff recommends approval of the application with conditions.

**EXISTING LAND USE:** 

Vacant

PROPOSED LAND USE:

Multifamily Residential (Fourplex)

SURROUNDING LAND USE:

NORTH:

Undeveloped

SOUTH:

Single Family Residential

EAST:

Multifamily Residential - 12 units per acre

WEST:

Mesa View Retirement Center

**EXISTING ZONING:** 

PR-6.15

PROPOSED ZONING:

PR-7.4 & RSF-4

SURROUNDING ZONING:

NORTH:

RSF-4 (Residential Single Family - 4 units per acre)

SOUTH:

RSF-4

EAST:

PR-12 (Planned Residential - 12 units per acre)

WEST: PR-28 (Planned Residential - 28 units per acre)

#### RELATIONSHIP TO COMPREHENSIVE PLAN:

The Grand Junction Growth Plan identifies the subject parcel in the "Residential Medium (4-7.9 units per acre)" land use category. The proposed density falls within the recommended density for the site.

#### **STAFF ANALYSIS:**

The staff analysis is divided into two sections: (1) a review of the development proposal and (2) analysis of the rezone criteria.

## The Development Proposal

The petitioner is requesting a rezone and preliminary plan approval for 68 units on about 9.2 acres located at the southeast corner of 7th Street and Horizon Drive. The property is presently zoned PR-6.15 and was the subject of an Outline Development Plan (ODP) approval for 72 condominium units and 4 single family lots in October 1995.

The revised proposal is for 68 units in 17 fourplex buildings; the proposal also calls for the existing single family residence (referred to as the Mahleris property) adjoining the site to the south to be rezoned back to RSF-4 from PR-6.15 since the previous single family lots on the Mahleris property are no longer part of this proposal. While the density request for the 9.2 acres on which the multifamily units are proposed is higher than the present zoning, the increase is due to the Mahleris property no longer being part of the proposal; the number of multifamily units has actually been reduced from 72 to 68.

The petitioner is also requesting that the street be private rather than a public street although the proposed street design would meet City standards. The request would permit the petitioner to create a gate or similar type of security feature at the entrance to the development. The private street request is subject to City Council approval and a proposal for a gate would require review and approval by staff with the final plan request. Given that the proposed street is a cul-de-sac and that there are no vehicular or non-vehicular linkages which would be adversely effected by the creation of a private street, staff is supportive of the proposal. The private street request will be scheduled for a City Council hearing in conjunction with the rezone request.

A traffic study was required with the preliminary plan which addressed the conditions of the ODP approval which are as follows:

- a) a peak hour gap analysis on 7th Street at the proposed location of entry,
- b) a signal timing analysis of there are insufficient gaps to allow left turns from the site,
- c) A measurement of sight distance on 7th Street from the proposed entry,
- d) An evaluation of the need for a right turn lane from the site.

A right turn lane into the site has been provided. Adequate sight distance was found to exist at the proposed street intersection. Sufficient gaps were found to exist to permit traffic exiting the site to turn left onto 7th Street. The City Development Engineer has identified a few remaining items which need to be in the traffic study although staff recommends that the petitioner be able to submit a revised final traffic study with the final plan.

Please refer to the project narrative and supplementary information supplied by the petitioner and attached to this staff report for additional details regarding the proposal.

## Analysis of Rezone Criteria

Section 4-4-4 of the Zoning and Development Code contains criteria which must be considered in the review of a rezone request. To minimize repetition, references are made to the previous section where applicable.

- A. Was the existing zone an error at the time of adoption?

  There is no evidence that the existing zone was an error at the time of adoption.
- B. Has there been a change of character in the area due to installation of public facilities, other zone changes, new growth trends, deterioration, development transitions, etc.?

The subject property is in close proximity to services and major roadways and other existing infrastructure. The proposal represents an attempt to concentrate growth close to existing infrastructure.

- C. Is there an area of community need for the proposed rezone?

  The project is a response to an anticipated market demand for the proposed unit types.
- D. Is the proposed rezone compatible with the surrounding area or will there be adverse impacts?

The petitioner has attempted to minimize conflicts with adjoining neighbors by proposing a unit type which closely resembles and is compatible with single family residential development.

- E. Will there be benefits derived by the community, or area, by granting the proposed rezone?
  - The proposal addresses an identified community need for multifamily housing.
- F. Is the proposal in conformance with the policies, intents and requirements of this Code, with the City Master Plan, and other adopted plans and policies? The proposed project density is within the density range recommended in the Grand Junction Growth Plan. The proposal is in general conformance with the intent and requirements of the Zoning and Development Code and the Horizon Drive Corridor guidelines.
- G. Are adequate facilities available to serve development for the type and scope suggested for the proposed zone?
   Adequate facilities are available to serve the proposed development.

Staff feels that the rezone request is supported by the rezone criteria.

#### STAFF RECOMMENDATION:

Staff recommends approval of the rezone request and preliminary plan for Horizon Village with the following condition:

1. the petitioner shall submit a revised traffic study with the final plan/plat request which addresses the remaining concerns identified by the City Development Engineer.

2. Private Sturt - Enfracing into a maintenance agreement of Control of the City.

#### SUGGESTED PLANNING COMMISSION MOTION:

Mr. Chairman, on item #RZP-96-157, a request for rezone from PR- 6.15 to PR- 7.4 and RSF-4, I move that we forward the rezone request to City Council with a recommendation of approval (STAFF RECOMMENDS APPROVAL).

Mr. Chairman, on item #RZP-96-157, a request for preliminary plan approval for Horizon Village, I move that we approve the application with the condition in the staff report dated August 28, 1996 (STAFF RECOMMENDS APPROVAL).

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# CUNNINGHAM INVESTMENT CO., INC.

SUITE 201

#### 121 SOUTH GALENA STREET ASPEN, COLORADO 81611

OFFICE (303) 925-8803

FAX (303) 925-8835

September 9, 1996

Michael T. Drollinger City of Grand Junction Community Development Department 250 N. 5th Street Grand Junction, CO 81501

UPS (970) 244-1439

RE: The Glen at Horizon Drive Horizon & North Seventh Streets Grand Junction, Colorado

Dear Mr. Drollinger:

Enclosed please find 10 sets of the photo images of proposed townhomes for The Glen at Horizon.

If you have any questions, please let us know.

Sincerely,

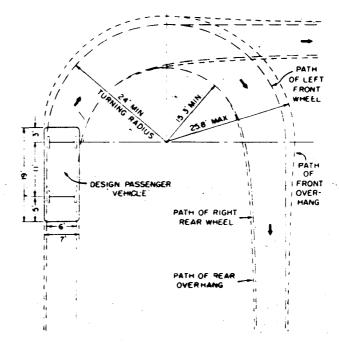
Leslie J. Henderson

Office Manager

Cunningham Investment Co., Inc.

:ljh

enclosures



P DESIGN VEHICLE

1" = 20'

# TYPE LEGAL DESCRIPTION(S) BELOW, USING ADDITIONAL SHEETS AS NECESSARY. USE SINGLE SPACING WITH A ONE INCH MARGIN ON EACH SIDE.

*********************************

That part of the N½ SW½ SE½ and that part of the S½ NW½ SE½ lying South and West of the main line of the canal of The Grand Valley Irrigation Company in Section 2, Township 1 South, Range 1 West of the Ute Meridian, in the City of Grand Junction, EXCEPT the residence located at 612 - 26½ Road and that portion of the real property located South of the North line of the driveway (as extended to the east and west property lines) leading from 26½ Road to such residence, such exception to be more particularly described by survey; AND EXCEPT portion of subject property as granted to County of Mesa, State of Colorado in deed recorded in Book 877 at Page 364; AND EXCEPT portion of subject property as granted to County of Mesa, State of Colorado in deed recorded in Book 885 at Page 100; AND EXCEPT portion of subject property as granted to The City of Grand Junction in deed recorded in Book 1489 at Page 547, AND EXCEPT portion of subject property dedicated as road and utility Right Of Way in instrument recorded in Book 1489 at Page 739, Mesa County, Colorado.